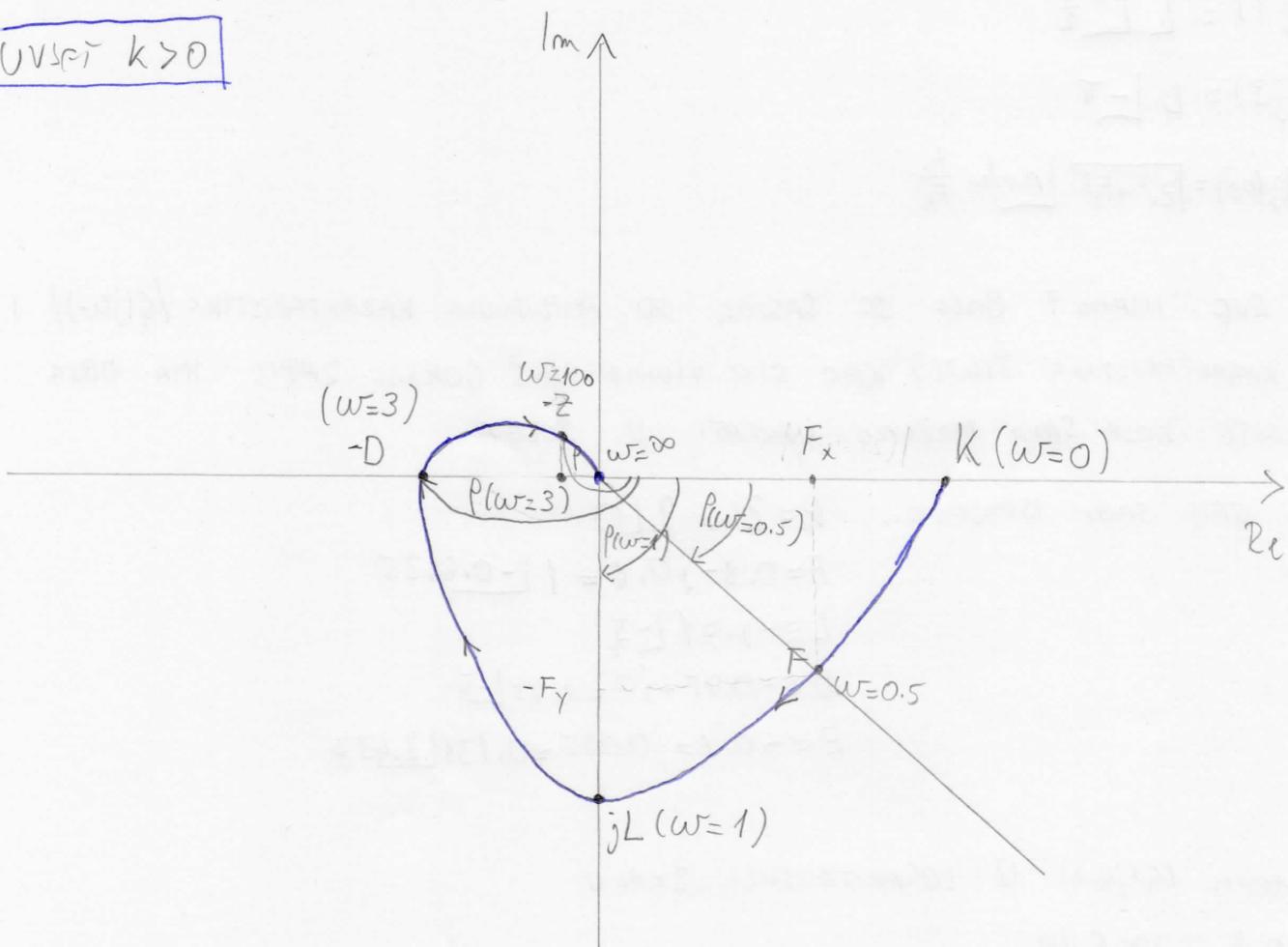


①

# TUTORIAL

## ① VEZA NYQUIST BODE

UVJETI  $k > 0$



\* MODIFICIRANO SAM ZADATAK KOJI JE BIO U ISPITU DA OBJASNIM VEZU  
IZMEĐU BODEA I NYQUISTA

- UZEO SAM 5 TOČAKA  $[k, F, L, D, Z]$  NA TIM TOČKAMA MI JE POZNATA  
FREKVENCija ( $w$ ) A ISČITATI MOŽEMO NJEN REALNI I IMAGINARNI DIO 12 GRAFA,  
ZA SVE TOČKE VELJEDI  $G(jw) = \text{Re} + j\text{Im}$  } ISČITAVAMO S GRAFA

- 1)  $K: w=0$  [ISČITANIO KORDINATE NA MJESU TOČKA  $k$ ]  $G(j0) = k + j0$
- 2)  $F: w=0.5$   $G(j0.5) = F_x - jF_y \Rightarrow$
- 3)  $L: w=1$   $G(j1) = 0 + jL$
- 4)  $D: w=3$   $G(j3) = -D + j0$
- 5)  $Z: w=100$   $G(j100) = -Z_x + jZ_y$

