

Lecture 14: Newton-Euler equations of motion

- Rigid body kinetics (Newton-Euler equations of motion)
 - Newton's law
 - Angular momentum
 - Inertia dyadic

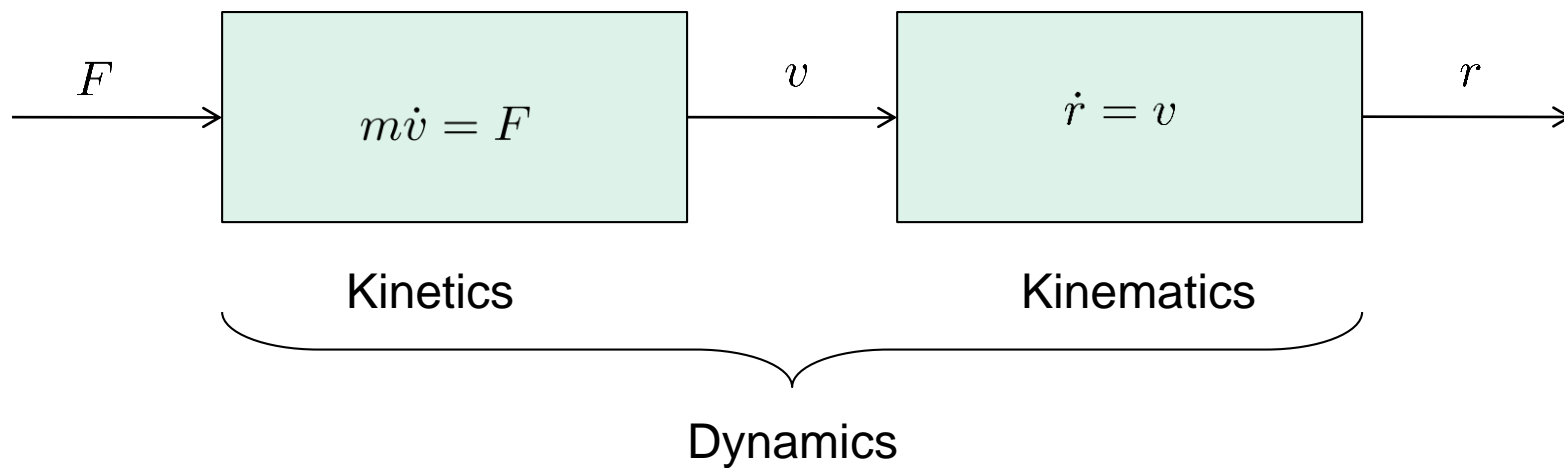
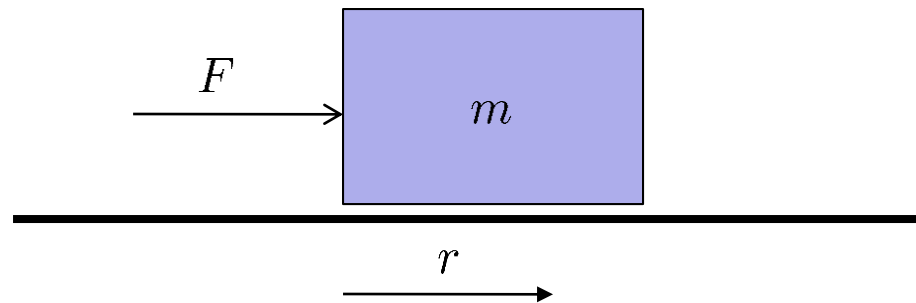
Book: Ch. 7.3

What is rigid body dynamics?

- Rigid body:
 - Wikipedia: “...a rigid body is an idealization of a solid body of finite size in which deformation is neglected.”
- Dynamics = Kinematics + Kinetics
- Kinematics
 - eb.com: “...branch of physics (...) concerned with the geometrically possible **motion** of a body or system of bodies **without consideration of the forces involved** (i.e., causes and effects of the motions).”
 - Book: Ch. 6
- Kinetics
 - eb.com: “...**the effect of forces and torques** on the **motion** of bodies having mass.”
 - Book: Ch. 7, 8.

Remark: Sometimes “dynamics” is used for “kinetics” only

Simplest scalar case



Differentiations of vectors (6.8.5, 6.8.6)

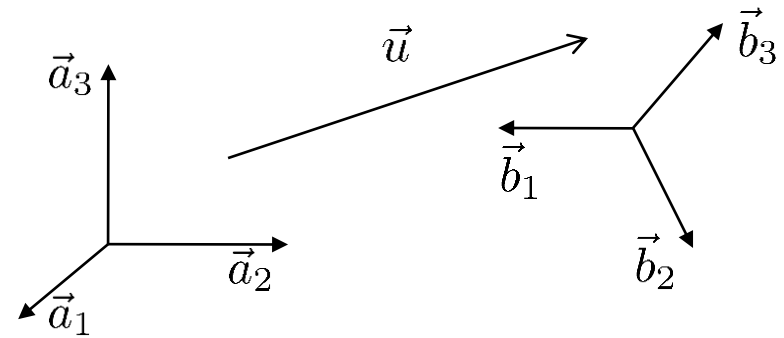
- Coordinate representation:

$$\mathbf{u}^a = \mathbf{R}_b^a \mathbf{u}^b$$

- Differentiation:

$$\dot{\mathbf{u}}^a = \mathbf{R}_b^a \dot{\mathbf{u}}^b + \dot{\mathbf{R}}_b^a \mathbf{u}^b$$

