Supplementary Materials for "The benefits of ambitious short-term targets when decarbonising the European electricity and heating energy system"

1. Historical Greenhouse Gases emissions in the European Union

The carbon budget from now onwards for the generation of electricity and the supply of heating in residential and services sector in Europe accounts for $21~\rm GtCO_2$. It has been estimated based on a global carbon budget of $800~\rm GtCO_2$ to avoid temperature increments above $2^{\circ}\rm C$ relative to preindustrial period with a probability of greater than 66% [1, 2]. The global budget is assumed to be split among regions according to a constant per-capita ratio which translates into a 6% share for Europe [3]. Out of the total emissions in Europe, the ratio corresponding to electricity and heating is considered constant and equal to present values. In 2017, electricity generation and heating in the residential and services sector emitted $1.56~\rm GtCO_2$ with represents, 43.5% of European emissions, [4] and Figure 1 .

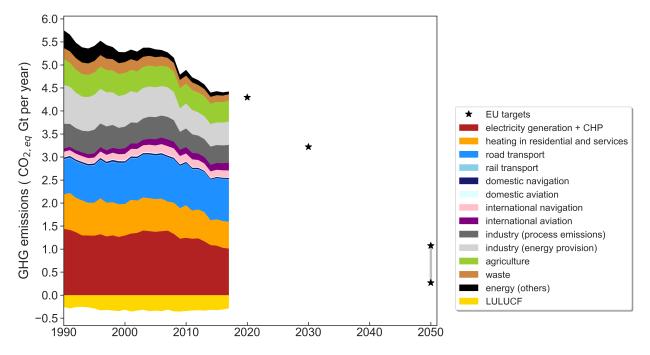


Figure 1: Sectoral distribution of historical emissions in the European Union [4]. The stars indicate committed EU reduction targets.

2. CO₂ restriction paths with equivalent budget

The 21 GtCO₂ budget B can be utilised following different transition paths. One option consists in assuming a linear CO₂ restriction path. Emissions will then reach zero in t_f

Preprint submitted to November 27, 2019

$$t_f = t_0 + \frac{2B}{e_0} \tag{1}$$

Where t_0 =2020, and e_0 represents the carbon emissions from electricity and heating sector in 2020, which are assumed to be the same as in 2017.

Alternatively, emissions can be assumed to follow a path defined by one minus the cumulative distribution function (CDF_{β}) of a beta distribution in which $\beta_1 = \beta_2$.

$$e(t) = e_0(1 - CDF_{\beta}(t))$$

$$CDF_{\beta}(t) = \int_{-\infty}^{t} PDF_{\beta}(t)dt$$

$$PDF_{\beta}(t) = \frac{\Gamma(\beta_1 + \beta_2)}{\Gamma(\beta_1) + \Gamma(\beta_2)} t^{\beta_1 - 1} (1 - t)^{\beta_2 - 1}$$
(2)

where Γ is the gamma function. The cumulative emissions fulfil $\int_{t_0}^{\infty} e(t)dt = B$.

The third option considered for the transition path is an exponential decay, following Raupach *et al.* [3]. In that case, emissions evolve as:

$$e(t) = e_0(1 + (r+m)t)e^{-mt}$$
(3)

where r is the initial linear growth rate, which here is assumed to be r=0, and the decay parameter m is determined by imposing the integral of the path to be equal to the budget.

$$B = \int_{t_0}^{\infty} e_0 (1 + (r + m)t) e^{-mt} dt$$

$$m = \frac{1 + \sqrt{1 + \frac{rB}{e_0}}}{\frac{B}{e_0}}$$
(4)

Although the exponential decay path approaches asymptotically to zero, we assume here that e(2050) = 0. By doing that, the final point of the different transition paths is equivalent and all of them achieve net-zero emissions by 2050.

- 3. Historical evolution of CO_2 emissions from heating supply in residential and services sector in European countries
- 4. Power plants in operation in Europe
- 5. Historical build rates for solar photovoltaics in European countries
- 6. Transition paths cautious and last-minute. Additional results

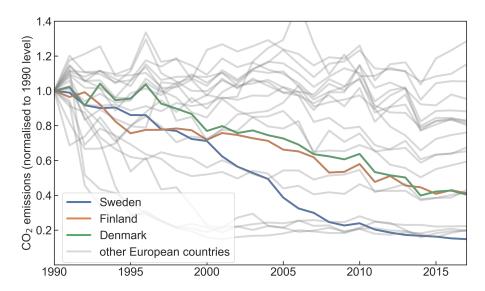


Figure 2: Historical ${\rm CO}_2$ emissions from heating in residential and services sector [4].

