# Lecture 21: Balance equations – Momentum and energy balances

- Recap balance laws
- The momentum balance
- The energy balance
- (Differential balance laws)

Book: Ch. 11.2, 11.4

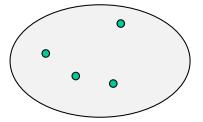
#### Lecture schedule change

- New lecture: 26.03.2019 10:15-12:00 in S3
- Cancelled lecture 04.04.2019

#### Process modeling and balance laws

- The balance laws are formulated for «conserved quantities»:
  - Mass (or other quantities that are «equivalent» to mass, such as moles, particles, etc.)
  - Momentum
  - Energy
- Process modeling is done by
  - 1. formulating the relevant balance laws, and
  - 2. finding the «closure relations» that is used to determine the flows in a balance law, as function of the state («inventory») of the balance law
- The state («inventory») of a balance law is what is used as a measure for the conserved quantity
  - Such as mass, moles, concentration, level, pressure, ... for mass balance,
  - velocity or flows for momentum balance, and
  - temperature for energy balance

# The basic physical principles



Consider a volume consisting of a fixed number of fluid particles, with total mass m, total momentum  $\vec{p}$  and total energy E. From basic physics (conservation laws), we know the following principles hold:

Conservation of mass (mass balance):

$$\frac{\mathrm{d}m}{\mathrm{d}t} = 0$$

Newton's second law (momentum balance)

$$\frac{{}^{i}\mathrm{d}\vec{p}}{\mathrm{d}t} = \vec{F}$$

Also holds for angular momentum,  $\vec{h} = \vec{r} \times \vec{p}$  :

$$\frac{{}^{i}\mathbf{d}}{\mathbf{d}t}\vec{h} = \vec{r} \times \vec{F} = \vec{T}$$

• First law of thermodynamics (conservation of energy, energy balance):

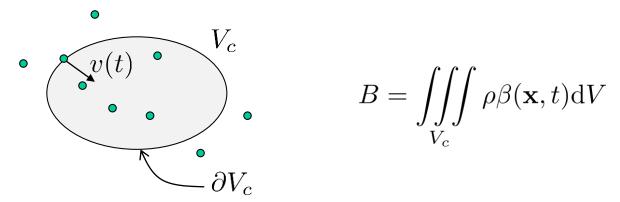
Rate of heat flowing into volume

Rate of heat flowing into volume from surroundings  $\frac{\mathrm{d}E}{\mathrm{d}t} = \dot{Q} - \dot{W}$ 

Rate at which work is done by the body at surroundings

#### The balance laws

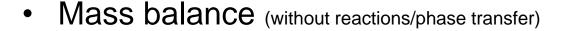
Assume a fixed control volume (of arbitrary size and shape),
 where fluid flows across the control volume



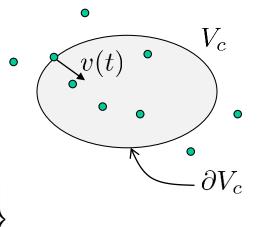
The general integral (macroscopic) balance law for B is

$$\frac{\mathrm{d}}{\mathrm{d}t}B = \left\{ \begin{array}{c} \text{transfer of } B \text{ through} \\ \text{surface } \partial V_c \text{ by} \\ \text{fluid flow (convection)} \end{array} \right\} + \left\{ \begin{array}{c} \text{other effects that} \\ \text{transfer } B \text{ into } V_c \\ \text{(indep. of fluid flow)} \end{array} \right\}$$

### The integral balance laws



$$\frac{\mathrm{d}}{\mathrm{d}t}m = \left\{ \begin{array}{c} \text{transfer of mass into} \\ V_c \text{ by fluid flow} \\ \text{across surface } \partial V_c \end{array} \right\}$$



Momentum (note: momentum is a vector)

$$\frac{\mathrm{d}}{\mathrm{d}t}\mathbf{p} = \left\{ \begin{array}{c} \text{transfer of momentum into} \\ V_c \text{ by fluid flow} \\ \text{across surface } \partial V_c \end{array} \right\} + \left\{ \begin{array}{c} \text{generation of momentum} \\ \text{in } V_c \text{ due to forces} \\ \text{acting on } V_c \end{array} \right\}$$

