

## Homework 3

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- A clear step-by-step description of your method, including pseudocode/algorithms for: (i) force/energy evaluation, (ii) time stepping, (iii) enforcement of Dirichlet constraints, and (iv) the path-planning or control law mapping the tracking error of node j to { $x_c$ ,  $y_c$ ,  $\theta_c$ }.

### (i) Force / Energy Evaluation

Stretching (per edge k between nodes k and k+1)

- Current edge length  $L_k = \|x_{k+1} - x_k\|$ .
- Rest length  $l_k$  (uniform =  $\Delta L$ ).
- Edge stretching energy  $E_k^S = \frac{1}{2}EA l_k (1 - L_k/l_k)^2$ .
- From this, assemble the 4-vector gradient (forces on k and k+1) and 4×4 Hessian into global vectors/matrices.

Bending (per interior node k using nodes k-1, k, k+1)

- Compute a discrete curvature scalar  $\kappa_k$  from the two adjacent edge directions.
- Bending energy  $E_k^B = \frac{1}{2} \frac{EI}{l_k} (\kappa_k - \kappa_k^0)^2$  (here  $\kappa_k^0 = 0$ ).
- Assemble the 6-vector gradient and 6×6 Hessian into global structures.

$F_s = 0; J_s = 0$

for each edge k = 1..N-1:

$(g4, H4) = \text{StretchGradHess}(k)$

scatter  $F_s := g4; J_s := H4$

$F_b = 0; J_b = 0$

for each interior node k = 2..N-1:

$(g6, H6) = \text{BendGradHess}(k-1, k, k+1)$

```
scatter Fb := g6; Jb := H6
```

```
F_int = Fs + Fb
```

```
J_int = Js + Jb
```

### (ii) Time Stepping (Implicit Backward Euler + Newton)

Goal: solve for positions at the next step  $q_{n+1}$  and then update velocity.

Residual and Jacobian at iterate q

- Velocity  $v = (q - q_n)/\Delta t$ .
- Inertia:  $F_{in} = m/\Delta t (v - u_n), J_{in} = M/\Delta t^2$ .
- Internal:  $(F_{int}(q), J_{int}(q))$  from (i).
- Damping:  $F_v = C v, J_v = C/\Delta t$ .
- Residual  $r = F_{in} - F_{int} - F_v - W$ .
- Jacobian  $J = J_{in} - J_{int} - J_v$ .

Newton loop (with constraints applied to free DOFs)

```
q = q_n
```

repeat:

```
    compute r, J
```

```
    take free dofs: r_free = r[free], J_free = J[free, free]
```

```
    Δq_free = solve(J_free, r_free)
```

```
    q[free] = q[free] - Δq_free
```

```
until ||r_free|| < tol or max_iters
```

```
q_{n+1} = q
```

```
u_{n+1} = (q_{n+1} - q_n)/Δt
```

### (iii) Dirichlet Constraints (Clamped/Prescribed DOFs)

We fix:

- Left end node  $(x_1, y_1) = \text{constants}$ .

- Right end two nodes to impose end-effector pose:
  - Tip node  $(x_N, y_N) = (x_c, y_c)$ .
  - Previous node  $(x_{N-1}, y_{N-1}) = (x_c - \Delta L \cdot \cos \theta_c, y_c - \Delta L \cdot \sin \theta_c)$ .

How it's enforced

1. Before each Newton solve, overwrite those DOFs in  $q$  with the prescribed values.
2. Build  $\text{fixed} = \{x_1, y_1, x_N, y_N, x_{N-1}, y_{N-1}\}$  and  $\text{free} = \text{all} \setminus \text{fixed}$ .
3. In Newton, only solve for the free subset (i.e., use  $r_{\text{free}}$ ,  $J_{\text{free}}$ ) and write back to  $q[\text{free}]$ . The fixed DOFs never change during the solve.

`ImposeRightEnd(q, x_c, y_c, theta_c, DeltaL):`

$$\begin{aligned} q[x_N] &= x_c; q[y_N] = y_c \\ q[x_{N-1}] &= x_c - \Delta L \cdot \cos(\theta_c) \\ q[y_{N-1}] &= y_c - \Delta L \cdot \sin(\theta_c) \end{aligned}$$

`BuildBCSets():`

$$\begin{aligned} \text{fixed} &= \{x_1, y_1, x_N, y_N, x_{N-1}, y_{N-1}\} \\ \text{free} &= \text{all\_dofs} \setminus \text{fixed} \end{aligned}$$

(iv) Control Law (Tracking error of node  $j \rightarrow \{x_c, y_c, \theta_c\}$ )

We drive the right end so that a chosen node  $j$  (here, the middle node) tracks a desired trajectory  $(x^*(t), y^*(t))$  using a simple PID on position error. We also rate-limit the commanded motion at the end effector.

At each time step

1. Measure middle node:  $(x_j, y_j)$ .
2. Compute errors:
  - $e_x = x^* - x_j$ ,  $e_y = y^* - y_j$ .
  - Approx. derivatives:  $\dot{e}_x \approx (x_j - x_j^{prev})/\Delta t$ , similarly for  $y$ .
3. Update integrals:  $I_x += e_x \Delta t$ ,  $I_y += e_y \Delta t$ .
4. PID increments:

