

# Life Cycle Greenhouse Gas Emissions from Uranium Mining and Milling in Canada: Supporting Information

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## 1 Facility Profiles

This study includes a detailed analysis of life cycle greenhouse gas (GHG) emissions during the uranium mining-milling phase of the nuclear fuel cycle for three paired mining-milling operations in northern Saskatchewan (SK), shown in Figure S1. These facilities are operated by AREVA Resources Canada Inc. (AREVA) and Cameco Corporation (Cameco).



Figure S1. Map of Major Uranium Mines and Mills in Saskatchewan

### *1.1 McArthur River Operation-Key Lake Operation (Cameco)*

This study includes data from operation at McArthur River-Key Lake from 2006-2013 inclusive. For some processes, data outside of this temporal boundary was available and was also included.

McArthur River Operation (McArthur River) is located approximately 600 km north of Saskatoon by air and 790 km north by truck.<sup>1</sup> Mining began in 1999.<sup>2</sup> Ore is processed underground yielding a slurry which is pumped to surface, loaded into specially designed containers, and trucked to the Key Lake mill.<sup>2</sup>

As of Dec. 31 2013, a total of 114,195,511 kg U<sub>3</sub>O<sub>8</sub> had been produced at McArthur River and as of that date, proven and probable reserves of 163,519,142 kg U<sub>3</sub>O<sub>8</sub> remain. According to the current life-of-mine plan, ore reserves will be exhausted in the 2030's, depending on future production rates.<sup>2,3</sup> Total reserves and mine lifespan are updated annually.

Key Lake Operation (Key Lake) is located approximately 570 km north of Saskatoon by air and 710 km by truck<sup>1</sup>. It began production in 1983, milling ore from the Gaertner and Deilmann open pits until 1997.<sup>4</sup> From 1983-2000, Key Lake shipped 78,492,376 kg U<sub>3</sub>O<sub>8</sub> sourced mainly from the Gaertner and Deilmann pits. In 2000, the Key Lake mill began to process ore from the McArthur River deposit, 72 km away by truck.<sup>4</sup> From 2000-2013, Key Lake shipped 77,737,681 kg U<sub>3</sub>O<sub>8</sub> sourced mainly from McArthur River.<sup>5</sup> Assuming that Key Lake processes the remaining reserves of McArthur River's uranium at an average recovery rate of 98.5%, it will ship another 161,000,000 kg U<sub>3</sub>O<sub>8</sub>.

### *1.2 Rabbit Lake Operation (Cameco)*

The Rabbit Lake facility began operation in 1975 and is: “the longest operating uranium production facility in North America, and the second largest uranium mill in the world.”<sup>6</sup> It is located approximately 670 km north of Saskatoon by air and 820 km by truck.<sup>1</sup>

Rabbit Lake Operation (Rabbit Lake) mill has previously obtained ore from Rabbit Lake open pit, Collins Bay A- B- and D- zones, and currently receives ore from Eagle Point underground mine using a drill and blast method.<sup>4</sup> From 1975-2013, Rabbit Lake produced 86,227,910 kg U<sub>3</sub>O<sub>8</sub> and additional production of 8,800,000 kg U<sub>3</sub>O<sub>8</sub> is expected from 2014-2018.<sup>7,8,9</sup> This study includes data from operation at Rabbit Lake from 2006-2013 inclusive.

### *1.3 McClean Lake Operation (AREVA)*

McClean Lake Operation (McClean Lake) began in 1995 with the mining of JEB open pit and the construction of the JEB Mill. AREVA claims that McClean Lake is the most technologically advanced uranium mill in the world, capable of processing ore from grades of less than 1% to 30% without dilution.<sup>10</sup> It is located approximately 700 km north of Saskatoon by air and 830 km by truck.<sup>1</sup>

From 1995-2008, five open pits were mined out and the mill processed their ore from 1999-2010. During this time, approximately 22,700,000 kg U<sub>3</sub>O<sub>8</sub> was produced.<sup>11</sup>

In 2005, the mill began an expansion project to increase its production capacity and allow it to receive ore from Cigar Lake underground mine, the world’s largest undeveloped high-grade uranium mine. In July 2010, the mill shut down as uranium stockpiles were depleted and expansion activities continued.<sup>11</sup> This study includes data

from operation at McClean Lake from the beginning of construction until the depletion of ore stockpiled from onsite open pits, i.e., 1995-2010 inclusive.

The McClean Lake mill began processing ore from Cigar Lake in 2014 and is expected to process all of Cigar Lake's 98,300,000+ kg  $U_3O_8$ .<sup>11,12</sup>

#### *1.4 Facilities Excluded from LCA*

In addition to the above-mentioned facilities, AREVA has provided details for the decommissioning of Cluff Lake Project (Cluff Lake), an operation that included underground and open pit uranium mines as well as a uranium mill. Mining and milling at Cluff Lake ended in 2002 and decommissioning activities began soon after. In 2013, the last buildings were demolished and site occupancy ceased. Active decommissioning is now complete and the site is in a period of long-term monitoring.<sup>13</sup> Cluff Lake Project is not considered for detailed analysis due to a lack of operational data. However, the recent decommissioning activities are used to help validate estimates of GHG emissions for decommissioning for the facilities considered as part of this study.

Cigar Lake Project (Cigar Lake) is a high-grade underground uranium mine located 69 km south of the McClean Lake mill, where ore slurry from the project will be shipped and processed.<sup>12</sup> The mine began construction in 2005 and its first shipment of ore slurry arrived at McClean Lake mill in March 2014.<sup>12,14</sup> Cigar Lake is expected to reach full-scale production in 2018.<sup>14</sup> Like Cluff Lake, this facility is not considered for detailed analysis due to lack of operational data.

Two other major uranium projects, the Midwest Project and the Millennium Mine Project, are under development in SK but are not yet under construction. They too are excluded from analysis.

Historical uranium projects in SK include Gunnar Mine (1955-1963), Lorado Mill (1957-1960), and Eldorado Mine (1953-1982).<sup>15,16</sup> These are excluded from analysis because of lack of data and because they do not reflect the current practices employed by the Canadian uranium mining and milling industries.

## 2 Methods

### 2.1 Data Collection

The mine-mill operators, AREVA and Cameco, have collaborated in this research by providing multiple years of data related to emissions-relevant activities including energy consumption, reagent consumption, transportation, mining and milling processes, facility history, infrastructure, and more. Additional data was obtained from the ecoinvent life cycle database.<sup>17</sup>

It is assumed that all data provided by the mine-mill operators is accurate and has been validated by each company's internal auditing program. Unless otherwise stated, data from the operators is not explicitly validated as part of this study.

Where data was not available, assumptions were made to fill information gaps. The associated uncertainty is assessed according to the methodology discussed in Section 2.5. The following sections note specific instances where the methodology employed deviates from that described in Section 2.5. Activity factors for most major processes along with their associated uncertainty are shown in Section 2.6, Table S9.

The life cycle approach requires the consideration of construction, operation, and decommissioning activities as well as emissions embodied in infrastructure, equipment, and materials.



