

Exercise 7 solutions - TFY4345 Classical Mechanics

2020

1 Inertia tensor

The inertia tensor of a solid object V with the mass density $\rho(\vec{r})$ is defined as

$$I_{ij} = \int_V \rho(\vec{r}) (\delta_{ij} r^2 - x_i x_j) dV.$$

We assume the slab is so thin that the z -direction can be neglected so the integral then becomes.

$$I_{ij} = \frac{M}{ab} \int_0^a dx \int_0^b dy (r^2 - x_i x_j).$$

We see that $I_{ij} = I_{ji}$, so inserting $x_1 = x$, $x_2 = y$, $x_3 = z$, $r = \sqrt{x^2 + y^2 + z^2}$, $z = 0$, the integral needed are

$$\begin{cases} I_{11} = \frac{M}{ab} \int_0^a dx \int_0^b dy (y^2 + z^2) = \frac{1}{3} M b^2 \\ I_{12} = \frac{M}{ab} \int_0^a dx \int_0^b dy (-xy) = -\frac{1}{4} M ab \\ I_{13} = \frac{M}{ab} \int_0^a dx \int_0^b dy (-xz) = 0 \\ I_{22} = \frac{M}{ab} \int_0^a dx \int_0^b dy (x^2 + z^2) = \frac{1}{3} M a^2 \\ I_{23} = \frac{M}{ab} \int_0^a dx \int_0^b dy (-yz) = 0 \\ I_{33} = \frac{M}{ab} \int_0^a dx \int_0^b dy (x^2 + y^2) = \frac{1}{3} M (a^2 + b^2) \end{cases}$$

This gives the inertia tensor

$$I = \begin{pmatrix} I_{11} & I_{12} & I_{13} \\ I_{21} & I_{22} & I_{23} \\ I_{31} & I_{32} & I_{33} \end{pmatrix} = \begin{pmatrix} \frac{1}{3} M b^2 & -\frac{1}{4} M ab & 0 \\ -\frac{1}{4} M ab & \frac{1}{3} M a^2 & 0 \\ 0 & 0 & \frac{1}{3} M (a^2 + b^2) \end{pmatrix}$$

b) Let $a = b$, and define $\beta = 1/3 M a^2$. Then,

$$I = \begin{pmatrix} \frac{1}{3} M b^2 & -\frac{1}{4} M ab & 0 \\ -\frac{1}{4} M ab & \frac{1}{3} M a^2 & 0 \\ 0 & 0 & \frac{1}{3} M (a^2 + b^2) \end{pmatrix} = \beta \begin{pmatrix} 1 & -\frac{3}{4} & 0 \\ -\frac{3}{4} & 1 & 0 \\ 0 & 0 & 2 \end{pmatrix}$$

The principal axes are the coordinate axis in which the inertia tensor is diagonal, and the corresponding values for the inertia tensor are the principal moments of inertia. Remembering our linear algebra we thus need to find the eigenvalues of the inertia tensor. The characteristic polynomial is

$$|I - \lambda 1| = \begin{vmatrix} \beta - \lambda & -\frac{3}{4}\beta & 0 \\ -\frac{3}{4}\beta & \beta - \lambda & 0 \\ 0 & 0 & 2\beta - \lambda \end{vmatrix} = (2\beta - \lambda) \left((\beta - \lambda)^2 - \frac{9}{16}\beta^2 \right) = 0$$

This has the solution $\lambda = 2\beta$, or

$$\lambda^2 - 2\beta\lambda + \left(\beta^2 - \frac{9}{16}\beta^2 \right) = 0 \implies \lambda = \frac{1}{2} \left(2\beta \pm \sqrt{(2\beta)^2 - 4 \left(\beta^2 - \frac{9}{16}\beta^2 \right)} \right) = \beta \left(1 \pm \frac{3}{4} \right).$$

This leaves us with the diagonalized inertia tensor, with the principal moments of inertia

$$I' = \begin{pmatrix} I'_{11} & 0 & 0 \\ 0 & I'_{22} & 0 \\ 0 & 0 & I'_{33} \end{pmatrix} = \beta \begin{pmatrix} 2 & 0 & 0 \\ 0 & \frac{1}{4} & 0 \\ 0 & 0 & \frac{7}{4} \end{pmatrix} = Ma^2 \begin{pmatrix} \frac{1}{12} & 0 & 0 \\ 0 & \frac{7}{12} & 0 \\ 0 & 0 & \frac{2}{3} \end{pmatrix}$$