- $\Delta x_c = K_p e_x + K_i I_x - K_d \dot{e}_x$
  - $\Delta y_c = K_p e_y + K_i I_y - K_d \dot{e}_y$
5. Proposed command:  $(x_c, y_c) \leftarrow (x_c, y_c) + (\Delta x_c, \Delta y_c)$ , set  $\theta_c = 0$ .
6. Rate limit (optional but used): limit the change from current tip to at most `rmax_step`.

```
EndEffectorPID(x_star, y_star, xj, yj, xj_prev, yj_prev,
```

```
    x_c_prev, y_c_prev, I, Δt, Kp, Ki, Kd, rmax_step,
```

```
    x_tip_curr, y_tip_curr):
```

```
ex = x_star - xj
```

```
ey = y_star - yj
```

```
ex_dot = (xj - xj_prev)/Δt
```

```
ey_dot = (yj - yj_prev)/Δt
```

```
I.x += ex * Δt
```

```
I.y += ey * Δt
```

```
dx_c = Kp*ex + Ki*I.x - Kd*ex_dot
```

```
dy_c = Kp*ey + Ki*I.y - Kd*ey_dot
```

```
x_c = x_c_prev + dx_c
```

```
y_c = y_c_prev + dy_c
```

```
θ_c = 0.0
```

```
# rate limiter relative to current tip
```

```
dx = x_c - x_tip_curr
```

```
dy = y_c - y_tip_curr
```

```
move = sqrt(dx*dx + dy*dy)
```

```
if move > rmax_step:
```

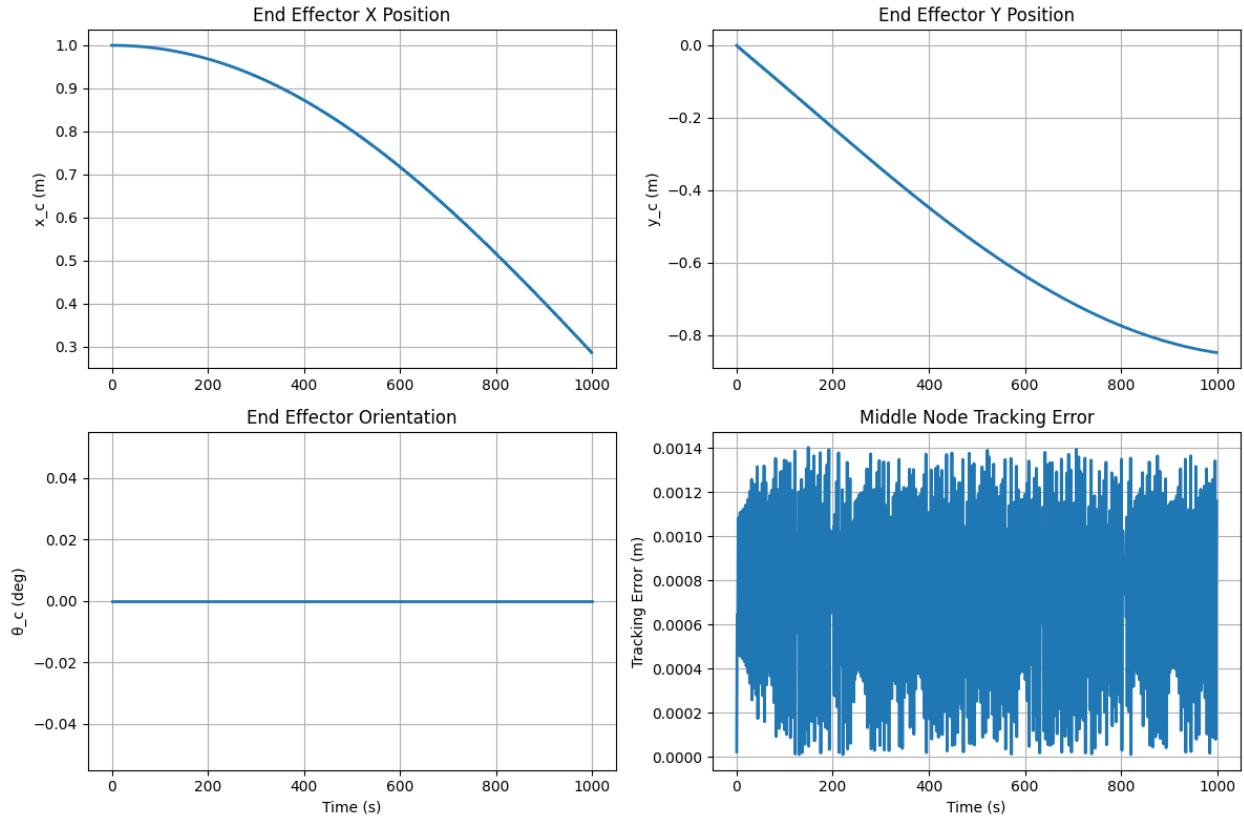
```
    s = rmax_step / move
```

```
    x_c = x_tip_curr + s*dx
```