### *2.1.1 Construction*

Construction activities include the transport of construction materials and employees to construct buildings, earthworks, and roads. At uranium mining facilities, it also includes development of the open pit or underground mine.

Since most construction activities occurred before the operating companies had begun systematically assessing and reporting their energy consumption and GHG emissions, there are no accessible records for early construction activities. In the absence of this data, emissions are estimated by comparison with similar facilities for which data or qualified estimates are available.

Energy consumption data during construction of McClean Lake Operation is partially available. Construction activities at McClean Lake include development of both the open pit mines and the uranium mill. Similar activities were undertaken in the development of both Rabbit Lake and Key Lake mills, both of which originally had open pit mines.<sup>18</sup> Data from McClean Lake is used to anchor emission estimates for direct and indirect energy consumption at these facilities.

Cigar Lake is an underground uranium mine with some similarities to McArthur River including a freezing program, the use of mining techniques that isolate employees from contact with high grade ore, and an ore crushing and grinding circuit located in the underground facility.<sup>12</sup> Some site-specific factors complicate the comparison of the two facilities, most notably setbacks at Cigar Lake resulting from three water inflow incidents between 2006 and 2008.<sup>12</sup> Data for energy consumption and employee transport for Cigar Lake are available for nine years.<sup>19</sup> The construction estimate for McArthur River

is informed by emission from Cigar Lake during this period, but also takes into account the differences between the projects.

Millennium Project is a proposed underground mine located approximately 600 km north of Saskatoon, midway between Key Lake and McArthur River. 20 GHG emission estimates for each production phase are provided in the project Environmental Impact Statement for two scenarios: 1) electricity provided to site in year two through decommissioning; and 2) electricity is not provided to site through life of mine.<sup>20</sup> Cameco states that the emission estimates are highly conservative.<sup>20</sup> These data are not used directly to estimate emissions for any of the facilities included in this study, as it is not directly comparable to any of those included. Rather, the Millennium EIS data were used to check the validity of the construction emissions estimates used in the current study.

The methods used to calculate emissions from direct and indirect energy consumption during the construction phase at these facilities introduces uncertainty to the calculated result. This uncertainty is included and calculated as described in Section 2.5.

### *2.1.2 Infrastructure and Equipment*

It is not possible to directly assess all of the materials present in each building and piece of equipment. However, a rigorous LCA using PCA requires these quantities to be estimated.

Estimates for materials used in the structure of buildings are based on the area and volume occupied by buildings at each site. For Cameco facilities, this information is available in the Preliminary Decommissioning Plans. For AREVA facilities, building area is estimated from site layout drawings found in annual regulatory reports. Building

heights for AREVA facilities are estimated based on similar buildings at Cameco sites and on observations made during a site tour. The mass of steel, aluminum, etc. used in the building structure per building unit volume are taken fromecoinvent Centre.<sup>17</sup>

Stationary equipment consists mostly of tanks, pipes, pumps, and hoists. Material types are listed in construction drawings, and mass in tanks and pumps are estimated based on their geometry as presented in engineering drawings. Tanks are modeled as cylinders, cones, and/or right rectangular prisms. Tanks are assigned a nominal wall thickness of 6.4mm. Where tanks are rubber lined, the lining is assigned a nominal thickness of 3.2mm. Pumps are modeled as solid steel cylinders. Material estimates based on these are then increased by 40% to account for other equipment such as cranes, ladders, stairs, piping, etc. The material estimate is further increased by 10% to account for equipment replacement.

For facilities where construction drawing were not available, materials usage is estimated. Based on the amount of materials used in the Key Lake mill, a *material intensity* is developed:

$$\begin{aligned} \textbf{Material Intensity} \left( \frac{\text{kg material}}{\text{m}^3 \text{ building}} \right) \\ = \frac{\text{Total Materials Estimated from Drawings (kg)}}{\text{Total Volume of Facility (m}^3\text{)}} \end{aligned} \quad (1)$$

Material estimates for buildings without drawings are then generated based on applying this *material intensity* to the building's known volume:

$$\text{Material Estimate} = \text{Material Intensity} \times \text{Building Volume} \times \text{Intensity Factor} \quad (2)$$

The *intensity factor* varies between 0 and 1 depending on the relative amount of equipment in a building compared to the Key Lake mill buildings. An *intensity factor* of 1 indicates that the building has a similar amount of equipment in it as a mill building whereas an *intensity factor* of 0 describes an empty building. The choice of this factor is based on the activities undertaken in these buildings and also on information gathered during site tours.

In addition to the equipment and materials discussed above, the items listed in Table S1 are also included for analysis.

Table S1. Additional Materials and Equipment Included in Analysis

	Data Source	
	McArthur River, Key Lake, Rabbit Lake	McClellan Lake
Materials		
Concrete in Foundations	(1)	*
Polyethylene Piping around Site	(1)	*
Fuel-Burning Equipment		
Small Boilers, Vaporizers, and Heating Units	(2)	(2)
Large Boilers, Vaporizers, and Heating Units	(2)	(2)
Diesel Generators	(2)	(2)
Vehicles		
Light Construction/Mining Equipment	(3)	(2)
Heavy Construction/Mining Equipment	(3)	(2)
Small Mobile Equipment	(3)	(2)
Buses	(3)	(2)

(1) Facility-Specific Preliminary Decommissioning Plans<sup>21,22,23</sup>

(2) Facility-Specific Annual Reports<sup>11,24</sup>

(3) Proprietary Data Provided by Facility Operator

\* Data unavailable. Estimate based on materials at Key Lake/total building footprint

### *2.1.3 Operational Activities*

Table S2 summarizes the operational data requested and received for each facility. Data for McArthur River, Key Lake, and Rabbit Lake was most often available from 2006-2013 with some additional data available for earlier years. Data for McClean Lake was available from 1995-2010. For all facilities, data gaps are generally more common in early years.

Table S2. Operational Data Requested and Received

Data Requested	Data Source	Years of Data Available			
		McArthur River	Key Lake	Rabbit Lake	McClean Lake
Operational Parameters					
People on Site (man-days worked)	(1,2)	8	9	5	15
Production Data					
Tonnes Ore Produced/Processed	(1)	14	13	8	16
kg U <sub>3</sub> O <sub>8</sub> Equivalents Processed/Shipped	(1)	14	13	8	16
Energy Consumption Data					
Electricity	(2)	8	9	8	11
Diesel	(2)	8	9	8	8
Propane	(2)	8	9	8	12
Gasoline	(2)	8	9	8	12
Transportation Data					
Flight Schedules	(2)	8	7	7	0*
Freight Reports	(2)	8	7	7	12
Fugitive Emission Data					
Domestic Wastewater Generation	(1)	0**	0**	0**	0**
Liquid/Solid Waste Generation	(1,2)	9	9	8	13
Process Emissions	(3)				
Concrete Usage (within mine)	(1)	12	N/A	8	N/A
Reagent Consumption	(1)	4	10	8	15
Explosive Usage	(2)	7	N/A	7	16

(1) Facility-Specific Annual Reports <sup>11,24</sup>

(2) Proprietary Data Provided by Facility Operator

(3) Calculation - Direct CO<sub>2</sub> emissions from reaction of carbonates with sulfuric acid added during milling process – carbonates present in ore and reagents - assumes 100% reaction

N/A – Not Applicable

\* None available, amount estimated based on number of people on site compared to McArthur River, corrected for relative distance from Saskatoon

\*\* Estimated assuming 255 L/day generation per man-day worked

#### *2.1.4 Corporate Activities*

For both operators, corporate headquarters (HQ) are located in Saskatoon, SK. Emissions from fuel and electricity consumption at HQ are allocated to each mine and mill. These allocations are likely conservative as both corporations are involved with uranium mining-milling operations outside Canada.