$\rightarrow \dot{\mathbf{R}}_b^a = \mathbf{R}_b^a (\boldsymbol{\omega}_{ab}^b)^\times$



$$\dot{\mathbf{u}}^a = \mathbf{R}_b^a \left[\dot{\mathbf{u}}^b + (\boldsymbol{\omega}_{ab}^b)^\times \mathbf{u}^b \right]$$

- On vector form:

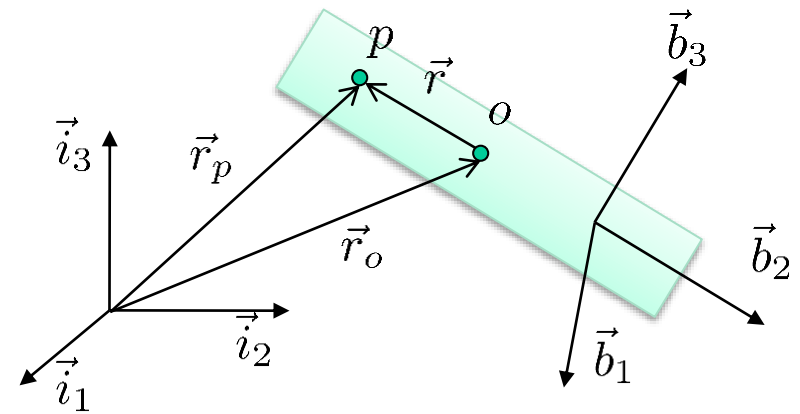
$$\frac{{}^a d}{dt} \vec{u} = \frac{{}^b d}{dt} \vec{u} + \vec{\omega}_{ab} \times \vec{u}$$

Note! Generally,

$$\dot{\mathbf{u}}^a \neq \mathbf{R}_b^a \dot{\mathbf{u}}^b$$

Rigid body kinematics

- Velocities and accelerations (Ch. 6.12)



$$\vec{v}_o := \frac{{}^i d}{dt} \vec{r}_o, \quad \vec{v}_p := \frac{{}^i d}{dt} \vec{r}_p$$

$$\vec{a}_o := \frac{{}^i d^2}{dt^2} \vec{r}_o, \quad \vec{a}_p := \frac{{}^i d^2}{dt^2} \vec{r}_p$$

$$\vec{\alpha}_{ib} := \frac{{}^i d}{dt} \vec{\omega}_{ib} = \frac{{}^b d}{dt} \vec{\omega}_{ib}$$

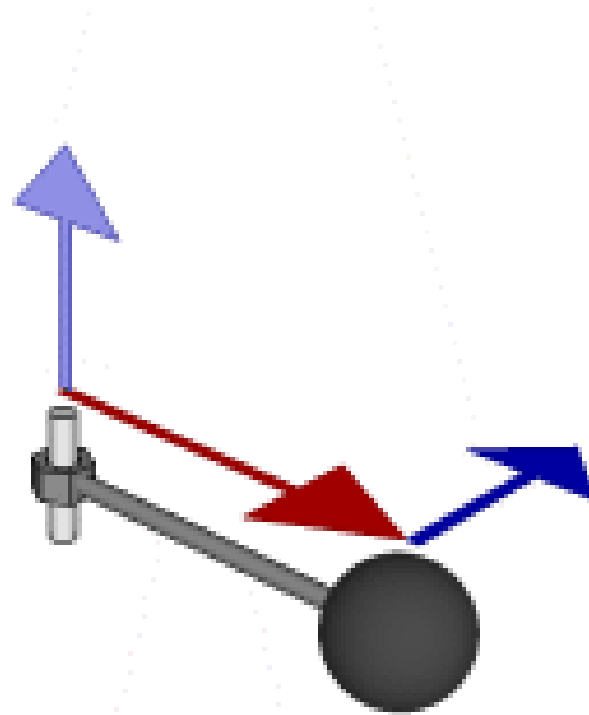
$$\begin{aligned} \vec{v}_p &= \vec{v}_o + \frac{{}^i d}{dt} \vec{r} \\ &= \vec{v}_o + \frac{{}^b d}{dt} \vec{r} + \vec{\omega}_{ib} \times \vec{r} \\ &= \vec{v}_o + \vec{\omega}_{ib} \times \vec{r}, \quad \vec{r} \text{ fixed.} \end{aligned}$$

$$\vec{a}_p = \vec{a}_o + \frac{{}^b d^2}{dt^2} \vec{r} + 2\vec{\omega}_{ib} \times \frac{{}^b d}{dt} \vec{r} + \vec{\alpha}_{ib} \times \vec{r} + \vec{\omega}_{ib} \times (\vec{\omega}_{ib} \times \vec{r})$$

$$\vec{a}_p = \vec{a}_o + \vec{\alpha}_{ib} \times \vec{r} + \vec{\omega}_{ib} \times (\vec{\omega}_{ib} \times \vec{r}), \quad \vec{r} \text{ fixed.}$$