Energy

$$\frac{\mathrm{d}}{\mathrm{d}t}E = \left\{ \begin{array}{c} \text{transfer of energy into} \\ V_c \text{ by fluid flow} \\ \text{across surface } \partial V_c \end{array} \right\} + \left\{ \begin{array}{c} \text{transfer of energy into} \\ V_c \text{ by heat transfer} \\ \text{and by work} \end{array} \right\}$$

#### The mass balance

In words

$$\frac{\mathrm{d}}{\mathrm{d}t}m = \left\{ \begin{array}{c} \text{transfer of mass into} \\ V_c \text{ by fluid flow} \\ \text{across surface } \partial V_c \end{array} \right\}$$

Mathematically

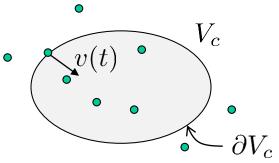
$$\frac{\mathrm{d}}{\mathrm{d}t}m = \frac{\mathrm{d}}{\mathrm{d}t} \iiint_{V_c} \rho \mathrm{d}V = -\iint_{\partial V_c} \rho \vec{v} \cdot \vec{n} \mathrm{d}A$$

• Often, we have one (or more) «point inflows»  $w_{\text{in},i}$ , and outflows  $w_{\text{out},i}$ . Then mass balance can be formulated as

$$\frac{\mathrm{d}}{\mathrm{d}t}m = \sum_{i} w_{\mathrm{in},i} - \sum_{i} w_{\mathrm{out},i}$$

"Convection"

#### The momentum balance



In words

$$\frac{\mathrm{d}}{\mathrm{d}t}\mathbf{p} = \left\{ \begin{array}{c} \text{transfer of momentum into} \\ V_c \text{ by fluid flow} \\ \text{across surface } \partial V_c \end{array} \right\} + \left\{ \begin{array}{c} \text{generation of momentum} \\ \text{in } V_c \text{ due to forces} \\ \text{acting on } V_c \end{array} \right\}$$

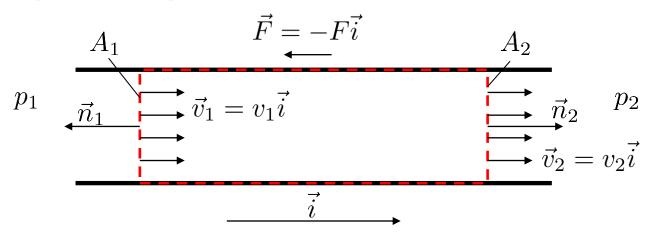
Mathematically

$$\frac{^{i}d}{dt}\vec{p} = \frac{^{i}d}{dt} \iiint_{V_{c}} \rho \vec{v} dV = - \iint_{\partial V_{c}} \rho \vec{v} \vec{v} \cdot \vec{n} dA + \vec{F}^{(r)}$$

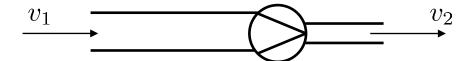
where  $\vec{F}^{(r)}$  is resultant force on fluid in control volume

(often: gravity (hydrostatic) and/or friction (hydrodynamic))