Proprietary data for natural gas and electricity consumption at corporate headquarters was supplied from 2006-2013 by Cameco and from 2003-2013 for AREVA.

Emissions from Cameco's headquarters are allocated one quarter each to Cameco's four main SK operations: McArthur River, Key Lake, Rabbit Lake, and Cigar Lake over the time period where data is available. Emissions from AREVA's headquarters are allocated one half each to Cluff Lake and to McClean Lake.

No other emissions-relevant activities are included as they are expected to fail the 0.1% cut-off criteria. As an example, materials used in the construction of corporate buildings are excluded from analysis. The footprint of corporate buildings is very small compared to the building footprint at the mines and mills. The latter contributes less than 0.2% to the emissions total.

#### *2.1.5 Decommissioning*

Decommissioning activities are described in each site's Preliminary Decommissioning Plan (PDP), a document submitted to the Saskatchewan Ministry of Environment. The PDP is updated in maximum 5-year intervals. This document, and the associated Preliminary Decommissioning Cost Estimate (PDCE), contains estimates for heavy equipment use, energy consumption, major material requirements (e.g. lime, concrete), and employee transportation during decommissioning activities.

PDP and PDCE documents are provided by Cameco for McArthur River, Key Lake, and Rabbit Lake. AREVA has provided a decommissioning plan summary for McClean Lake and a detailed decommissioning report for Cluff Lake which has been in the decommissioning phase since 2002, the last buildings demolished in 2013. Decommissioning plans at each facility are compared to decommissioning activities at Cluff Lake to ensure the reasonableness of the results.

#### *2.1.6 Land Use Change*

The facilities are located in the unmanaged forests of Canada's western boreal shield ecozone.<sup>25</sup> Forest productivity is low due to long cold winters (January daily average is -25°C)<sup>26</sup>, short cool summers (July averages +15°C), low decomposition rates and nutrient availability<sup>27</sup>, and presence of discontinuous permafrost and outcropping of Precambrian granite. The unmanaged boreal forests were assigned a pre-development net ecosystem productivity rate of 31 g-C m<sup>-2</sup> yr<sup>-1</sup> (i.e., net carbon sink) with an uncertainty range of 20 to 40 g-C m<sup>-2</sup> yr<sup>-1</sup>. This is the net ecosystem productivity in this region between 1990 and 2008 as estimated by Stinson et al.<sup>28</sup> Saskatchewan's managed forests are typically located further south and have higher carbon densities (i.e., Mg-C ha<sup>-1</sup>) than Saskatchewan's unmanaged western boreal shield forests (Figure 5; Kurz et al.<sup>27</sup>). For this reason, the net ecosystem productivity values used in this study may be conservative estimates.

During mine-mill construction, the boreal forests are cleared. During decommissioning, the mine-mill sites are reclaimed in accordance with approved decommissioning plans. During the disturbance period, the disturbed area within the mine-mills footprints is assigned a net annual carbon flux of zero (i.e., neither a sink nor



a source) resulting in a net annual GHG emission rate of  $31 \text{ g-C m}^{-2} \text{ yr}^{-1}$  (i.e.,  $1,137 \text{ kg CO}_2\text{e ha}^{-1} \text{ yr}^{-1}$ ).

Increased emissions from soil carbon loss in response to forest harvesting and conversion to industrial use are not considered in the assessment. This term can likely be ignored due to low decomposition rates in this ecozone.<sup>27</sup>

The disturbance period is assumed to begin at facility construction and to end 15-years after the active decommissioning period for each facility when the area is assumed to return to net carbon compensation.<sup>27</sup> The total disturbance period for the facilities, based on historical production and the life-of-mine plans used for this study, are 56, 67, and 75 years.

The disturbed areas for the three mine-mills are currently 410, 540, and 917 ha per mine-mill.<sup>21,22,23,29</sup> These areas have grown over time as the facilities have expanded (e.g., new deposits are developed, waste rock and tailings areas are expanded, borrow pits are developed) and may shrink before facilities are decommissioned due to ongoing reclamation activities. The land use change emissions estimate in this study neglects these periods of growth and pre-decommissioning reclamation and so the emissions estimate may be somewhat overstated.

## *2.2 Inventory of Emissions Sources*

Operational activities for each mine-mill pair were divided by (i.e., normalized to) total  $\text{U}_3\text{O}_8$  production during the operational periods included in the study period (2006 – 2013 for McArthur River, Key Lake, and Rabbit Lake, and 1995 – 2010 for McClean Lake). Activities at corporate headquarters during these operational periods are also included and normalized in the same way.

All of the facilities considered have experienced major production changes throughout their lives. For example, some mills have been in operation longer than the mines from which they currently source their ore. Earlier mining-milling activities involved different mining-milling methods, ore grades, and environmental and safety requirements. No data is currently available to perform a detailed PCA for these early  $\text{U}_3\text{O}_8$  production periods.

The full construction and decommissioning periods, including upstream activities associated with equipment and infrastructure, were included in the inventory for all facilities. Construction and decommissioning activities were normalized to each facility's estimated lifetime  $\text{U}_3\text{O}_8$  production.

Future production is uncertain as it relies on the accuracy of reserve estimates, ore grades, future uranium prices, and other environmental and socio-economic factors. It is assessed as follows:

- Base Case
  - Development proceeds as per *Life-of-Mine Plan* (i.e., 100% of proven and probable reserves are utilized)
- Worst Case
  - 70% of proven and probable reserves are utilized
- Best Case
  - 100% of proven and probable reserves are utilized
  - 50% utilization of measured, indicated, and inferred resources
  - 25% increase in both reserves and resources due to future exploration

Data for reserves and resources is taken from facility technical and environmental reports.<sup>12,3,8</sup>

### 2.3 Emission Factors

Emission factors are available from a number of sources depending on the activity type. For most direct emissions, emission factors are obtained via literature review. For most upstream activities, emission factors are drawn from the ecoinvent v3.0 database.<sup>17</sup>

At a minimum, CO<sub>2</sub>, CH<sub>4</sub>, and N<sub>2</sub>O emissions are considered for all activities. Unit processes in the ecoinvent v3.0 database<sup>17</sup> includes a number of other GHG releases in addition to these three. These also contribute to the total emissions estimate, but their impact is small.

Tables S3 to S6 list the unit processes and materials considered in this study along with their emission factors. The stated emission factors are mean values. In the software model, each factor is assigned a confidence interval, usually as a lognormal probability distribution. For activities that have a lot of natural variation, or where the data quality is

low, the confidence intervals are larger. When processes are well understood and consistent, the confidence intervals are smaller.

