Lecture 8: Stability, Padé approximations

- Stability of Runga-Kutta methods
 - A-stability
 - Aliasing
 - L-stability
 - Padé approximations
 - (Nonlinear stability: AN-, B- and algebraic stability)

Book: 14.6

Explicit Runge-Kutta (ERK) methods

• IVP: $\dot{y} = f(y, t), \quad y(0) = y_0$

• ERK:
$$k_1 = f(y_n, t_n)$$

$$k_2 = f(y_n + ha_{21}k_1, t_n + c_2h)$$

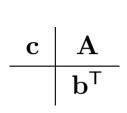
$$k_3 = f(y_n + h(a_{31}k_1 + a_{32}k_2), t_n + c_3h)$$

$$\vdots$$

$$k_{\sigma} = f(y_n + h(a_{\sigma,1}k_1 + a_{\sigma,2}k_2 + \ldots + a_{\sigma,\sigma-1}k_{\sigma-1}), t_n + c_{\sigma}h)$$

$$y_{n+1} = y_n + h(b_1k_1 + b_2k_2 + \ldots + b_{\sigma}k_{\sigma})$$

Butcher array:



Recap: Test system, stability function

One step method (typically: Runge-Kutta):

$$y_{n+1} = y_n + h\phi(y_n, t_n)$$

Apply it to scalar test system:

$$\dot{y} = \lambda y$$

• We get:

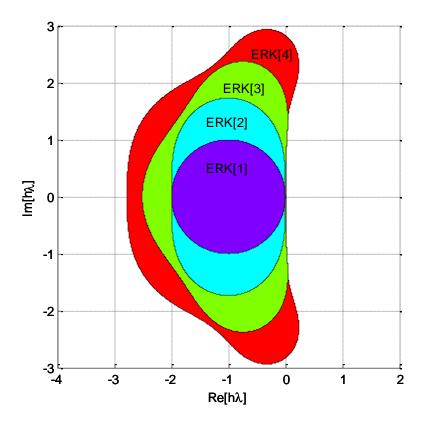
$$y_{n+1} = R(h\lambda)y_n$$

where $R(h\lambda)$ is stability function

The method is stable (for test system!) if

$$|R(h\lambda)| \le 1$$

Stability regions for ERK methods



Implicit Runge-Kutta (IRK) methods

• IVP: $\dot{y} = f(y, t), \quad y(0) = y_0$

• IRK:
$$k_{1} = f(y_{n} + h(a_{1,1}k_{1} + a_{1,2}k_{2} + \dots + a_{1,\sigma}k_{\sigma}), t_{n} + c_{1}h)$$

$$k_{2} = f(y_{n} + h(a_{2,1}k_{1} + a_{2,2}k_{2} + \dots + a_{2,\sigma}k_{\sigma}), t_{n} + c_{2}h)$$

$$k_{3} = f(y_{n} + h(a_{3,1}k_{1} + a_{3,2}k_{2} + \dots + a_{3,\sigma}k_{\sigma}), t_{n} + c_{3}h)$$

$$\vdots$$

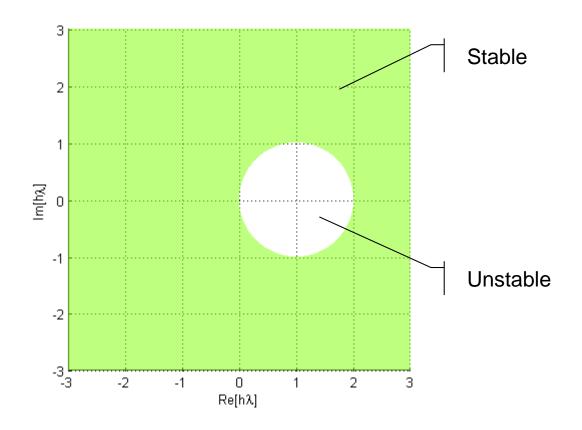
$$k_{\sigma} = f(y_{n} + h(a_{\sigma,1}k_{1} + a_{\sigma,2}k_{2} + \dots + a_{\sigma,\sigma}k_{\sigma}), t_{n} + c_{\sigma}h)$$

$$y_{n+1} = y_{n} + h(b_{1}k_{1} + b_{2}k_{2} + \dots + b_{\sigma}k_{\sigma})$$

Butcher array:

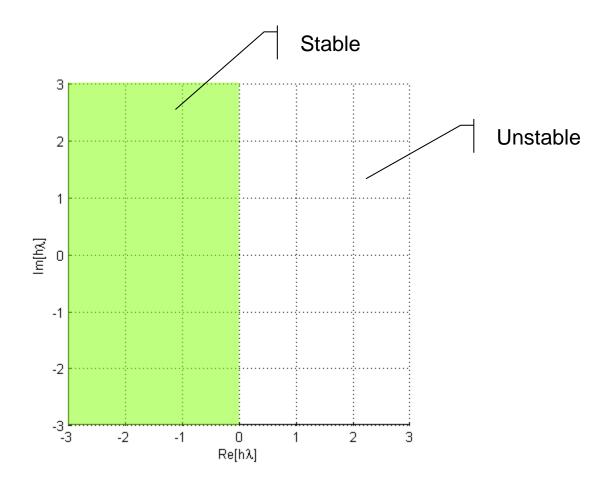
Stability regions for implicit methods

Implicit Euler



Stability regions for implicit methods

Trapezoidal rule and implicit midpoint rule:

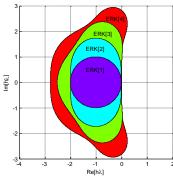


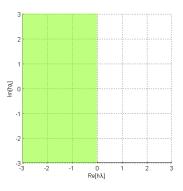
Why use IRK methods?

 IRK methods are much more complex (since we have to solve a set of nonlinear equations for each step) than ERK methods, so why use them?

– Accuracy? Stability?

- Not because of accuracy
 - Even if an IRK method may have higher accuracy for a given number of stages, it is easy and cheap to achieve same accuracy for ERK by increasing the number of stages
- It's because of the much larger stability region!
- When is this important?
 - Stiff systems!

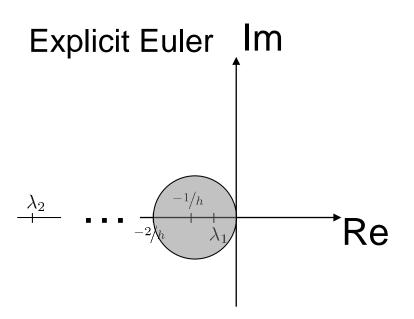




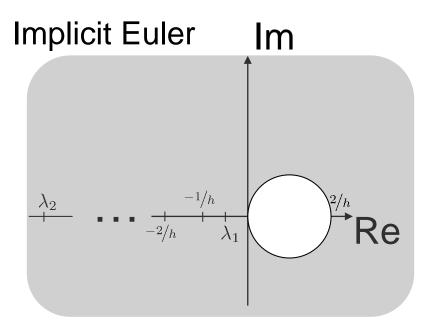
Stiff system

$$\dot{y}_1 = \lambda_1 y_1$$
$$\dot{y}_2 = \lambda_2 y_2$$

$$\lambda_2 << \lambda_1 < 0$$



must choose a small *h* for stability

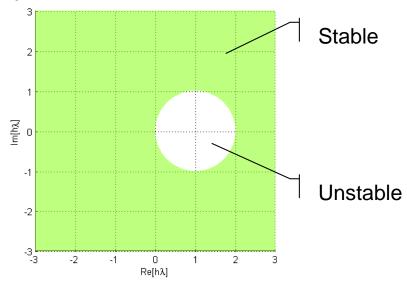


can choose all h for stability

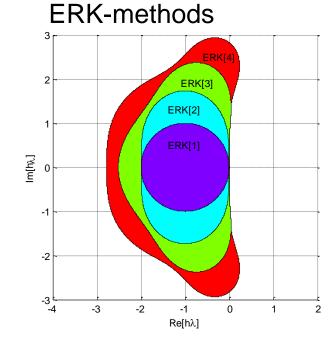
Example 221

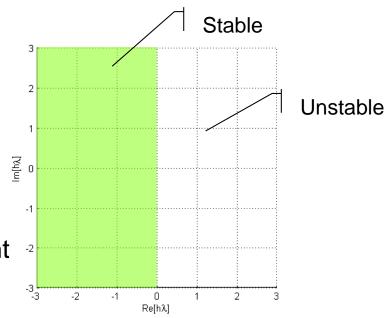
ERK vs IRK stability regions

Implicit Euler



Trapezoidal/ Implicit Midpoint





Aliasing I

Aliasing II

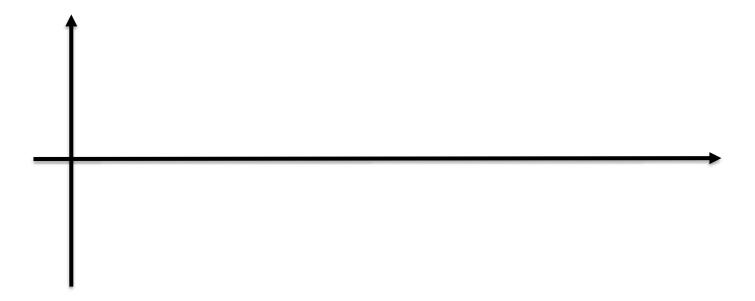
Assume:

Test system I
$$\dot{y} = \lambda y \; ; \; \lambda = \sigma + j\omega \qquad \qquad \dot{y} = \mu y$$

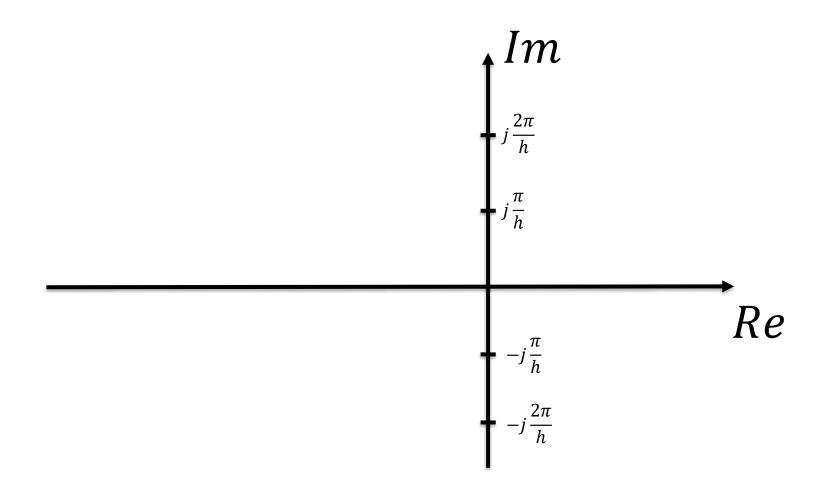
$$y_L(t_n; t_{n+1}) = e^{h\lambda} y_n \qquad \qquad y_L(t_n; t_{n+1}) = e^{h\mu} y_n$$

When are these two systems the same?

Visualisation I

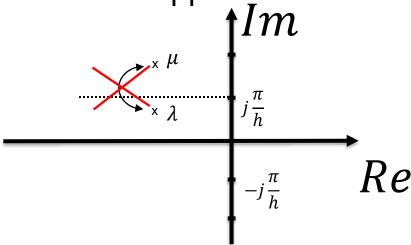


Visualisation II



L-stability I

• Assume μ eigenvalues and we want to suppress: $\dagger Im$

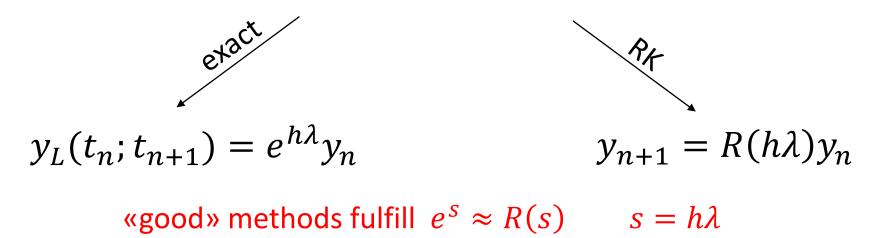


L-stability II

Example – L-stability

Padé-approximation I

Test system: $\dot{y} = \lambda y$



Padé-approximation II

Def: Padé approximation $P_m^k(s)$ of e^s is the rational function:

$$P_m^k(s) = \frac{1 + \beta_1 s + \dots + \beta_k s^k}{1 + \gamma_1 s + \dots + \gamma_m s^m},$$

