

# STEEL DESIGN TO EUROCODE 3

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# GENERAL PRINCIPLES

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**THE LIMIT STATE DESIGN METHOD CAN BE SUMMARISED AS FOLLOWS:**

- **IDENTIFYING RELEVANT LIMIT STATES AT WHICH STRUCTURAL BEHAVIOUR IS TO BE CHECKED**
- **FOR EACH OF THESE STATES DETERMINING RELEVANT LOADS/ACTIONS AND RESULTING DESIGN EFFECTS**
- **CHECKING THAT NONE OF THE LIMIT STATES ARE EXCEEDED**

# LIMIT STATE DESIGN

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THIS CAN BE EXPRESSED MATHEMATICALLY AS

$$R_d \geq S_d$$

WHERE

$S_d$  IS THE DESIGN EFFECT OF THE LOADS I.E. INTERNAL FORCES AND MOMENTS,  
AND IS GIVEN BY

$$S_d = f_n \{ \gamma_{f1} F_{k,1}, \gamma_{f2} F_{k,2}, \gamma_{f3} F_{k,3} \dots \}$$

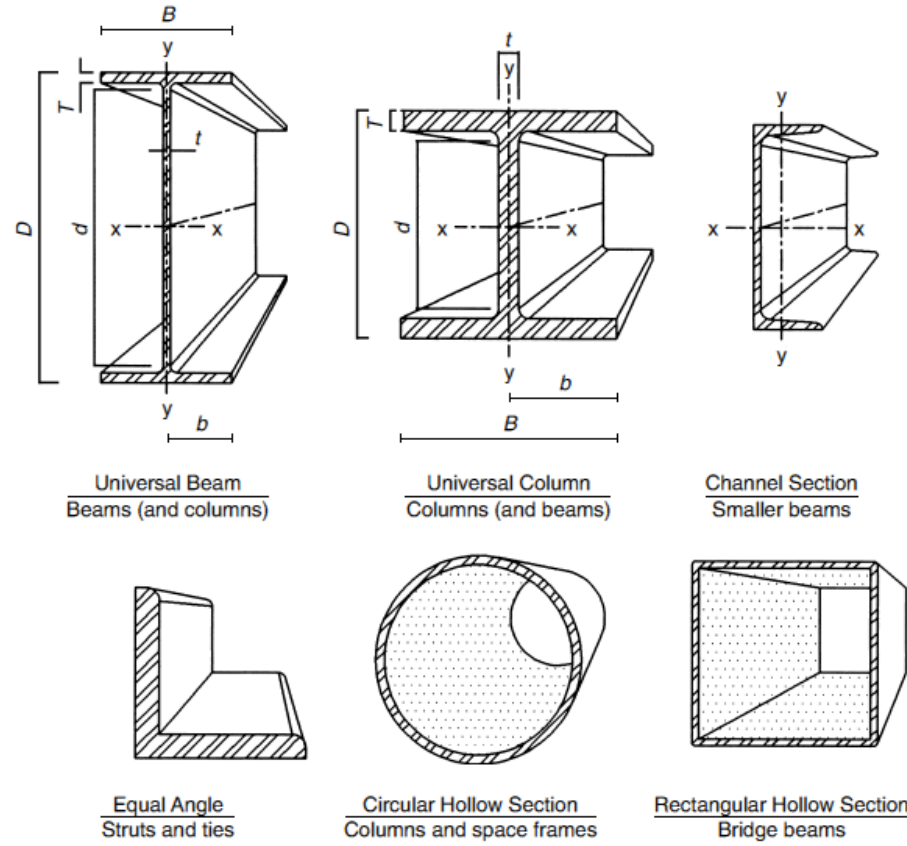
$R_d$  IS THE DESIGN STRENGTH OF ELEMENT OR STRUCTURE AND IS GIVEN BY

$$R_d = f_n \{ f_1 / \gamma_{m1}, f_2 / \gamma_{m2}, f_3 / \gamma_{m3} \dots \}$$