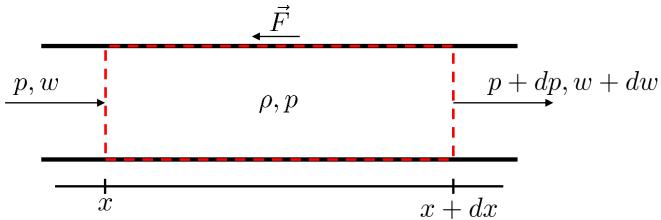
# **Example: Pipeflow**



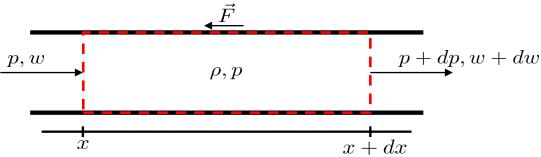
# Example: Water-Jet



### Example: Transmission line I



### Example: Transmission line II



### The energy balance

v(t)  $\partial V_c$   $\partial V_c$ 

In words

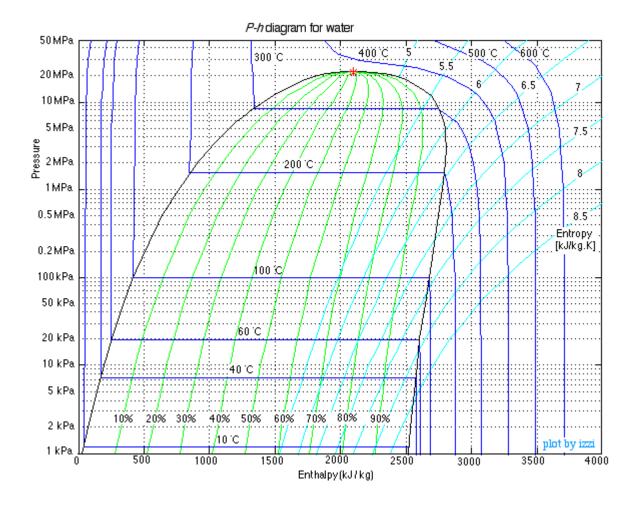
$$\frac{\mathrm{d}}{\mathrm{d}t}E = \left\{ \begin{array}{c} \text{transfer of energy into} \\ V_c \text{ by fluid flow} \\ \text{across surface } \partial V_c \end{array} \right\} + \left\{ \begin{array}{c} \text{transfer of energy into} \\ V_c \text{ by heat transfer} \\ \text{and by work} \end{array} \right\}$$

Mathematically

$$\frac{\mathrm{d}}{\mathrm{d}t}E = \frac{\mathrm{d}}{\mathrm{d}t} \iiint_{V_c} \rho e \mathrm{d}V = -\iint_{\partial V_c} \rho e \vec{v} \cdot \vec{n} \mathrm{d}A + \dot{Q} - \dot{W}$$
Energy flow by convection

What is the energy of a fluid?

# P-h-diagram for water



### Energy

$$\frac{\mathrm{d}}{\mathrm{d}t}E = \frac{\mathrm{d}}{\mathrm{d}t} \iiint_{V_c} \rho e \mathrm{d}V = -\iint_{\partial V_c} \rho e \vec{v} \cdot \vec{n} \mathrm{d}A + \dot{Q} - \dot{W}$$

 The energy of a fluid of mass m, moving with a velocity v at a height z in a gravitational field:

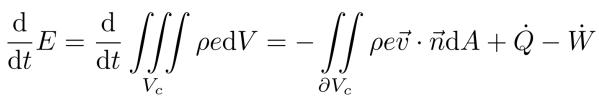
$$E = \underbrace{U}_{\text{internal}} + \underbrace{\frac{1}{2}mv^2}_{\text{energy}} + \underbrace{mgz}_{\text{potential}}$$

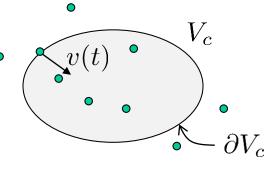
$$\underbrace{\text{energy}}_{\text{energy}}$$

Specific energy:

$$e = u + \frac{1}{2}v^2 + gz$$

#### Heat and work flow





Heat flow

$$\dot{Q} = \iint_{\partial V_c} \vec{j}_Q \cdot \vec{n} dA$$

Work flow

$$\dot{W} = \iint_{\partial \dot{V}_c} p \vec{v} \cdot \vec{n} dA + \underbrace{\dot{W}_s}_{\text{shaft work}}$$

### Enthalpy

The energy balance can be written

$$\frac{\mathrm{d}}{\mathrm{d}t} \iiint_{V_c} \rho e \mathrm{d}V = -\iint_{\partial V_c} \rho \left( e + \frac{p}{\rho} \right) \vec{v} \cdot \vec{n} \mathrm{d}A - \dot{W}_s + \dot{Q}$$

where the first term on the RHS is convection and flow work

Define enthalpy as

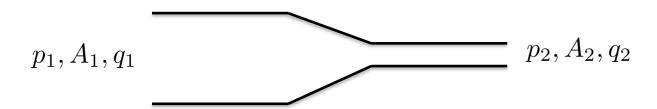
$$h = u + \frac{p}{\rho}$$

Then

$$\frac{\mathrm{d}}{\mathrm{d}t} \iiint\limits_{V_c} \rho \left( u + \frac{1}{2}v^2 + gz \right) \mathrm{d}V = - \iint\limits_{\partial V_c} \rho \left( h + \frac{1}{2}v^2 + gz \right) \vec{v} \cdot \vec{n} \mathrm{d}A - \dot{W}_s + \dot{Q}$$

# Example: Streamline

# **Example: Restriction**



#### Internal energy and enthalpy

Specific heat capacities:

$$c_v := \left. \frac{\partial u}{\partial T} \right|_{\text{constant volume}} \qquad c_p := \left. \frac{\partial h}{\partial T} \right|_{\text{constant pressure}}$$

