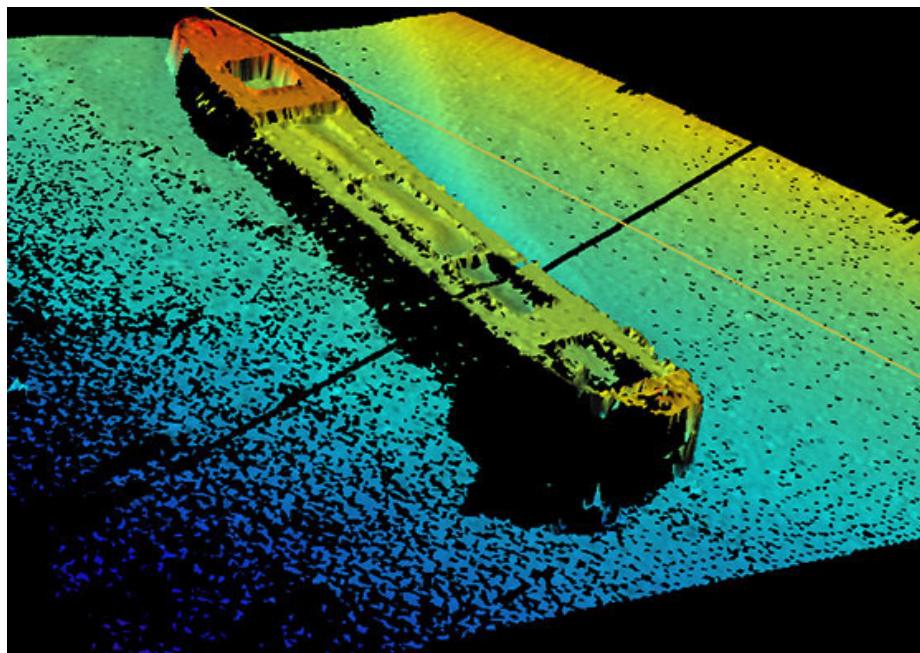


**TMR4585**  
**Processing and error**  
**propagation**

**2019**

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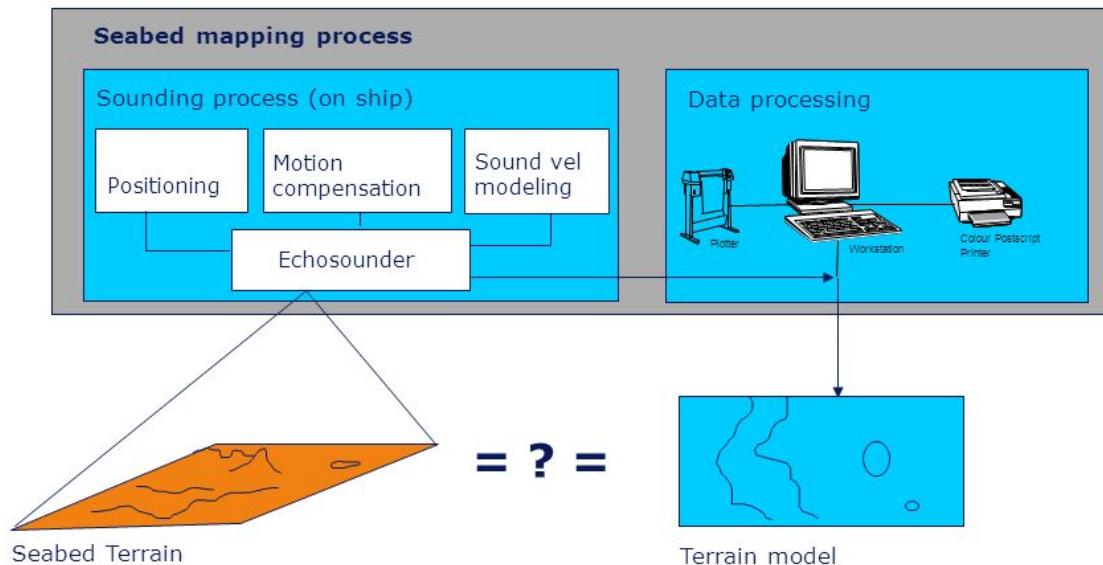
# Kahoot



# Learning objectives

- Data processing
- Error propagation
- Error budgets
- Timing and latency
- Calibrations

# Seabed mapping from ping to map



**How well does the terrain model represent the seabed terrain?**

# Sonar survey data processing

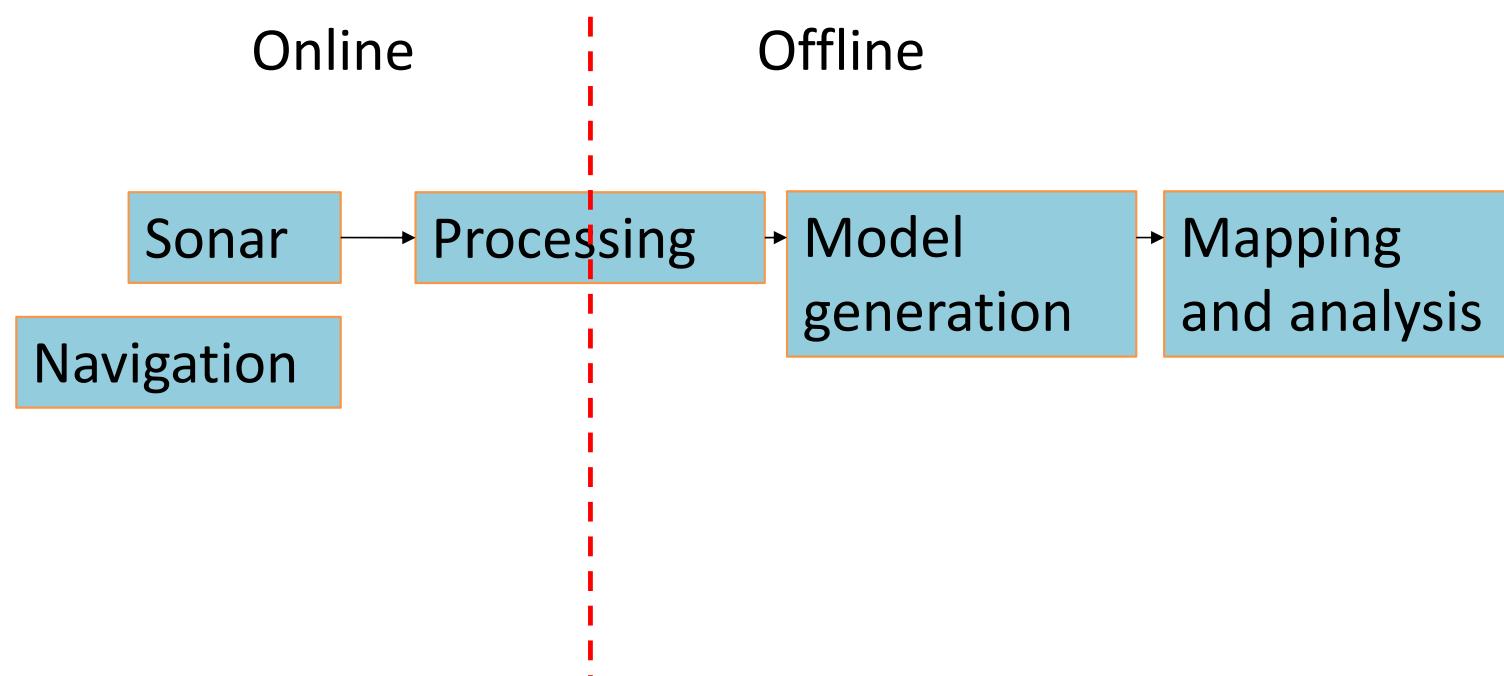
## Online

- Logging
- Data storage
- Data integrity
  - Frozen signals
  - Standard deviation
  - Jumps

## Offline

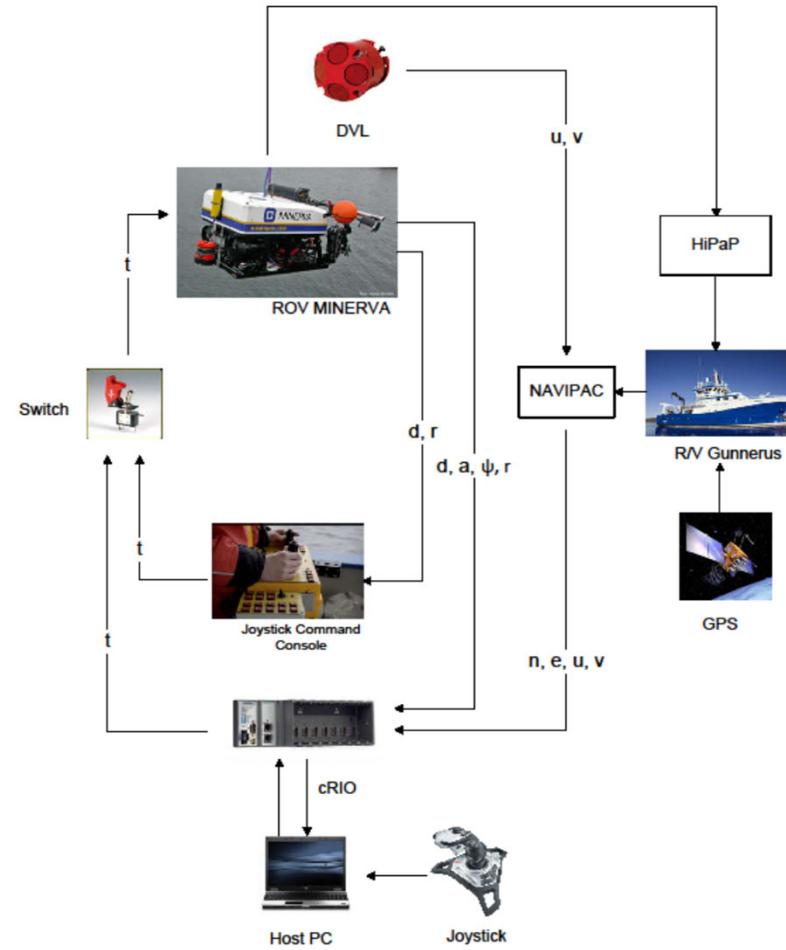
- Compensation
  - Motion
  - Speed of sound
- Data filtering
- Gridding
- Modelling
- Maps

