Mark Cannon, Michaelmas Term 2018

Reading: Kouvaritakis & Cannon, Sections 2.1–2.6 and 3.1–3.3 or Maciejowski Chapters 2, 3, 6, 8

## **Prediction equations**

1. A system with model

$$x_{k+1} = Ax_k + Bu_k, y_k = Cx_k$$

$$A = \begin{bmatrix} 1 & 0.1 \\ 0 & 2 \end{bmatrix}, B = \begin{bmatrix} 0 \\ 0.5 \end{bmatrix}, C = \begin{bmatrix} 1 & 0 \end{bmatrix}$$

is to be controlled using an unconstrained predictive control law that minimizes the predicted performance cost

$$J_k = \sum_{i=0}^{N-1} (y_{i|k}^2 + \lambda u_{i|k}^2) + y_{N|k}^2, \qquad \lambda = 1.$$

(a). Show that the state predictions can be written in the form

$$\mathbf{x}_k = \mathcal{M} x_k + \mathcal{C} \mathbf{u}_k, \quad \mathbf{u}_k = \begin{bmatrix} u_{0|k} & u_{1|k} & \cdots & u_{N-1|k} \end{bmatrix}^{\mathsf{T}}$$
 and evaluate  $\mathcal C$  and  $\mathcal M$  for a horizon of  $N=3$ .

(b). For N=3, determine the matrices H, F and G in

$$J_k = \mathbf{u}_k^{\mathsf{T}} H \mathbf{u}_k + 2x_k^{\mathsf{T}} F^{\mathsf{T}} \mathbf{u}_k + x_k^{\mathsf{T}} G x_k.$$

- (c). Give expressions for the derivatives  $\partial J/\partial u_{i|k}$  for i=0,1,2. Hence verify that the gradient of J is  $\nabla_{\bf u}J=2H{\bf u}+2Fx$ .
- 2. (a). For the plant model and cost given in Question 1, show that the unconstrained predictive control law for N=3 is linear feedback:

$$u_k = Lx_k, \quad L = -\begin{bmatrix} 0.1948 & 0.1168 \end{bmatrix}.$$

2

Hence show that the closed-loop system is unstable.

(b). Write some Matlab code to evaluate  $\mathcal{C}_i$  for  $i=1,\ldots,N$ , and to determine H and F for any given horizon length N. Show that the predictive control law does not stabilize the system if N<6.

## Infinite horizon cost and constraints

- 3. (a). Explain why the predictive control law of Question 1 necessarily stabilizes the system if the cost is minimized subject to  $x_{N|k}=0$ . (Hint: what is the infinite horizon cost when this constraint is used?)
  - (b). How would you modify the cost of Question 1 in order to achieve closed loop stability without including the constraint  $x_{N|k}=0$ ? Why would this be preferable?
- 4. A predictive controller minimizes the predicted performance index:

$$J_k = \sum_{i=0}^{\infty} (y_{i|k}^2 + u_{i|k}^2)$$

at each time-step k subject to input constraints:  $-1 \le u_{i|k} \le 2$  for all  $i \ge 0$ . The system output y is related to the control input u via

$$x_{k+1} = Ax_k + Bu_k, \quad y_k = Cx_k$$

$$A = \begin{bmatrix} -2 & 1 \\ 0 & 1 \end{bmatrix}, \quad B = \begin{bmatrix} 1 \\ 1 \end{bmatrix}, \quad C = \begin{bmatrix} 1 & 1 \end{bmatrix}.$$

- (a). Why is the MPC optimization performed repeatedly, at  $k=0,1,2\ldots$ , instead of just once, at k=0?
- (b). If the mode 2 feedback law is  $u_k = \begin{bmatrix} 2 & -1 \end{bmatrix} x_k$ , show that

$$J_k = \sum_{i=0}^{N-1} (y_{i|k}^2 + u_{i|k}^2) + x_{N|k}^{\top} \begin{bmatrix} 13 & -1 \\ -1 & 2 \end{bmatrix} x_{N|k}$$

where N is the length of the mode 1 prediction horizon.

4

(c). Show that the constraints

$$-1 \le u_{i|k} \le 2, \quad i = 0, 1, \dots, N+1$$

ensure that the predictions satisfy  $-1 \le u_{i|k} \le 2$  for all  $i \ge 0$ .