(found in tables for different fluids, often assumed constant)

 If assumed constant, implies that energy and enthalpy is (linear) function of temperature only:

$$\frac{\mathrm{d}u}{\mathrm{d}t} = c_v \frac{\mathrm{d}T}{\mathrm{d}t}$$

$$u(T_2) - u(T_1) = c_v (T_2 - T_1)$$

$$\frac{\mathrm{d}h}{\mathrm{d}t} = c_p \frac{\mathrm{d}T}{\mathrm{d}t}$$

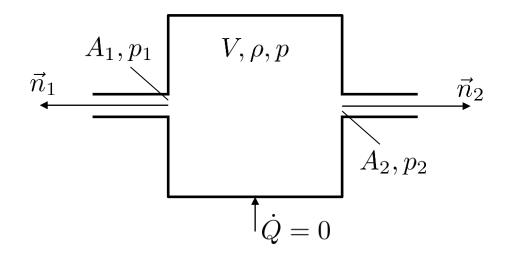
$$h(T_2) - h(T_1) = c_p (T_2 - T_1)$$

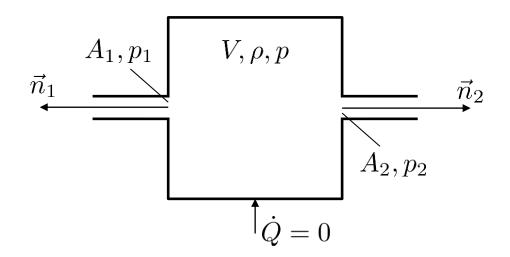
For ideal gases:

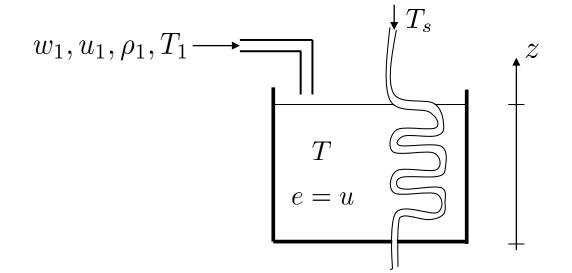
$$c_v = c_p + R$$

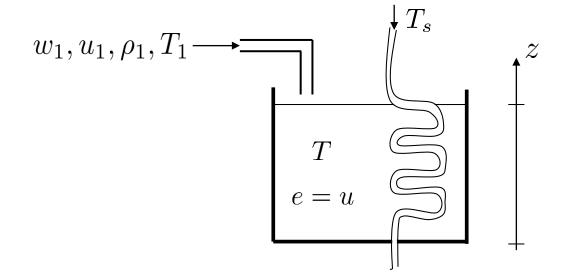
For incompressible fluids (often assumed for liquids):

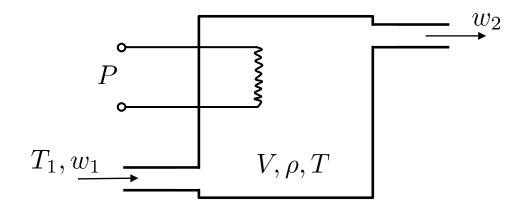
$$c_v = c_p$$











#### Homework

- Read 4.1 4.3
- Check Slide 26-30 (differential balance)

#### Differential mass balance

Recall the integral mass balance:

$$\frac{\mathrm{d}}{\mathrm{d}t} \iiint\limits_{V_c} \rho \mathrm{d}V = - \iint\limits_{\partial V_c} \rho \vec{v} \cdot \vec{n} \mathrm{d}A$$
 
$$\boxed{ \text{Mathematics (obvious?)} } \qquad \boxed{ \text{Divergence theorem} }$$
 
$$\frac{\mathrm{d}}{\mathrm{d}t} \iiint\limits_{V_c} \rho \mathrm{d}V = \iiint\limits_{V_c} \frac{\partial \rho}{\partial t} \mathrm{d}V \qquad \qquad \iint\limits_{\partial V_c} \rho \vec{v} \cdot \vec{n} \mathrm{d}A = \iiint\limits_{V_c} \vec{\nabla} \cdot (\rho \vec{v}) \mathrm{d}V$$

That is:

$$\iiint\limits_{V} \frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \vec{v}) dV = 0$$