# LIMIT STATES RELEVANT TO THE DESIGN OF STEEL STRUCTURES

ULTIMATE	SERVICEABILITY
<ul style="list-style-type: none"><li>• <b>STRENGTH (INCLUDING GENERAL YIELDING, RUPTURE, BUCKLING AND FORMING A MECHANISM)</b></li><li>• <b>STABILITY AGAINST OVERTURNING AND SWAY STABILITY</b></li><li>• <b>FRACTURE DUE TO FATIGUE</b></li><li>• <b>BRITTLE FRACTURE</b></li></ul>	<ul style="list-style-type: none"><li>• <b>DEFLECTION</b></li><li>• <b>VIBRATION</b></li><li>• <b>WIND INDUCED OSCILLATION</b></li><li>• <b>DURABILITY</b></li></ul>

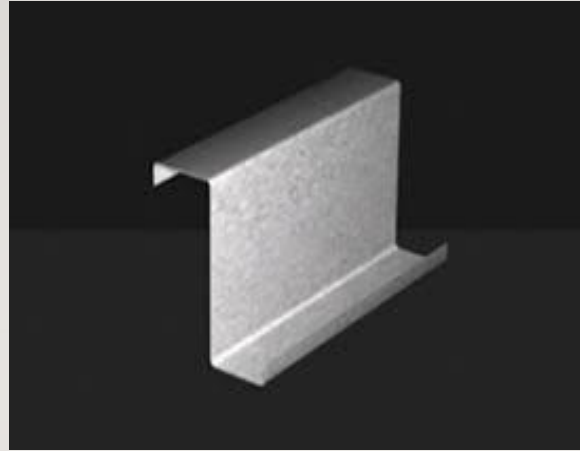
# STANDARD ROLLED STEEL SECTION







SIGMA BEAM



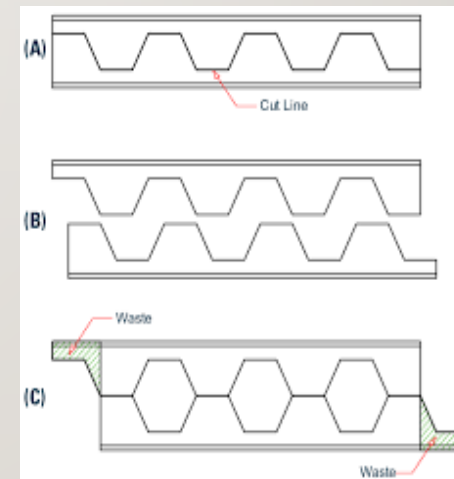
ZED BEAM