which approximates e^s the best given k and m

Padé approximations to es

m	0	1	2	3
0	1	$\frac{1+s}{1}$	$\frac{1+s+\frac{1}{2}s^2}{1}$	$\frac{1+s+\frac{1}{2}s^2+\frac{1}{6}s^3}{1}$
1	$\frac{1}{1-s}$	$\frac{1+\frac{1}{2}s}{1-\frac{1}{2}s}$	$\frac{1 + \frac{2}{3}s + \frac{1}{6}s^2}{1 - \frac{1}{3}s}$	$\frac{1 + \frac{3}{4}s + \frac{1}{4}s^2 + \frac{1}{24}s^3}{1 - \frac{1}{4}s}$
2	$\frac{1}{1-s+\frac{1}{2}s^2}$	$\frac{1 + \frac{1}{3}s}{1 - \frac{2}{3}s + \frac{1}{6}s^2}$	$\frac{1 + \frac{1}{2}s + \frac{1}{12}s^2}{1 - \frac{1}{2}s + \frac{1}{12}s^2}$	$\frac{1 + \frac{3}{5}s + \frac{3}{20}s^2 + \frac{1}{60}s^3}{1 - \frac{2}{5}s + \frac{1}{20}s^2}$
3	$\frac{1}{1-s+\frac{1}{2}s^2-\frac{1}{6}s^3}$	$\frac{1 + \frac{1}{4}s}{1 - \frac{3}{4}s + \frac{1}{4}s^2 - \frac{1}{24}s^3}$	$\frac{1 + \frac{2}{5}s + \frac{1}{20}s^2}{1 - \frac{3}{5}s + \frac{3}{20}s^2 - \frac{1}{60}s^3}$	$\frac{1 + \frac{1}{2}s + \frac{1}{10}s^2 + \frac{1}{120}s^3}{1 - \frac{1}{2}s + \frac{1}{10}s^2 - \frac{1}{120}s^3}$

- m = 0: Explicit Runge-Kutta methods with $p = \sigma$
- m = k: Gauss, Lobatto IIIA/IIIB (incl. implicit mid-point, trapezoidal)
- m = k+1: Radau-methods (incl. implicit Euler)
- m = k+2: Lobatto IIIC

Padé approximations to es

m	0	1	2	3
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1	$\frac{1}{1-s}$	$\frac{1+\frac{1}{2}s}{1-\frac{1}{2}s}$	$\frac{1 + \frac{2}{3}s + \frac{1}{6}s^2}{1 - \frac{1}{3}s}$	$\frac{1 + \frac{3}{4}s + \frac{1}{4}s^2 + \frac{1}{24}s^3}{1 - \frac{1}{4}s}$
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3	$\frac{1}{1 - s + \frac{1}{2}s^2 - \frac{1}{6}s^3}$	$\frac{1 + \frac{1}{4}s}{1 - \frac{3}{4}s + \frac{1}{4}s^2 - \frac{1}{24}s^3}$	$\frac{1 + \frac{2}{5}s + \frac{1}{20}s^2}{1 - \frac{3}{5}s + \frac{3}{20}s^2 - \frac{1}{60}s^3}$	$\frac{1 + \frac{1}{2}s + \frac{1}{10}s^2 + \frac{1}{120}s^3}{1 - \frac{1}{2}s + \frac{1}{10}s^2 - \frac{1}{120}s^3}$
		L-stab	le L-stab	le A-sta

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Padé approximations as stability function

- 1. Assume $k \le m \le k+2$ In that case $\left|P_m^k(s)\right| \le 1$ if $Re[s] \le 0$
- 2. $|P_m^m(j\omega)| = 1$ if $\omega \to \infty$
- 3. Assume m > kIn that case $|P_m^k(s)| \to 0$ if $\omega \to \infty$

One step methods with stability function $R(s) = P_m^k(s)$ are:

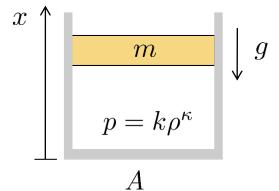
- A-stable if k = m
- L-stable if m = k + 1 or m = k + 2

Pneumatic spring example, again

Model from Newton's 2nd law:

$$\ddot{x} + g(1 - x^{-\kappa}) = 0$$

"mass-spring-damper with nonlinear spring"



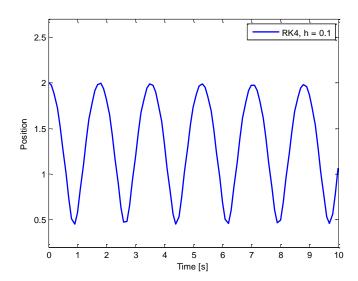
• On state-space form $\dot{y} = f(y, t)$

$$\begin{pmatrix} \dot{y}_1 \\ \dot{y}_2 \end{pmatrix} = \begin{pmatrix} y_2 \\ -g(1-y_1^{-\kappa}) \end{pmatrix}$$