# Processing sonar mapping data

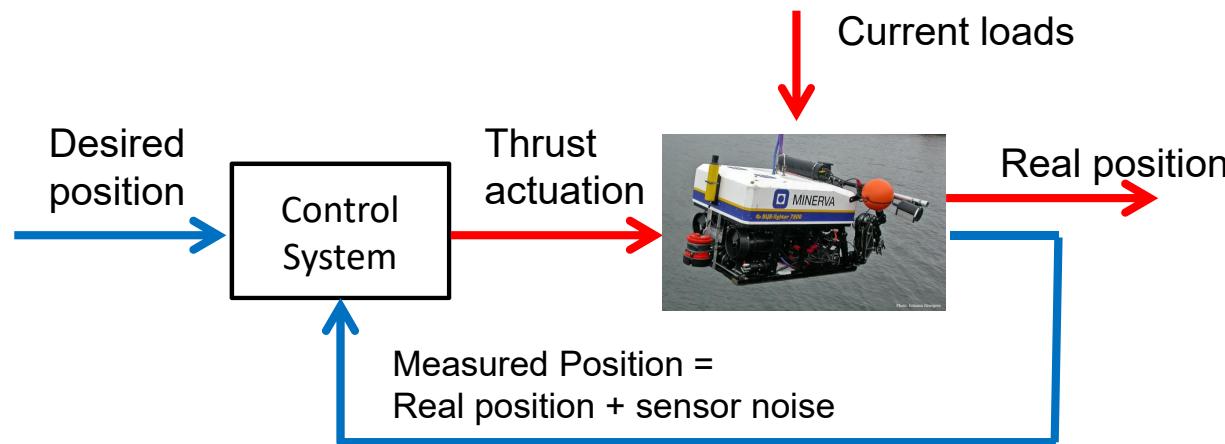


# Control systems

- Minerva implementation



## Feedback control



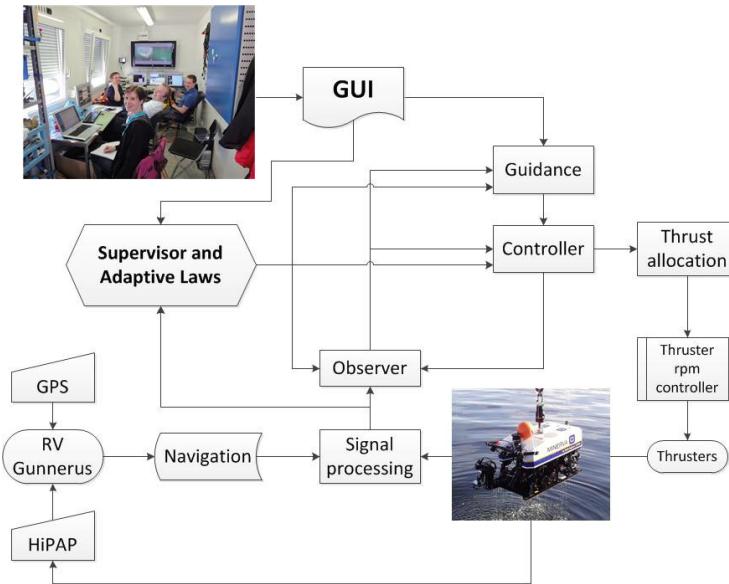
**The control system will dominate the dynamics, and we have to consider a new dynamic system – “closed-loop system”**

**The control system is also a dynamic system with**

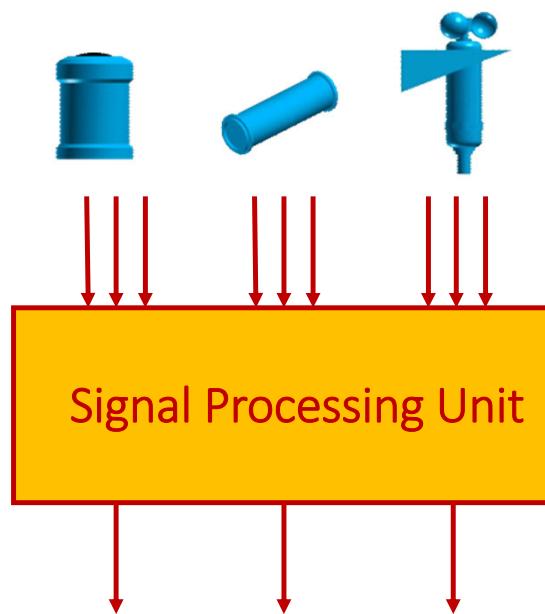
- internal states – state feedback or output feedback using observers
- actuator dynamics, saturation, control allocation, power limitation
- sensor dynamics, integration and accuracy
- computers conducting real time control

# Control system

- Station keeping
- Track lines
- GUI – user
- Guidance
- Navigation
- Controller



# Signal processing



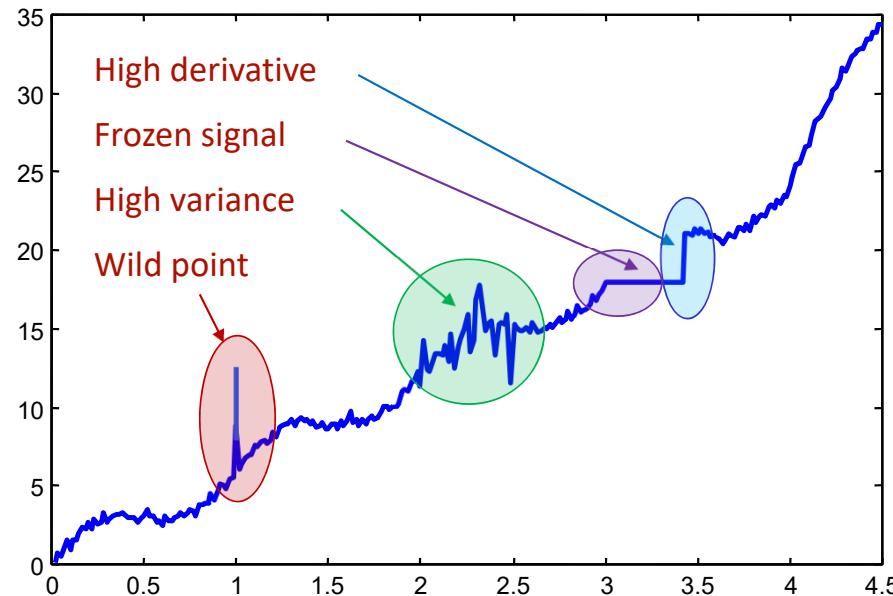
HW Signal Communication already checked

Features:

- Online Signal Quality Check
- Online weighting of sensor signals
- Multiple signal voting algorithms
- Filtering and smoothing of signals

# Signal processing - example

Examples of four different signal failures the signal QA module is detecting.



# Signal quality checking

Three level testing:

1. Tests on individual signals
  - Range check
  - Variance check
  - Wild point detection and removal
2. Sensor voting
  - Detection of sensor drift
3. Sensor weighting
  - Unbiased minimum variance measurements
  - Manual weighting

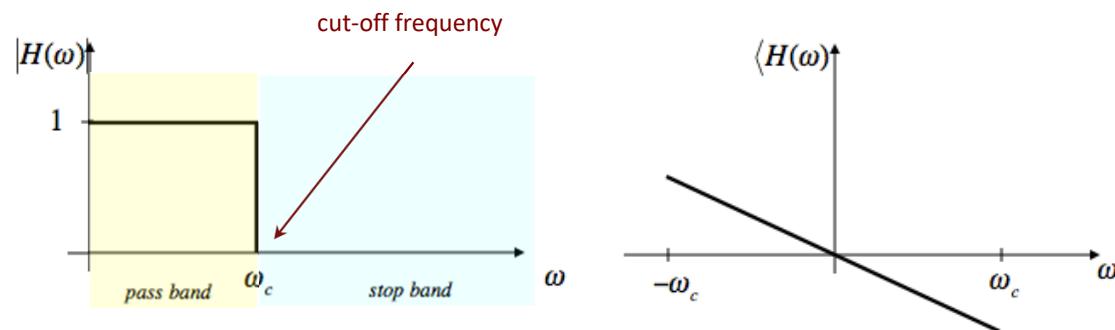
If observer (state estimator such as Kalman filter):

4. Observer test/Prediction error (Innovation/injection term)

# Conventional filters used in marine control systems

- Low pass filter suppressing e.g. noise
- High pass filter
- Band stop filters, e.g. notch filter
- Band pass filter
- Cascaded low pass and notch filter for wave filtering

## Ideal Filters: lowpass case



**Linear Phase:** all the harmonic components in the passband are delayed of the same amount of time.

In other words: delay  $t_0$  independent by the angular velocity:

$$f(t-t_0) \rightarrow F(\omega)e^{-j\omega t_0}$$

Can this filter be realized?