SIGMA AND ZED SHEETING RAILS

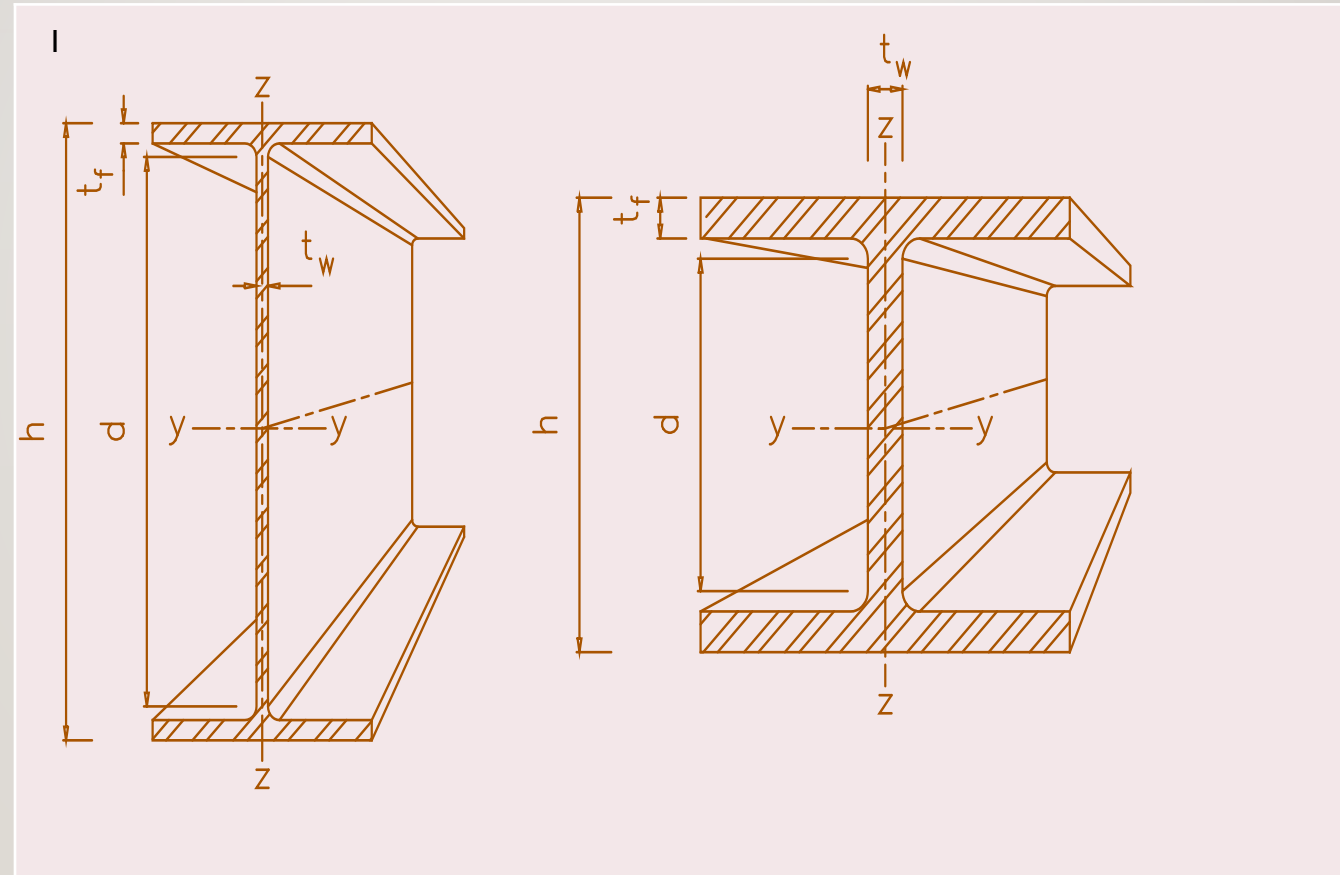


CASTELLATED BEAM



MANUFACTURING PROCESS

# MEMBER DEFINITIONS AND AXES USED IN EC3



# CHARACTERISTIC LOADS/ACTIONS

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**CHARACTERISTIC PERMANENT ( $g_k, G_k$ ), VARIABLE ( $q_k, Q_k$ ) AND WIND ACTIONS ( $W_k$ ) ARE OBTAINED FROM:**

- **EN 1991: ACTIONS ON STRUCTURES (EC1)**
- **MANUFACTURER'S LITERATURE**

## **OTHER DOCUMENTS**

- **BS 6399: PART 1 – DEAD AND IMPOSED LOADS**
  - **BS648 – WEIGHT OF BUILDING MATERIALS**
  - **CP3: CHAPTER V: PART 2 / BS 6399: PART 2 – WIND LOADS**
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# SCOPE OF EUROCODE 1