(2)

SADA MJEMANO ZAPIS TIH KOMPLEKSNIH BROSCVA:

$$G(j\omega) = R + jLm = |G(j\omega)| \angle \phi(\omega)$$

$$1) K: G(j0) = k \angle 0^\circ$$

$$2) F: G(j0.5) = \sqrt{F_x^2 + F_y^2} \angle \arctan \frac{F_y}{F_x}$$

$$3) L: G(j1) = L \angle -\frac{\pi}{2}$$

$$4) D: G(j3) = D \angle -\pi$$

$$5) Z: G(j100) = \sqrt{Z_x^2 + Z_y^2} \angle \arctan \frac{Z_y}{Z_x}$$

\* SADA SVC IMAMO: BODE SC SASTOJI OD AMPLITUDNE KARAKTERISTIKE  $|G(j\omega)|$  I FASNE KARAKTERISTIKE  $\phi(\omega)$ . KAO ŠTO VIDIMO NAŠ GORNJI ZAPISIMA IMA OBIGA KOMPONENTI KOJE SAMO MOŽEĆE UKUĆATI U BODEM

$$\text{ZADAJEM SAM SVE BROJCEV: } k = 2 = 2 \angle 0^\circ$$

$$F = 0.8 - j0.6 = 1 \angle -0.6435^\circ$$

$$L = -j = 1 \angle -\frac{\pi}{2}$$

$$D = -0.25 + j0 = 0.25 \angle -\pi$$

$$Z = -0.1 + j0.085 = 0.131 \angle 2.437^\circ$$

\* PRETVARAN  $|G(j\omega)|$  U LOGARITMSKU SKALU

$$k 20 \log 2 \approx 6 \text{ dB}$$

$$F 20 \log 1 = 0$$

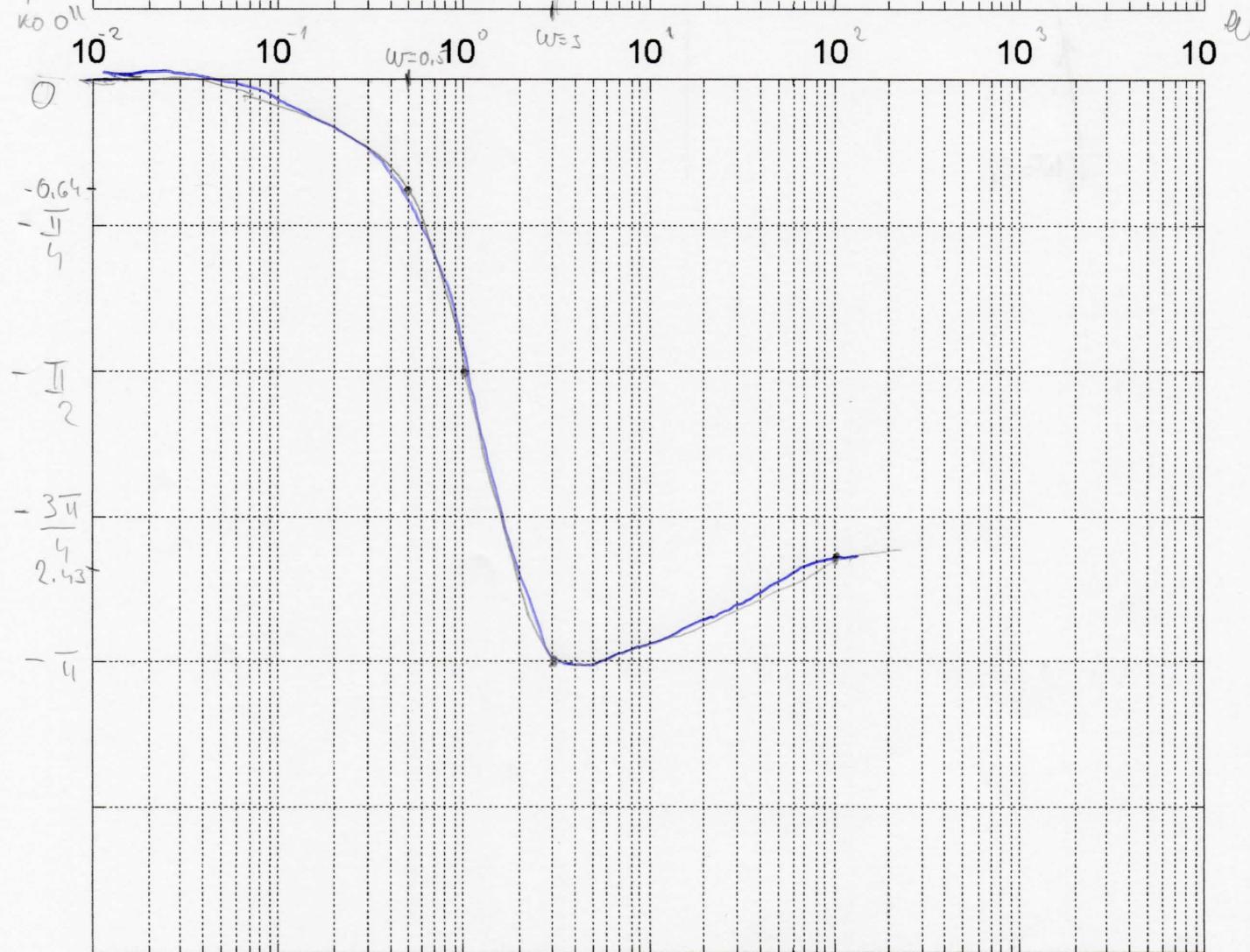
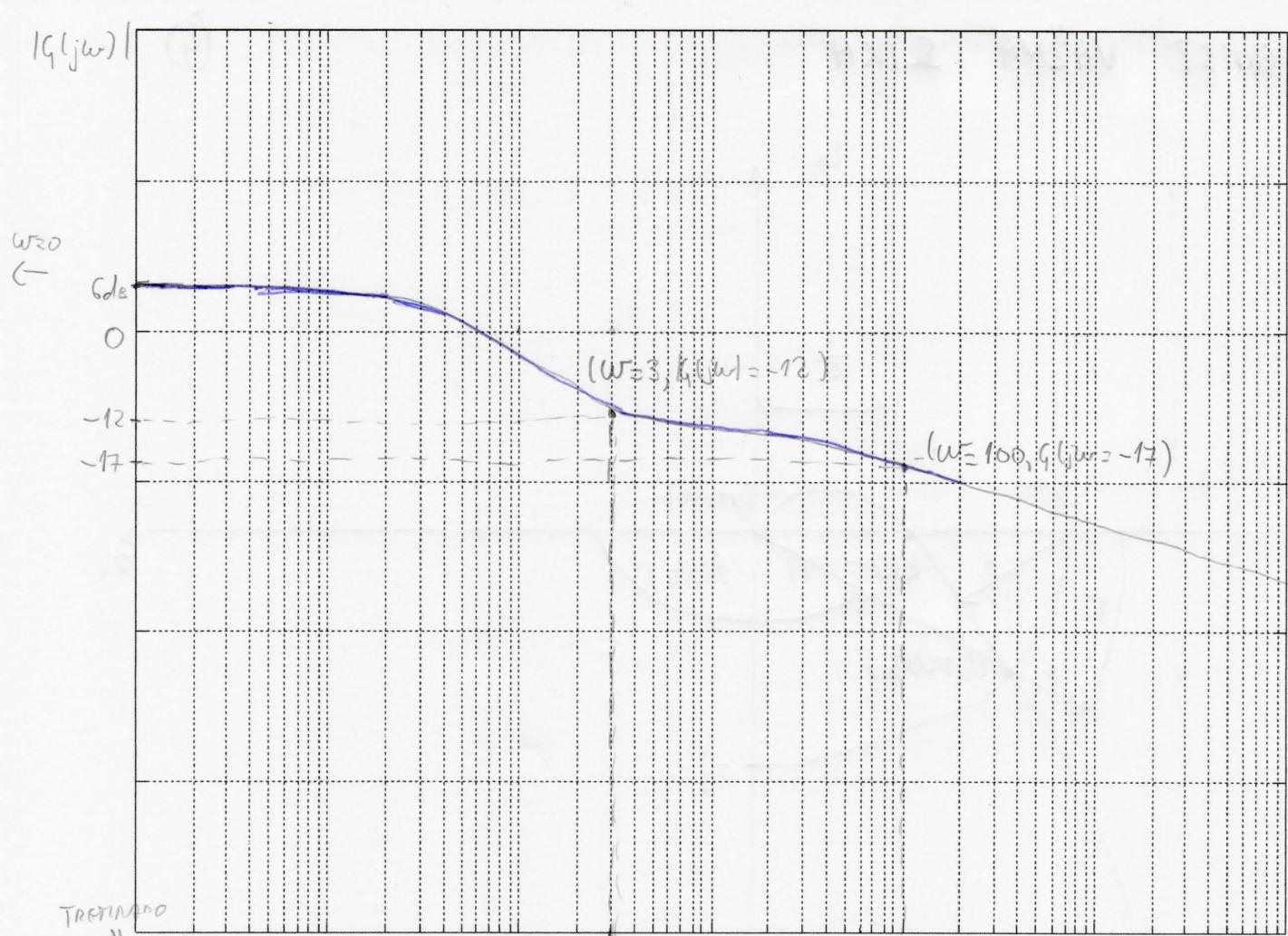
$$L 20 \log 1 = 0$$