A number of assumptions have been made to estimate emission factors in the tables. Examples include using the life cycle emission factor of an industrial boiler to estimate the emission factor for a diesel generator. This type of estimate is used only with processes and materials that make a small overall contribution to the calculated results. The encoded uncertainties are adjusted to reflect this lack of precision.

This approach to estimating emission factors should not introduce large uncertainties into the model. In most cases, these estimates are extrapolations made on a mass basis. This means that the resulting estimate will include the correct mass of material and should contain relatively similar proportions of materials (e.g. both pieces are primarily steel with some copper, aluminum, rubber, etc.). The amount of energy used in fabrication and transportation are similarly scaled by mass.

Table S3. Major Emission Factors Used in This Study – Energy, Explosives, Processes

Process	Unit	Emission Factors (kg CO <sub>2</sub> e/Unit)			Data Source	Notes
		Direct	Indirect	Life Cycle		
Energy						
Propane Consumption	L	1.54	0.43	1.97	32 - Direct, 17 - Indirect	upstream emissions are primarily from processing and transport
Diesel Consumption	L	2.79	0.58	3.36	32 - Direct, 17 - Indirect	upstream emissions are primarily from processing
Gasoline Consumption	L	2.3	0.66	2.96	32 - Direct, 17 - Indirect	upstream emissions are primarily from processing
Natural Gas Consumption	m <sup>3</sup>	1.83	0.25	2.08	30 - Direct, 17 - Indirect	upstream emissions from processing, methane leakage, and flaring
Electricity Consumption	kWh			0.768		average grid mix 2004-2013 <sup>33</sup>
Coal, Gas, Imports, and Other	kWh			0.987	34 - Combustion 17 – Other Emissions	77.7% of SaskPower net electricity generation 2004-2013 <sup>33</sup> ; 0.940/0.987 kg CO <sub>2</sub> e from combustion; imports assumed to be predominantly coal and natural gas; other is assumed insignificant
Hydro	kWh			0.0072	35 (median value)	19.4% of SaskPower net electricity generation 2004-2013 <sup>33</sup>
Wind	kWh			0.0109	35 (median value)	2.9% of SaskPower net electricity generation 2004-2013 <sup>33</sup>
Explosives					stoichiometry – direct, 17- indirect	
AN/FO	kg	0.18	8.69	8.87		94.2%wt ammonium nitrate and 5.8%wt fuel oil
AN/FO plus Inert	kg	0.16	6.49	6.65		60%wt ammonium nitrate, 35%wt carbonic acid, and 5%wt fuel oil
Emulsion-Type	kg	0.19	8.04	8.23		79%wt ammonium nitrate, 15%wt sodium nitrate, and 6%wt fuel oil
Process Emissions						
CaCO <sub>3</sub> Decomposition	kg CaCO <sub>3</sub>	0.44		0.44		based on stoichiometry of complete reaction
Na <sub>2</sub> CO <sub>3</sub> Decomposition	kg Na <sub>2</sub> CO <sub>3</sub>	0.42		0.42		based on stoichiometry of complete reaction
Waste Disposal						
Domestic Solid Waste	kg	0.62		0.62	36	methane emissions only; based on waste composition
Contam. Solid Waste	kg	0.08-0.62			36	methane emissions only; based on waste composition
Liquid Organic Waste	kg	0-30.4			37,38	varies based on composition, degree of degradation, degradation processes
Domestic Wastewater	m <sup>3</sup>	0.462		0.462	17	
Land Use Change	ha/year			1137	28	reduction of existing ecosystem services (carbon sequestration) due to conversion of boreal forest to industrial site; assumes land at disturbed site operates as neither carbon source or sink

Table S4. Major Emission Factors Used in This Study – Infrastructure and Stationary Equipment

Process	Unit	Life Cycle Emission Factor (kg CO <sub>2</sub> e/Unit)	Data Source	Notes
Infrastructure				
Building, Steel Hall	m <sup>3</sup>	47.1	17	based on 50mx30mx7m building of steel construction; direct emissions from diesel used during construction; indirect emission primarily from steel, aluminum, brick production
Reinforcing Steel	kg	2.60	17	
Aluminum	kg	14.7	17	
Brick	kg	0.33	17	
Concrete			40 – Cement, 17- Remainder	based on concrete recipes from McArthur River - 19 cement production ~98% of total emissions
Construction	m <sup>3</sup>	394		weighted average for several concrete types used in raise filling
Raise filling	m <sup>3</sup>	360		
Shotcrete	m <sup>3</sup>	396		
Grout	m <sup>3</sup>	711		
Mud Slab	m <sup>3</sup>	201		
Building Equipment				
Steel, low-alloyed	kg	2.40	17	
Chromium steel	kg	1.36	17	
Cast Iron	kg	2.21	17	
Rubber	kg	3.13	17	
Polyethylene Pipe	m	9.99	17	1m length of 200mm diameter polyethylene pipe containing 3.15 kg polyethylene, scaled up or down based on relative cross sectional area of pipe material
Industrial Furnace, 1 MW	pc	14,000	17	1 MW industrial furnace, 4766 kg; scaled up or down based on relative mass
Boiler, 0.5 MW	pc	16,600	17	based on 0.5 MW boiler, 2678 kg, which, in turn is an interpolation of a 0.1 MW boiler and 1 MW industrial furnace (589 kg and 4766 kg respectively); scaled up or down based on relative mass
Diesel Generator, 1.6 MW	pc	60,100	17	materials and production emissions based on 1MW Industrial furnace, scaled up by relative mass (20400 kg/4766 kg)
Fan/Blower (720 m <sup>3</sup> /hr)	kg	1120	17	Based on 182kg blower/heat exchanger, scaled by mass

Table S5. Major Emission Factors Used in This Study – Transport and Mobile Equipment

Process	Unit	Life Cycle Emission Factor (kg CO <sub>2</sub> e/Unit)	Data Source	Notes
Transport				
Flights, excluding fuel	flt hr	5.26	17	Emissions from airport infra: 2.93 kg CO <sub>2</sub> e, aircraft production: 2.33 kg CO <sub>2</sub> e
Jet Fuel	L	3.07	17,41	Upstream emissions primarily from processing; Jet fuel consumption varies from 430 to 510 L/flt hr between sites
Freight, Reagents, Fuel				
5-6 axle van/flatdeck	km	1.62	17,32	Emissions from: diesel burning: 1.33 kg CO <sub>2</sub> e; rest is vehicle production, maint, and road infra; based on 0.47L/km fuel economy 42
8 axle flatdeck	km	2.23	17,32	Emissions from: diesel burning: 1.49 kg CO <sub>2</sub> e; rest is vehicle production, maint, and road infra; based on 0.523L/km fuel economy 42
9 axle/special configs	km	2.35	17,32	Emissions from: diesel burning: 1.89 kg CO <sub>2</sub> e; rest is vehicle production, maint, and road infra; based on 0.672L/km fuel economy 42
Unknown type	T-km	0.0646	17	Emissions from diesel burning: 0.0430 kg CO <sub>2</sub> e; rest is vehicle production, maint, and road infra; based on 8-axle flatdeck with nominal 34.5T cargo
Vehicles				
Light vehicle	pc	16,100	17	production and maintenance; based on 1524 kg light duty vehicle; emission factor scaled up or down based on relative vehicle weight
Light mobile construction	pc	34,300	17	production and maintenance; based on 3000 kg tractor; emission factor scaled up or down based on relative vehicle weight
Heavy mobile construction	pc	83,800	17	production and maintenance; based on 15,372 kg truck; emission factor scaled up or down based on relative vehicle weight