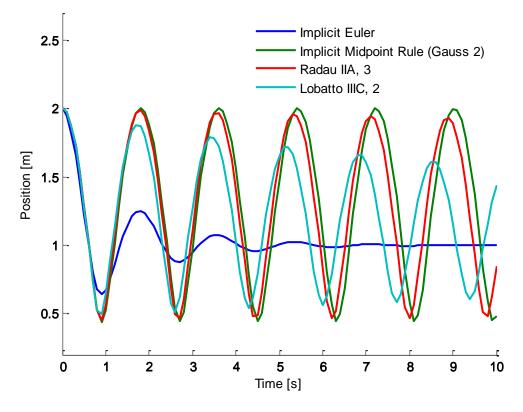
Linearization about equilibrium:

$$\frac{\partial f}{\partial y} = \begin{pmatrix} 0 & 1 \\ -g\kappa & 0 \end{pmatrix}, \qquad \lambda_{1,2} = \pm j\omega_0, \quad \omega_0 = \sqrt{g\kappa} \approx 3.7$$

Simulation



h = 0.5 (stability limit for RK4)

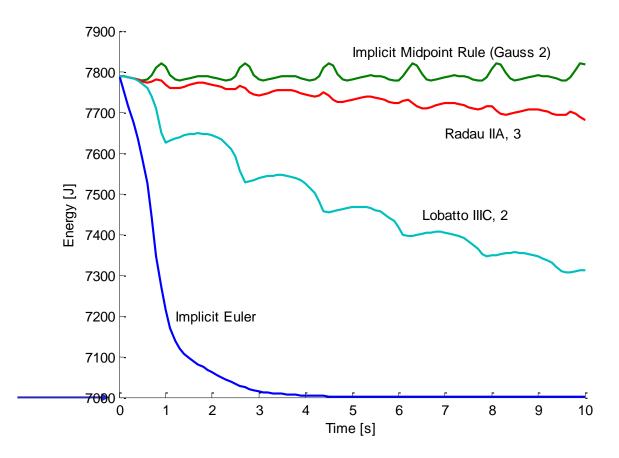


Padé approximations to es

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1	$\frac{1}{1-s}$	$\frac{1+\frac{1}{2}s}{1-\frac{1}{2}s}$	$\frac{1 + \frac{2}{3}s + \frac{1}{6}s^2}{1 - \frac{1}{3}s}$	$\frac{1 + \frac{3}{4}s + \frac{1}{4}s^2 + \frac{1}{24}s^3}{1 - \frac{1}{4}s}$
2	$\frac{1}{1-s+\frac{1}{2}s^2}$	$\frac{1 + \frac{1}{3}s}{1 - \frac{2}{3}s + \frac{1}{6}s^2}$	$\frac{1 + \frac{1}{2}s + \frac{1}{12}s^2}{1 - \frac{1}{2}s + \frac{1}{12}s^2}$	$\frac{1 + \frac{3}{5}s + \frac{3}{20}s^2 + \frac{1}{60}s^3}{1 - \frac{2}{5}s + \frac{1}{20}s^2}$
3	$\frac{1}{1 - s + \frac{1}{2}s^2 - \frac{1}{6}s^3}$	$\frac{1 + \frac{1}{4}s}{1 - \frac{3}{4}s + \frac{1}{4}s^2 - \frac{1}{24}s^3}$	$\frac{1 + \frac{2}{5}s + \frac{1}{20}s^2}{1 - \frac{3}{5}s + \frac{3}{20}s^2 - \frac{1}{60}s^3}$	$\frac{1 + \frac{1}{2}s + \frac{1}{10}s^2 + \frac{1}{120}s^3}{1 - \frac{1}{2}s + \frac{1}{10}s^2 - \frac{1}{120}s^3}$
		L-stab	le L-stab	le A-s

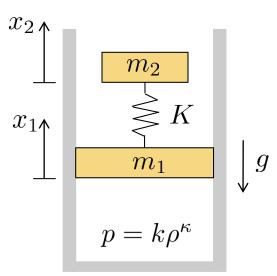
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Energy



Pneumatic spring with resonant load

Equations of motion (Newton's law):



Linearization around equilibrium:

$$J = \begin{pmatrix} 0 & 1 & 0 & 0 \\ -g\frac{m_1+m_2}{m_1}\kappa(x_1^*)^{-(\kappa-1)} - \frac{\omega_2^2}{2} & 0 & \frac{\omega_2^2}{2} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{\omega_2^2}{2} & 0 & -\frac{\omega_2^2}{2} & 0 \end{pmatrix}$$