$$D 20 \log 0.25 \approx -12$$

$$Z 20 \log 0.131 \approx -17.65$$

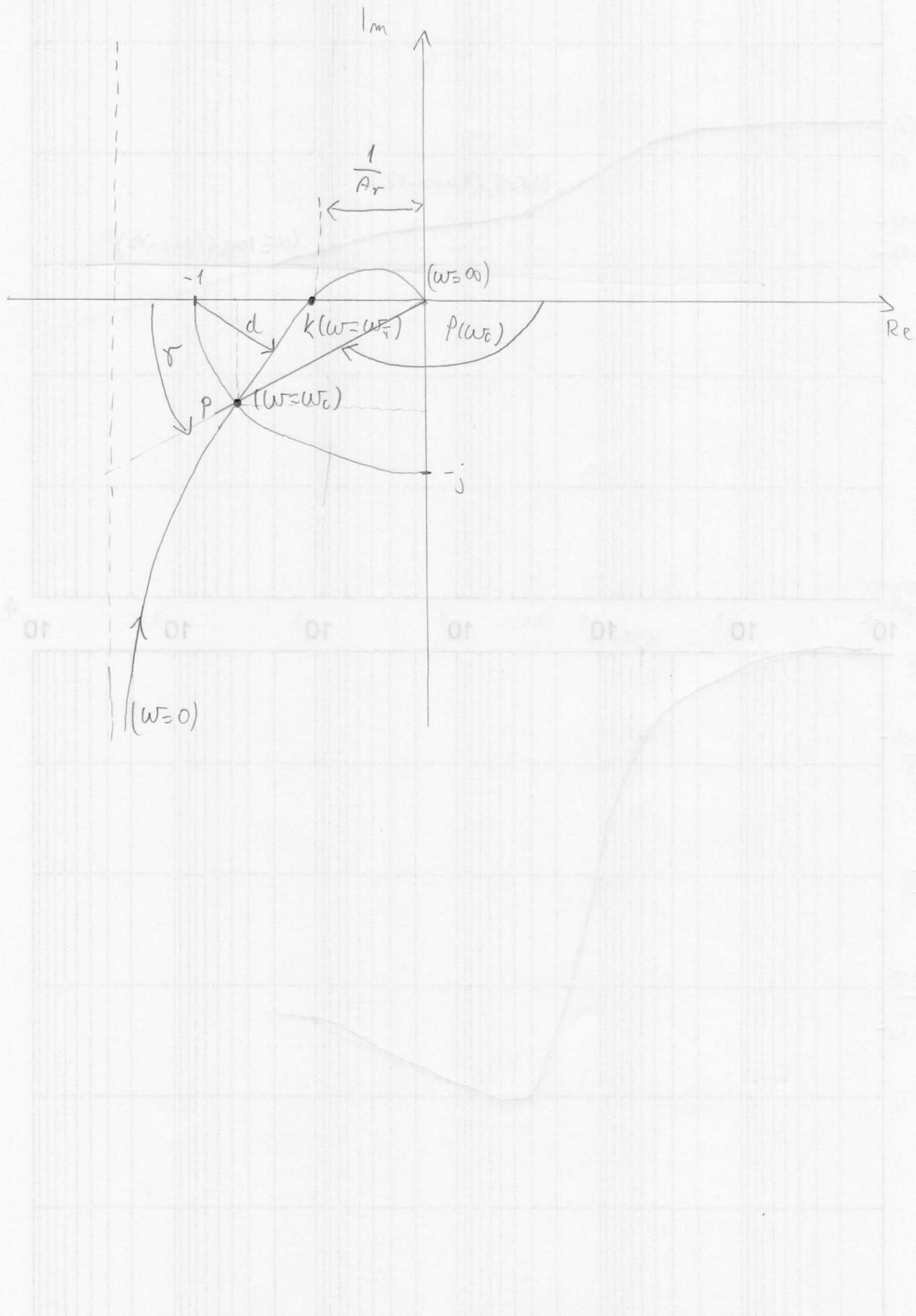
\* BODE HA LINLOGU, MALE ČUJNO 12GLPDA, ALI TO JE JER SAM UZEO ČUJNO BROSEVCE.

(3)