Response of a passband ideal filter (Fourier Transform) is described by

not causal

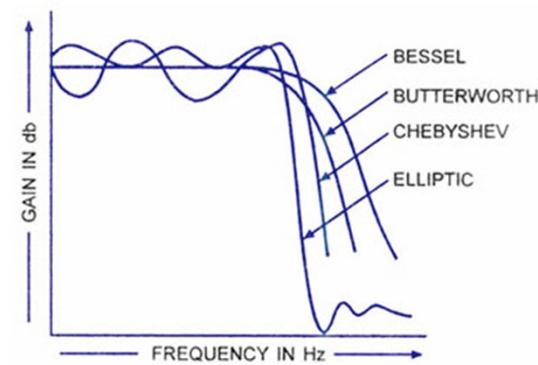


cannot be obtained!

$$y(t) = \frac{\sin(\omega_c t)}{t} \text{ (sinc):}$$

## Low pass filters comparison

Causal filter type.	Gain approximation	Linearity of the phase
Butterworth	good	good
Chebyshev	good	bad
Elliptic	very good	very bad
Bessel	bad	good



A first order low-pass filter with time constant  $T_f$  can be designed according to:

$$h_{lp}(s) = \frac{1}{1+T_f s} \quad \omega_b < \frac{1}{T_f} < \omega_e \quad \left[ \frac{\text{rad}}{\text{s}} \right]$$

This filter will suppress disturbances over the frequency  $\frac{1}{T_f}$   
 remember the effect on the Bode diagram?

## Butterworth Filter

- Good characteristics concerning the **passband**.
- **Transition band** characteristics are less good.
- It doesn't have linear phase in the passband but we can consider it as a good approximation.
- It can realize **higher order** low-pass filters:

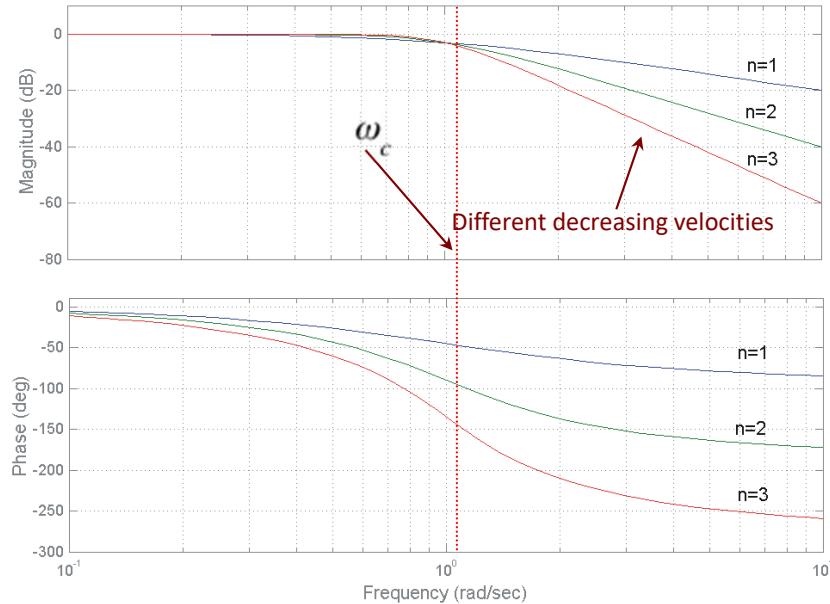
$$h_{lp}(s) = \frac{1}{p(s)}$$

$p(s)$  is found by solving the Butterworth polynomial:

$$p(s)p(-s) = 1 + \left(\frac{s}{j\omega_f}\right)^{2n}$$

$$\begin{aligned} (n=1) \quad h_{lp}(s) &= \frac{1}{1 + \frac{s}{\omega_f}} \\ (n=2) \quad h_{lp}(s) &= \frac{\omega_f^2}{s^2 + 2\zeta\omega_f s + \omega_f^2}; \quad \zeta = \sin(45^\circ) \\ (n=3) \quad h_{lp}(s) &= \frac{\omega_f^2}{s^2 + 2\zeta\omega_f s + \omega_f^2} \cdot \frac{1}{1 + \frac{s}{\omega_f}}; \quad \zeta = \sin(30^\circ) \\ (n=4) \quad h_{lp}(s) &= \prod_{i=1}^2 \frac{\omega_f^2}{s^2 + 2\zeta_i\omega_f s + \omega_f^2}; \quad \zeta_1 = \sin(22.5^\circ), \quad \zeta_2 = \sin(67.5^\circ) \end{aligned}$$

## Butterworth Filter



- cut frequency independent from the order N of the filter;
- attenuation magnitude in the stop band depends by the order N of the filter
- no oscillations in the passband or in the stop-band;
- no general rule about the phase.

$$n=1: b(s) = \frac{\omega_c}{s+\omega_c}$$

$$\dot{x}_f + \omega_c x_f = \omega_c x$$

$$n=2: b(s) = \frac{\omega_c^2}{s^2 + \sqrt{2}\omega_c s + \omega_c^2}$$

$$\ddot{x}_f + \sqrt{2}\omega_c \dot{x}_f + \omega_c^2 x_f = \omega_c^2 x$$

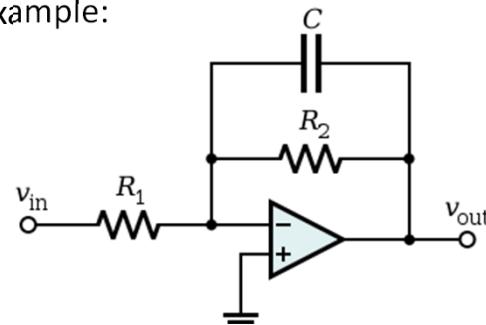
$$n=3: b(s) = \frac{\omega_c^3}{(s^2 + \omega_c s + \omega_c^2)(s + \omega_c)}$$

$$\dddot{x}_f + 2\omega_c \ddot{x}_f + 2\omega_c^2 \dot{x}_f + \omega_c^3 x = \omega_c^3 x$$

## How to practical realize an analog filter?

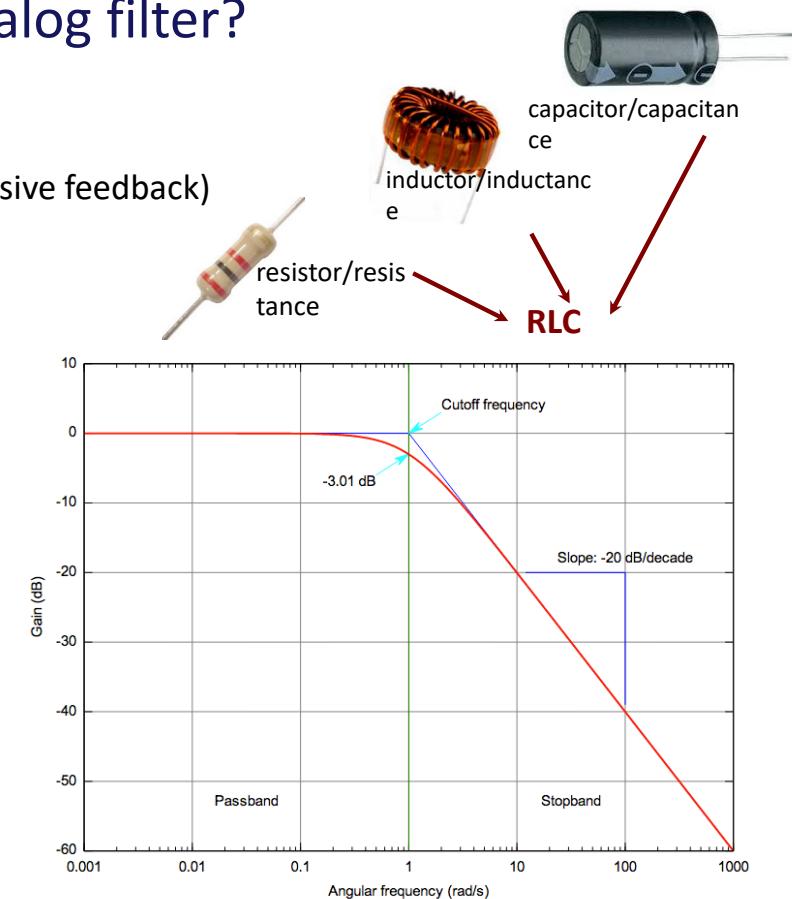
- RLC filters
- active RC filters (operational amplifier + passive feedback)
- ...

Example:



$$v_{\text{out}} = \frac{1}{1+s \cdot \tau} v_{\text{in}}$$

$$\tau = R_2 C \quad f_c = \frac{1}{2\pi R_2 C}$$



## High pass filters

High pass filters design can be seen as “complementary” as the low pass filter design.

They may be designed by substituting

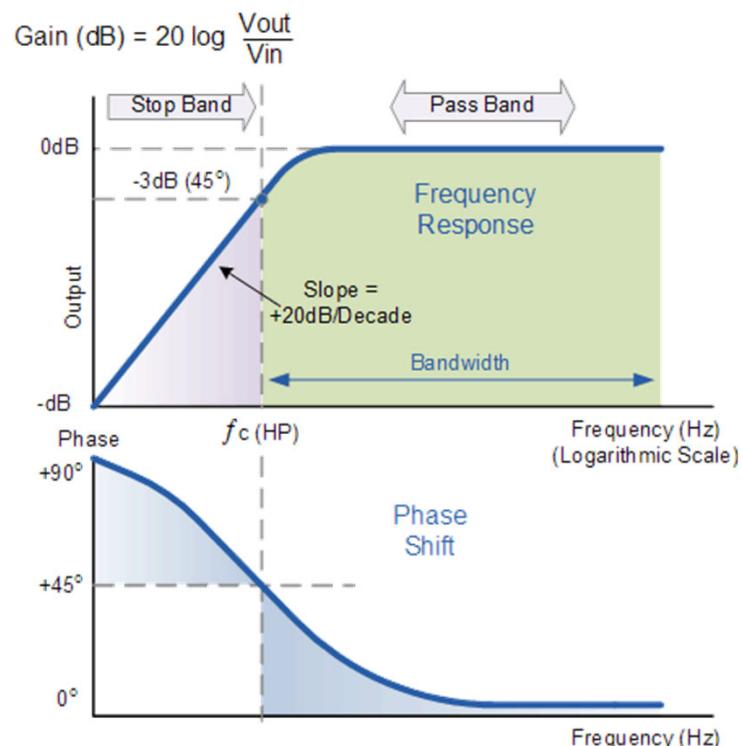
$$s \rightarrow \frac{1}{s}, \quad \omega_c \rightarrow T_c$$

In the equation describing low pass filter, e.g.