Torque, and linear/angular momentum

$$\boldsymbol{\tau} = \mathbf{r} \times \mathbf{F}$$
$$\mathbf{L} = \mathbf{r} \times \mathbf{p}$$



Source: Wikipedia

- Book:
 - Torque: \vec{N}, \vec{T}
 - Angular momentum: \vec{h}

EoM with reference of CoM

$$\vec{F}_{bc} = m\vec{a}_c$$

$$\vec{T}_{bc} = \vec{M}_{b/c} \cdot \vec{\alpha}_{ib} + \vec{\omega}_{ib} \times \left(\vec{M}_{b/c} \cdot \vec{\omega}_{ib} \right)$$

Inertia dyadic I

$$\vec{M}_{b/c} = - \int_b \vec{r}^\times \cdot \vec{r}^\times$$

Inertia matrix

- Found for each rigid body by calculating

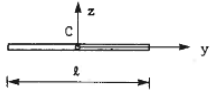
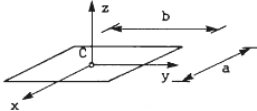
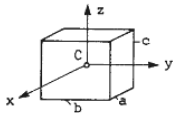
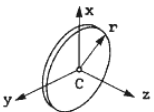
$$M_{b/c}^b = \int_b (\mathbf{r}^b)^\top \mathbf{r}^b I - \mathbf{r}^b (\mathbf{r}^b)^\top dm = \int_b \begin{pmatrix} y^2 + z^2 & -xy & -xz \\ -xy & x^2 + z^2 & -yz \\ -xz & -yz & x^2 + y^2 \end{pmatrix} dm$$

- Constant in body-fixed coordinate system!
- Not constant in inertial coordinate system

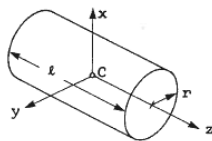
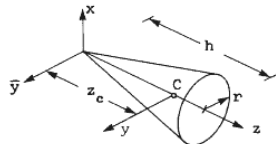
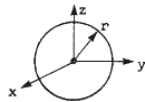
$$M_{b/c}^i = R_b^i M_{b/c}^b (R_b^i)^\top$$

- Books and wikipedia have tables for common geometries, otherwise computer programs calculates, or can be calculated/identified based on experiments
- Typically, axis in body-system chosen as body symmetri axis, giving zeros in inertia matrix. If symmetric about all axis, the inertia matrix becomes diagonal.

Finding moments of inertia

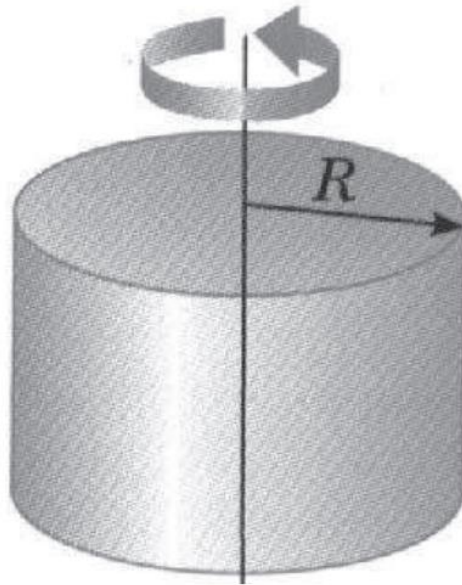
<p>Homogen slank stav</p> 	$I_z = \frac{1}{12} m l^2$ $I_{\bar{z}} = \frac{1}{3} m l^2$
<p>Tynn rektangulær plate</p> 	$I_z = \frac{1}{12} m (a^2 + b^2)$ $I_x = \frac{1}{12} m b^2$ $I_y = \frac{1}{12} m a^2$
<p>Rektangulært prisme</p> 	$I_z = \frac{1}{12} m (a^2 + b^2)$
<p>Tynn sirkulær skive</p> 	$I_z = \frac{1}{2} m r^2$ $I_x = I_y = \frac{1}{4} m r^2$

From F. Irgens, Dynamikk

<p>Sirkulær sylinder</p> 	$I_z = \frac{1}{2} m r^2$ $I_x = I_y = \frac{1}{12} m (3r^2 + l^2)$
<p>Tynt sylinderskall</p>	$I_z = m r^2$ $I_x = I_y = \frac{1}{2} m r^2 + \frac{1}{12} m l^2$
<p>Rett sirkulær kjegle</p> 	$I_z = \frac{1}{10} m r^2$ $I_y = \frac{3}{20} m r^2 + \frac{3}{80} m h^2$ $I_{\bar{y}} = \frac{3}{20} m r^2 + \frac{3}{5} m h^2$ $z_c = 3h/4$
<p>Kule</p> 	$I_C = \frac{2}{5} m r^2$
<p>Kuleskall</p>	$I_C = \frac{2}{3} m r^2$

- http://en.wikipedia.org/wiki/List_of_moment_of_inertia_tensors
- For other/general rigid bodies (vessels/planes/etc.), computer programs can find moments of inertia