② NYQUIST VAŽNA SLIKA

④



③ NYQUIST TIPICKÝ ČLANOK

⑤

$\uparrow \text{Im}$

$$G(s) = \frac{k}{s}$$

$\rightarrow \text{Re}$

$\omega = \infty$

$\omega = 0$

$\uparrow \text{Im}$

$$G(j\omega) = \frac{k}{\omega^2}$$

$\rightarrow \text{Re}$

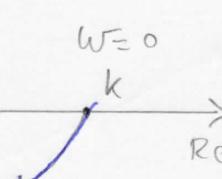
$\omega = 0$



$\uparrow \text{Im}$

$$G(s) = \frac{k}{Ts + 1}$$

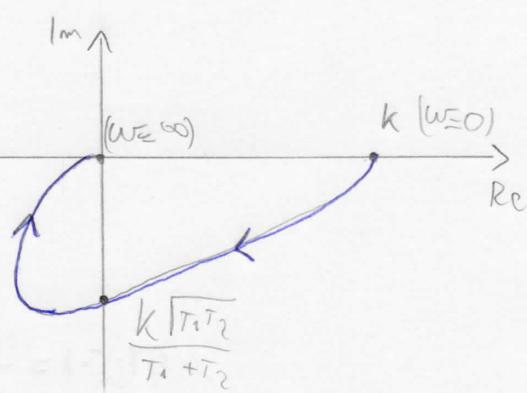
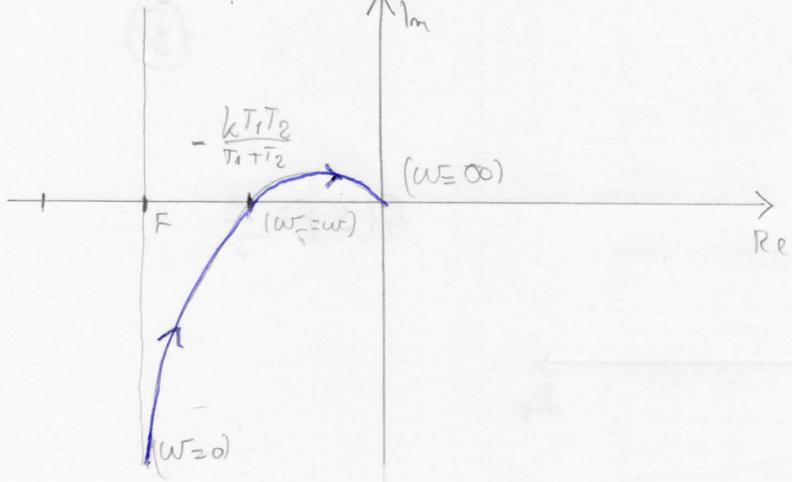
$\omega = \infty$



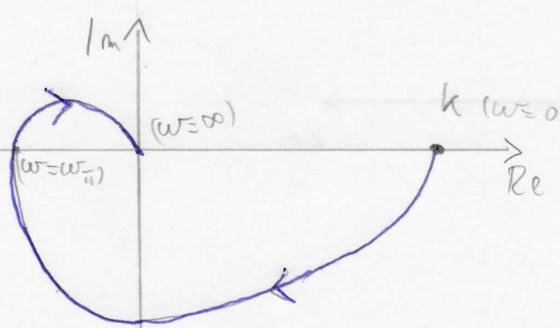
$\rightarrow \text{Re}$

(6)

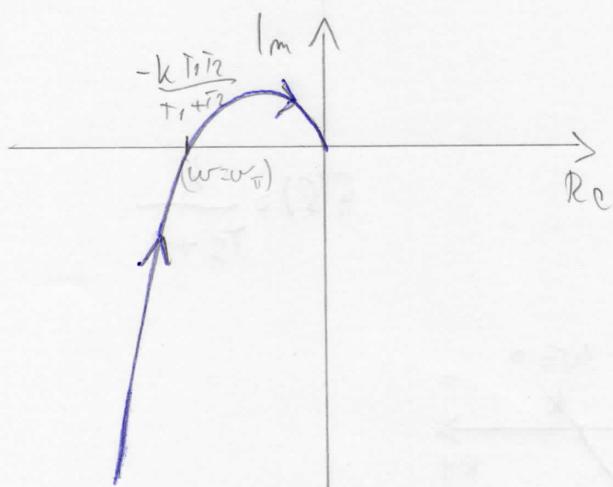
$$G(s) = \frac{k}{s(T_1 s + 1)} = \frac{k}{T_1 s^2 + s}$$



$$G(s) = \frac{k}{(T_1 s + 1)(T_2 s + 1)} = \frac{k}{T_1 T_2 s^2 + s(T_1 + T_2)}$$



$$G(s) = \frac{k}{(s+a)(s+b)(s+c)} = \frac{k}{a_3 s^3 + a_2 s^2 + a_1 s + 1}$$



$$G(s) = \frac{k}{s(T_1 s + 1)(T_2 s + 1)}$$

## ④ PID REGULATORI

⑦

PID - PROPORCIONALNO - INTEGRALNO - D-GRIVACISNI REGULATOR

$$U(t) = \underbrace{K_p e(t)}_{P} + \underbrace{K_i \int_0^t e(\tilde{t}) d\tilde{t}}_{I} + \underbrace{K_d \frac{d e(t)}{dt}}_{D}$$

$U(t)$  - UPRAVLJAČKI SIGNAL

$e(t)$  - REGULACIJSKO ODSTUPANJE

MOGUĆE KOMBINACIJE P, I, D, PI, PD, PID...

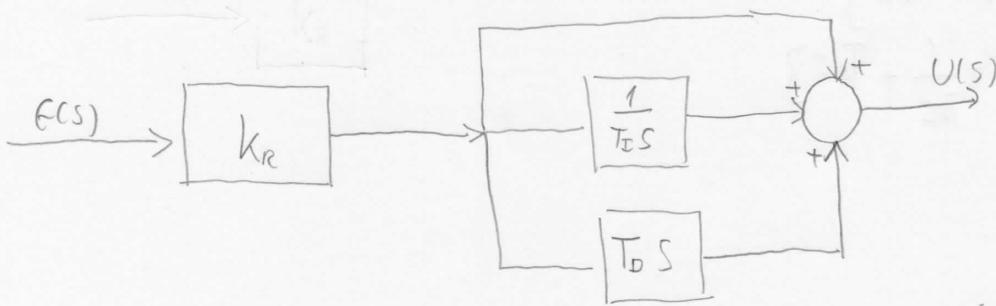
2-12 VEDBE REGULATORA [SERIJSKA | PARALELNA]