Table S6. Major Emission Factors Used in This Study – Reagents

Reagents	Unit	Life Cycle Emission Factor (kg CO <sub>2</sub> e /Unit)	Data Source	Notes
Steel grinding balls	kg	2.05	17	
Coagulants, flocculants, anti-scalants	kg	2.14	17	Modeled as ‘organic chemicals’
Sulfur	kg	0.02	17	
Lime	kg	0.10	17	
Kerosene	kg	0.59	17	
Ammonia	kg	2.07	17	
Barium Chloride	kg	2.30	17	Modeled as ‘inorganic chemicals’
Hydrogen Peroxide	kg	1.30	17	
Citric Acid	kg	28.3	17	
Potassium Permanganate	kg	1.61	17	
Hydrochloric Acid (w/o water)	kg	1.72	17	
Isobutanol	kg	3.02	17	
Versene (EDTA)	kg	4.31	17	
Sodium Hydroxide (w/o water)	kg	1.38	17	
Tertiary Amine	kg	3.15	17	Modeled as ‘triethyl amine’
Nitrogen, Liquid	kg	0.60	17	
Sodium Bicarbonate	kg	0.95	17	
Sulfuric Acid	kg	0.12	17	
Oxygen, Liquid	kg	0.62	17	
Quicklime	kg	1.09	17	
Iron Sulfate	kg	0.25	17	
Magnetite	kg	1.09	17	
Kerosene	kg	0.59	17	
Sodium Chlorate	kg	4.39	17	



## 2.4 Conversion from kg CO<sub>2</sub>e/kg U<sub>3</sub>O<sub>8</sub> to g CO<sub>2</sub>e/kWh

Emission intensity estimates from the uranium mining-milling phase of the nuclear fuel cycle are generally reported as g CO<sub>2</sub>e/kWh ( $I_{kWh}$ ) which is not directly comparable to the results of the current study ( $I_{U_3O_8}$  presented in kg CO<sub>2</sub>e/kg U<sub>3</sub>O<sub>8</sub>). The final value for  $I_{kWh}$  will be different depending on the type of reactor used and its operating parameters, namely burn-up ( $B$ ) and thermal efficiency ( $\eta_{th}$ ). The yield of enriched uranium per unit of natural uranium ( $\eta_{enr}$ ) is also important.

A unit conversion can be performed as follows:

$$I_{kWh} = \frac{I_{U_3O_8}}{B \times \eta_{th} \times \eta_{enr}} \quad (3)$$

Using an example in Fthenakis and Kim<sup>43</sup>, a light water reactor (LWR) may burn-up at  $B = 42 \text{ MW}_{th}\text{d/kg U}$ , operate at  $\eta_{th} = 0.3$ , and require the enrichment of 7 kg U to generate a 1 kg enriched U fuel with 3.8% U-235 content ( $\eta_{enr}=0.1429$ ). Using these parameters yields the following conversion factor:

$$\frac{I_{kWh}}{I_{U_3O_8}} = 2.7 \times 10^{-5} \frac{\text{kg } U_3O_8}{\text{kWh}}$$

Heavy water reactors (HWR) burn-up at approximately  $B = 8 \text{ MW}_{th}\text{d/kg U}$ , have a similar thermal efficiency, and do not require uranium enrichment ( $\eta_{enr}=1$ ).<sup>44,45</sup> This yields an emission intensity factor of  $2.0 \times 10^{-5} \frac{\text{kg } U_3O_8}{\text{kWh}}$ .

Note that these calculations required the conversion of mass U to U<sub>3</sub>O<sub>8</sub> and MWd to kWh. The factors and assumptions used in the above calculation are not always included in the studies reviewed.

## 2.5 Uncertainty

Myriad factors introduce uncertainty to the calculated emission intensity for each facility including data gaps and uncertainty in emission factors.

Where gaps on activity data within the specified operational period exist, the uncertainty in the calculated activity factor is based on the number of years without data and the year-to-year variation of the known data using a lognormal probability distribution. The lognormal distribution was chosen because it provided a good representation of the variation in the available data. Uncertainty in operational activity data is only assessed from 2006 to 2013 for McArthur River, Key Lake, and Rabbit Lake. It is assessed from 1995 to 2010 for McClean Lake.

The 95% confidence interval used to fill data gaps for any given year is calculated as follows:

$$95\%CI = e^{\mu \pm 2\sigma} \quad (4)$$

where:

$\mu$  = mean of log-transformed data

$\sigma$  = standard deviation of log-transformed data

Uncertainty is propagated to the calculated total for each activity factor using the root sum of squares method:

$$2\sigma_T = \frac{\sqrt{n(2\sigma)^2}}{n_T} \quad (5)$$

where:

$2\sigma_T$  = total uncertainty in summed log-transformed data

$n$  = number of years without data within specified operational period

$n_T$  = total number of years within specified operational period

And the overall confidence interval of the activity factor is:

$$95\%CI = e^{\mu \pm 2\sigma_T} \quad (6)$$

The uncertainty factor is encoded in SimaPro as the square of the geometric standard deviation ( $\sigma_g^2$ ):

$$\sigma_g^2 = e^{2\sigma_T} \quad (7)$$

This method considers variation year-by-year and ignores changes in operation, production volumes, and ore grade. Inclusion of these other parameters would likely reduce the uncertainty in the result, but the calculation is not straightforward and, as will be shown in Section 3.3, is not required to produce a reasonably precise result.

When the above method cannot be applied (e.g., emission factors, infrastructure and equipment), uncertainty is assessed based on the methodology used in the SimaPro software and ecoinvent database, described in Weidema et al.<sup>46</sup> The methodology is also endorsed in the Greenhouse Gas Protocol, which itself provides reporting standards, sector guidance, and calculation tools for quantifying and reporting GHG emissions for companies and organizations around the world.<sup>47</sup>

The probability distribution of each parameter is defined by assessing and combining six categories of uncertainty:

1. Basic Uncertainty
2. Reliability
3. Completeness
4. Temporal Correlation
5. Geographical Correlation
6. Further Technological Correlation

The first, *Basic Uncertainty*, is applied in absence of sampled data. It is modeled as a lognormal probability distribution with the square of the geometric standard deviation ranging from 1 to 3 depending on the inherent uncertainty in the type of data as per Table S7.