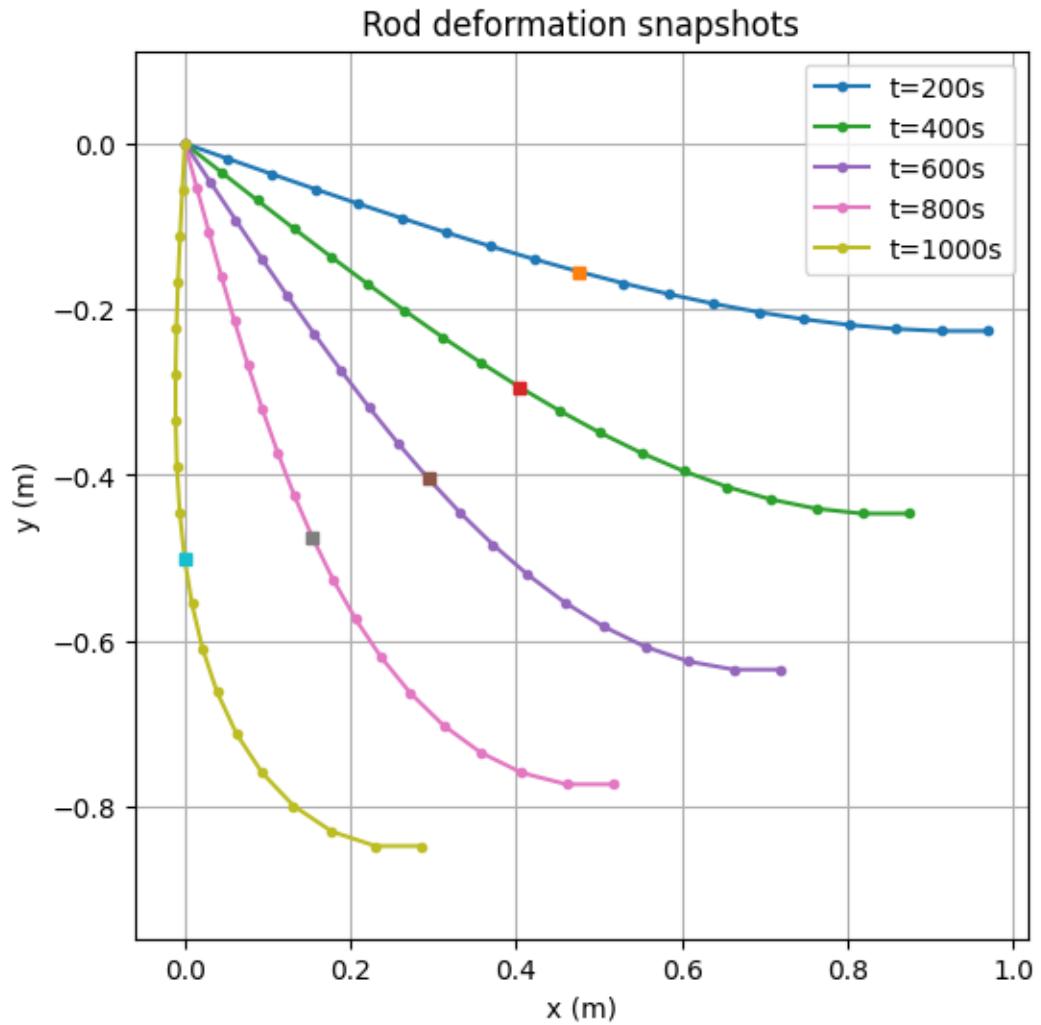
$$y_c = y_{tip\_curr} + s^* dy$$

return  $x_c, y_c, \theta_c, l$

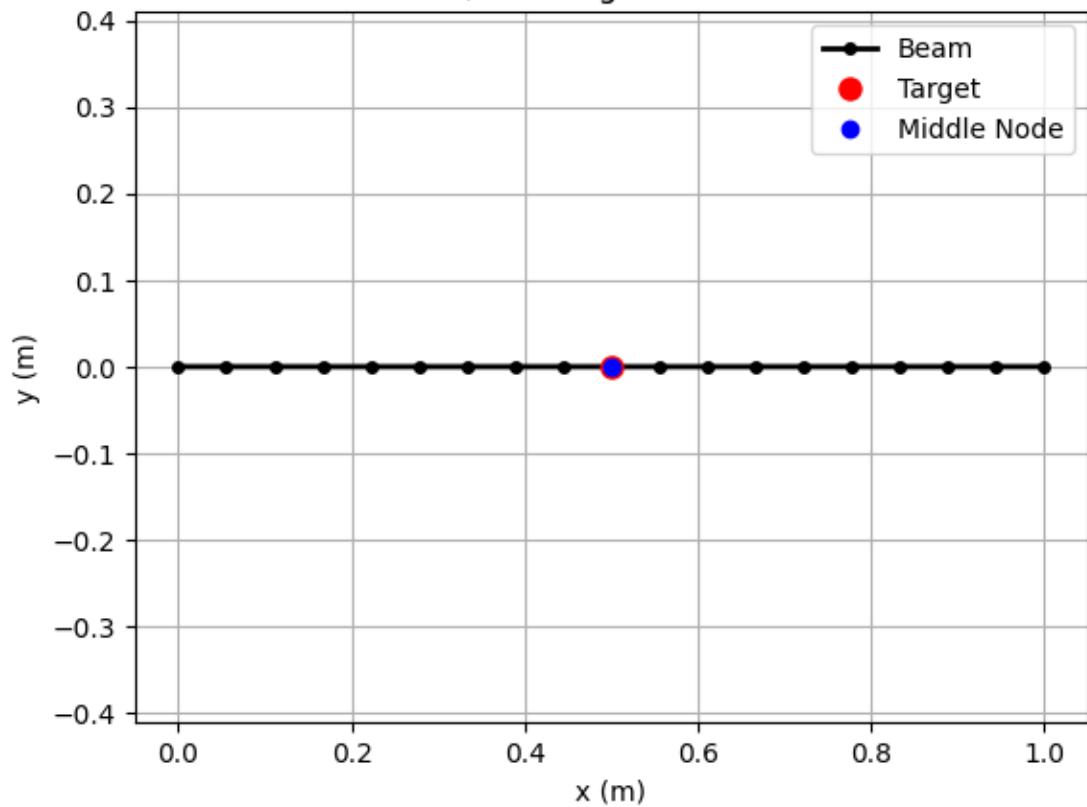
- Plots of the control inputs  $x_c(t)$ ,  $y_c(t)$ ,  $\theta_c(t)$  over time.