PARALELNA 12VEDBA

$$G_{RP}(s) = k_r + \frac{k_i}{s} + K_d s$$

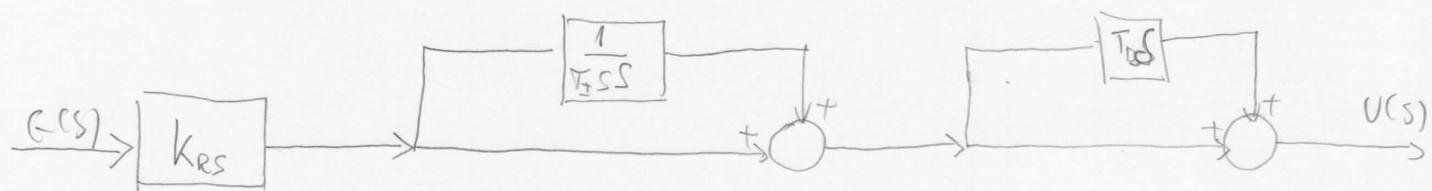
$$\text{SUPSTITUCIJA} \quad k_r = k_r \quad T_I = \frac{k_r}{k_i} \quad T_D = \frac{k_d}{k_r}$$

$$G_{RP}(s) = k_r \left[ 1 + \frac{1}{T_I s} + T_D s \right] \rightarrow \text{LOGALNI PID}$$



SERIJSKA 12VEDBA

$$G_{RS}(s) = k_{rs} \left[ 1 + \frac{1}{T_{IS} s} \right] \left[ 1 + T_{DS} s \right]$$



PARALELNO  $\Rightarrow$  SERIJSKA PRETIVODA

⑧

$$K_{RS} = \frac{C}{2} k_R \quad \bar{T}_{IS} = \frac{C}{2} \bar{T}_I \quad \bar{T}_{DS} = \frac{C}{2} \bar{T}_D$$

$$C = 1 + \sqrt{1 - \frac{4 \bar{T}_D}{\bar{T}_I}}$$

SERIJSKO  $\Rightarrow$  PARALELNA PRETIVODA

$$\text{UVSET: } \bar{T}_I \geq 4 \bar{T}_D$$

$$k_R = K_{RS} \frac{\bar{T}_{IS} + \bar{T}_{DS}}{\bar{T}_{IS}}$$

$$\bar{T}_{IS} = \bar{T}_I + \bar{T}_{DS}$$

$$\bar{T}_D = \frac{\bar{T}_{IS} \cdot \bar{T}_{DS}}{\bar{T}_{IS} + \bar{T}_{DS}}$$

REALNI PID REGULATOR

$$G_{RR} = k_R \left[ 1 + \frac{1}{\bar{T}_I s} + \frac{\bar{T}_D s}{1 + \bar{T}_r s} \right]$$

$$\bar{T}_D = (5 \div 20) \bar{T}_r$$

SERIJSKI REGULATORI [IDEALNI]

PI  $G_R(s) = k_R \left[ 1 + \frac{1}{\bar{T}_I s} \right]$

PD  $G_R(s) = k_R \left[ 1 + \bar{T}_D s \right]$

PID  $G_R(s) = k_R \left[ 1 + \frac{1}{\bar{T}_I s} + \bar{T}_D s \right]$

## (5) POSTUPCI PARAMETRIZACIJE REGULATORA

(9)

### (1) ZIEGLER-NICHOLSOVA METODA RUB STABILNOSTI ZN1

- EKSPERIMENT U ZATVORENOM KRUGU

KUHARICA:

(1) UGASIMO SVA DIFLOVANSA OSIM PROPORTIONALNOG, NAŠ ZADANI PI, PID, P  
REGULATOR MJEŠAVAN SA  $G_R(s) = K_{KR}$

(2) NAPREDNO RUB STABILNOSTI [NYQUIST, HURWITZ, BODE] OCITANO KUR I TKE

(3) PREMA TABLICI 12 FORMULA ODGOVORNO PARAMETRE NAŠEG REGULATORA

PRIMJER PZI 2009 4.c) [NISAN RJEŠENJE U PRVOM SCANU]

\* PRIGIJOSNA FUNKCIJA DOBIJELA POD a)

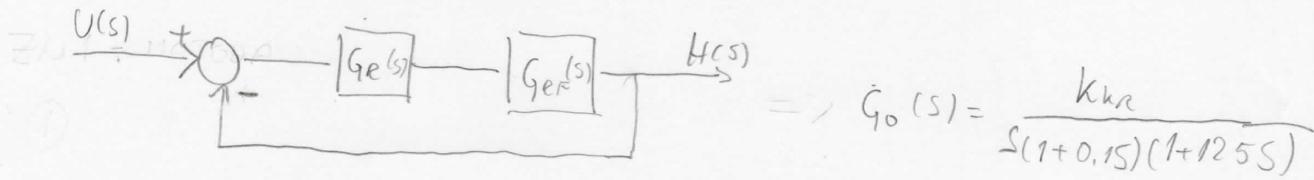
$$G_p(s) = \frac{H(s)}{X_v(s)} = \frac{5}{(1+0.1s)(1+125s)}$$

$$* ZADANA JE G_{REF}(s) = \frac{X_v(s)}{U(s)} = \frac{1}{T_i s} = \frac{1}{5s} \quad T_i = 5$$