Inertia matrix, examples



Homogeneous Disk

$$I_{disk} = \frac{1}{4}mr^2 \begin{bmatrix} 1 + \frac{1}{3}\frac{h^2}{r^2} & 0 & 0 \\ 0 & 1 + \frac{1}{3}\frac{h^2}{r^2} & 0 \\ 0 & 0 & 2 \end{bmatrix}$$

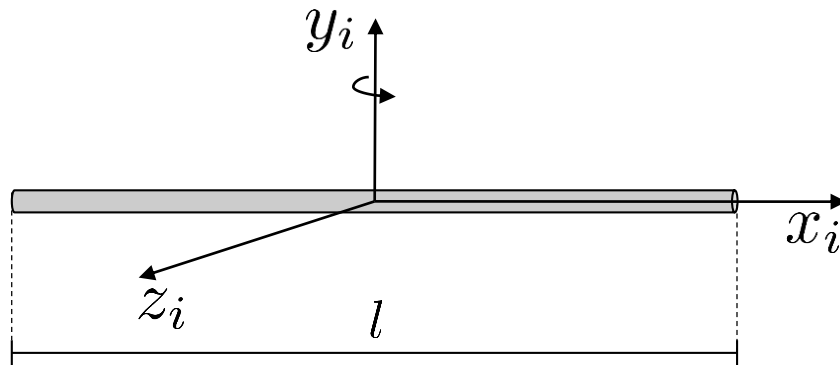


F/A-18

$$I = \begin{bmatrix} 23 & 0 & 2.97 \\ 0 & 15.13 & 0 \\ 2.97 & 0 & 16.99 \end{bmatrix} \text{ kslug} - \text{ft}^2$$

1 slug = 14.6 kg
1 ft = 0.304 m

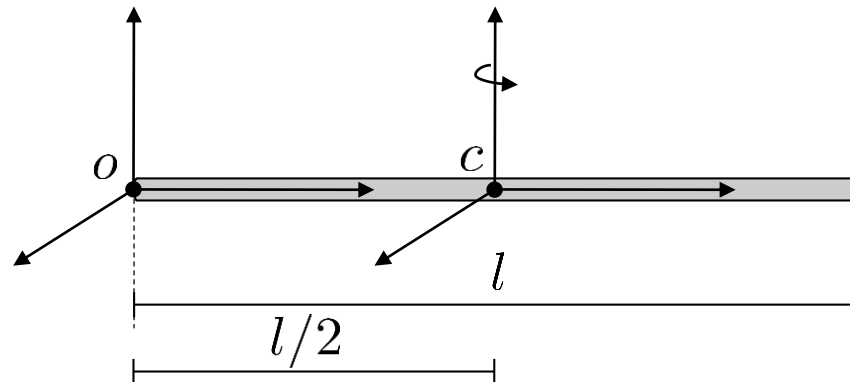
Example: Slender beam



Parallel axis theorem

$$\begin{aligned}\vec{M}_{b/o} &= \vec{M}_{b/c} - m(\underline{r}_g^b)^\times (\underline{r}_g^b)^\times \\ &= \vec{M}_{b/c} + m [(\underline{r}_g^b)^T \underline{r}_g^b \mathbf{I} - \underline{r}_g^b (\underline{r}_g^b)^T]\end{aligned}$$

Example:



Summary: EoM rigid body kinetics I

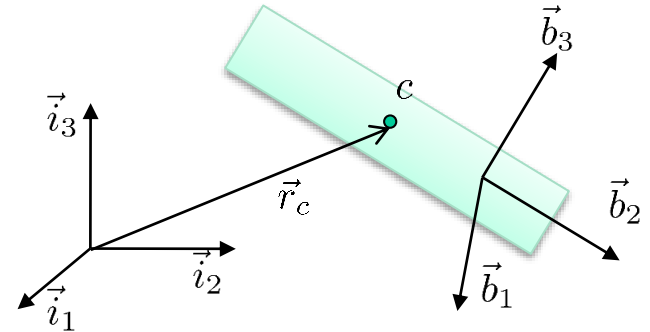
Summary: EoM rigid body kinetics II

Newton-Euler EoM

- Referenced to center of mass (CoM):

$$\vec{F}_{bc} = m\vec{a}_c$$

$$\vec{T}_{bc} = \vec{M}_{b/c} \cdot \vec{\alpha}_{ib} + \vec{\omega}_{ib} \times \left(\vec{M}_{b/c} \cdot \vec{\omega}_{ib} \right)$$



- Sometimes convenient to have them referenced to other point o:

- Forces and moments in o:

$$\vec{F}_{bo} = \vec{F}_{bc}$$

$$\vec{T}_{bo} = \vec{T}_{bc} + \vec{r}_g \times \vec{F}_{bc}$$

- Use

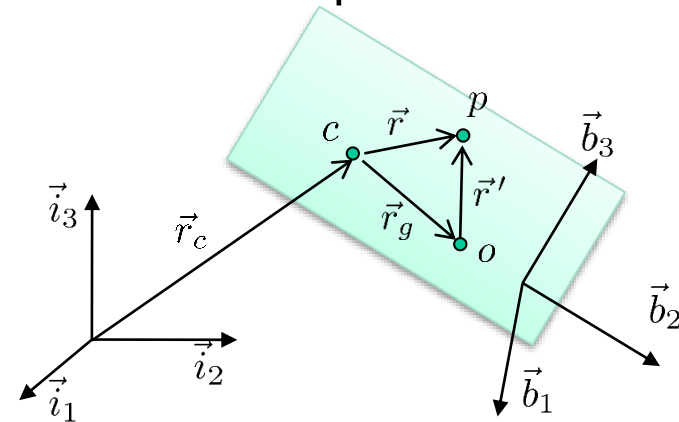
$$\vec{a}_c = \vec{a}_o + \vec{\alpha}_{ib} \times \vec{r}_g + \vec{\omega}_{ib} \times (\vec{\omega}_{ib} \times \vec{r}_g)$$

- Define

$$\vec{M}_{b/o} := - \int_b (\vec{r}')^\times (\vec{r}')^\times dm$$

$$\vec{F}_{bo} = m (\vec{a}_o + \vec{\alpha}_{ib} \times \vec{r}_g + \vec{\omega}_{ib} \times (\vec{\omega}_{ib} \times \vec{r}_g))$$

$$\vec{T}_{bo} = \vec{r}_g \times \vec{a}_o + \vec{M}_{b/o} \cdot \vec{\alpha}_{ib} + \vec{\omega}_{ib} \times \left(\vec{M}_{b/o} \cdot \vec{\omega}_{ib} \right)$$



- Useful when CoM changes – no need to recalculate inertia matrix – still need to know CoM

Traits of Newton-Euler EoM

(and a preview: Lagrange EoM)

Newton-Euler EoM:

- Involves working with vectors
 - Lagrange: Algebraic manipulations
- Forces and moments are central
 - Lagrange: Energy and work are central
- All forces in the system must be considered
 - Lagrange: Forces of constraint are implicitly eliminated with the use of generalized coordinates (and generalized forces)
- Somewhat complicated to use by hand, but can be implemented in computer systems
 - Lagrange: Easier to do by hand, not suitable for complex systems
- d'Alembert's principle: Elimination of forces of constraint (Ch. 7.7)
 - Can simplify application of Newton-Euler EoM
 - Kane's EoM (Ch. 7.8, 7.9)
 - Starting point for Lagrange EoM (Ch. 8.2)

$$\vec{F}_{bc} = m\vec{a}_c$$

$$\vec{T}_{bc} = \vec{M}_{b/c} \cdot \vec{\alpha}_{ib} + \vec{\omega}_{ib} \times (\vec{M}_{b/c} \cdot \vec{\omega}_{ib})$$

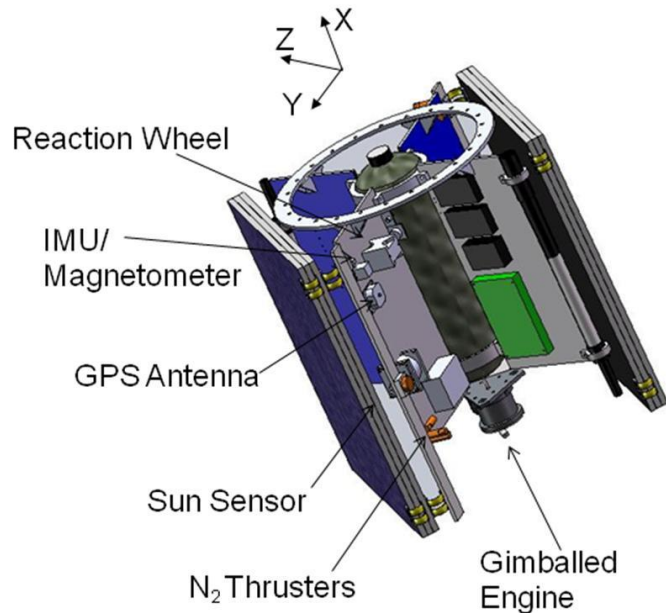
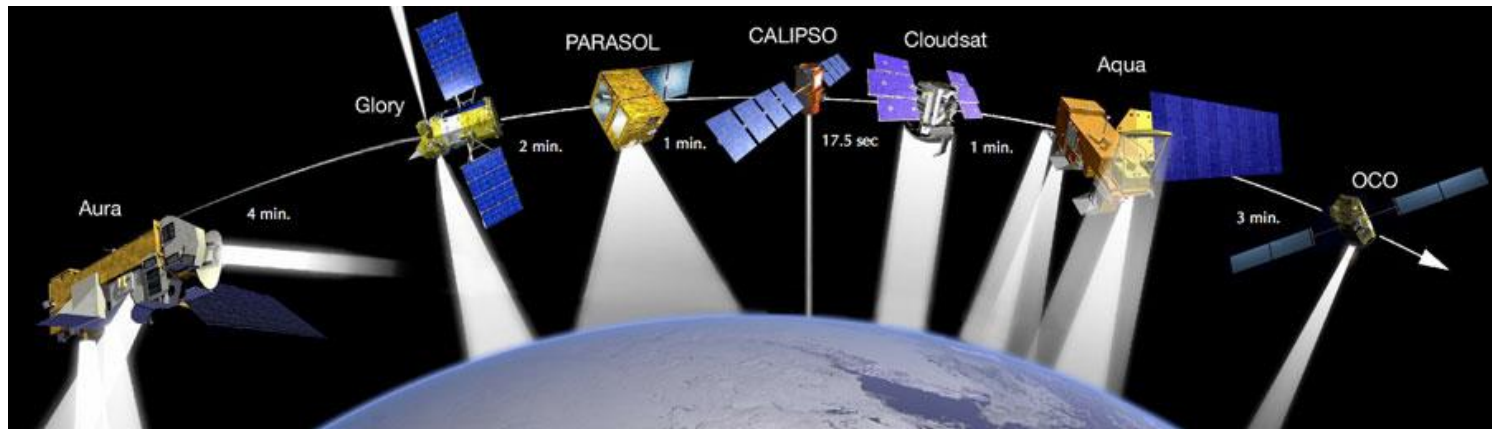
Kinematics