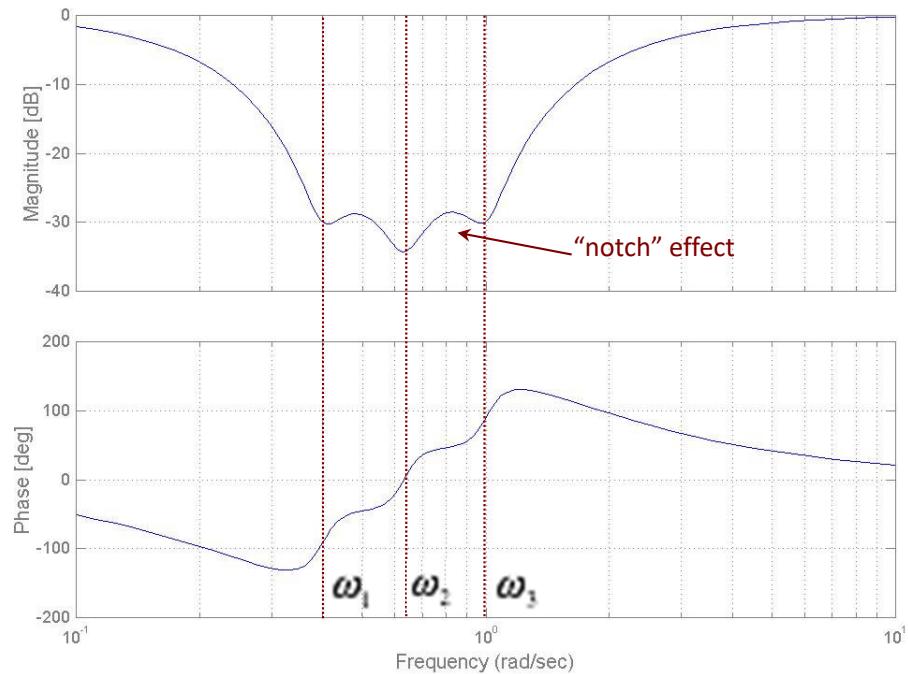
$$b(s) = \frac{\omega_c}{s + \omega_c} = \frac{1}{\frac{s}{\omega_c} + 1}$$

The corresponding high pass filter becomes

$$b^{hp}(s) = \frac{T_c}{\frac{1}{s} + T_c} = \frac{sT_c}{1 + sT_c}$$



## Band-stop Filters



Example:  
Third order filter

$$h_e = \prod_{i=1}^3 \frac{s^2 + 2\zeta_{si}\omega_i s + \omega_i^2}{s^2 + 2\zeta_{di}\omega_i s + \omega_i^2}$$