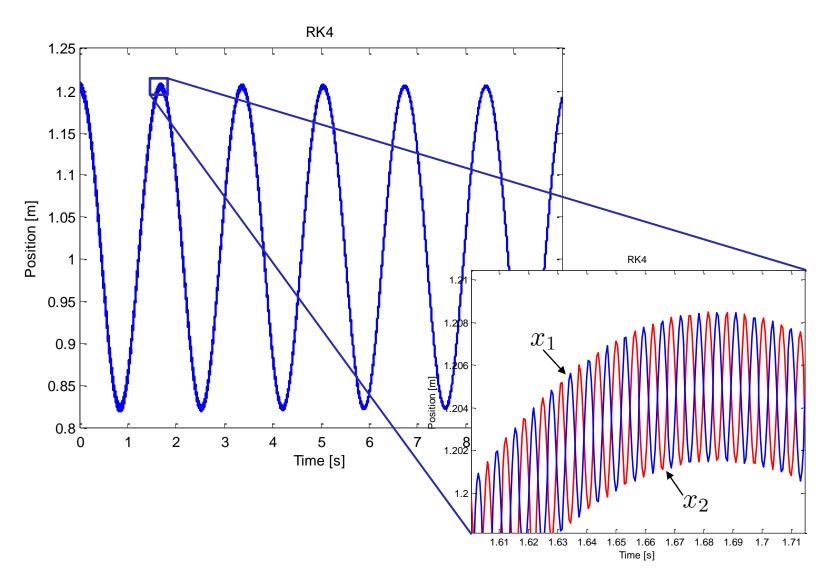
Eigenvalues:

$$\lambda_{1,2} = \pm j\omega_1, \quad \omega_1 = 3.7 \text{ rad/s}$$

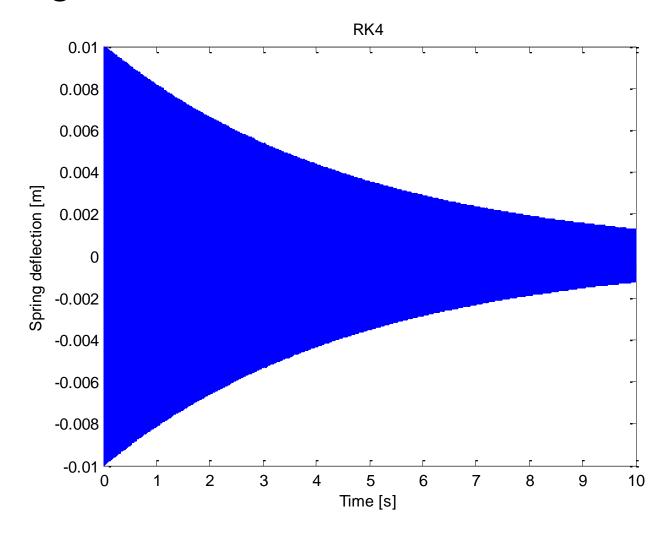
 $\lambda_{3,4} = \pm j\omega_2, \quad \omega_2 = 1000 \text{ rad/s}$