Table S7. Basic Uncertainty Factors from Weidema et al.<sup>46</sup>

	Basic Uncertainty Factor $U_1 = \sigma_{g1}^2$
Demand of:	
Energy	1.05
Materials	1.05
Transport services	2.00
Infrastructure	3.00
Pollutants emitted to air:	
CO <sub>2</sub>	1.05
CH <sub>4</sub>	1.50
N <sub>2</sub> O	1.50

The other five sources of uncertainty are applied using the indicator score definitions shown in Figure S2 and their associated uncertainty factors, listed in Table S8. Figure S2 only shows definitions for the extreme values of each indicator score. Full definitions are available in Weidema et al.<sup>46</sup>

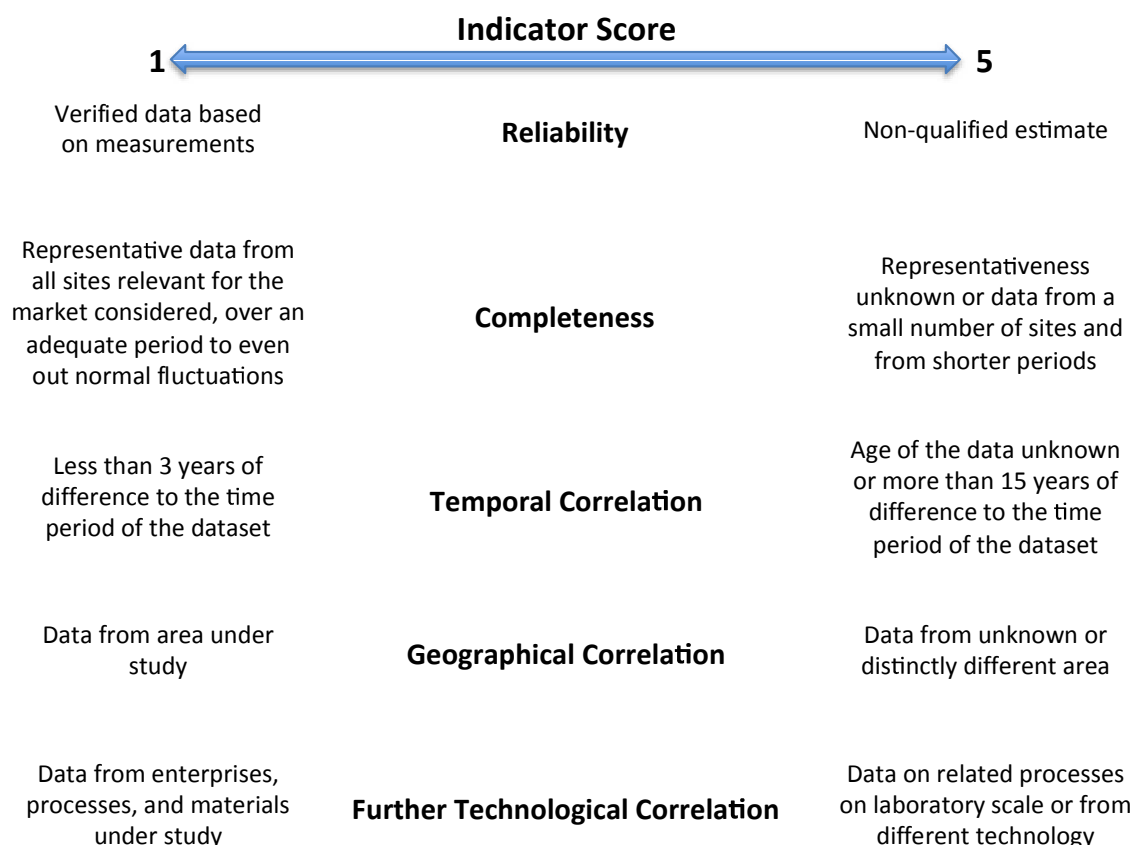


Figure S2. Indicator Score Range and Definitions Used in Assessing Uncertainty Factors <sup>46</sup>

Table S8. Elemental Factors Used in Assessing Total Uncertainty Factor. Reported as square of geometric standard deviation <sup>46</sup>

Indicator Score	1	2	3	4	5
Reliability	1.00	1.05	1.10	1.20	1.50
Completeness	1.00	1.02	1.05	1.10	1.20
Temporal Correlation	1.00	1.03	1.10	1.20	1.50
Geographical Correlation	1.00	1.01	1.02	1.05	1.20
Technological Correlation	1.00	1.05	1.20	1.50	2.00

Total uncertainty is calculated using the following formula:

$$\sigma_g^2 = \exp \sqrt{[\ln(U_1)]^2 + [\ln(U_2)]^2 + [\ln(U_3)]^2 + [\ln(U_4)]^2 + [\ln(U_5)]^2 + [\ln(U_6)]^2} \quad (8)$$

where:

$U_1$ = basic uncertainty factor

$U_2$ = uncertainty factor of reliability

$U_3$ = uncertainty factor of completeness

$U_4$ = uncertainty factor of temporal correlation

$U_5$ = uncertainty factor of geographical correlation

$U_6$ = uncertainty factor of further technological correlation; and

$U_n$  = the square of the element's geometric standard deviation.

The uncertainties in each parameter are propagated to the total result using the Monte Carlo method. In this method, each parameter is varied randomly within its probability distribution. The total result is calculated repeatedly based on the assigned values of its constituent parameters. With repeated calculation, a probability distribution for the total emerges. In this study, each total was calculated based on 5000 runs and a 95% confidence interval is reported.

Due to the qualitative aspect of this methodology, a confidence interval calculated in this way is not a precise value. Rather, it provides an indication of the overall uncertainty in the results and the relative uncertainty in the processes that make up the system model.

Uncertainty values for most major activity factors and emissions factors are shown in Table S9.

## 2.6 *Life Cycle Inventory Data*

Activity and emission factor data have been compiled according to the methodology and sources described in Sections 2.1, 2.2, 2.3, and 2.5. Table S9 summarizes the values for these factors for most major processes for the production-weighted average result (see main body of manuscript Section 5.5). In total, the activities indicated in Table S9 account for 98.8% of the life cycle GHG emissions assessed in this study.

Table S9 also indicates the level of uncertainty in the activity and emission factors presented. These uncertainties were calculated using the methodology stated in Section 2.5 and are presented as the square of the geometric standard deviation ( $\sigma_g^2$ ) of a lognormal probability distribution, consistent with how the factors are encoded in SimaPro. Each emission factor includes the aggregate emissions and uncertainty in all of its underlying processes. In propane consumption, for example, this includes the emissions and uncertainty during resource extraction, processing, transportation, and fuel combustion. For those emission factors taken from the ecoinvent v3.0 life cycle database<sup>17</sup> (see Section 2.3), uncertainty data also comes from ecoinvent.