Derivatives of position and orientation as function of velocity and angular velocity

Kinetics

Derivatives of velocity and angular velocity as function of applied forces and torques

Satellite attitude dynamics



<http://satellite.mit.edu/>

$$\vec{F}_{bc} = m\vec{a}_c$$

$$\vec{T}_{bc} = \vec{M}_{b/c} \cdot \vec{\alpha}_{ib} + \vec{\omega}_{ib} \times (\vec{M}_{b/c} \cdot \vec{\omega}_{ib})$$

Example: Satellite I

- Assume the body-fixed frame is chosen such that

$$M_{b/c}^b = \begin{pmatrix} m_{12} & 0 & 0 \\ 0 & m_{22} & 0 \\ 0 & 0 & m_{33} \end{pmatrix}$$

$$\begin{pmatrix} m_{12} & 0 & 0 \\ 0 & m_{22} & 0 \\ 0 & 0 & m_{33} \end{pmatrix} \begin{pmatrix} \dot{\omega}_1 \\ \dot{\omega}_2 \\ \dot{\omega}_3 \end{pmatrix} + \begin{pmatrix} 0 & \omega_3 & \omega_2 \\ \omega_3 & 0 & -\omega_1 \\ -\omega_2 & \omega_1 & 0 \end{pmatrix} \begin{pmatrix} m_{12} & 0 & 0 \\ 0 & m_{22} & 0 \\ 0 & 0 & m_{33} \end{pmatrix} \begin{pmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{pmatrix} = \begin{pmatrix} T_1 \\ T_2 \\ T_3 \end{pmatrix}$$

Example: Satellite II

Airplane EoM (from book about airplane dynamics)

$$X - mgS_\theta = m(\dot{u} + qw - rv)$$

$$Y + mgC_\theta S_\Phi = m(\dot{v} + ru - pw)$$

$$Z + mgC_\theta C_\Phi = m(\dot{w} + pv - qu)$$

Force equations

$$m \left(\dot{\mathbf{v}}_c^b + (\boldsymbol{\omega}_{ib}^b)^\times \mathbf{v}_c^b \right) = \mathbf{F}_{bc}^b$$

$$L = I_x \dot{p} - I_{xz} \dot{r} + qr(I_z - I_y) - I_{xz} pq$$

$$M = I_y \dot{q} + rp(I_x - I_z) + I_{xz}(p^2 - r^2)$$

$$N = -I_{xz} \dot{p} + I_z \dot{r} + pq(I_y - I_x) + I_{xz} qr$$

Moment equations

$$\mathbf{M}_{b/c}^b \dot{\boldsymbol{\omega}}_{ib}^b + (\boldsymbol{\omega}_{ib}^b)^\times \mathbf{M}_{b/c}^b \boldsymbol{\omega}_{ib}^b = \mathbf{T}_{bc}^b$$