\* TRAŽI NAŠ REGULATOR RAZINA FLUIDA - REGULATOR JE P-TIPA

PRIGIJOSNA ZA RAZINU FLUIDA  $G_{RF}(s) = \frac{H(s)}{U(s)}$

$$H(s) = \frac{5 \cdot X_v(s)}{(1+0.1s)(1+125s)} = \frac{5 \cdot \frac{1}{5s}}{(1+0.1s)(1+125s)} \Rightarrow \frac{H(s)}{U(s)} = G_{RF}(s) = \frac{1}{(1+0.1s)(1+125s)s}$$



ZN1 - METODA

(1) GASIMO SVR U REGULATORU OSIN  $K_{KR} = s G_R(s) = k_{kr}$

(2) TRAŽIMO RUB STABILNOSTI [JA ĆU PREDKO HURWITZA]

$$L = 1 + G_o = 0$$

$$s[12.5s^2 + 125.1s + 1] + k_{kr} = 0$$

$$12.5s^3 + 125.1s^2 + s + k_{kr} = 0 -$$

I)  $k_{kr} > 0$

(10)

$$\text{II) } \begin{vmatrix} 1 & k_{ke} \\ 12,5 & 125,1 \end{vmatrix} = 125,1 - 12,5k_{ke} > 0$$

$$k_{ke} < 10$$

$$k \in [0, 10]$$

GLEDANO GDJE SUSTAV DASCI OSCILACIJE

$$G_Z(s) = \frac{k_{ke}}{12,5s^2 + 125,1s^2 + s + k_{ke}}$$

GLEDANO Polovac za  $k_{ke} = 0$

$$k_{ke} = 10$$

$k_{ke} = 2309$  Polova dasci oscilatoran odziv

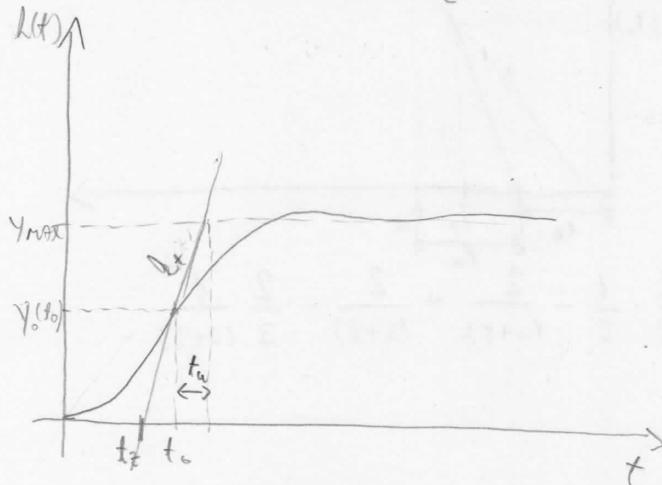
(3) UZMEMO TABLICE

$$ZN1 \rightarrow P \rightarrow k_k = 0,5k_{ke} = \frac{10}{2} = 5$$

$$\boxed{k_{ke} = 5}$$

## ② ZN2-METODA - ZIEGLER-NICHOLSOVA METODA PRUČLARNE FUNKCIJE

- ZN2 METODA SE RADI OTVORENI REGULACIJSKI KRUG
- TOČKA INFLEKCIJE  $h(t)$  JE Mjesto gdje VRISEDI  $h''(t_0) = 0$
- VRISEME ZADRIJAVANJA  $t_z$  JE Mjesto gdje TANGENTA SJEGE t-OS



JED. TANGENTE

$$y - y_o(t_0) = h_t(t - t_0)$$

KUHARIĆA:

- ① PRETVORITI  $G_0(s)$  U  $H(s)$   $\left[ \frac{1}{s}, G_0(s) = H(s) \right]$
- ② VRAĆITI U VRFHENSKU DOMENU  $H(s) \rightarrow h(t)$
- ③ DODIRIVATI DVA PUTA  $[h''(t_0) = 0]$  IZ TOGA IZVUĆI  $t_0$
- ④ UVRŠTITI DOBIVENI  $t_0$  U  $h'(t)$   $[h'(t_0) = h_t]$
- ⑤ UVRŠTITI  $t_0$  U  $h(t)$   $[h(t_0) = y_o(t_0)]$
- ⑥ NAPISATI JED. TANGENTE  $[y - y_o(t_0) = h_t(t - t_0)]$
- ⑦ NAĆI STACIONARNO STANJE OD  $H(s)$  PECKO LINIJE
- ⑧ NAĆI  $t_z$  KAO NULJOČKU PRAVCA TANGENTE
- ⑨ NAĆI  $t_a$  KAO  $[y_{MAX} - y_o(t) = h_t[(t_z + t_a) - t_0]]$
- ⑩ POMOĆU TABLICE ODrediti PARAMETER REGULATORA