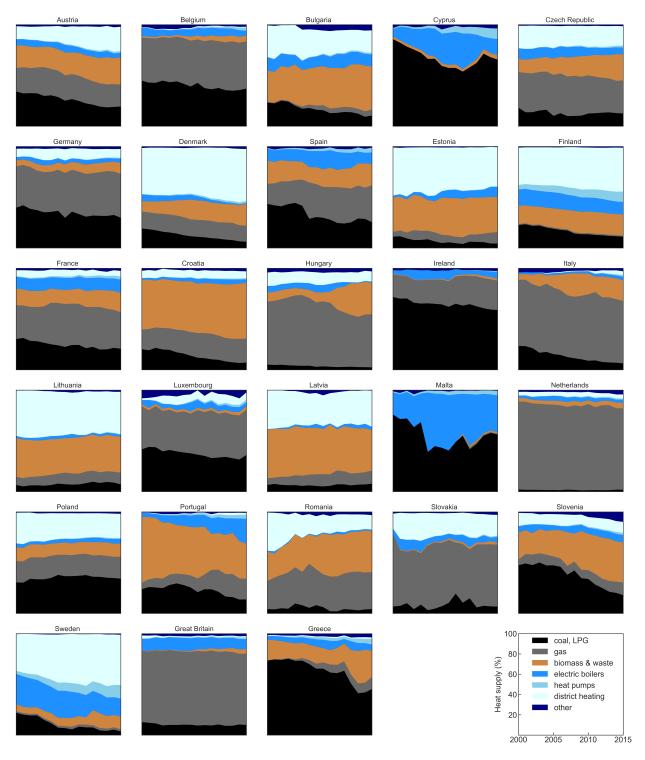


Figure 3: Historical share of technologies used to supply heating in residential and services sector [5].

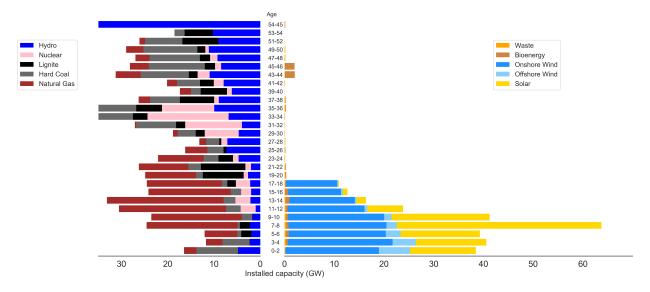


Figure 4: Age distribution of European power plants in operation[6, 7]

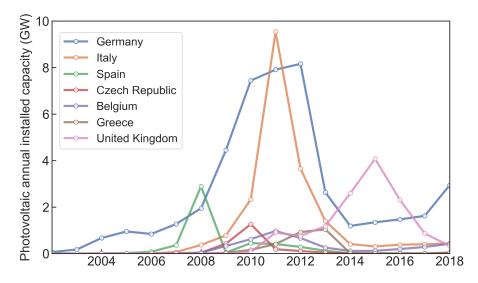


Figure 5: Photovoltaic annual build rates for those European countries with a prominent peak [7]. The sharp increase and subsequent decrease in the installation rates were caused by country-specific successive changes in the regulatory frameworks. See for instance [8, 9].

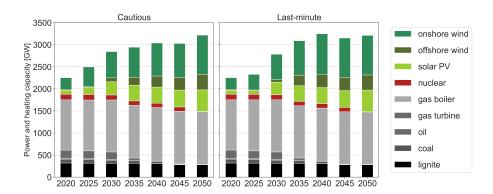


Figure 6: Installed capacities for different technologies throughout transition paths cautious and last-minute shown in Fig. 1 in the main text.

Figure 7: Primary energy in every country in 2050. (left) Cautious transition path, (right) Greenfield optimization for 2050.