- At least five snapshots of the beam shape (node positions) during the motion

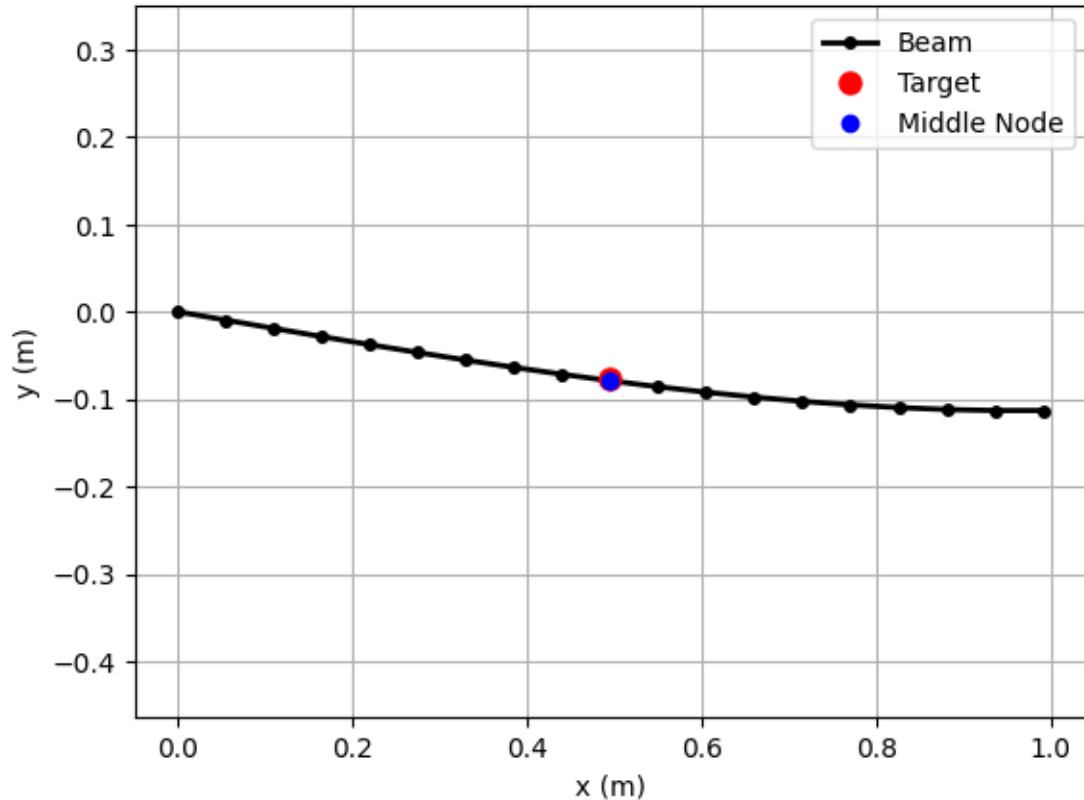


$t = 1.00\text{s}$ , Tracking Error = 0.0000 m



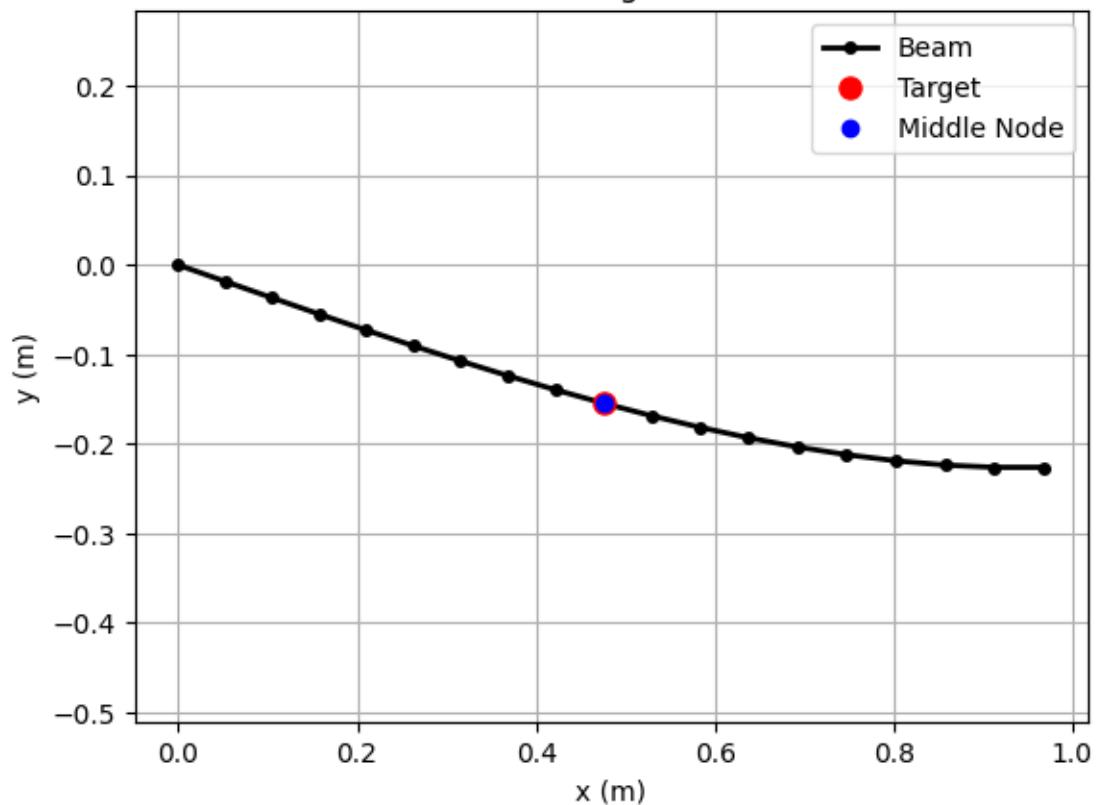
Step 1/1000,  $t = 1.00\text{s}$ , Err = 0.0000 m