$$\zeta_{di} = 1$$

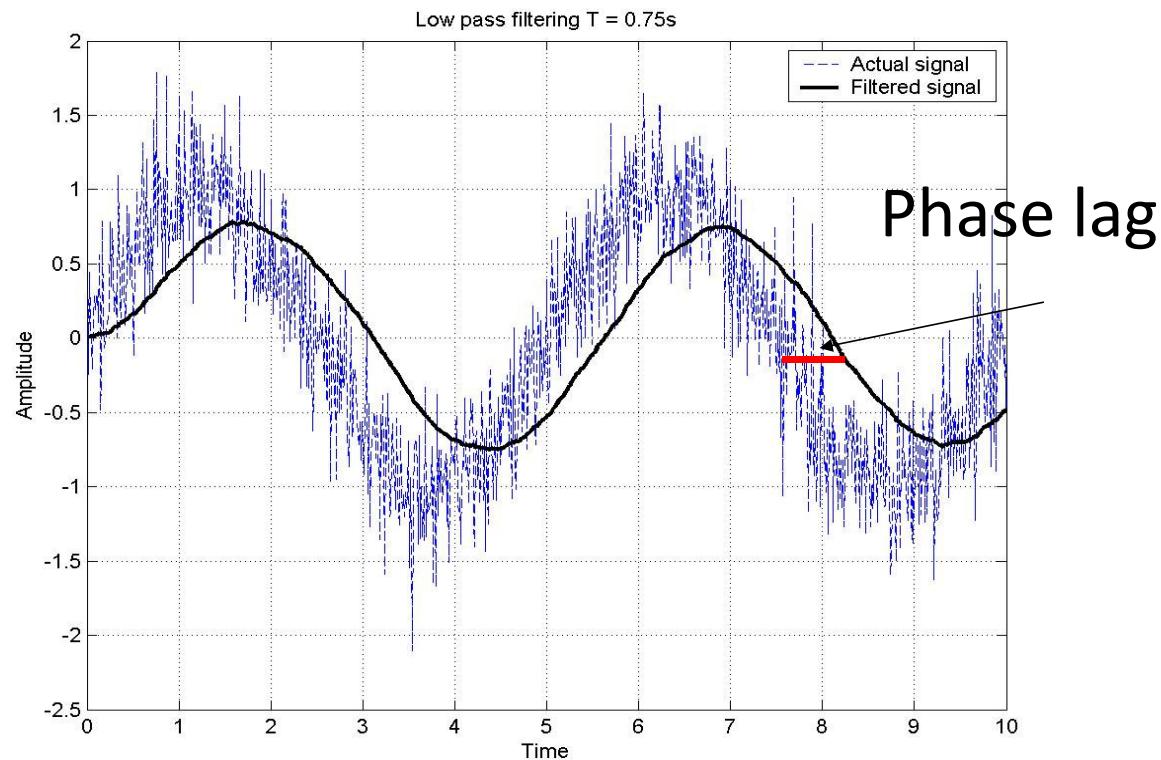
$$\zeta_{di} = 0.1$$

$$\omega_1 = 0.4$$

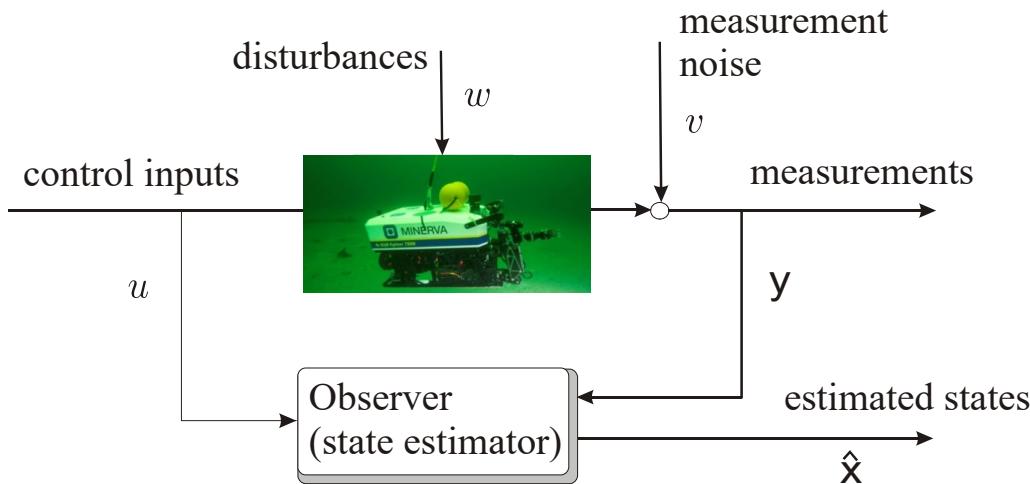
$$\omega_2 = 0.63$$

$$\omega_3 = 1.0$$

## Low pass filter



# Observer: filtering and state estimation

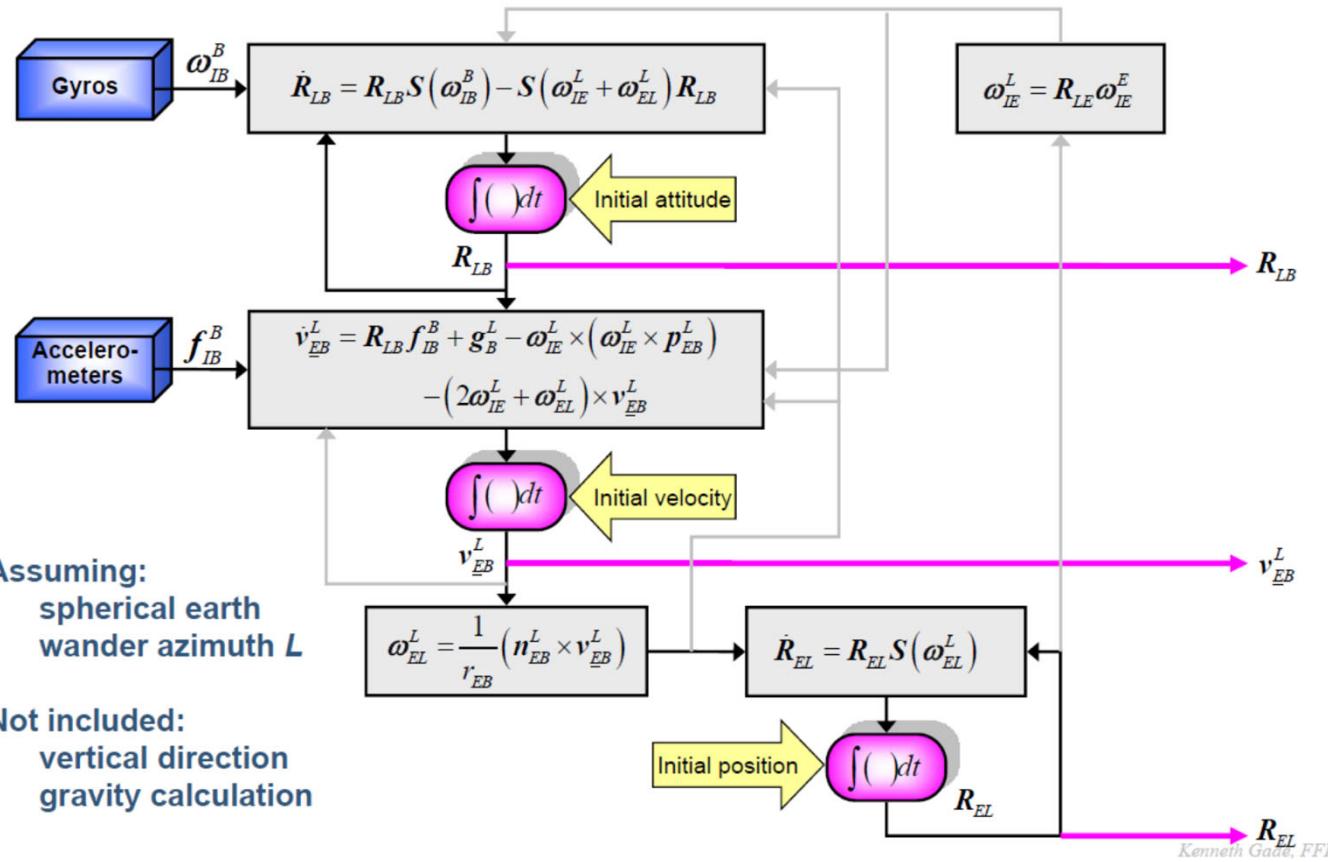


## Definition

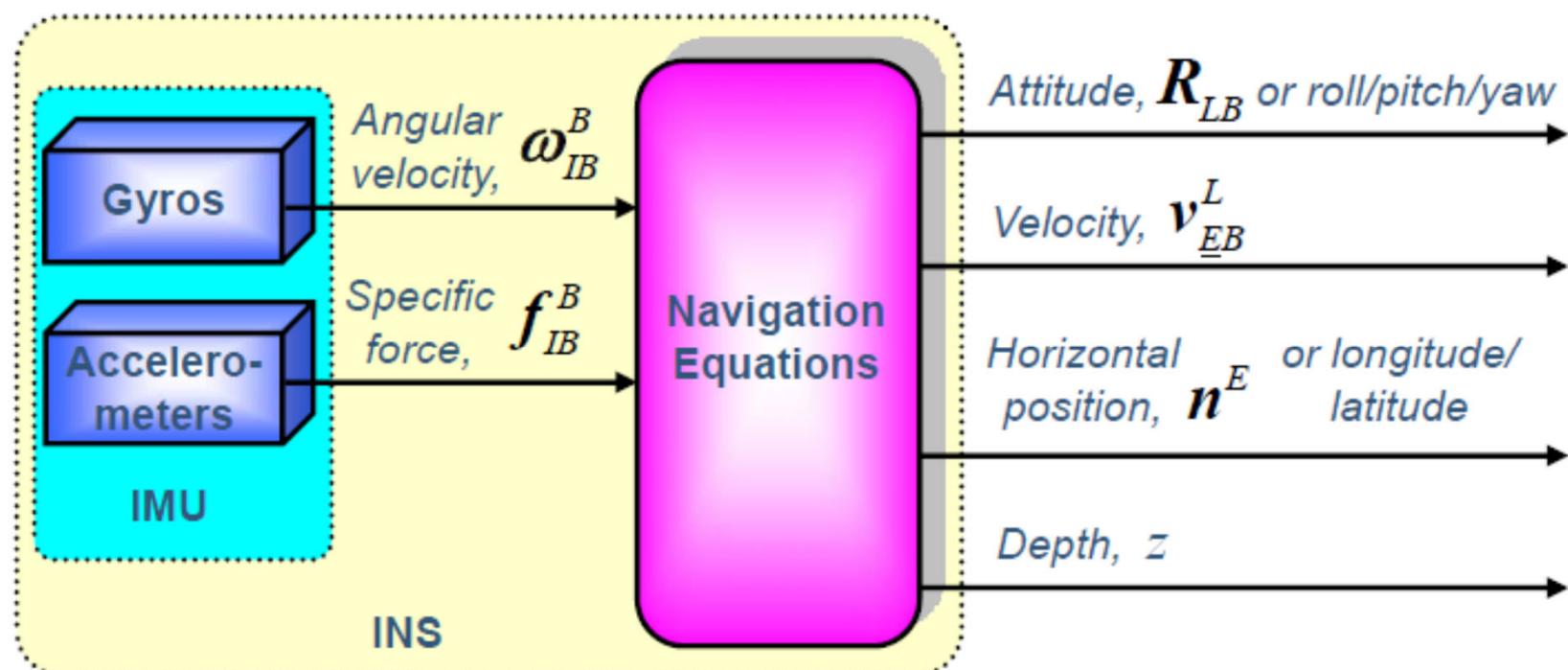
An observer or state estimator produces the state of a system from measurements of inputs and outputs

Observers reduce the phase lag and also can be used to estimate variables that are not measured.

# Inertial navigation



# Inertial navigation



# Kalman filter

- A Kalman filter is a recursive algorithm for estimating *states* in a system.
- Examples of states:
  - Position, velocity etc for a vehicle
  - pH-value, temperature etc for a chemical process
- Two sorts of information are utilized:
  - **Measurements** from relevant sensors
  - **Mathematical model** of the system (describing how the different states depend on each other, and how the measurements depend on the states)
- In addition the *accuracy* of the measurements and the model must be specified.

# Kalman filter algorithm

1. At  $t_0$  the Kalman filter is provided with an *initial estimate*, including its uncertainty (covariance matrix).
2. Based on the mathematical model and the initial estimate, a new estimate valid at  $t_1$  is *predicted*. The uncertainty of the *predicted estimate* is calculated based on the initial uncertainty, and the accuracy of the model (*process noise*).
3. Measurements valid at  $t_1$  give new information about the states. Based on the accuracy of the measurements (*measurement noise*) and the uncertainty in the predicted estimate, the two sources of information are weighed and a new *updated estimate* valid at  $t_1$  is calculated. The uncertainty of this estimate is also calculated.
4. At  $t_2$  a new estimate is predicted as in step 2, but now based on the updated estimate from  $t_1$ .

The prediction and the following update are repeated each time a new measurement arrives.

***If the models/assumptions are correct, the Kalman filter will deliver optimal estimates.***



# Kalman filter equations

State space model:

$$\begin{aligned}\mathbf{x}_k &= \boldsymbol{\Phi}_{k-1} \mathbf{x}_{k-1} + \boldsymbol{\nu}_{k-1}, \quad \boldsymbol{\nu}_k \sim N(\mathbf{0}, \mathbf{V}_k) \\ \mathbf{y}_k &= \mathbf{D}_k \mathbf{x}_k + \boldsymbol{w}_k, \quad \boldsymbol{w}_k \sim N(\mathbf{0}, \mathbf{W}_k)\end{aligned}$$

Initial estimate ( $k = 0$ ):

$$\hat{\mathbf{x}}_0 = E(\mathbf{x}_0), \quad \hat{\mathbf{P}}_0 = E\left((\mathbf{x}_0 - \hat{\mathbf{x}}_0)(\mathbf{x}_0 - \hat{\mathbf{x}}_0)^T\right)$$

State and covariance prediction:

$$\begin{aligned}\bar{\mathbf{x}}_k &= \boldsymbol{\Phi}_{k-1} \hat{\mathbf{x}}_{k-1} \\ \bar{\mathbf{P}}_k &= \boldsymbol{\Phi}_{k-1} \hat{\mathbf{P}}_{k-1} \boldsymbol{\Phi}_{k-1}^T + \mathbf{V}_{k-1}\end{aligned}$$

Measurement update (using  $y_k$ ):

$$\begin{aligned}\hat{\mathbf{x}}_k &= \bar{\mathbf{x}}_k + \mathbf{K}_k (\mathbf{y}_k - \mathbf{D}_k \bar{\mathbf{x}}_k) \\ \hat{\mathbf{P}}_k &= (\mathbf{I} - \mathbf{K}_k \mathbf{D}_k) \bar{\mathbf{P}}_k\end{aligned}$$

Kalman gain matrix:

$$\mathbf{K}_k = \bar{\mathbf{P}}_k \mathbf{D}_k^T \left( \mathbf{D}_k \bar{\mathbf{P}}_k \mathbf{D}_k^T + \mathbf{W}_k \right)^{-1}$$