Table S9. Life Cycle Inventory Data Including Uncertainty

Process	Activity Factor for Production- Weighted Average	Units	Activity Factor Uncertainty ( $\sigma_g^2$ )	Emission Factor	Units	Emission Factor Uncertainty ( $\sigma_g^2$ )
Electricity	22.0	kWh/kg U <sub>3</sub> O <sub>8</sub>	1.01	0.768	kg CO <sub>2</sub> e/kWh	1.14
Propane	4.76	L/kg U <sub>3</sub> O <sub>8</sub>	1.00	1.97	kg CO <sub>2</sub> e/L	1.06
Diesel	0.968	L/kg U <sub>3</sub> O <sub>8</sub>	1.01	3.36	kg CO <sub>2</sub> e/L	1.05
Reagent Consumption						
- Ammonia	0.404	kg/kg U <sub>3</sub> O <sub>8</sub>	1.00	2.07	kg CO <sub>2</sub> e/kg	1.33
- Lime/Quicklime*	2.91	kg/kg U <sub>3</sub> O <sub>8</sub>	1.00	0.426	kg CO <sub>2</sub> e/kg	**
- Hydrogen Peroxide	0.202	kg/kg U <sub>3</sub> O <sub>8</sub>	1.08	1.30	kg CO <sub>2</sub> e/kg	1.23
Construction, Infrastructure and Equipment						
- Electricity	0.894	kWh/kg U <sub>3</sub> O <sub>8</sub>	**	0.768	kg CO <sub>2</sub> e/kWh	1.14
- Propane	0.196	L/kg U <sub>3</sub> O <sub>8</sub>	**	1.97	kg CO <sub>2</sub> e/L	1.06
- Diesel	0.0887	L/kg U <sub>3</sub> O <sub>8</sub>	**	3.36	kg CO <sub>2</sub> e/L	1.05
- Gasoline	0.0133	L/kg U <sub>3</sub> O <sub>8</sub>	**	2.96	kg CO <sub>2</sub> e/L	1.07
- Flights to Site*	1.52E-04	flt.hr/kg U <sub>3</sub> O <sub>8</sub>	**	1409	kg CO <sub>2</sub> e/flt.hr	1.36
- Building Materials (Primarily steel and aluminum)	2.17E-03	m <sup>3</sup> building volume/kg U <sub>3</sub> O <sub>8</sub>	**	47.1	kg CO <sub>2</sub> e/m <sup>3</sup>	1.57
Truck Transport						
- 5-6 axle van/flatdeck	0.269	km/kg U <sub>3</sub> O <sub>8</sub>	1.04	1.62	kg CO <sub>2</sub> e/km	1.58
- 8 axle flatdeck	0.154	km/kg U <sub>3</sub> O <sub>8</sub>	1.27	2.23	kg CO <sub>2</sub> e/km	1.58
- 9 axle/special configurations	0.032	km/kg U <sub>3</sub> O <sub>8</sub>	1.19	2.35	kg CO <sub>2</sub> e/km	1.58
- Unknown type (bulk)	11.7	T.km/kg U <sub>3</sub> O <sub>8</sub>	1.05	0.0646	kg CO <sub>2</sub> e/T.km	1.58
Flights to Site*	9.92E-04	flt.hr/kg U <sub>3</sub> O <sub>8</sub>	1.13	1431	kg CO <sub>2</sub> e/flt.hr	1.36
Concrete Production*	3.75E-03	m <sup>3</sup> /kg U <sub>3</sub> O <sub>8</sub> (all types)	1.00	381	kg CO <sub>2</sub> e/m <sup>3</sup>	**

\* Emission factor varies between sites. Value given is weighted average.

\*\* Uncertainty included in assessment, but not possible to disaggregate



Table S9 cont. Life Cycle Inventory Data Including Uncertainty

Process	Activity Factor for Production- Weighted Average	Units	Activity Factor Uncertainty ( $\sigma_g^2$ )	Emission Factor	Units	Emission Factor Uncertainty ( $\sigma_g^2$ )
Use of Explosives						
- AN/FO	2.76E-02	kg/kg U <sub>3</sub> O <sub>8</sub>	1.00	8.87	kg CO <sub>2</sub> e/kg	1.47
- AN/FO plus Inert	2.25E-02	kg/kg U <sub>3</sub> O <sub>8</sub>	1.11	6.65	kg CO <sub>2</sub> e/kg	1.40
- Emulsion-Type	4.11E-02	kg/kg U <sub>3</sub> O <sub>8</sub>	1.05	8.23	kg CO <sub>2</sub> e/kg	1.43
Process Emissions						
- CaCO <sub>3</sub> Decomposition	1.43	kg CaCO <sub>3</sub> /kg U <sub>3</sub> O <sub>8</sub>	**	0.440	kg CO <sub>2</sub> e/kg	1.00
- Na <sub>2</sub> CO <sub>3</sub> Decomposition	4.49E-02	kg Na <sub>2</sub> CO <sub>3</sub> /kg U <sub>3</sub> O <sub>8</sub>	1.07	0.420	kg CO <sub>2</sub> e/kg	1.00
Decommissioning						
- Electricity	4.98E-01	kWh/kg U <sub>3</sub> O <sub>8</sub>	**	0.768	kg CO <sub>2</sub> e/kWh	1.14
- Propane	2.23E-02	L/kg U <sub>3</sub> O <sub>8</sub>	**	1.97	kg CO <sub>2</sub> e/L	1.06
- Diesel	4.44E-02	L/kg U <sub>3</sub> O <sub>8</sub>	**	3.36	kg CO <sub>2</sub> e/L	1.05
Wastes						
- Domestic Solid Waste	0.122	kg/kg U <sub>3</sub> O <sub>8</sub>	**	0.620	kg CO <sub>2</sub> e/kg	**
- Contaminated Solid Waste*	0.404	kg/kg U <sub>3</sub> O <sub>8</sub>	**	0.343	kg CO <sub>2</sub> e/kg	**
- Liquid Organic Waste*	0.168	kg/kg U <sub>3</sub> O <sub>8</sub>	**	2.37	kg CO <sub>2</sub> e/kg	**
- Domestic Wastewater	8.31E-03	m <sup>3</sup> /kg U <sub>3</sub> O <sub>8</sub>	3.01	0.462	kg CO <sub>2</sub> e/m <sup>3</sup>	1.60
Gasoline	0.127	L/kg U <sub>3</sub> O <sub>8</sub>	1.01	2.96	kg CO <sub>2</sub> e/L	1.07
Corporate Headquarters						
- Electricity	0.263	kWh/kg U <sub>3</sub> O <sub>8</sub>	**	0.768	kg CO <sub>2</sub> e/kWh	1.14
- Natural Gas	3.07E-02	m <sup>3</sup> /kg U <sub>3</sub> O <sub>8</sub>	**	2.08	kg CO <sub>2</sub> e/m <sup>3</sup>	1.06
Land Use Change	2.33E-04	ha.yr/kg U <sub>3</sub> O <sub>8</sub>	1.05	1137	kg CO <sub>2</sub> e/ha.yr	1.44

\* Emission factor varies between sites. Value given is weighted average.

\*\* Uncertainty included in assessment, but not possible to disaggregate

### 3 Supporting Results

Table S10 shows the GHG emission intensity for each facility by process.