$t = 100.00\text{s}$ , Tracking Error = 0.0013 m



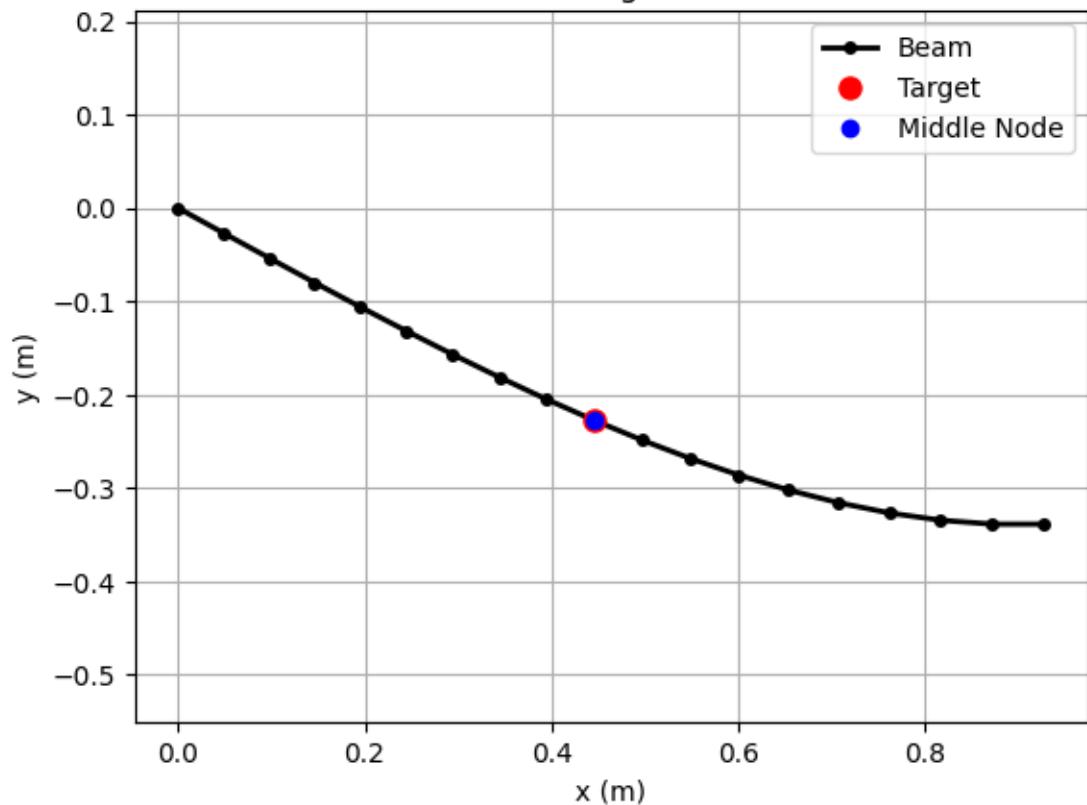
Step 100/1000,  $t = 100.00\text{s}$ , Err = 0.0013 m

$t = 200.00\text{s}$ , Tracking Error = 0.0008 m



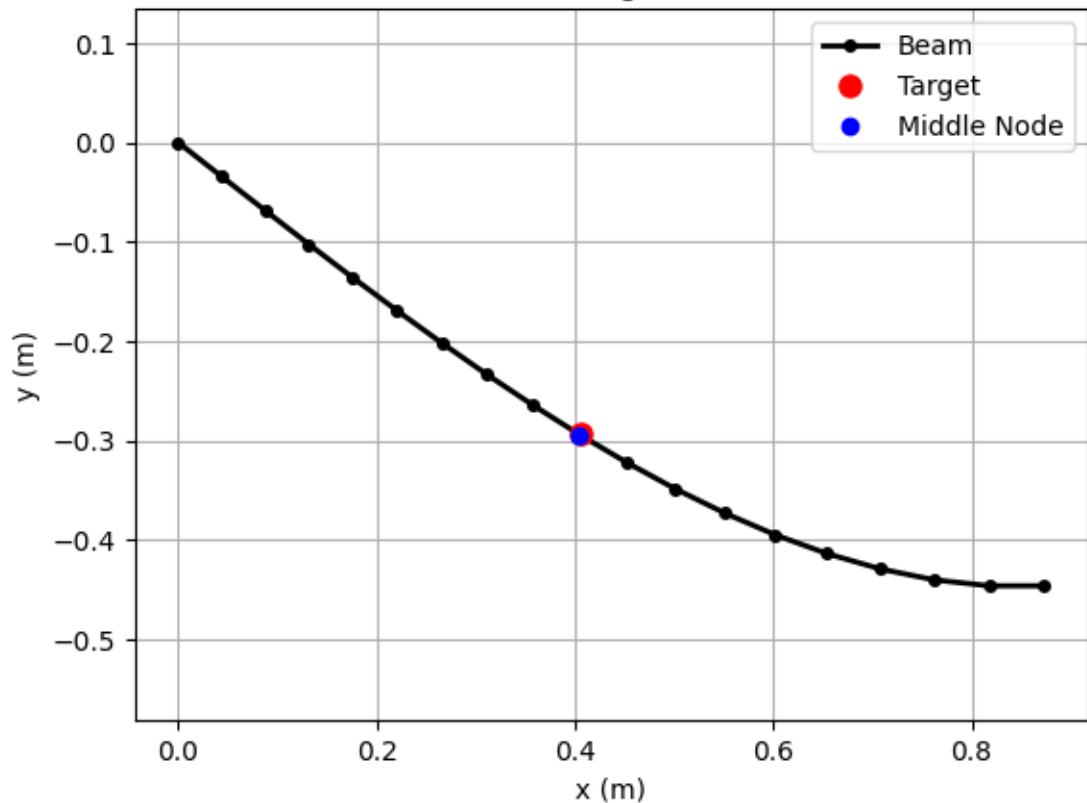
Step 200/1000,  $t = 200.00\text{s}$ , Err = 0.0008 m