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Document No	Subject
<b>BS EN 1991-1-1</b>	<b>Densities, self-weight and imposed loads for buildings</b>
<b>BS EN 1991-1-2</b>	<b>Actions on structures exposed to fire</b>
<b>BS EN 1991-1-3</b>	<b>Snow loads</b>
<b>BS EN 1991-1-4</b>	<b>Wind loads</b>
<b>BS EN 1991-1-5</b>	<b>Thermal actions</b>
<b>BS EN 1991-1-6</b>	<b>Actions during execution</b>
<b>BS EN 1991-1-7</b>	<b>Accidental actions due to impact and explosions</b>
<b>BS EN 1991-2</b>	<b>Traffic loads on bridges</b>
<b>BS EN 1991-3</b>	<b>Actions induced by cranes and machinery</b>
<b>BS EN 1991-4</b>	<b>Actions in silos and tanks</b>

# **DESIGN LOADS/ACTION – ULTIMATE LIMIT STATES**

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**DESIGN LOADS/ACTIONS AT ULTIMATE LIMIT STATE FOR STRENGTH AND STABILITY CALCULATIONS – THE CHARACTERISTIC LOADS/ACTIONS ARE MULTIPLIED BY A PARTIAL SAFETY FACTOR TAKEN FROM EN 1990 (EC0).**

**SEVERAL LOAD CASES MAY NEED TO BE CONSIDERED TO OBTAIN A “WORST CASE” ENVELOP OF FORCES AND MOMENTS AROUND THE STRUCTURE.**



# DESIGN VALUE OF ACTIONS (EN 1990)

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THE DESIGN VALUE OF ACTION EFFECTS,  $E_d$ , ASSUMING THE STRUCTURE IS SUBJECTED TO BOTH A PERMANENT ACTION AND A VARIABLE ACTION CAN BE ASSESSED USING THE FOLLOWING EXPRESSION

$$E_d = \sum_{j \geq 1} \gamma_{G,j} G_{k,j} + \gamma_{Q,1} Q_{k,1}$$

THE DESIGN VALUE OF AN ACTION EFFECT DUE TO A PERMANENT ACTION AND TWO (OR MORE) VARIABLE ACTIONS E.G. IMPOSED PLUS WIND LOAD, IS OBTAINED USING THE FOLLOWING EXPRESSION:

$$E_d = \sum_{j \geq 1} \gamma_{G,j} G_{k,j} + \gamma_{Q,1} Q_{k,1} + \sum_{i \geq 2} \gamma_{Q,i} \psi_{0,i} Q_{k,i}$$

# PARTIAL LOAD FACTORS

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## PARTIAL LOAD FACTORS FOR COMMON LOAD COMBINATIONS (BASED ON EN 1990)

### COMMON LOAD COMBINATIONS AND FACTORS

- $1.35G_k$  “+”  $1.5Q_k$
- $1.35G_k$  “+”  $1.5W_k$
- $1.00G_k$  “+”  $1.5W_k$  (uplift)
- $1.35G_k$  “+”  $1.5Q_k$  “+”  $0.75W_k$
- $1.35G_k$  “+”  $1.05Q_k$  “+”  $1.5W_k$



# DESIGN LOADS/ACTION – SERVICEABILITY LIMIT STATES

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TO OBTAIN DESIGN LOADING AT SERVICEABILITY LIMIT  
STATE FOR CALCULATION OF DEFLECTIONS USE THE  
MOST ADVERSE REALISTIC COMBINATION OF  
UNFACTORED IMPOSED LOADS/VARIABLE ACTIONS.

