CSE380 HW04

Mason Schechter

October 29 2020

1 Introduction

Here, we will be solving the steady-state heat equation:

$$-k\nabla^2 T(x,y) = q(x,y) \tag{1}$$

where k is the thermal conductivity, T is the material temperature, and q is a heat source term. The expanded form of (1) in 1 dimension is:

$$-k\frac{\delta^2 T(x)}{\delta x^2} = q(x) \tag{2}$$

The expanded form of (1) in 2 dimensions is:

$$-k\left(\frac{\delta^2 T(x)}{\delta x^2} + \frac{\delta^2 T(y)}{\delta y^2}\right) = q(x, y) \tag{3}$$

To solve the steady-state heat equation in 1 and 2 dimensions, we will first need to approximate the value of the second derivative terms in these equations. To do this, we will use 2nd- and 4th-order central finite-difference approximations. The resulting linear system from these numerical methods will be solved using two iterative solution mechanisms: Jacobi and Gauss-Seidel.

2 1 Dimension Approximations

Here, we are going to approximate the steady-state heat equation in 1 dimension. In the above diagram, T_i is the temperature at the point x = i, where $x \in [0, L]$. In this node-based scheme, we will be using constant mesh spacing of N points, such that the distance between a point, T_i , and the previous point, T_{i-1} or $T(x - \Delta x)$, or the next point, T_{i+1} or $T(x + \Delta x)$, is the same distance $\Delta x = L/N$.

We are assuming:

- 1. The mesh spacing is constant
- 2. Dirichlet boundary conditions are applied for any incomplete stencil
- 3. The values at the boundaries will be provided through manufactured solutions.
- 4. T(x) is smooth and continuous for all $x \in [0, L]$
- 5. The values T_i and q_i are not changing over time

The 2nd-order approximation for the second derivative in (2) is:

$$\frac{\delta^2 T(x)}{\delta x^2} \approx \frac{T_{i-1} - 2T_i + T_{i+1}}{\Delta x^2} \tag{4}$$

Substituting this approximation into (2) gives us:

$$T_{i-1} - 2T_i + T_{i+1} \approx -\frac{q_i \Delta x^2}{k} \tag{5}$$

where the truncation error of this approximation is on the order of Δx^2 . The resulting linear system looks like this:

$$\begin{bmatrix} 1 & 0 & 0 & \cdots & \cdots & \cdots & 0 \\ 1 & -2 & 1 & 0 & \cdots & \cdots & 0 \\ 0 & 1 & -2 & 1 & 0 & \cdots & 0 \\ 0 & \ddots & \ddots & \ddots & \ddots & \ddots & 0 \\ 0 & \ddots & \ddots & \ddots & \ddots & \ddots & 0 \\ 0 & \ddots & \ddots & \ddots & \ddots & \ddots & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} T_0 \\ T_1 \\ T_2 \\ \vdots \\ T_{L-1} \\ T_L \end{bmatrix} = \begin{bmatrix} -\frac{q_0 \Delta x^2}{k} \\ -\frac{q_1 \Delta x^2}{k} \\ -\frac{q_1 \Delta x^2}{k} \\ \vdots \\ -\frac{q_{L-1} \Delta x^2}{k} \\ -\frac{q_L \Delta x^2}{k} \end{bmatrix}$$

Each interior (non-boundary) row contains 3 non-zero entries and N-3 zeros.

The 4th-order approximation for the second derivative in (2) is:

$$\frac{\delta^2 T(x)}{\delta x^2} \approx \frac{-T_{i-2} + 16T_{i-1} - 30T_i + 16T_{i+1} - T_{i+2}}{12\Delta x^2} \tag{6}$$

Substituting this approximation into (2) gives us:

$$-\frac{1}{12}T_{i-2} + \frac{4}{3}T_{i-1} - \frac{5}{2}T_i + \frac{4}{3}T_{i+1} - \frac{1}{12}T_{i+2} \approx -\frac{q_i\Delta x^2}{k}$$
 (7)

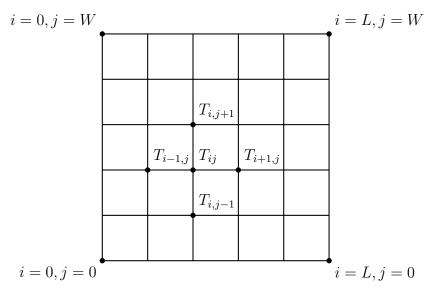
where the truncation error of this approximation is on the order of Δx^4 . The resulting

linear system looks like this:

$$\begin{bmatrix} 1 & 0 & 0 & \dots & \dots & \dots & \dots & 0 \\ 0 & 1 & 0 & 0 & \dots & \dots & \dots & \dots & 0 \\ -\frac{1}{12} & \frac{4}{3} & -\frac{5}{2} & \frac{4}{3} & -\frac{1}{12} & 0 & \dots & \dots & 0 \\ 0 & -\frac{1}{12} & \frac{4}{3} & -\frac{5}{2} & \frac{4}{3} & -\frac{1}{12} & 0 & \dots & 0 \\ 0 & \ddots & 0 \\ 0 & \ddots & 0 \\ 0 & \dots & \dots & 0 & -\frac{1}{12} & \frac{4}{3} & -\frac{5}{2} & \frac{4}{3} & -\frac{1}{12} \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} T_0 \\ T_1 \\ T_2 \\ \vdots \\ \vdots \\ T_{L-2} \\ T_{L-1} \\ T_L \end{bmatrix} = \begin{bmatrix} -\frac{q_0 \Delta x^2}{k} \\ -\frac{q_1 \Delta x^2}{k} \\ -\frac{q_2 \Delta x^2}{k} \\ \vdots \\ \vdots \\ -\frac{q_{L-2} \Delta x^2}{k} \\ -\frac{q_{L-1} \Delta x^2}{k} \\ -\frac{q_{L-1} \Delta x^2}{k} \end{bmatrix}$$

Each interior row has 5 non-zero entries and N-5 zeros.