- (d). Derive a bound on  $J_{k+1}^* J_k^*$ , where  $J_k^*$  is the optimal value of  $J_k$ . Hence show that  $\sum_{k=0}^{\infty} \left(y_k^2 + u_k^2\right) \leq J_0^*$  along trajectories of the closed loop system.
- (e). Is the closed loop system stable? Explain your answer.
- 5. (a). Explain the function of terminal constraints in a model predictive control strategy for a system with input or state constraints. Define two principal properties that must be satisfied by a terminal constraint set.
  - (b). A discrete time system has the state space model

$$x_{k+1} = Ax_k + Bu_k, \quad A = \begin{bmatrix} 0.3 & -0.9 \\ -0.4 & -2.1 \end{bmatrix}, \quad B = \begin{bmatrix} 0.5 \\ 1 \end{bmatrix}$$

and constraints

$$|[x]_1 + [x]_2| \le 1$$
,  $|[x]_1 - [x]_2| \le 1$ ,  $x = \begin{bmatrix} [x]_1 \\ [x]_2 \end{bmatrix}$ 

(i). If the terminal feedback law is  $u_k=Kx_k$ ,  $K=\begin{bmatrix}0.4 & 1.8\end{bmatrix}$ , show that the following set is a valid terminal constraint set

$${x: |[x]_1 + [x]_2| \le 1, |[x]_1 - [x]_2| \le 1}.$$

- (ii). Describe a procedure for determining the largest terminal constraint set for the case of a general feedback gain K.
- (c). What are the main considerations that govern the choice of the prediction horizon N?

## Integral action and disturbances

6. The vertical position y of a machine tool positioning platform is controlled by a motor which applies a vertical force F to the platform (Figure 1). The platform has mass M and carries a variable load of mass m; the unloaded weight of the platform is balanced by a counter-weight. The force F is proportional to the voltage V applied to the motor, so that  $F = K_V V$  where  $K_V$  is a fixed gain.

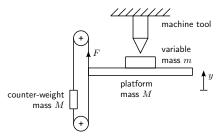


Figure 1. Machine tool and positioning platform

Assuming m is small enough that  $M+m\approx M$ , the unknown load constitutes a (constant) disturbance in the discrete-time model of the system for sampling interval T:

$$x_{k+1} = Ax_k + Bu_k + Dw, \quad e_k = Cx_k$$

$$A = \begin{bmatrix} 1 & T \\ 0 & 1 \end{bmatrix}, \quad B = \frac{K_V}{2M} \begin{bmatrix} T^2/2 \\ T \end{bmatrix}, \quad D = -\frac{g}{2M} \begin{bmatrix} T^2/2 \\ T \end{bmatrix}, \quad C = \begin{bmatrix} 1 & 0 \end{bmatrix}$$

where e is the error in y relative to a desired steady-state height  $y^0$ , and

$$x_k = \begin{bmatrix} y(kT) - y^0 \\ \dot{y}(kT) \end{bmatrix}, \quad u_k = v(kT), \quad w = m.$$

(a). For the model parameters  $M=10\,{\rm kg},\,K_V=7\,{\rm N\,V^{-1}},\,T=0.1\,{\rm s},$  the LQ-optimal feedback law with respect to the cost

$$J_k = \sum_{i=0}^{\infty} (e_{k+i}^2 + \lambda u_{k+i}^2), \quad \lambda = 10^{-4}$$

is  $u_k = Kx_k$ ,  $K = \begin{bmatrix} -66.0 & -19.4 \end{bmatrix}$ . Determine the maximum steady state error  $y - y^0$  with this controller if the mass of the load is limited to the range:

$$m \leq 0.5 \,\mathrm{kg}$$
.

- (b). Explain how to modify the cost and model dynamics in order to obtain a stabilizing LQ-optimal controller giving zero steady-state error.
- (c). The motor input voltage is subject to the constraints

$$-1 < V < 1$$

A predictive controller is to be designed based on the predicted cost:

$$J_k = \sum_{i=0}^{\infty} (e_{i|k}^2 + v_{i|k}^2 + \lambda u_{i|k}^2), \quad \lambda = 10^{-4}$$

where  $v_{i+1|k} = v_{i|k} + e_{i|k}$  is the prediction of the integrated error.

(i). For a predicted input sequence with N degrees of freedom, show that  $J_k$  can be re-written as

$$J_k = \sum_{i=0}^{N-1} \left( e_{i|k}^2 + v_{i|k}^2 + \lambda u_{i|k}^2 \right) + \|\xi_{N|k}^\top\|_P^2$$

and define  $\xi$  and P. What is the implied mode 2 feedback law?

- (ii). Briefly explain how the constraints on V can be incorporated in a robust MPC strategy for this system (i.e. for all values of m in the range  $m \leq 0.5\,\mathrm{kg}$ ).
- 7. Assume that, for the given initial condition x(0), the optimization of J subject to the robust constraints determined in Question 6 is initially feasible. Will the online optimization remain feasible at all future sampling times? What can be said about the steady-state value of y? Will the optimal value of the cost necessarily decrease monotonically, and what can be concluded about the convergence of the state  $x_k$  to zero in closed-loop operation?