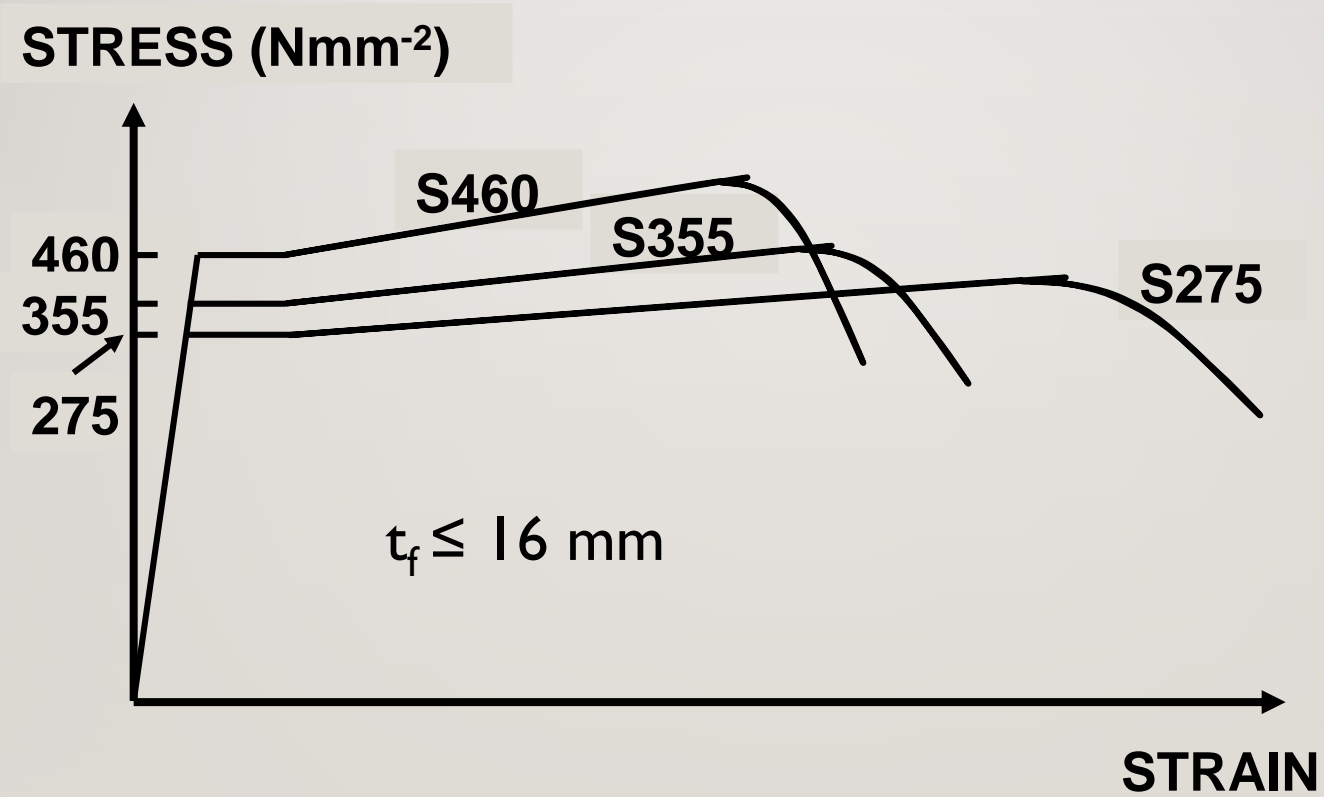
# **CHARACTERISTIC AND DESIGN STRENGTHS**

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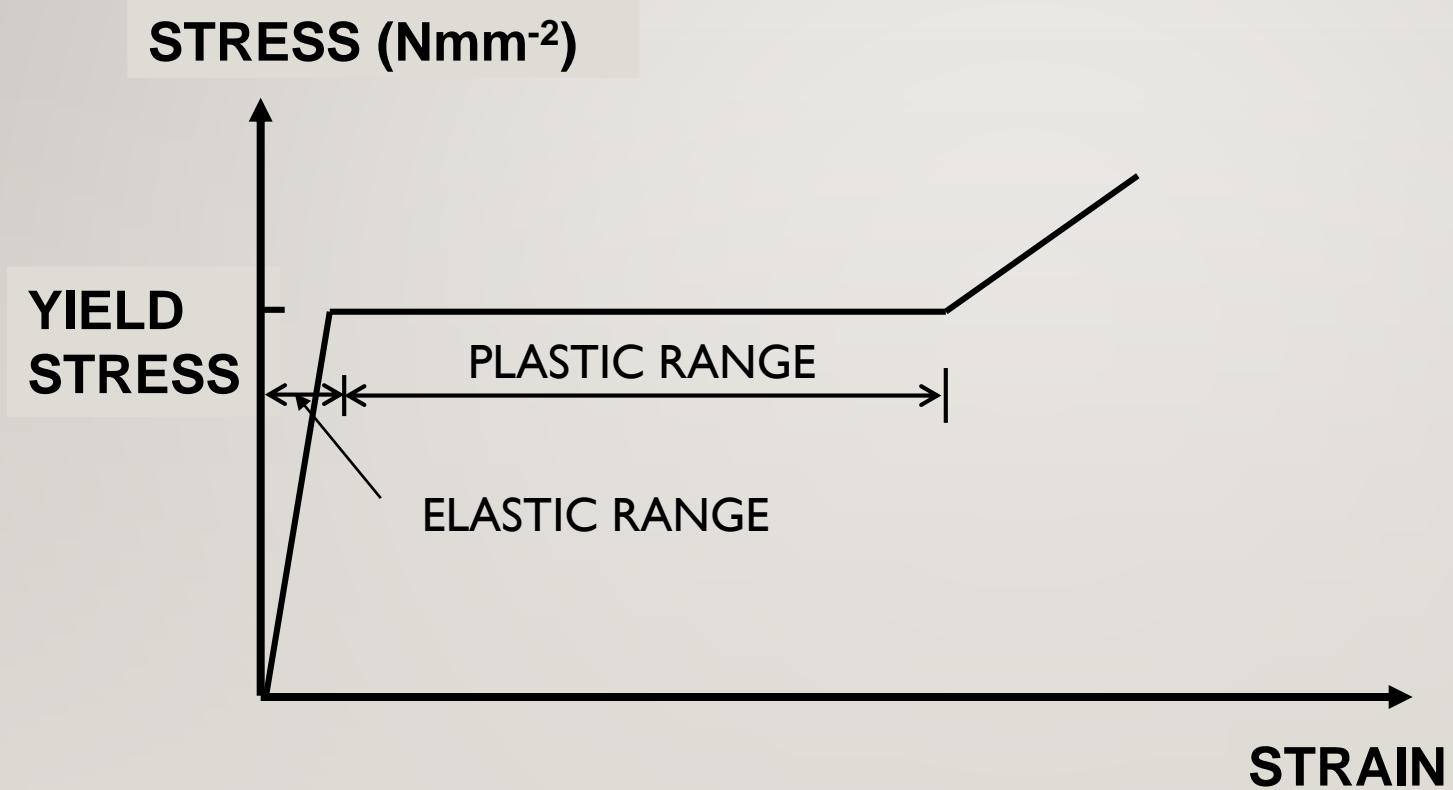
**STRUCTURAL STEEL IS MANUFACTURED IN FOUR BASIC GRADES: S235, S275, S355 AND S460, IN WHICH 'S' STANDS FOR STRUCTURAL STEEL AND 235, 275, ETC DENOTE THE YIELD STRENGTH OF THE MATERIAL**