$$p = \dot{\Phi} - \dot{\psi} S_\theta$$

$$q = \dot{\theta} C_\Phi + \dot{\psi} C_\theta S_\Phi$$

$$r = \dot{\psi} C_\theta C_\Phi - \dot{\theta} S_\Phi$$

Body angular velocities
in terms of Euler angles
and Euler rates

$$\dot{\theta} = q C_\Phi - r S_\Phi$$

$$\dot{\Phi} = p + q S_\Phi T_\theta + r C_\Phi T_\theta$$

$$\dot{\psi} = (q S_\Phi + r C_\Phi) \sec \theta$$

Euler rates in terms of
Euler angles and body
angular velocities

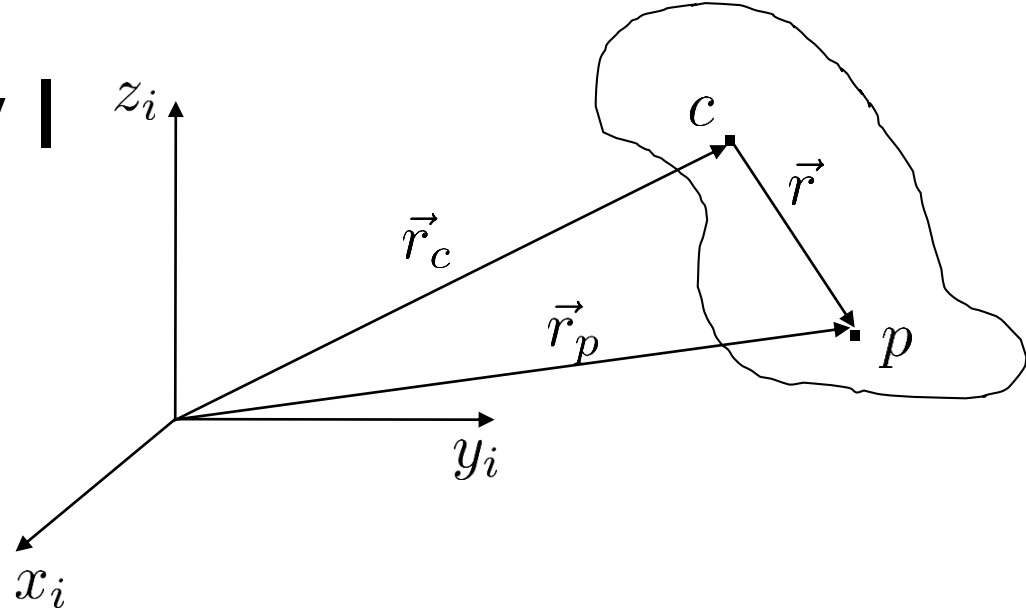
$$\dot{\boldsymbol{\phi}} = \mathbf{E}_d^{-1}(\boldsymbol{\phi}) \boldsymbol{\omega}_{ib}^b$$

Velocity of aircraft in the fixed frame in terms of Euler angles and
body velocity components

$$\begin{bmatrix} \frac{dx}{dt} \\ \frac{dy}{dt} \\ \frac{dz}{dt} \end{bmatrix} = \begin{bmatrix} C_\theta C_\psi & S_\Phi S_\theta C_\psi - C_\Phi S_\psi & C_\Phi S_\theta C_\psi + S_\Phi S_\psi \\ C_\theta S_\psi & S_\Phi S_\theta S_\psi + C_\Phi C_\psi & C_\Phi S_\theta S_\psi - S_\Phi C_\psi \\ -S_\theta & S_\Phi C_\theta & C_\Phi C_\theta \end{bmatrix} \begin{bmatrix} u \\ v \\ w \end{bmatrix}$$

$$\dot{\mathbf{r}}_c^i = \mathbf{v}_c^i = \mathbf{R}_b^i \mathbf{v}_c^b$$

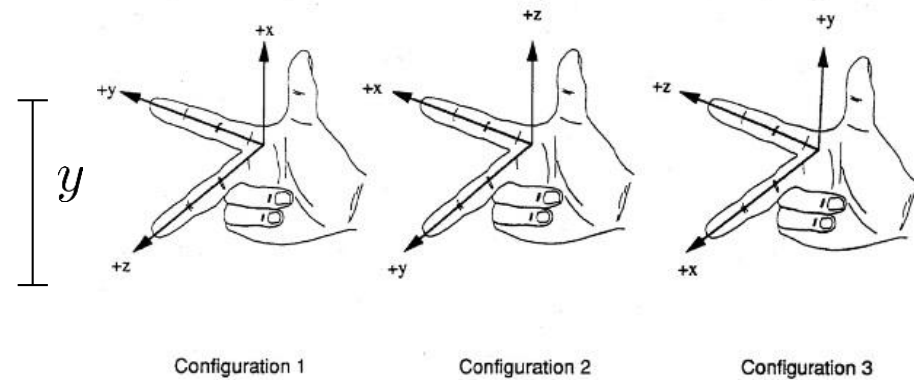
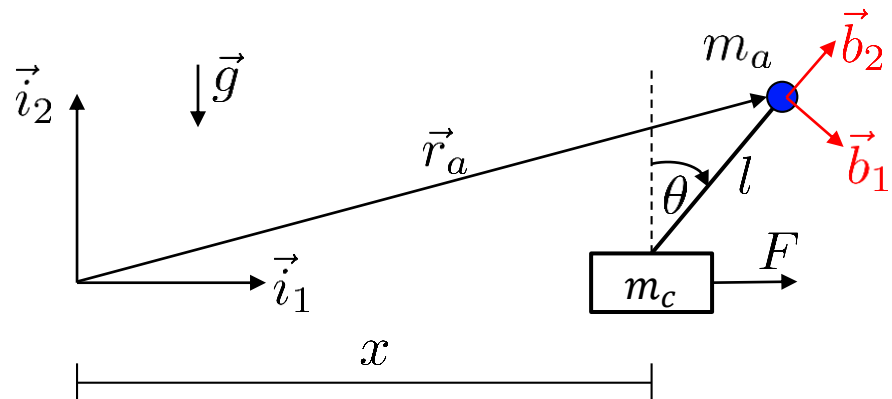
Kinematic energy I