8. A production planning problem involves optimizing the quantity u of stock manufactured in each week. The quantity x of stock that remains unsold at the start of week k+1 is given by

$$x_{k+1} = x_k + u_k - w_k, \quad k = 0, 1, \dots$$

where the quantity  $w_k$  that is sold in each week is unknown in advance but is expected to be equal to a known constant  $\hat{w}$ . Limits on storage and manufacturing capacities imply that x and y can only take values in the intervals

$$0 < x_k < X$$
,  $0 < u_k < U$ .

The desired level of stock in storage is  $x^*$ , and the planned values  $u_{0|k}, u_{1|k}, \ldots$  are to be optimized at time k given a measurement of the value of  $x_k$  by minimizing a cost

$$J_k = \sum_{i=0}^{\infty} e_{i|k}^2$$
,  $e_{i|k} = x_{i|k} - x^*$ .

- (a). What are the advantages of using a receding horizon control strategy in this application instead of an open-loop control sequence computed at k=0?
- (b). Assume that  $w_k = \hat{w}$  for all  $k = 0, 1, \ldots$ 
  - (i). Show that the unconstrained optimal control law is  $u_k = \hat{w} e_k$ .
  - (ii). Show that, for a mode 1 horizon of N, the infinite horizon cost can be expressed

$$J_k = \sum_{i=0}^{N} e_{i|k}^2 \; ,$$

and state the corresponding mode 2 feedback law.

(iii). Show that constraints are satisfied over an infinite horizon if  $0 \le x_{i|k} \le X$  and  $0 \le u_{i|k} \le U$  for  $0 \le i \le N-1$ , and

$$\max\{0, \hat{w} + x^* - U\} \le x_{N|k} \le \min\{X, \hat{w} + x^*\}.$$

What assumptions on  $\hat{w}$ ,  $x^*$ , U and X are needed?.

(c). Assume now that the future value of w is unknown and may take any value in an interval:  $0 \leq w_k \leq W$ . Suggest how to express the planned sequence  $u_{0|k}, u_{1|k}, u_{2|k}$  in terms of the free variables in the receding horizon optimization problem, and justify your answer by determining the predictions  $e_{1|k}, e_{2|k}, e_{3|k}$ .

## Some answers

1. (a). 
$$C = \begin{bmatrix} 0.15 & 0.05 & 0 \\ 2 & 1 & 0.5 \end{bmatrix}$$
  
(b).  $H = \begin{bmatrix} 1.025 & 0.0075 & 0 \\ 0.0075 & 1.0025 & 0 \\ 0 & 0 & 1 \end{bmatrix}$ ,  $F = \begin{bmatrix} 0.2 & 0.12 \\ 0.05 & 0.035 \\ 0 & 0 \end{bmatrix}$ ,  $G = \begin{bmatrix} 4 & 1.1 \\ 1.1 & 0.59 \end{bmatrix}$ 

2. (a). Closed loop poles for 
$$N = 3$$
:  $eig(A + BL) = 1.01, 1.93$ 

(b). 
$$N$$
 4 5 6 7  $eig(A+BL)$  1.03,1.69 1.11  $\pm$  0.15i 0.86  $\pm$  0.10i 0.95,0.58

3. (b). In 
$$J_k$$
, replace  $y_{N|k}^2$  with  $\|x_{N|k}\|_P^2$ ,  $P = \begin{bmatrix} 22.46 & 4.098 \\ 4.098 & 12.79 \end{bmatrix}$ 

4. (d). 
$$J_{k+1}^* - J_k^* \le -(y_k^2 + u_k^2)$$

(e). x = 0 is locally asymptotically stable

6. (a). 
$$|y - y^0| \le 0.0106 \,\mathrm{m}$$
 in steady state

(c). 
$$\xi$$
: augmented predicted state,  $\xi = \begin{bmatrix} x & v \end{bmatrix}^{\mathsf{T}}$ ,  $P$ : the solution of 
$$P - \left( \begin{bmatrix} A & 0 \\ C & I \end{bmatrix} + \begin{bmatrix} B \\ 0 \end{bmatrix} K_{\xi} \right)^{\mathsf{T}} P \left( \begin{bmatrix} A & 0 \\ C & I \end{bmatrix} + \begin{bmatrix} B \\ 0 \end{bmatrix} K_{\xi} \right) = \begin{bmatrix} C^{\mathsf{T}} C & 0 \\ 0 & 1 \end{bmatrix} + \lambda K_{\xi}^{\mathsf{T}} K_{\xi},$$

Mode 2 feedback law:  $u=K_\xi x$ , e.g. LQ-optimal  $K_\xi=-\begin{bmatrix}201.4 & 29.6 & 48.2\end{bmatrix}$ 

8. (c). 
$$u_{i|k}=\hat{w}-e_{i|k}+c_{i|k}$$
, where  $c_{i|k}=$  for  $i=0,\ldots,N-1$  are decision variables, and  $c_{i|k}=0$  for  $i\geq N$