Position of the two masses

RK4 with time step h = 0.0005

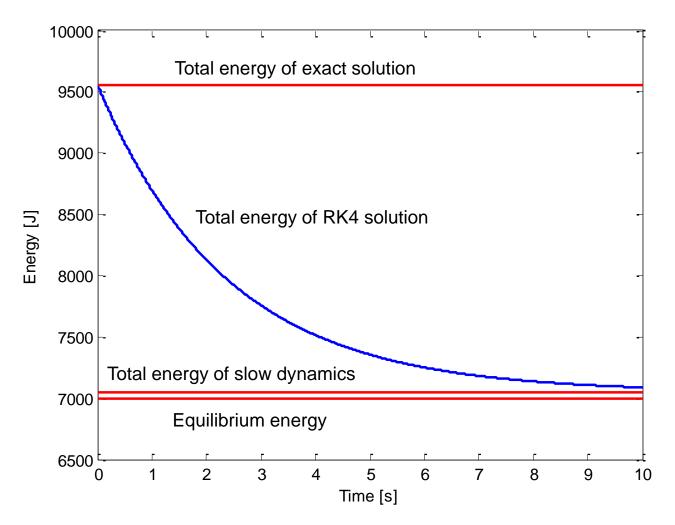


Spring deflection, RK4 with h = 0.0005



Oscillation is lightly damped by integration method

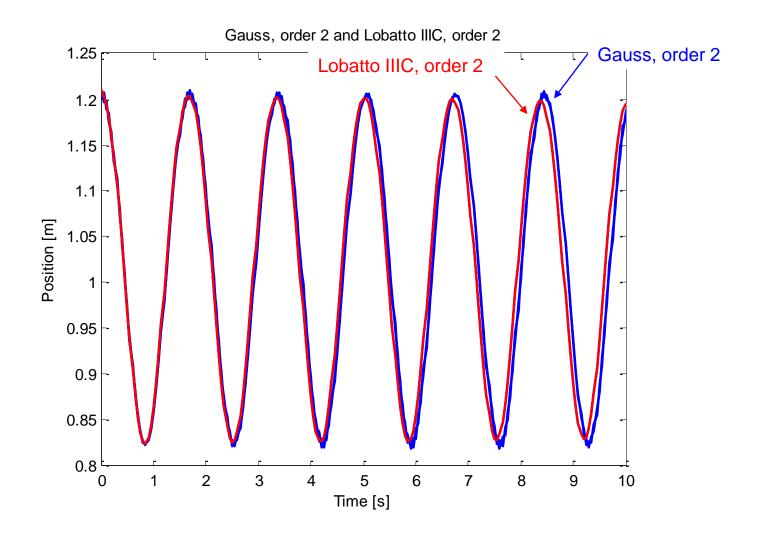
Energy of RK4 solution, h = 0.0005



Energy related to fast dynamics slowly damped out

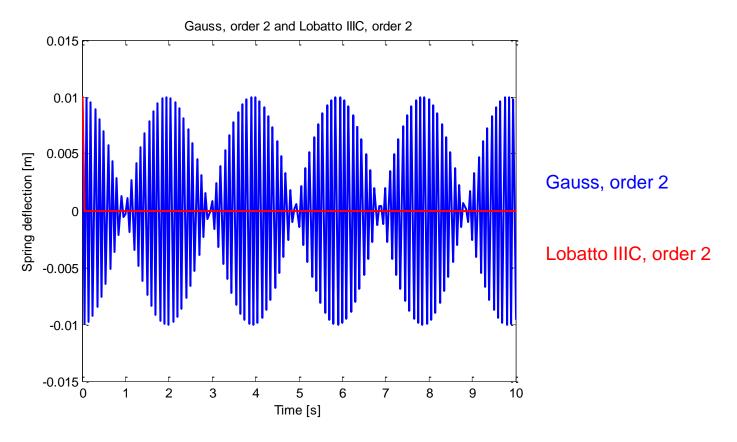
Position of the two masses

Gauss, order 2 and Lobatto IIIC, order 2, h = 0.05



Spring deflection

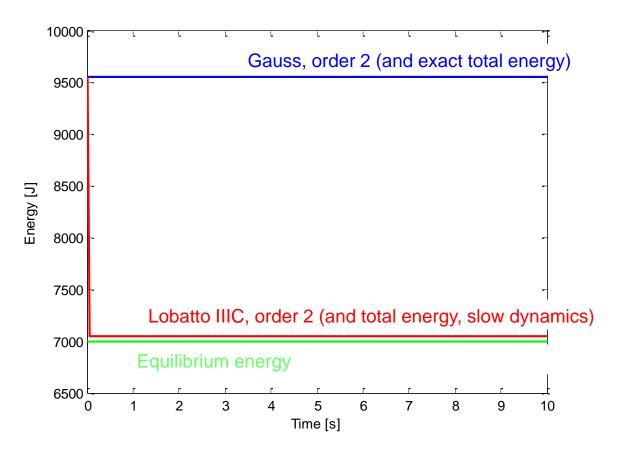
Gauss, order 2 and Lobatto IIIC, order 2, h = 0.05



- Gauss method gives no damping, but shifts fast dynamics and energy to frequencies below Nyquist frequency, $\omega_N = \frac{\pi}{h} = \frac{\pi}{0.05} = 62.8$
- Lobatto IIIC dampens out fast dynamics in one step

Total energies

Gauss, order 2 and Lobatto IIIC, order 2, h = 0.05



- Gauss does not dampen energies at all (same as exact total energy)
- Lobatto IIIC dampens out energy associated with fast dynamics in very few steps, to the energy of slow dynamics

Modelica

- Replacable / redeclare
- Choices
- Check out:
 - http://book.xogeny.com/components/architectures/replaceable/

Homework

- Check out the Modelica Circuit example (uploaded on Blackboard).
 - Look at the structure replaceable / redeclare
 - Read:
 http://book.xogeny.com/components/architectures/replaceable/
- Read 14.7.