$t = 300.00\text{s}$ , Tracking Error = 0.0008 m



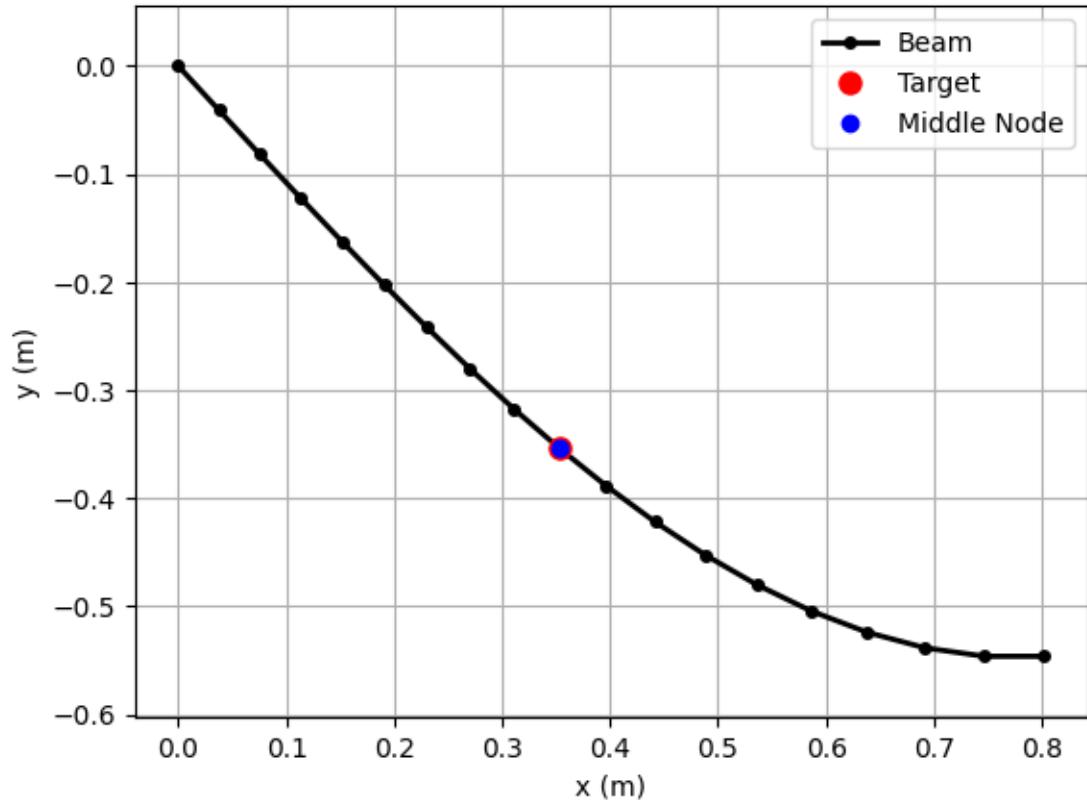
Step 300/1000,  $t = 300.00\text{s}$ , Err = 0.0008 m

$t = 400.00\text{s}$ , Tracking Error = 0.0010 m



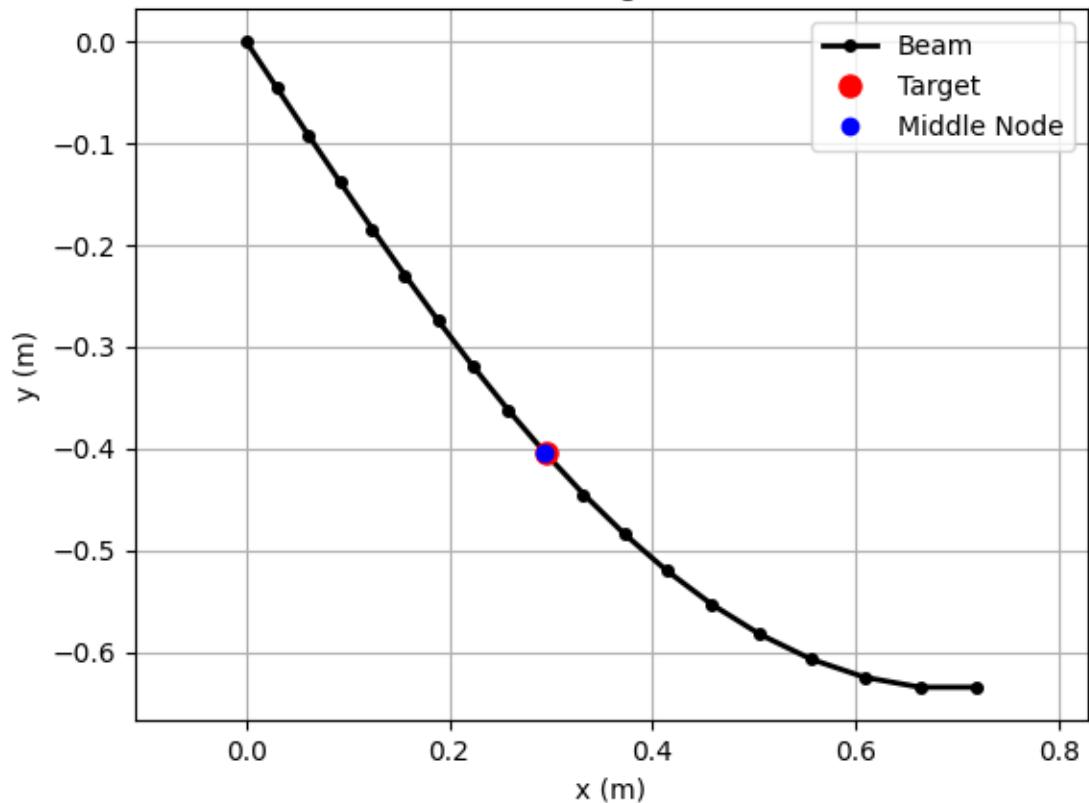
Step 400/1000,  $t = 400.00\text{s}$ , Err = 0.0010 m