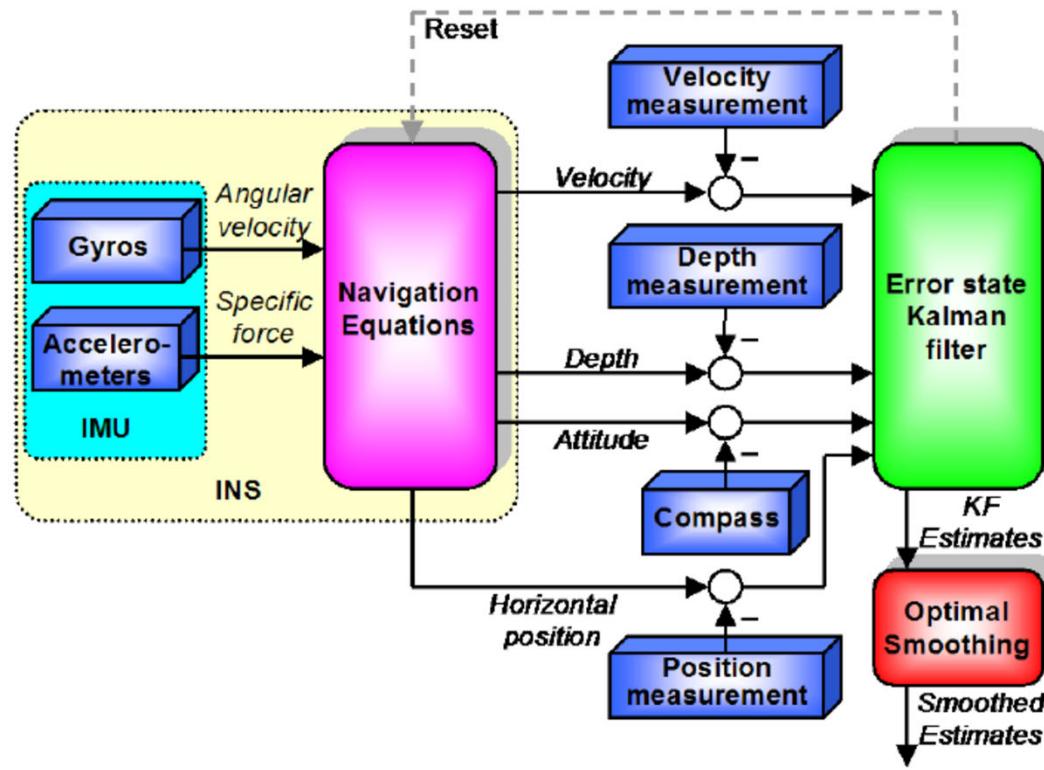
# Kalman Filter Design for Navigation

- **Objective:** Find the vehicle position, attitude and velocity with the best accuracy possible
- **Possible basis:**
  - Sensor measurements (measurements)
  - System knowledge (mathematical model)
  - Control variables (measurements)
- We utilize sensor measurements and knowledge of their behavior (error models).
- This information is combined by means of an error-state Kalman filter.

# Measurements

Sensor	Measurement	Symbol
IMU	Angular velocity, specific force	$\omega_{IB}^B, f_{IB}^B$
DGPS/USBL	Horizontal position measurement	$p_{EB}^E$
Pressure sensor	Depth	
DVL	AUV velocity (relative the seabed) projected into the body (B) coordinate system	$v_{EB}^B$
Compass	Heading (relative north)	$\psi_{north}$

# Aided Inertial Navigation System





# Kalman filter equations

State space model:

$$\begin{aligned}\mathbf{x}_k &= \Phi_{k-1} \mathbf{x}_{k-1} + \mathbf{v}_{k-1}, & \mathbf{v}_k &\sim N(\mathbf{0}, V_k) \\ \mathbf{y}_k &= \mathbf{D}_k \mathbf{x}_k + \mathbf{w}_k, & \mathbf{w}_k &\sim N(\mathbf{0}, W_k)\end{aligned}$$

Initial estimate ( $k = 0$ ):

$$\hat{\mathbf{x}}_0 = E(\mathbf{x}_0), \quad \hat{\mathbf{P}}_0 = E\left((\mathbf{x}_0 - \hat{\mathbf{x}}_0)(\mathbf{x}_0 - \hat{\mathbf{x}}_0)^T\right)$$

State and covariance prediction:

$$\begin{aligned}\bar{\mathbf{x}}_k &= \Phi_{k-1} \hat{\mathbf{x}}_{k-1} \\ \bar{\mathbf{P}}_k &= \Phi_{k-1} \hat{\mathbf{P}}_{k-1} \Phi_{k-1}^T + V_{k-1}\end{aligned}$$

Measurement update (using  $y_k$ ):

$$\begin{aligned}\hat{\mathbf{x}}_k &= \bar{\mathbf{x}}_k + \mathbf{K}_k (\mathbf{y}_k - \mathbf{D}_k \bar{\mathbf{x}}_k) \\ \hat{\mathbf{P}}_k &= (\mathbf{I} - \mathbf{K}_k \mathbf{D}_k) \bar{\mathbf{P}}_k\end{aligned}$$

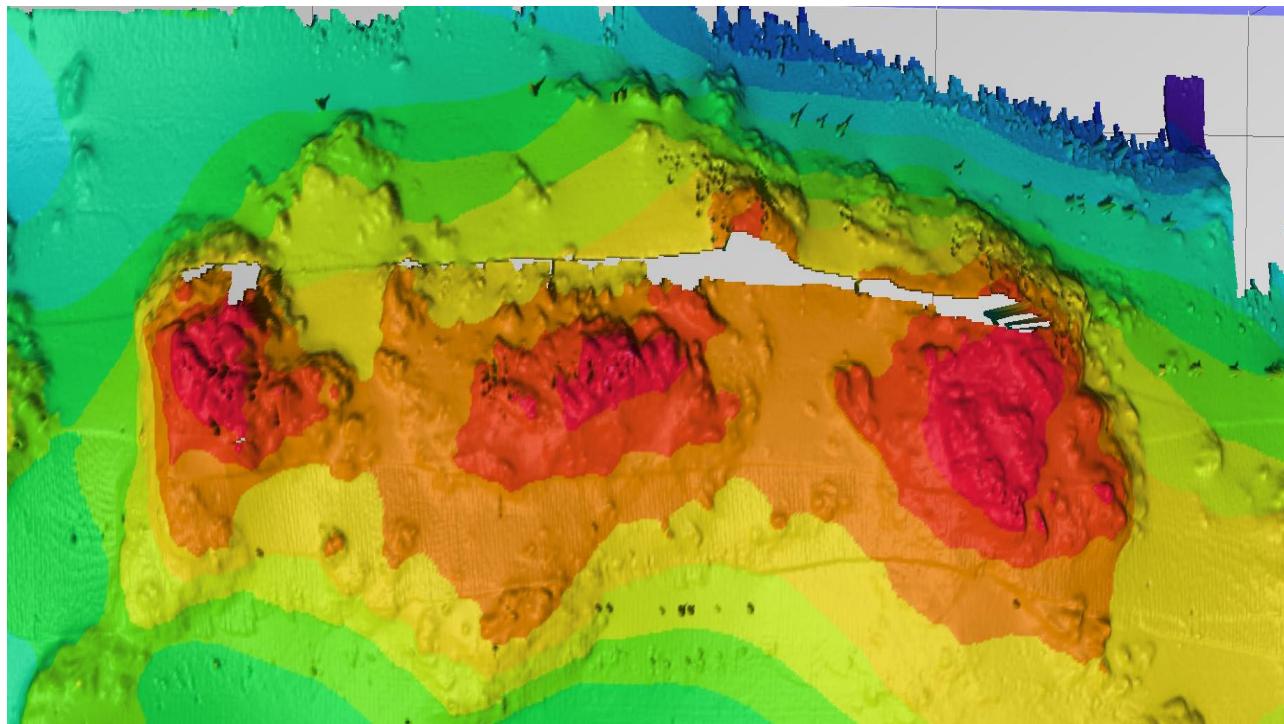
Kalman gain matrix:

$$\mathbf{K}_k = \bar{\mathbf{P}}_k \mathbf{D}_k^T \left( \mathbf{D}_k \bar{\mathbf{P}}_k \mathbf{D}_k^T + W_k \right)^{-1}$$

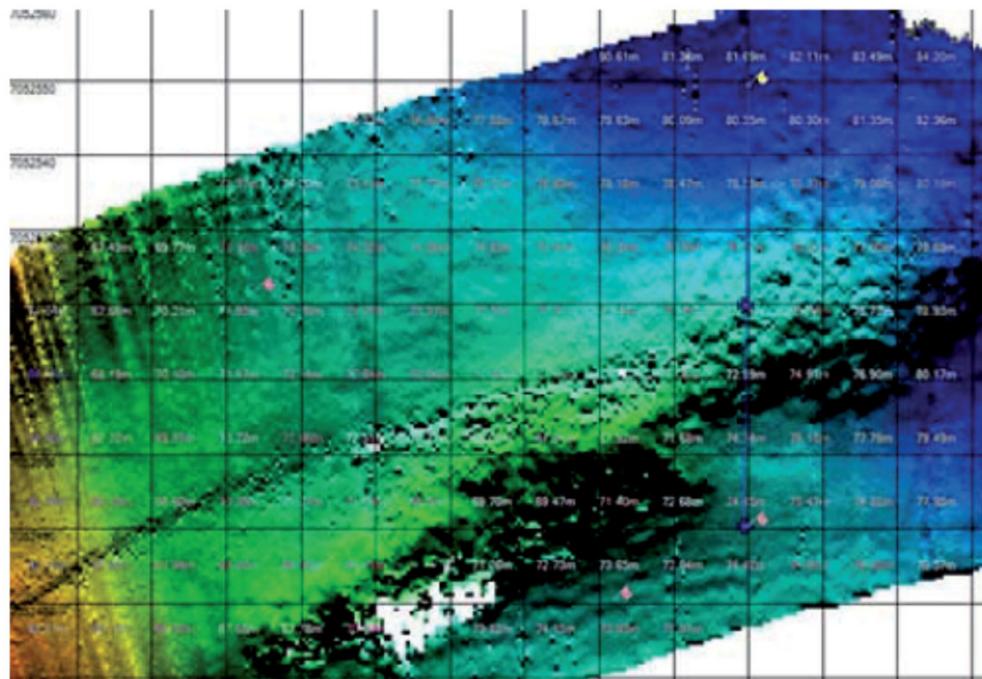
# Accuracy in seabed mapping

- Errors
  - Stochastics
  - Systematic errors
  - Blunders
- Instrument accuracy
- Navigation accuracy
- Set up integrity
  - Offset
  - Time
  - Angular
  - Level arms
- Environmental parameters