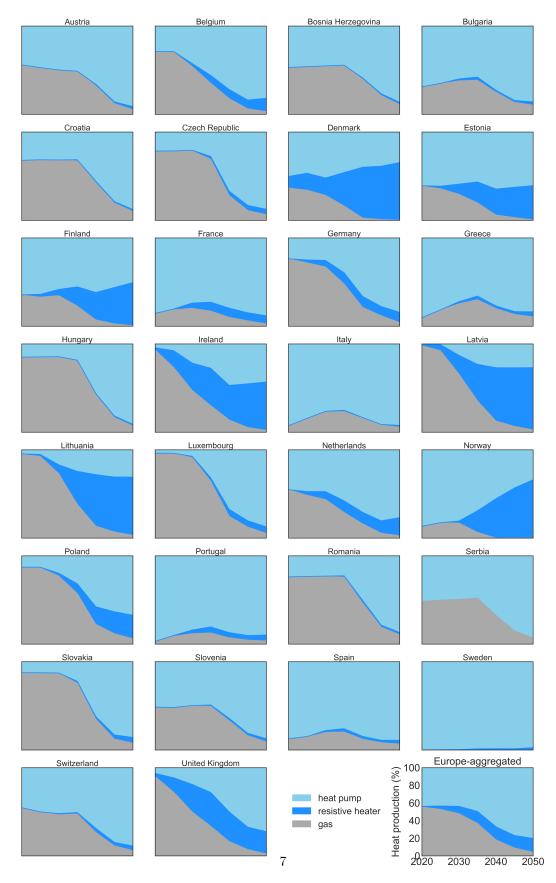


Figure 8: Evolution of technologies used to supply heating in residential and services sector in the cautious path.

7. Model description

In every time step, the optimisation objective, that is, the total annualised system cost is calculated as:

$$\min_{\substack{G_{n,s}, E_{n,s}, \\ F_{\ell}, g_{n,s,t}}} \left[\sum_{n,s} c_{n,s} \cdot G_{n,s} + \sum_{n,s} \hat{c}_{n,s} \cdot E_{n,s} + \sum_{\ell} c_{\ell} \cdot F_{\ell} + \sum_{n,s,t} o_{n,s,t} \cdot g_{n,s,t} \right]$$
(5)

where $c_{n,s}$ are the fixed annualised costs for generator and storage power capacity $G_{n,s}$ of technology s in every bus n, $\hat{c}_{n,s}$ are the fixed annualised costs for storage energy capacity $E_{n,s}$, c_{ℓ} are the fixed annualised costs for bus connectors F_{ℓ} , and $o_{n,s,t}$ are the variable costs (which in some cases include CO_2 tax), for generation and storage dispatch $g_{n,s,t}$ in every hour t. Bus connectors ℓ include transmission lines but also converters between the buses implemented in every country (see Figure ??), for instance, heat pumps that connect the electricity and heating bus.

The optimisation of the system is subject to several constraints. First, hourly demand $d_{n,t}$ in every bus n must be supplied by generators in that bus or imported from other buses. $f_{\ell,t}$ represents the energy flow on the link l and $\alpha_{n,\ell,t}$ indicates both the direction and the efficiency of flow on the bus connectors. $\alpha_{n,\ell,t}$ can be time dependent such as in the case of heat pumps whose conversion efficiency depends on the ambient temperature.

$$\sum_{s} g_{n,s,t} + \sum_{\ell} \alpha_{n,\ell,t} \cdot f_{\ell,t} = d_{n,t} \quad \leftrightarrow \quad \lambda_{n,t} \quad \forall n,t$$
 (6)

The Lagrange multiplier $\lambda_{n,t}$, also known as Karun-Kush-Tucker (KKT), associated with the demand constraint indicates the marginal price of the energy carrier in the bus n, e.g., local marginal electricity price in the electricity bus.

Second, the maximum power flowing through the links is limited by their maximum physical capacity F_{ℓ} . For transmission links, $\underline{f}_{\ell,t} = -1$ and $\overline{f}_{\ell,t} = 1$, which allows both import and export between neighbouring countries. For a unidirectional converter e.g., a heat resistor, $\underline{f}_{\ell,t} = 0$ and $\overline{f}_{\ell,t} = 1$ since a heat resistor can only convert electricity into heat.

$$\underline{f}_{\ell,t} \cdot F_{\ell} \le f_{\ell,t} \le \overline{f}_{\ell,t} \cdot F_{\ell} \qquad \forall \ell, t . \tag{7}$$

For interconnecting transmission lines, the lengths l_{ℓ} are set by the distance between the geographical mid-points of each country, so that some of the transmission within each country is also reflected in the optimisation. A factor of 25% is added to the line lengths to account for the fact that transmission lines cannot be placed as the crow flies due to land use restriction. For the transmission lines capacities F_{ℓ} , a safety margin of 33% of the installed capacity is used to satisfy n-1 requirements [10].