$t = 500.00\text{s}$ , Tracking Error = 0.0012 m



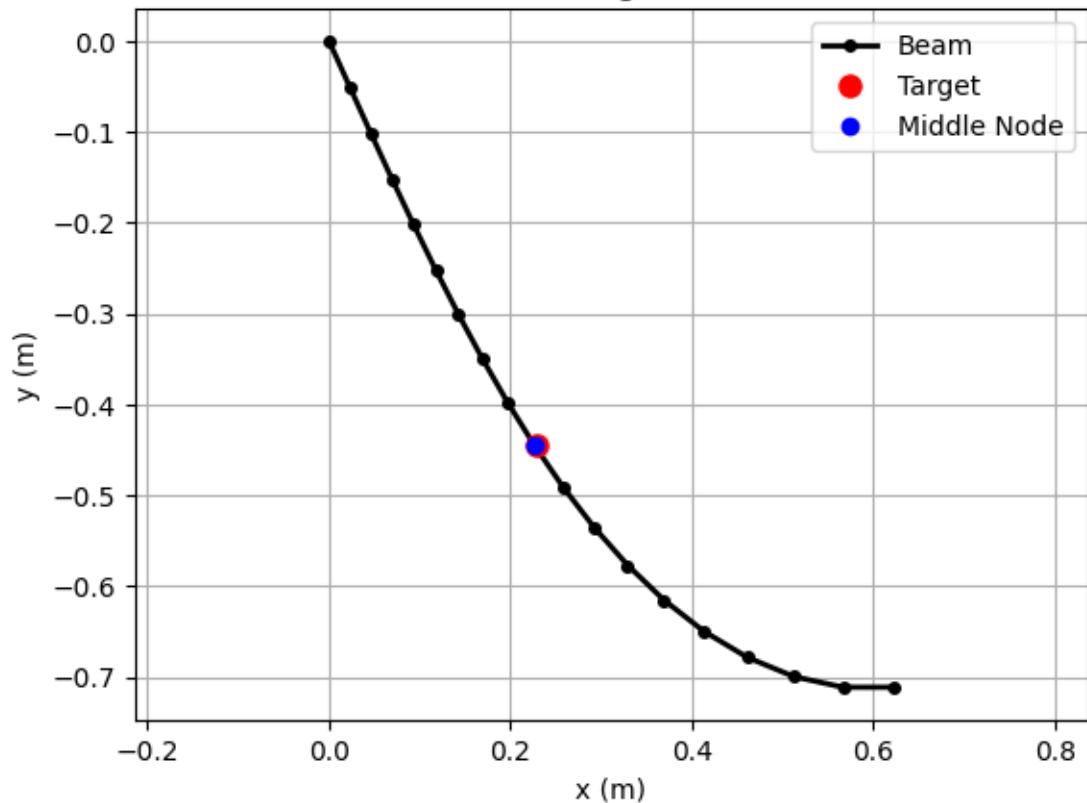
Step 500/1000,  $t = 500.00\text{s}$ , Err = 0.0012 m

$t = 600.00\text{s}$ , Tracking Error = 0.0005 m



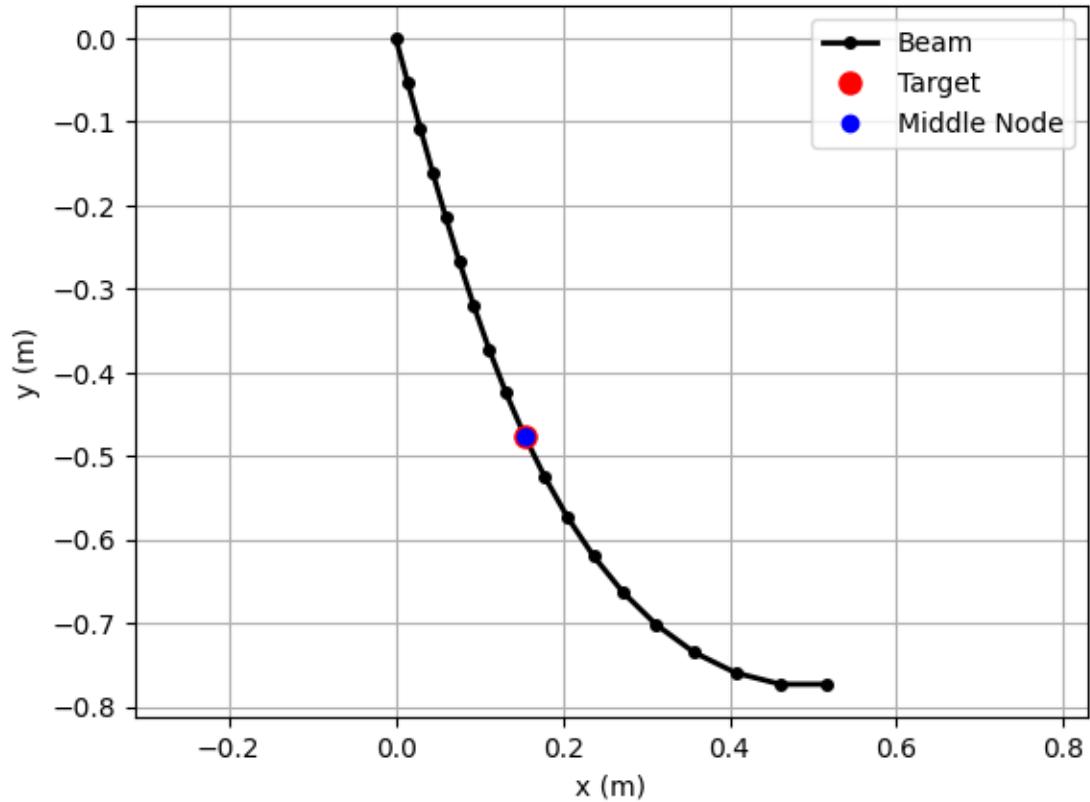
Step 600/1000,  $t = 600.00\text{s}$ , Err = 0.0005 m