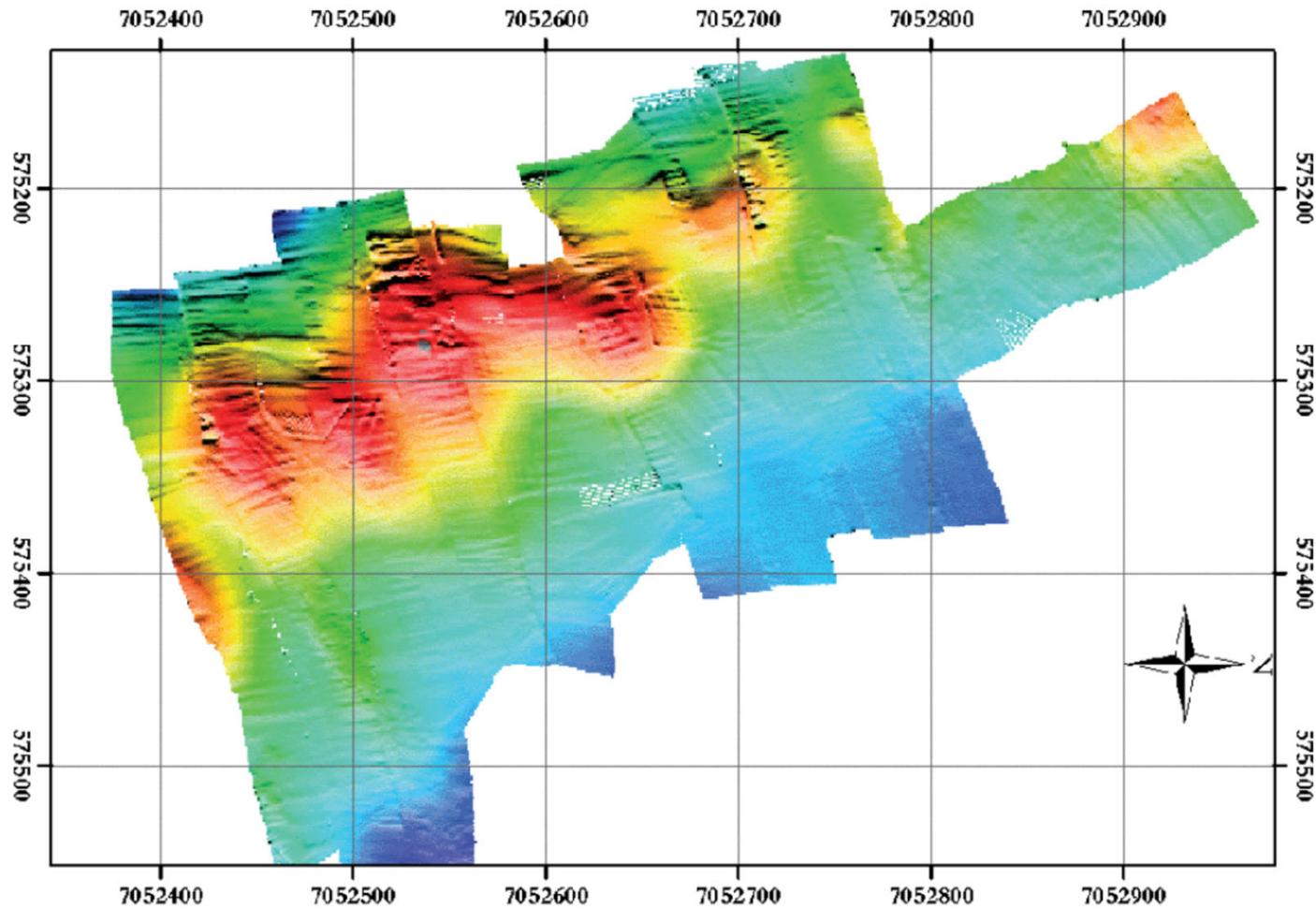
# Results – EM 3002



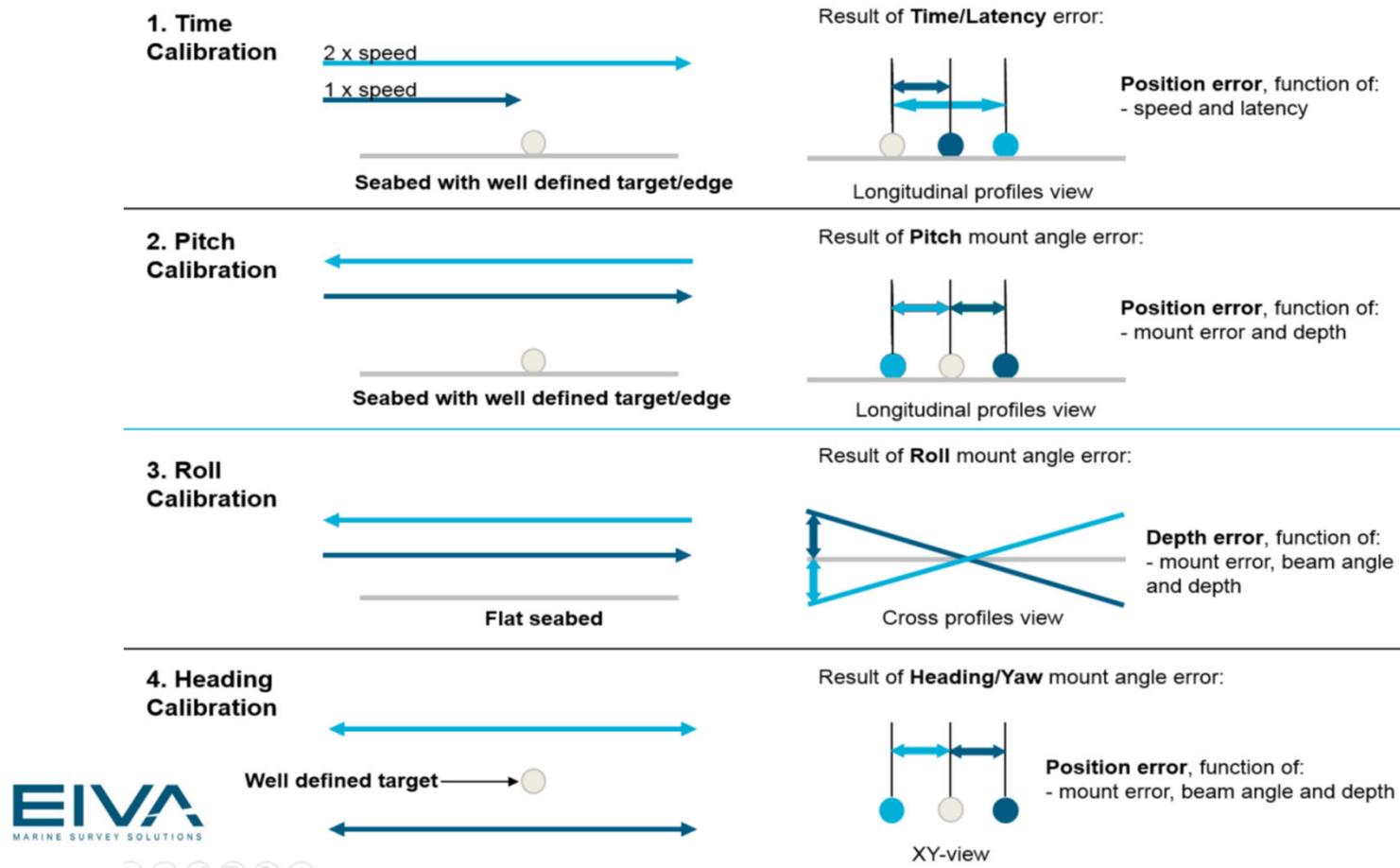
# MBE



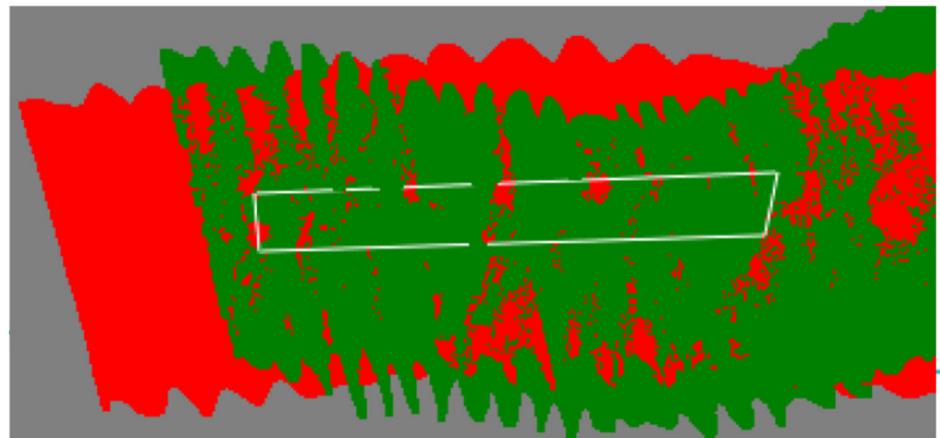
# MBE



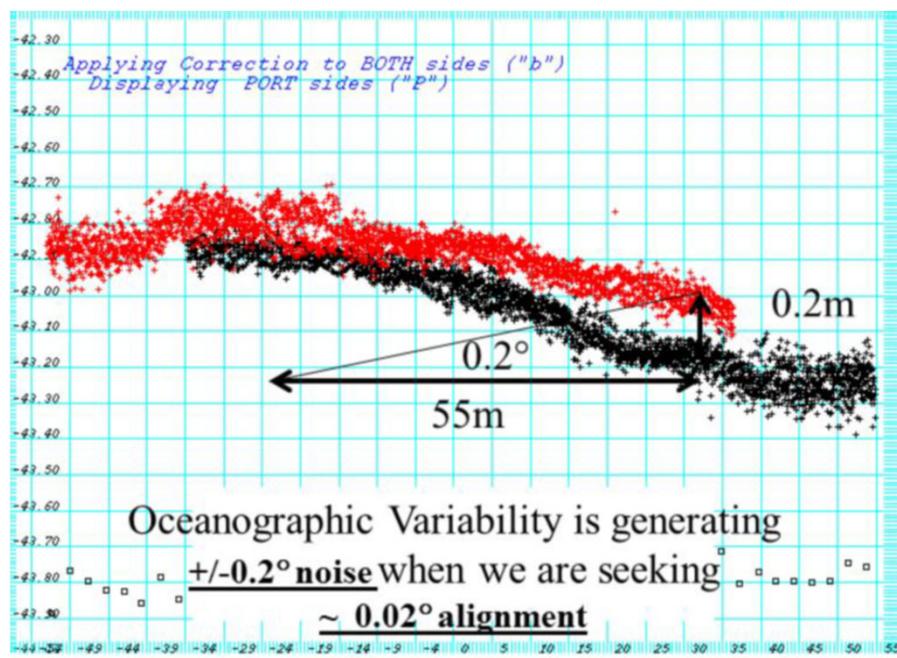
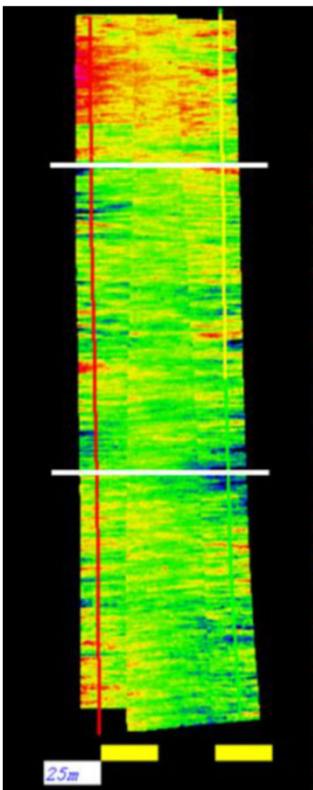
# Patch test



# Patch test



# MBE



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# Error propagation

$$x = f(a, b, c)$$

$$dx_i = f(da_i, db_i, dc_i)$$

$$dx = \left( \frac{\delta x}{\delta a} \right)_{b,c} da, \quad \left( \frac{\delta x}{\delta b} \right)_{a,c} db, \quad \left( \frac{\delta x}{\delta c} \right)_{a,b} dc$$

$$\sigma_x^2 = \left( \frac{\delta x}{\delta a} \right)^2 \sigma_a^2 + \left( \frac{\delta x}{\delta b} \right)^2 \sigma_b^2 + \left( \frac{\delta x}{\delta c} \right)^2 \sigma_c^2$$

$$x = a + b - c \qquad \qquad \sigma_x = \sqrt{\sigma_a^2 + \sigma_b^2 + \sigma_c^2}$$

Assuming cross terms cancel out

# LAW OF PROPAGATION OF VARIANCES

$$A = b + 2bc + 3d$$

A = the unknown quantity

b, c, and d = the known quantities

$$\sigma_A^2 = \left( \frac{\partial A}{\partial b} \right)^2 \sigma_b^2 + \left( \frac{\partial A}{\partial c} \right)^2 \sigma_c^2 + \left( \frac{\partial A}{\partial d} \right)^2 \sigma_d^2 + 2 \left( \left( \frac{\partial A}{\partial b} \right) \left( \frac{\partial A}{\partial c} \right) \sigma_{bc} + \left( \frac{\partial A}{\partial b} \right) \left( \frac{\partial A}{\partial d} \right) \sigma_{bd} + \left( \frac{\partial A}{\partial c} \right) \left( \frac{\partial A}{\partial d} \right) \sigma_{cd} \right)$$

$$\left( \frac{\partial A}{\partial b} \right) = 1 + 2c \quad \left( \frac{\partial A}{\partial c} \right) = 2b \quad \left( \frac{\partial A}{\partial d} \right) = 3$$

$$\sigma_A^2 = (1+2c)^2 \sigma_b^2 + (2b)^2 \sigma_c^2 + (3)^2 \sigma_d^2$$

$$\sigma_A^2 = (1+4c+4c^2) \sigma_b^2 + 4b^2 \sigma_c^2 + 9 \sigma_d^2$$

# Error propagation for a USBL set up

USBL positioning

- $P_s$  – ship position
- $\omega$  – bearing angle