Table S10. GHG Emissions Intensity (kg CO<sub>2</sub>e/kg U<sub>3</sub>O<sub>8</sub>) by Facility and Process

	Mine-Mill A	Mine-Mill B	Mine-Mill C	Production-Weighted Average
<b>Average Ore Grade (% U<sub>3</sub>O<sub>8</sub>)</b>	0.74	1.54	4.53	3.81
<b>Process</b>				
Electricity	36.4	18.2	13.6	16.9
Propane	19.7	15.6	7.1	9.4
Diesel	6.4	7.3	2.3	3.3
Reagent Consumption	3.1	9.0	1.8	2.6
Construction, Infrastructure and Equipment	3.7	0.5	1.9	2.0
Truck Transport	3.1	2.6	1.3	1.6
Flights to Site	3.0	2.3	1.1	1.4
Concrete Production*	0.4	0.0	1.7	1.4
Use of Explosives	1.0	6.5	0.1	0.7
Process Emissions	0.7	0.4	0.7	0.6
Decommissioning	1.8	0.1	0.4	0.6
Wastes	0.7	0.1	0.7	0.6
Gasoline	0.7	0.6	0.3	0.4
Corporate Headquarters	0.5	0.2	0.2	0.3
Land Use Change	0.4	0.2	0.2	0.3
<b>Total (kg CO<sub>2</sub>e/kg U<sub>3</sub>O<sub>8</sub>)</b>	<b>81</b>	<b>64</b>	<b>34</b>	<b>42</b>
<b>Total (g CO<sub>2</sub>e/kWh - LWR)</b>	<b>2.2</b>	<b>1.7</b>	<b>0.91</b>	<b>1.1</b>

\* concrete used in mining, not in infrastructure

### 3.1 Correlations

Shown in Figure S3, is the negative correlation ( $N=28$ ;  $r=-0.727$ ) between annual emissions from energy consumption and ore-grade. This trend reflects the reduced energy expenditure required to obtain the same quantity of uranium from ores of higher grade. This correlation is complicated by the differences in the grade of ore mined compared to what enters the milling circuit in any given year.

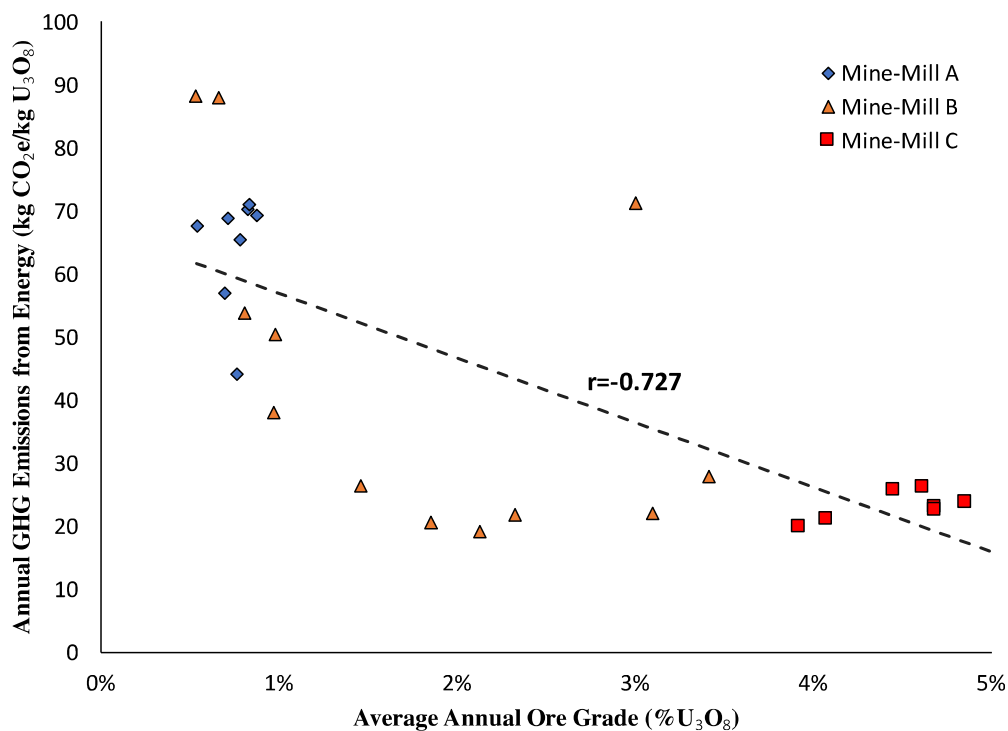


Figure S3. Annual GHG Emissions from Energy

Emissions from reagent consumption, Figure S4, correlate weakly with the average annual ore grade entering the milling circuit (N=28,  $r=-0.480$ ). Differences at the same mill and among the mills reflect differences in ore grade and extraction processes.

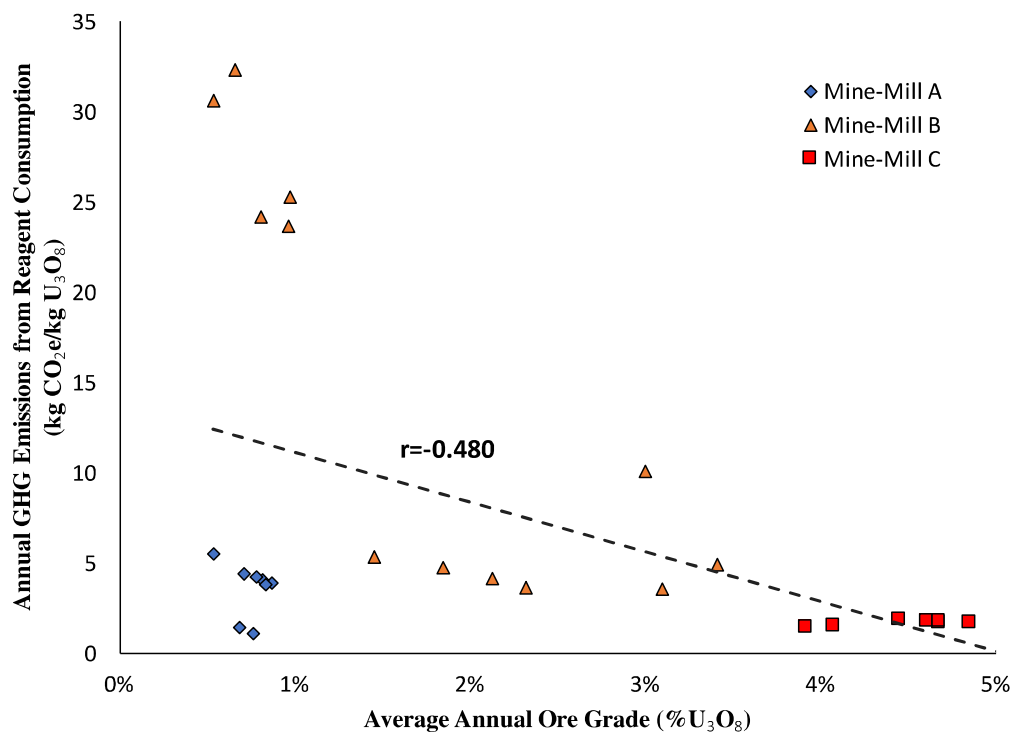


Figure S4. Annual GHG Emissions from Reagent Consumption

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