This inertia tensor corresponds to rotation around a different set axes, the principal axes $\boldsymbol{\omega}^{(1)}, \boldsymbol{\omega}^{(2)}, \boldsymbol{\omega}^{(3)}$, than the original, which corresponds to rotation around the xyz -axes. The defining feature of the principal axes is that

$$I\boldsymbol{\omega}^{(i)} = I'_i\boldsymbol{\omega}^{(i)},$$

so we need to find the normalized eigenvalues of I . The equations for these are

$$I\boldsymbol{\omega}^{(i)} = \beta \begin{pmatrix} 1 & -\frac{3}{4} & 0 \\ -\frac{3}{4} & 1 & 0 \\ 0 & 0 & 2 \end{pmatrix} \begin{pmatrix} \omega_1^{(i)} \\ \omega_2^{(i)} \\ \omega_3^{(i)} \end{pmatrix} = I'_{ii} \begin{pmatrix} \omega_1^{(i)} \\ \omega_2^{(i)} \\ \omega_3^{(i)} \end{pmatrix} \implies \begin{cases} \beta(\omega_1^{(i)} - \frac{3}{4}\omega_2^{(i)}) = I'_{ii}\omega_1^{(i)} \\ \beta(-\frac{3}{4}\omega_1^{(i)} + \omega_2^{(i)}) = I'_{ii}\omega_2^{(i)} \\ 2\beta\omega_3^{(i)} = I'_{ii}\omega_3^{(i)} \end{cases}$$

We can immediately see that $i = 3$ gives

$$\boldsymbol{\omega}^{(3)} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} \implies I\boldsymbol{\omega}^{(3)} = I'_{33}\boldsymbol{\omega}^{(3)} = \frac{2}{3}Ma^2\boldsymbol{\omega}^{(3)}$$

$i = 1$, $I'_{11} = \frac{1}{4}\beta$ gives

$$\begin{cases} \beta(\omega_1^{(i)} - \frac{3}{4}\omega_2^{(i)}) = \frac{1}{4}\beta\omega_1^{(i)} \\ \beta(-\frac{3}{4}\omega_1^{(i)} + \omega_2^{(i)}) = \frac{1}{4}\beta\omega_2^{(i)} \\ 2\beta\omega_3^{(i)} = \frac{1}{4}\beta\omega_3^{(i)} \end{cases} \implies \boldsymbol{\omega}^{(1)} = \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ 1 \\ 0 \end{pmatrix}$$

while $i = 2$, $I'_{22} = \frac{7}{4}\beta$ gives

$$\begin{cases} \beta(\omega_1^{(i)} - \frac{3}{4}\omega_2^{(i)}) = \frac{7}{4}\beta\omega_1^{(i)} \\ \beta(-\frac{3}{4}\omega_1^{(i)} + \omega_2^{(i)}) = \frac{7}{4}\beta\omega_2^{(i)} \\ 2\beta\omega_3^{(i)} = \frac{1}{4}\beta\omega_3^{(i)} \end{cases} \implies \boldsymbol{\omega}^{(2)} = \frac{1}{\sqrt{2}} \begin{pmatrix} -1 \\ 1 \\ 0 \end{pmatrix}$$

2 Rotated tilted slab

a)

We are given the moment of inertia around the principal axes

$$I = M \begin{pmatrix} \frac{1}{12}a^2 & 0 & 0 \\ 0 & \frac{1}{12}b^2 & 0 \\ 0 & 0 & \frac{1}{12}(a^2 + b^2) \end{pmatrix}$$

and the angular momentum is given by

$$\mathbf{L} = I\boldsymbol{\omega} = \sum_i I_i \omega_i \mathbf{e}_i.$$

By looking at the illustration, we can express

$$\sin(\theta) = \frac{b}{\sqrt{a^2 + b^2}}, \quad \cos(\theta) = \frac{a}{\sqrt{a^2 + b^2}},$$

The the angular velocity vector in the principal axis system is then

$$\boldsymbol{\omega} = \sum_i \omega_i \mathbf{e}_i = \omega(-\sin(\theta)\mathbf{e}_1 + \cos(\theta)\mathbf{e}_2) = \frac{1}{12} \frac{\omega}{\sqrt{a^2 + b^2}} (-b\mathbf{e}_1 + a\mathbf{e}_2)$$

The angular momentum vector is therefore

$$\mathbf{L} = \frac{1}{12} M\omega(-a^2 \sin(\theta)\mathbf{e}_1 + b^2 \cos(\theta)\mathbf{e}_2)$$

or

$$\mathbf{L} = \frac{1}{12} \frac{M\omega}{\sqrt{a^2 + b^2}} (-a^2 b \mathbf{e}_1 + b^2 a \mathbf{e}_2)$$

We see that in general, the angular momentum and velocity vector are not parallel.

b)

The angle between two vectors is given by the dot product,

$$\boldsymbol{\omega} \cdot \mathbf{L} = \omega L \cos(\alpha) \implies \alpha = \arccos\left(\frac{\boldsymbol{\omega} \cdot \mathbf{L}}{\omega L}\right).$$

These quantities are given by

$$\begin{aligned}\boldsymbol{\omega} \cdot \mathbf{L} &= \frac{1}{12} M \left(\frac{\omega}{\sqrt{a^2 + b^2}} \right)^2 (a^2 b^2 + a^2 b^2) = \frac{1}{12} \frac{2M}{a^2 + b^2} (ab\omega)^2 \\ L^2 = \mathbf{L} \cdot \mathbf{L} &= \left(\frac{M\omega}{\sqrt{a^2 + b^2}} \right)^2 ((a^2 b)^2 + (b^2 a)^2) = \left(\frac{1}{12} M\omega \right)^2 \left(a^2 b^2 \frac{a^2 + b^2}{a^2 + b^2} \right) = \left(\frac{1}{12} abM\omega \right)^2 \\ \Rightarrow \alpha &= \arccos \left(\frac{1}{12} \frac{2M}{a^2 + b^2} (ab\omega)^2 \middle/ \frac{1}{12} abM\omega^2 \right) = \arccos \left(\frac{2ab}{a^2 + b^2} \right).\end{aligned}$$