3 2 Dimension Approximations



Here, we are going to approximate the steady-state heat equation in 2 dimensions. In the above diagram of our node-based scheme, T_{ij} is the temperature at the point x=i,y=j or T(x=i,y=j), where $x\in[0,L]$ and $y\in[0,W]$. We are assuming a square domain, such that L=W. We will be using the same number of discretization points, N, for each dimension, such that $\Delta x=\Delta y=\Delta n$. However, we will need to make a mapping from this 2-D coordinate system to a 1-D vectored system. We will use the equation $h=i+j(N_x)=i+j(N_y)$ where N_x and N_y are the number of discretization points in the x- and y-directions, respectively. Again, they are the same value for the following solutions. Our new mesh grid will look like this:

$$h = WN + L = N^{2}$$

$$T_{h+N}$$

$$T_{h-1} T_{h} T_{h+1}$$

$$T_{h-N}$$

$$h = 0 h = 1 h = 2 h = L$$

We are assuming:

- 1. The mesh spacing is constant, such that $N_x = N_y$, therefore $\Delta x = \Delta y = \Delta n$
- 2. The domain is square, such that L = W
- 3. Dirichlet boundary conditions are applied for any incomplete stencil
- 4. The values at the boundaries will be provided through manufactured solutions.
- 5. T(x,y) is smooth and continuous for all $x \in [0,L]$ and all $y \in [0,W]$
- 6. The values T_{ij} and q_{ij} are not changing over time

The 2nd-order approximation for the second derivative terms in (3) is:

$$\frac{\delta^2 T(x)}{\delta x^2} \approx \frac{T_{h-1} - 2T_h + T_{h+1}}{\Delta x^2} \tag{8}$$

$$\frac{\delta^2 T(y)}{\delta y^2} \approx \frac{T_{h-N} - 2T_h + T_{h+N}}{\Delta y^2} \tag{9}$$

Substituting this approximation into (3) gives us:

$$T_{h-N} + T_{h-1} - 4T_h + T_{h+1} + T_{h+N} \approx -\frac{q_h \Delta n^2}{k}$$
 (10)

where the truncation error of this approximation is on the order of Δn^2 . The resulting

linear system looks like this:

Each interior row contains 5 non-zero entries and N-5 zeros.

The 4th-order approximation for the second derivative terms in (3) is:

$$\frac{\delta^2 T(x)}{\delta x^2} \approx \frac{-T_{h-2} + 16T_{h-1} - 30T_h + 16T_{h+1} - T_{h+2}}{12\Delta n^2}$$
 (11)

$$\frac{\delta^2 T(y)}{\delta y^2} \approx \frac{-T_{h-2N} + 16T_{h-N} - 30T_h + 16T_{h+N} - T_{h+2N}}{12\Delta n^2}$$
 (12)

Substituting this approximation into (3) gives us:

$$-\frac{1}{12}T_{h-2N} + \frac{4}{3}T_{h-N} - \frac{1}{12}T_{h-2} + \frac{4}{3}T_{h-1} + 5T_h + \frac{4}{3}T_{h+1} - \frac{1}{12}T_{h+2} + \frac{4}{3}T_{h+N} - \frac{1}{12}T_{h+2N} \approx -\frac{q_h \Delta n^2}{12k}$$
(13)

where the truncation error of this approximation is on the order of Δn^4 . The resulting coefficient matrix looks like this:

Each interior row has 9 non-zero entries. The resulting linear system looks like this:

$$A \begin{bmatrix} \vdots \\ T_{h-1} \\ T_h \\ T_{h+1} \\ \vdots \\ \vdots \\ \vdots \\ T_{N^2-1} \\ T_{N^2} \end{bmatrix} = \begin{bmatrix} -\frac{q_0 \Delta n^2}{k} \\ -\frac{q_1 \Delta n^2}{k} \\ -\frac{q_2 \Delta n^2}{k} \\ \vdots \\ \vdots \\ -\frac{q_{N^2-2} \Delta n^2}{k} \\ -\frac{q_{N^2-1} \Delta n^2}{k} \\ -\frac{q_{N^2-2} \Delta n^2}{k} \end{bmatrix}$$

4 Jacobi Method

```
Initialize two, 1 \times N^2 T vectors, T_{old} and T_{new};

Set each value in T_{old} to 0;

while currentError > errorThreshold do

| for each h from 0 to N^2 do

| solve for T_h with the values from T_{old} for the other components;

| store result T_h in T_{new};

| end

| currentError = ||T_{old} - T_{new}|| / T_{old};

| T_{old} = T_{new}

| end
```

Estimated memory needed ≈ 8 bytes x $2N^2$

5 Gauss-Seidel Method

Estimated memory needed ≈ 8 bytes x $2N^2$

```
Initialize two, 1xN^2 T vectors, T_{old} and T_{new};

Set each value in T_{old} to 0;

T_{new} = T_{old};

while currentError > errorThreshold do

| for each h from 0 to N^2 do
| solve for T_h with the values from T_{new} for the other components;
| store result T_h in T_{new};

end

currentError = ||T_{old} - T_{new}|| / T_{old};

T_{old} = T_{new};
end
```