Kahoot

 https://play.kahoot.it/#/k/694ab821-e4e0-421a-a5d6-0d297fd2cf1c

Self-study section

Example: "Lambert's problem"

IVP:

$$\dot{u} = \frac{1}{100} - (\frac{1}{100} + u + v)(1 + (u + 1000)(u + 1)), \quad u(0) = 0$$

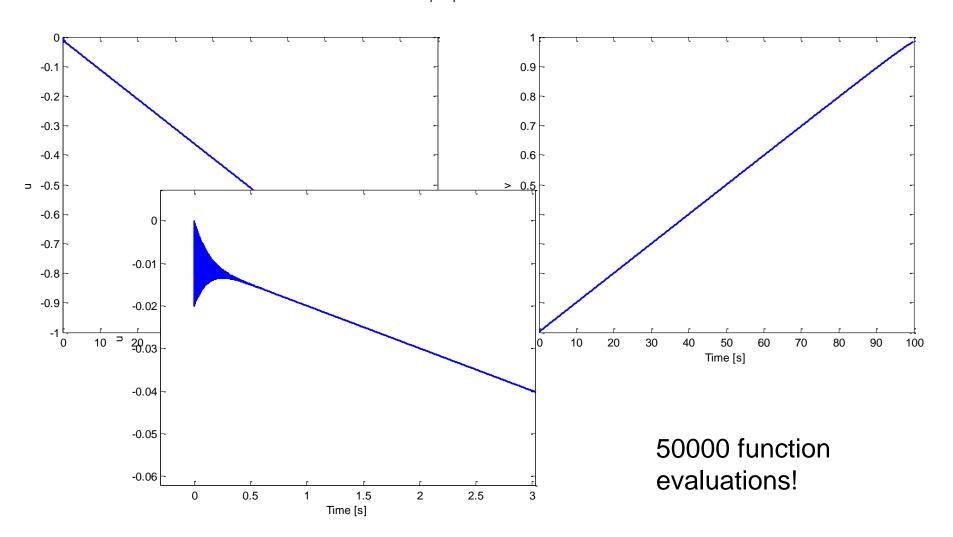
$$\dot{v} = \frac{1}{100} - (\frac{1}{100} + u + v)(1 + v^2), \quad v(0) = 0$$

- Task: Simulate from t = 0 s til t = 100 s
- Eigenvalues:

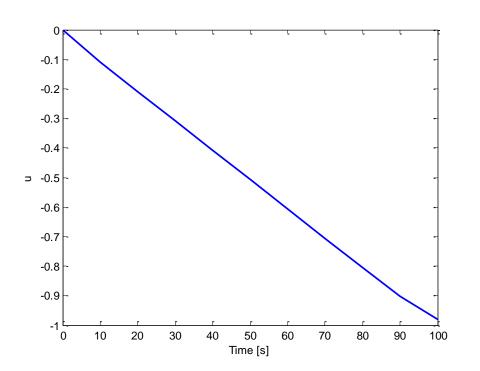
$$(u, v) = (0, 0) \Rightarrow \lambda_1 \approx -1000, \lambda_2 \approx -0.01$$
$$(u, v) = (-.5, .5) \Rightarrow \lambda_1 \approx -500, \lambda_2 \approx -0.03$$
$$(u, v) = (-1, 1) \Rightarrow \lambda_1 \approx -11, \lambda_2 \approx -1$$

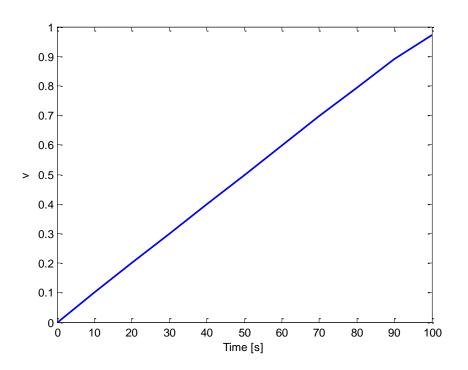
Using Euler (explicit), h = 0.002

 $h|\lambda| \le 2$



Attempt 3: Euler implicit, h = 10





149 function evaluations! (dependent on solution algorithm)

Comparisons