For example, with $b = 1, a = 2$, we get $\alpha = 36.9^\circ, \theta = 26.6^\circ$.

c)

The rotational kinetic energy is given by

$$T = \frac{1}{2} \boldsymbol{\omega} \cdot \mathbf{L} = \frac{1}{12} \frac{(ab)^2}{a^2 + b^2} M \omega^2.$$

3 Cone rolling on a plane

a)

The axis x_3 is always straight above the line OA , and has therefore the same angular velocity around the z -axis, $\dot{\phi}$. Observing the figure, we see that the center of mass is at a distance $\ell \cos(\alpha)$ from the z -axis, so the center of mass velocity is

$$V_{CM} = \ell \cos(\alpha) \dot{\phi}$$

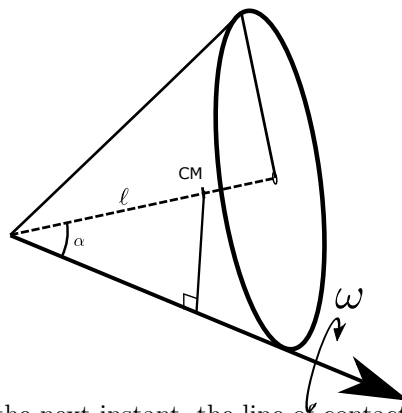
b)

The fact that the contact point of the cone and the plane is just a line, and that it rotates without slipping, means that at every instant all points in the cone rotates just as they would have if the cone were just rotating around a line. However, in the next instant, the line of contact has moved, so it has an instantaneous axis of rotation along the the line OA . We can find the angular velocity using how the center-of-mass moves with respect to OA . The center-of-mass is at a length $\ell \sin(\alpha)$ from the xy -plane, so the angular velocity of the cone is

$$\omega = \frac{V_{cm}}{\ell \sin(\alpha)} = \frac{\cos(\alpha)}{\sin(\alpha)} \dot{\phi}$$

c)

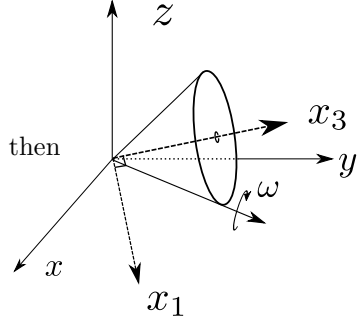
The figure shows two of the principal axis, the third one is into the page and not shown, perpendicular to x_1 and x_3 . z, x_1, x_3 and $\boldsymbol{\omega}$ are all in the same plane. The moment of inertia tensor in this can be expressed in this system as



$$\boldsymbol{\omega} = \sum_i \omega_i \mathbf{e}_i,$$

and due to our choice of x_2 , $\omega_2 = 0$. The two other components are then

$$\begin{aligned}\omega_1 &= \omega \sin(\alpha) = \cos(\alpha) \dot{\phi}, \\ \omega_3 &= \omega \cos(\alpha) = \frac{\cos^2(\alpha)}{\sin(\alpha)} \dot{\phi}\end{aligned}$$



d)

The kinetic energy of a rotating object is

$$\begin{aligned}\frac{1}{2} \boldsymbol{\omega}^T I \boldsymbol{\omega} &= \frac{3}{20} M \begin{pmatrix} \omega_1 & 0 & \omega_3 \end{pmatrix} \begin{pmatrix} R^2 + 4H^2 & 0 & 0 \\ 0 & R^2 + 4H^2 & 0 \\ 0 & 0 & 2R^2 \end{pmatrix} \begin{pmatrix} \omega_1 \\ 0 \\ \omega_3 \end{pmatrix} = \frac{3}{20} M \left(\omega_1^2 (R^2 + 4H^2) + 2\omega_3^2 R^2 \right) \\ &= \frac{3}{40} M \dot{\phi}^2 \left(\cos^2(\alpha) \left(\left[\frac{\sin(\alpha)}{\cos(\alpha)} \right]^2 H^2 + 4H^2 \right) + 2 \frac{\cos^4(\alpha)}{\sin^2(\alpha)} \left[\frac{\sin(\alpha)}{\cos(\alpha)} \right]^2 H^2 \right) \\ &= \frac{3}{40} M \dot{\phi}^2 H^2 \left(\sin^2(\alpha) + 4 \cos^2(\alpha) + 2 \cos^2(\alpha) \right) = \frac{3}{40} M \dot{\phi}^2 H^2 \left(1 + 5 \cos^2(\alpha) \right)\end{aligned}$$

where we use that $R \cos(\alpha) = H \sin(\alpha)$.