Third, for every hour the maximum capacity that can provide a generator or storage is bounded by the product between installed capacity $G_{n,s}$ and availabilities $\underline{g}_{n,s,t}$, $\bar{g}_{n,s,t}$. For instance, for solar generators $\underline{g}_{n,s,t}$ is zero and $\bar{g}_{n,s,t}$ refers to the capacity factor at time t

$$\underline{g}_{n,s,t} \cdot G_{n,s} \le g_{n,s,t} \le \overline{g}_{n,s,t} \cdot G_{n,s} \qquad \forall n, s, t . \tag{8}$$

The maximum power capacity for generators is limited by potentials $\bar{G}_{n,s}$ that are estimated taking into account physical and environmental constraints:

$$0 \le G_{n,s} \le \bar{G}_{n,s} \qquad \forall n,s . \tag{9}$$

The storage technologies have a charging efficiency η_{in} and rate $g_{n,s,t}^+$, a discharging efficiency η_{out} and rate $g_{n,s,t}^-$, possible inflow $g_{n,s,t,\text{inflow}}$ and spillage $g_{n,s,t,\text{spillage}}$, and standing loss η_0 . The state of charge $e_{n,s,t}$ of every storage has to be consistent with charging and discharging in every hour and is limited by the energy capacity of the storage $E_{n,s}$. It should be remarked that the storage energy capacity $E_{n,s}$ can be optimised independently of the storage power capacity $G_{n,s}$.

$$e_{n,s,t} = \eta_0 \cdot e_{n,s,t-1} + \eta_{in} |g_{n,s,t}^+| - \eta_{out}^{-1} |g_{n,s,t}^-| + g_{n,s,t,\text{inflow}} - g_{n,s,t,\text{spillage}}, 0 \le e_{n,s,t} \le E_{n,s} \quad \forall n, s, t.$$
(10)

So far, equations (6) to (10) represent mainly technical constraints but additional constraints can be imposed to bound the solution.

The interconnecting transmission expansion can be limited by a global constraint

$$\sum_{\ell} l_{\ell} \cdot F_{\ell} \le \text{CAP}_{LV} \qquad \leftrightarrow \quad \mu_{LV} , \qquad (11)$$

where the sum of transmission capacities F_{ℓ} multiplied by the lengths l_{ℓ} is bounded by a transmission volume cap CAP_{LV}. In this case, the Lagrange/KKT multiplier μ_{LV} represents the shadow price of a marginal increase in transmission volume.

The maximum CO_2 allowed to be emitted by the system CAP_{CO_2} can be imposed through the constraint

$$\sum_{n,s,t} \varepsilon_s \frac{g_{n,s,t}}{\eta_{n,s}} + \sum_{n,s} \varepsilon_s (e_{n,s,t=0} - e_{n,s,t=T}) \le \text{CAP}_{CO2} \quad \leftrightarrow \quad \mu_{CO2}$$
 (12)

where ε_s represents the specific emissions in CO₂-tonne-per-MWh_{th} of the fuel s, $\eta_{n,s}$ the efficiency and $g_{n,s,t}$ the generators dispatch. In this case, the Lagrange/KKT multiplier represents the shadow price of CO₂, *i.e.*, the additional price that should be added for every unit of CO₂ to achieve the CO₂ reduction target in an open market.

8. Sectors description and data

TODO: Add data references for electricity demand and annual demand, methodology description for modelling hourly heat demand. Describe modelling approach for wind and solar PV time series and reference repositories. Describe temperature-dependency of heat pumps. Describe operation of CHP power plants. Reference data for initially installed electricity and heat generation capacities. Describe path of deployment of district heating. Describe path of electrification of transport. Include formula for LCOE estimation.

9. Cost assumptions

Figure 9: Cost evolution assumed for the different technologies.