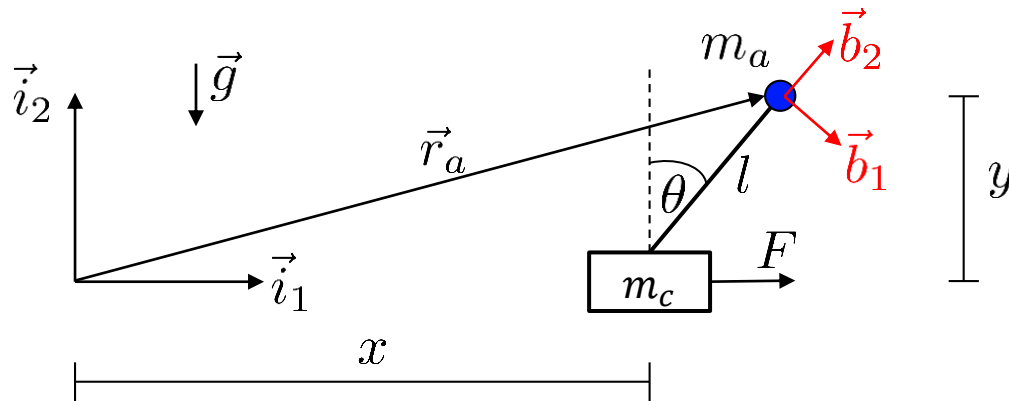
Kinematic energy II

$$K = \frac{1}{2}m(\underline{v}_c^b)^T \underline{v}_c^b + \frac{1}{2}(\underline{\omega}_c^b)^T M_{b/c}^b \underline{\omega}_c^b$$

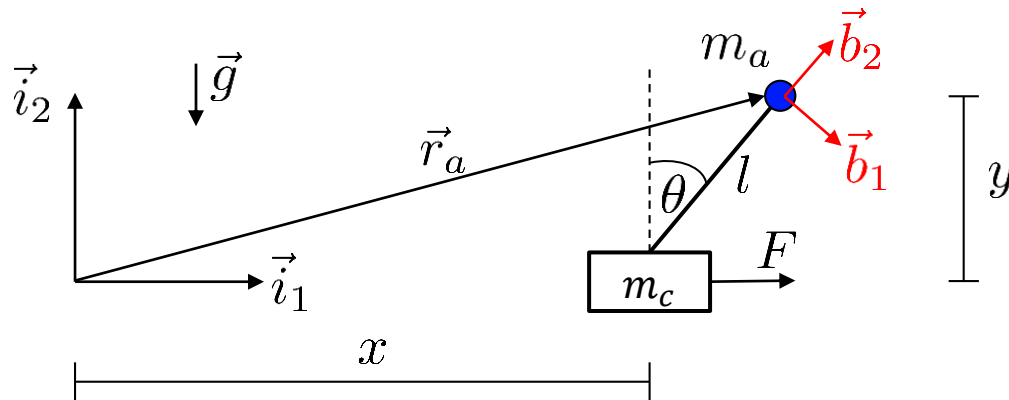
Example: Inverted pendulum



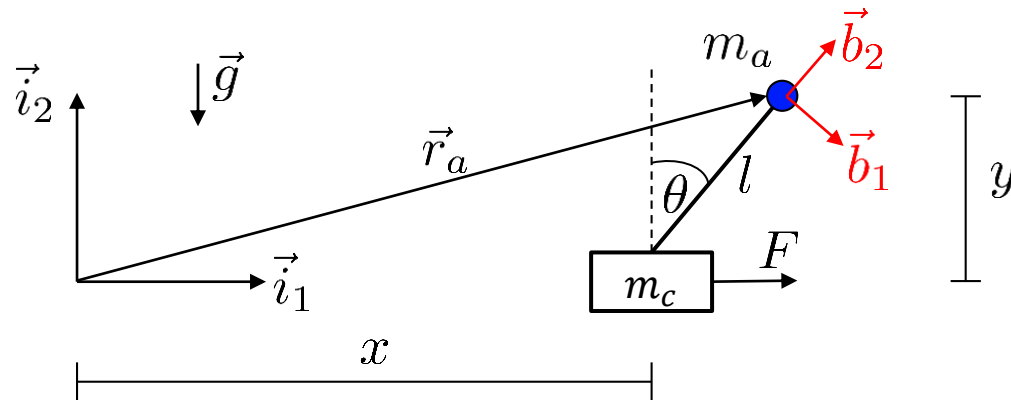
Example: Inverted pendulum - kinematics



Example: Inverted pendulum – kinetics I

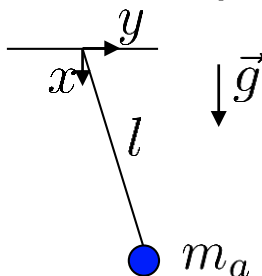


Example: Inverted pendulum – kinetics II

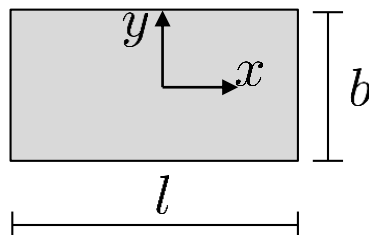


Homework

- Find the equation of motion of a pendulum using Newton's law:



- Find the moment of inertia of a rectangular plate



- Try to find the acceleration of the inverted pendulum (slide 26) using only the inertial frame (check your result by transforming the acceleration to the body frame)
- Read 5.1-5.3