$t = 700.00\text{s}$ , Tracking Error = 0.0011 m



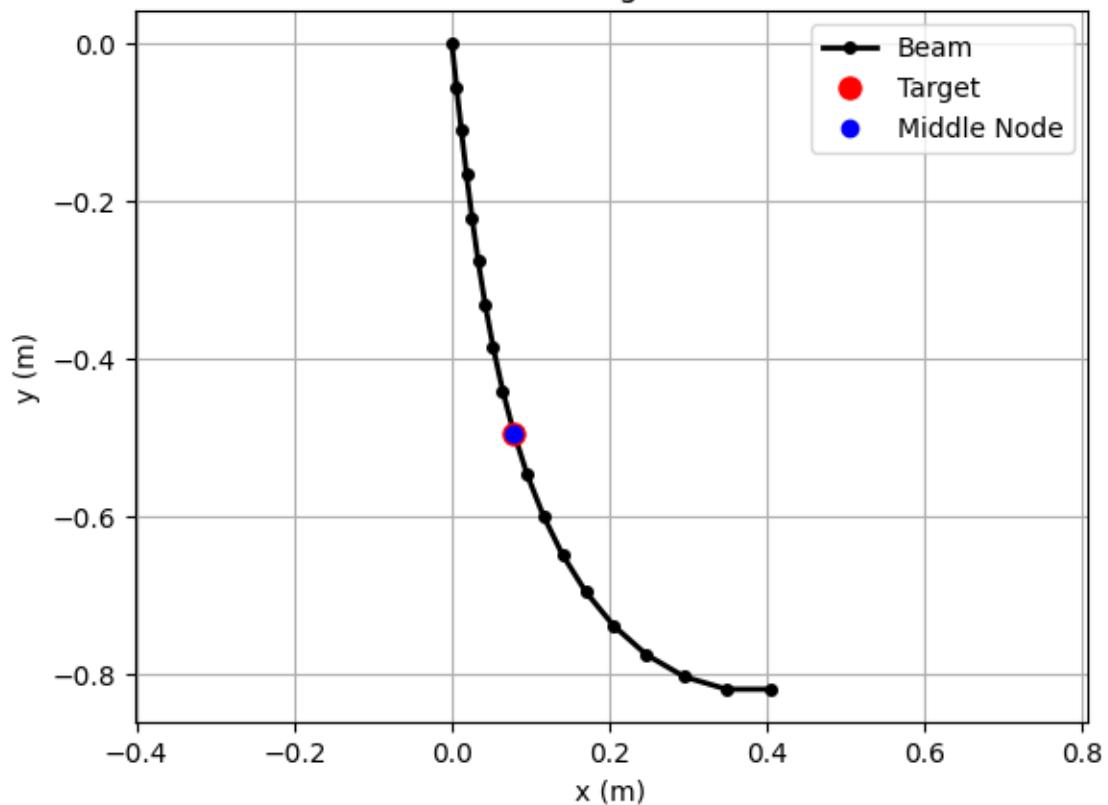
Step 700/1000,  $t = 700.00\text{s}$ , Err = 0.0011 m

$t = 800.00\text{s}$ , Tracking Error = 0.0011 m



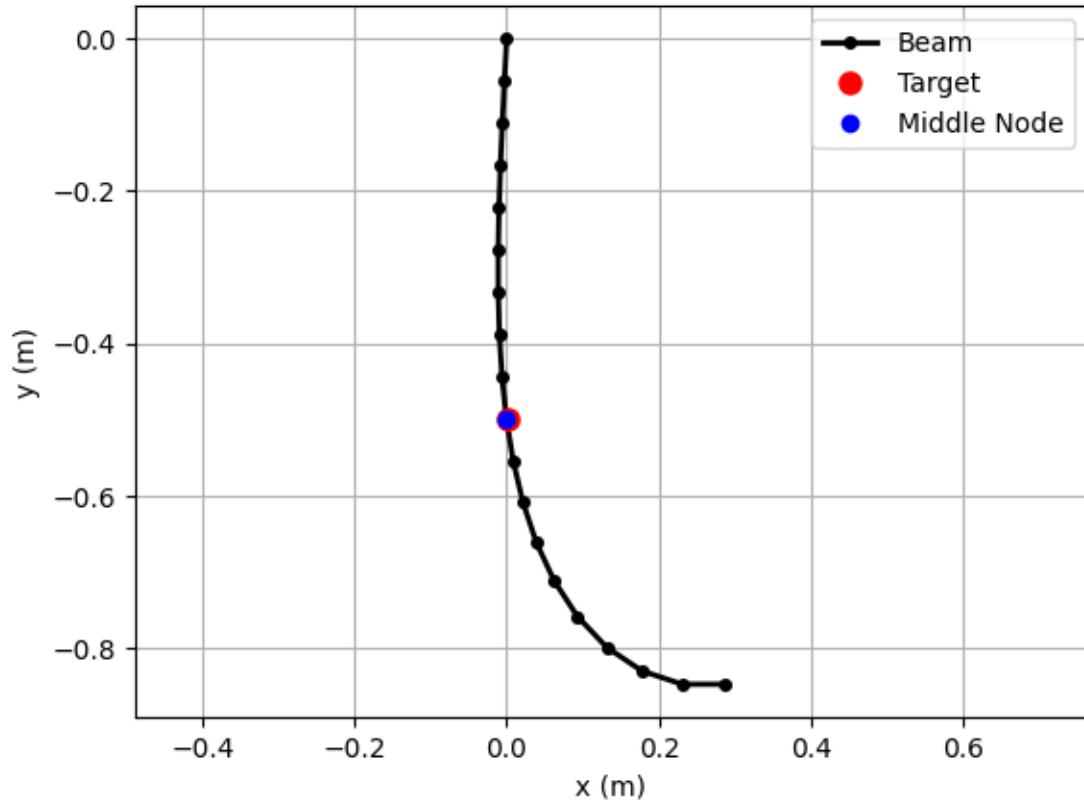
Step 800/1000,  $t = 800.00\text{s}$ , Err = 0.0011 m

$t = 900.00\text{s}$ , Tracking Error = 0.0003 m



Step 900/1000,  $t = 900.00\text{s}$ , Err = 0.0003 m

$t = 1000.00\text{s}$ , Tracking Error = 0.0012 m



Step 1000/1000,  $t = 1000.00\text{s}$ , Err = 0.0012 m

- A brief discussion of feasibility limits due to the robot's workspace and joint limits; explain how you handle infeasible commands (e.g., saturation or trajectory re-timing).

The robot's feasible motion is limited by its workspace (the rod length and curvature capacity), joint orientation limits, and actuator rate constraints. Commands that move the end effector beyond the rod's reachable region, require excessive bending, or exceed maximum step size are considered infeasible. To handle these, the controller applies saturation and rate limiting—each command is clamped to a maximum allowable displacement per time step (`max_step`) to prevent unrealistic or unstable motions. If a command still exceeds workspace boundaries, it is projected back into the feasible region, and the controller's integral term is frozen to avoid windup. In persistent cases, the reference trajectory can be slowed (re-timed) to maintain smooth and feasible motion within all physical limits.