This must hold for arbitrary control volumes, which implies

$$\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \vec{v}) = 0$$

Differential mass balance, also called *continuity equation* or *advection equation* 

#### Alternative formulations

The differential mass balance

$$\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \vec{v}) = 0$$

From definition of nabla operator, this is the same as

$$\frac{\partial \rho}{\partial t} + \sum_{i=1}^{3} \frac{\partial}{\partial x_i} (\rho v_i) = 0, \quad \mathbf{v} = (v_1, v_2, v_3)^{\mathsf{T}}$$

If we introduce the material derivative,

$$\frac{\mathrm{D}\phi}{\mathrm{D}t} := \frac{\partial\phi}{\partial t} + \mathbf{v}^{\mathsf{T}}\nabla\phi = \frac{\partial\phi}{\partial t} + \sum_{i=1}^{3} \frac{\partial\phi}{\partial x_{i}}v_{i}$$

The material derivative is the derivative following a particle (as opposed to the derivative at a fixed point in space)

and use product rule, we can write

$$\frac{\mathrm{D}\rho}{\mathrm{D}t} + \rho\nabla \cdot \vec{v} = 0$$

#### Differential momentum and energy balances

Differential momentum balance for inviscid fluid (Euler's equation)

$$\rho \frac{\mathrm{D}\vec{v}}{\mathrm{D}t} = -\vec{\nabla}p + \rho\vec{f}$$
, where  $\rho\vec{f}$  is the mass force (e.g. gravity)

• For viscous (Newtonian) fluids, the differential momentum balance is the famous *Navier-Stokes* equation:

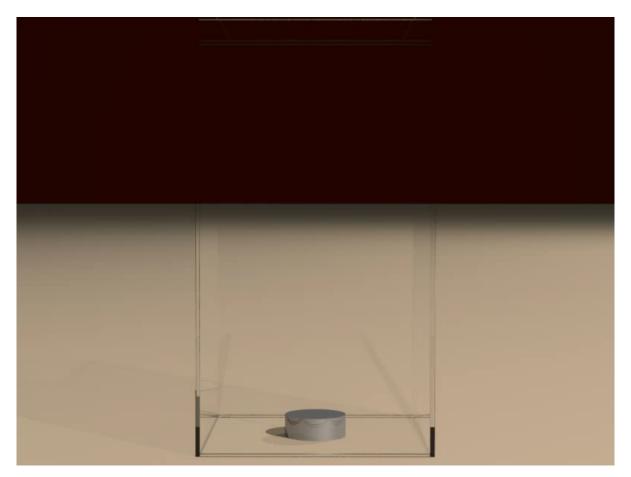
$$\rho \frac{\mathbf{D}\vec{v}}{\mathbf{D}t} = -\vec{\nabla}p + \mu \vec{\nabla}^2 \vec{v} + \rho \vec{f}$$

Differential energy balance (for example)

$$\rho \frac{\mathbf{D}}{\mathbf{D}t} \left( \frac{1}{2} \vec{v}^2 + u \right) = -\vec{\nabla} \cdot (p\vec{v}) - \vec{\nabla} \cdot \vec{j}_Q + \rho \vec{v} \cdot \vec{f}$$

### Computational fluid dynamics

 CFD = solving momentum + mass balances (that is, Navier-Stokes + continuity equation) for different setups



http://physbam.stanford.edu/~fedkiw/

# Example of differential energy balances: The heat equation of a solid

The energy balance:

$$\rho \frac{\mathbf{D}}{\mathbf{D}t} \left( \frac{1}{2} \vec{v}^2 + u \right) = -\vec{\nabla} \cdot (p\vec{v}) - \vec{\nabla} \cdot \vec{j}_Q + \rho \vec{v} \cdot \vec{f}$$

Solid: Disregard kinetic and potential energy, no velocity:

$$\rho \frac{\partial u}{\partial t} = -\vec{\nabla} \cdot \vec{j}_Q$$

We need a «closure relation». Here in the form of Fourier's law:

$$\vec{j}_Q = -\alpha \vec{\nabla}(\rho c_p T)$$

Combined with

$$\frac{\partial u}{\partial t} = c_p \frac{\partial T}{\partial t}$$

we get

$$\frac{\partial T}{\partial t} - \alpha \vec{\nabla} \cdot \vec{\nabla} T = 0$$

In one dimension:

$$\frac{\partial T(x,t)}{\partial t} - \alpha \frac{\partial^2 T(x,t)}{\partial x^2} = 0$$