# ACTUAL STRESS-STRAIN CURVES



# IDEALISED STRESS STRAIN CURVE

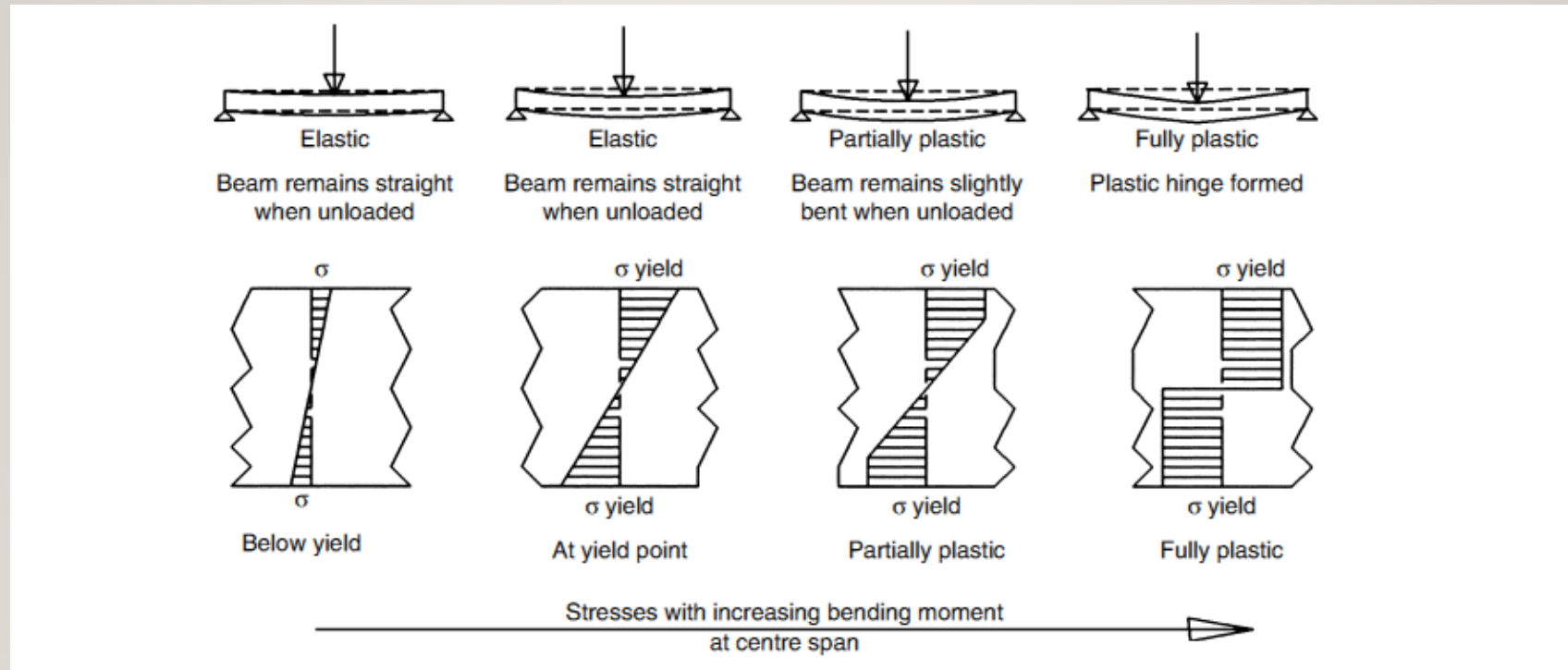




# STEEL GRADE, YIELD & ULTIMATE STRENGTHS (EXTRACTED FROM EN10025-2: 2019:TABLE 6)

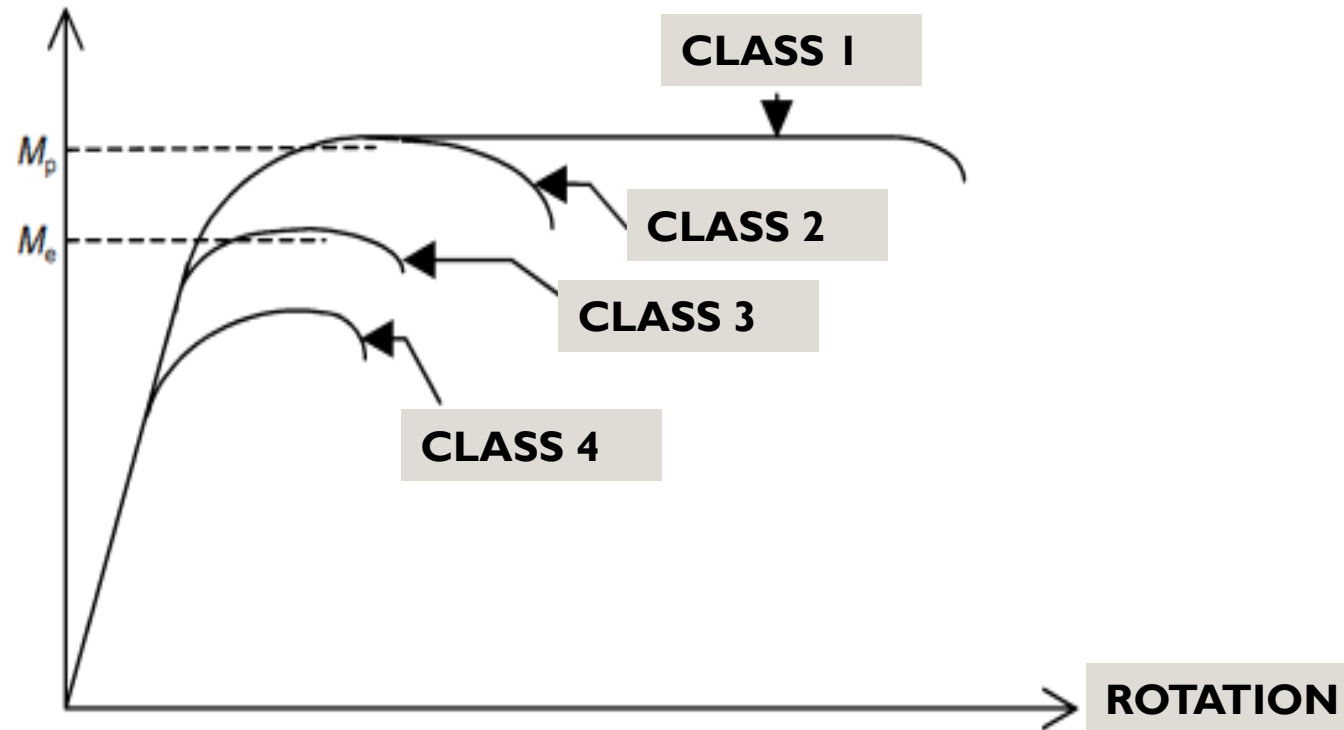
STEEL GRADE	THICKNESS OF FLANGE $t_f$ (mm)	YIELD STRENGTH, $f_y$ (Nmm <sup>-2</sup> )	ULTIMATE STRENGTH, $f_u$ (Nmm <sup>-2</sup> )
S235	$\leq 16$	235	360
	$> 16 \leq 40$	225	360
	$> 40 \leq 100$	215	360
S275	$\leq 16$	275	430
	$> 16 \leq 40$	265	410
	$> 40 \leq 63$	255	410
S355	$\leq 16$	355	510
	$> 16 \leq 40$	345	470
	$> 40 \leq 63$	335	470

# BENDING FAILURE OF A BEAM



# BEHAVIOUR IN BENDING OF DIFFERENT CLASSES OF SECTION

APPLIED MOMENT



ROTATION

# LIMITING WIDTH TO THICKNESS RATIOS (BASED ON TABLE 5.2, EC3)

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TYPE OF ELEMENT (ALL ROLLED SECTIONS)	Class of section		
	(1)	(2)	(3)
OUTSTAND ELEMENT OF COMPRESSION FLANGE	$c/t \leq 9\epsilon$	$c/t \leq 10\epsilon$	$c/t \leq 14\epsilon$
WEB WITH NEUTRAL AXIS AT MID-DEPTH	$c/t \leq 72\epsilon$	$c/t \leq 83\epsilon$	$c/t \leq 124\epsilon$
WEB WHERE THE WHOLE CROSS-SECTION IS SUBJECT TO AXIAL COMPRESSION ONLY	$c/t \leq 33\epsilon$	$c/t \leq 38\epsilon$	$c/t \leq 42\epsilon$
Note. $\epsilon = (235/f_y)^{1/2}$			