10. References

[1] C. Figueres, H. J. Schellnhuber, G. Whiteman, J. Rockström, A. Hobley, S. Rahmstorf, Three years to safeguard our climate, Nature News 546 (7660) 593. doi:10.1038/546593a.

URL http://www.nature.com/news/three-years-to-safeguard-our-climate-1.22201

[2] G. Peters, How much carbon dioxide can we emit?

 $URL\ \texttt{https://cicero.oslo.no/en/posts/climate/how-much-carbon-dioxide-can-we-emit}$

[3] M. R. Raupach, S. J. Davis, G. P. Peters, R. M. Andrew, J. G. Canadell, P. Ciais, P. Friedlingstein, F. Jotzo, D. P. Vuuren, C. L. Quéré, Sharing a quota on cumulative carbon emissions, Nature Climate Change 4 (10) (2014) 873–879. doi:10.1038/nclimate2384.

 $URL\ {\tt https://www.nature.com/articles/nclimate2384}$

[4] National emissions reported to the UNFCCC and to the EU Greenhouse Gas Monitoring Mechanism, EEA.

URL https://www.eea.europa.eu/data-and-maps/data/national-emissions-reported-to-the-unfccc-and-to-the-eu-greenhouse-gas

[5] L. Mantzos, T. Wiesenthal, N. Matei, S. Tchung-Ming, M. Rzsai, H. P. Russ, A. Soria, JRC-IDEES: Integrated Database of the European Energy Sectordoi:10.2760/182725.

URL http://www.sciencedirect.com/science/article/pii/S0360544216310295

[6] powerplantmatching.

URL https://github.com/FRESNA/powerplantmatching

[7] Renewable Capacity Statistics 2019, IRENA.

URL https://www.irena.org/publications/2019/Mar/Renewable-Capacity-Statistics-2019

[8] Photovoltaics Report, Tech. rep., Fraunhofer ISE (2019).

Table 1: Cost assumption per technology and year.

| Technology ¹ | 2020 | 2025 | 2030 | 2035 | 2040 | 2045 | 2050 | source |
|----------------------------------|------|------|------|------|------|------|------|--------|
| Battery inverter | | | | | | | | |
| Battery storage | | | | | | | | |
| Coal power plant | | | | | | | | |
| Combined heat and power | | | | | | | | |
| Direct air capture | | | | | | | | |
| Electric boiler | | | | | | | | |
| Electrolysis | | | | | | | | |
| Fuel cell | | | | | | | | |
| Gas boiler central | | | | | | | | |
| Gas boiler individual | | | | | | | | |
| Heat pump central | | | | | | | | |
| Heat pump individual | | | | | | | | |
| High voltage direct current line | | | | | | | | |
| Hot water tank central | | | | | | | | |
| Hot water tank individual | | | | | | | | |
| Hydro reservoir | | | | | | | | |
| Hydrogen storage | | | | | | | | |
| Lignite power plant | | | | | | | | |
| Methanation | | | | | | | | |
| Nuclear | | | | | | | | |
| Offshore wind | | | | | | | | |
| Oil power plant | | | | | | | | |
| Onshore wind | | | | | | | | |
| Open cycle gas turbine | | | | | | | | |
| Pumped hydro storage | | | | | | | | |
| Run of river | | | | | | | | |
| Solar PV rooftop | | | | | | | | |
| Solar PV utility | | | | | | | | |

¹ Sorted by alphabet.

Table 2: Efficiency, lifetime and FOM cost per technology, include references.

- $\label{lem:url} URL\ https://www.ise.fraunhofer.de/content/dam/ise/de/documents/publications/studies/Photovoltaics-Report.pdf$
- [9] M. Victoria, C. Gallego, I. Anton, G. Sala, Past, Present and Future of Feed-in Tariffs in Spain: What are their Real Costs?, 27th European Photovoltaic Solar Energy Conference and Exhibition (2012) 4612-4616doi:10.4229/ 27thEUPVSEC2012-6CV.3.49. URL http://www.eupvsec-proceedings.com/proceedings?paper=17736
- [10] T. Brown, P. Schierhorn, E. Tröster, T. Ackermann, Optimising the european transmission system for 77% renewable electricity by 2030 10 (1) 3–9. doi:10.1049/iet-rpg.2015.0135.