- $\nu$  – depression angle

$$P_{USBL} = P_S + \begin{bmatrix} c_\omega & -s_\omega & 0 \\ s_\omega & c_\omega & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c_\nu & 0 & s_\nu \\ 0 & 1 & 0 \\ -s_\nu & 0 & c_\nu \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ r \end{bmatrix} = P_S + \begin{bmatrix} c_\omega s_\nu \\ s_\omega s_\nu \\ c_\nu \end{bmatrix} r$$

$$P_{USBL} = P_S + R_{z,\omega} R_{y,\nu} [0, 0, r]^T$$

$$\sigma_{USBL,X}^2 \approx \sigma_{S,X}^2 + \left( \frac{\delta X}{\delta \omega} \right)^2 \sigma_\omega^2 + \left( \frac{\delta X}{\delta \nu} \right)^2 \sigma_\nu^2 + \left( \frac{\delta X}{\delta r} \right)^2 \sigma_r^2$$

$$\sigma_{USBL,X}^2 \approx \sigma_{S,X}^2 + \left( \frac{\delta c_\omega s_\nu r}{\delta \omega} \right)^2 \sigma_\omega^2 + \left( \frac{\delta c_\omega s_\nu r}{\delta \nu} \right)^2 \sigma_\nu^2 + \left( \frac{\delta c_\omega s_\nu r}{\delta r} \right)^2 \sigma_r^2$$

$$\sigma_{USBL,X}^2 \approx \sigma_{S,X}^2 + (-s_\omega s_\nu r)^2 \sigma_\omega^2 + (c_\omega c_\nu r)^2 \sigma_\nu^2 + (c_\omega s_\nu)^2 \sigma_r^2$$

# Example

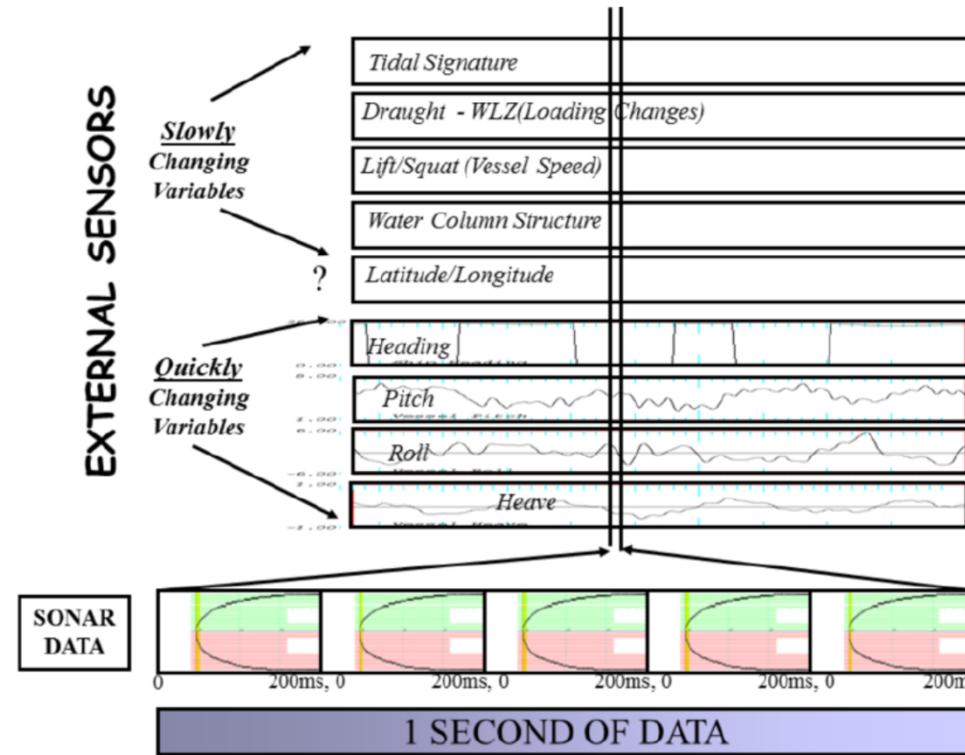
Measurement	Instrument	Example	Stddev
Range	USBL HiPaP	200	0.1 [m]
Depression angle	USBL HiPaP	70	0.12 [deg]
Bearing angle	USBL HiPaP	40	0.12 [deg]
Position	GPS - Seatex DPS 116	0	0.5 [m]

$$P_{USBL} = P_S + R_{z,\omega} R_{y,\nu} [0, 0, r]^T$$

$$\sigma_{USBL,X}^2 \approx 0.5^2 + (-\sin(40) \cdot \sin(70) \cdot 200)^2 (0.12 \cdot \frac{\pi}{180})^2 + (\cos(40) \cdot \cos(70) \cdot 200)^2 (0.12 \cdot \frac{\pi}{180})^2 + (\cos(40) \cdot \sin(70))^2 (0.1)^2$$

$$\sigma_{USBL,X} \approx \sqrt{\sigma_{USBL,X}^2} = 0.5755 \text{ m}$$

# Timing and latency



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# Learning objectives

- Data processing
- Error propagation
- Error budgets
- Timing and latency
- Calibrations

# More reading

## Processing

- Anonsen 2013
- Kebkal 2017

## Error propagation

- Jalving 1999
- Gade 2005