$$G_o(s) = \frac{4}{(s+1)(s+2)(s+3)} =$$

(1) PRETVARANJE  $G_o(s)$  U  $H(s)$

$$H(s) = \frac{4}{s(s+1)(s+2)(s+3)}$$

(2) VRAĆANJE U VREMENSKI DOMEN

$$H(s) = \frac{C_{11}}{s} + \frac{C_{21}}{(s+1)} + \frac{C_{31}}{(s+2)} + \frac{C_{41}}{(s+3)} \Rightarrow H(s) = \frac{2}{3} \cdot \frac{1}{s} - \frac{2}{(s+1)} + \frac{2}{(s+2)} - \frac{2}{3} \cdot \frac{1}{(s+3)}$$

$$h(t) = \frac{2}{3} - 2e^{-t} + 2e^{-2t} - \frac{2}{3}e^{-3t}$$

(3) DERIVIRANJE DVA PUTA  $h'(t)$   $h''(t)$  I TRAŽIMO  $t_0$  IZ  $h''(t_0) = 0$

$$h'(t) = 2e^{-t} - 4e^{-2t} + 2e^{-3t}$$

$$h''(t) = -2e^{-t} + 8e^{-2t} - 6e^{-3t}$$

$$h''(t_0) = 0 ; e^{-t_0} = x$$

$$-2x + 8x^2 - 6x^3 = 0$$

$$x_1 = 1 \quad x_2 = \frac{1}{3} \quad x_3 = 0 \Rightarrow \begin{array}{l} 1) e^{-t_0} = 1 \\ t_0 \neq 0 \end{array} \quad \begin{array}{l} 2) e^{-t_0} = \frac{1}{3} \\ t_0 = \ln 3 \end{array} \quad \begin{array}{l} 3) e^{-t_0} = 0 \\ e^{-t_0} \neq 0 \end{array}$$

(4) UVREŠTAVANJE  $t_0$  U  $h'(t)$

$$h'(t_0) = \frac{8}{27} = k_t$$

(5) UVREŠTAVANJE  $t_0$  U  $h(t)$

$$h(t_0) = \frac{16}{81}$$

(6) PIŠEMO JED. TANGENCIJE

$$h - h(t_0) = k_t(t - t_0) \Rightarrow h - \frac{16}{81} = \frac{8}{27} [t - \ln 3]$$

(7) TRAŽIMO STACIONARNO STANJE  $[S, T]$

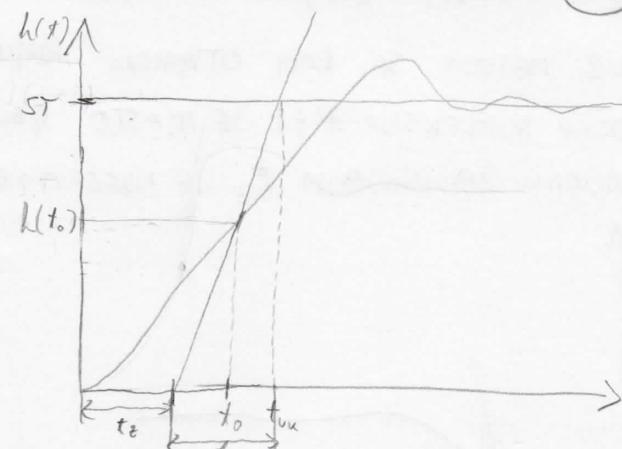
$$\lim_{s \rightarrow 0} s H_o(s) = \lim_{s \rightarrow 0} G_o(s) = \frac{4}{s} = \frac{2}{3} = k_s$$

(8) TRAŽIMO  $t_2$  KAO MULROCKU TANGENCIJU

$$0 - \frac{16}{81} = \frac{8}{27} [t_2 - \ln 3] \Rightarrow t_2 = 0,4319$$

(9) TRAŽIMO  $t_u$  KAO Mjesecne godine tangencija srednje  $S, T$

$$\frac{2}{3} - \frac{16}{81} = \frac{8}{27} [(t_u + t_2) - \ln 3] \Rightarrow t_u = 2,25$$



(10) UVREŠTAVANJE BROJEVI U TABLICI

$$k_R = \frac{1,2 t_u}{t_2 k_s} = 9,377$$

$$T_E = 0,8639$$

$$T_B = 0,21585$$

$$G_R(s) = 9,37 \left[ 1 + \frac{1}{0,86s} + 0,22 T_B s \right]$$

### ③ INTEGRALNI KRITERIJI

1. SE KRITERIS

$$I = \int_0^{\infty} [e(t) - e_{\infty}]^2 dt = I[r_1, r_2, \dots, r_m]$$

① TREBANO PRONAĆI REGULACIJSKO ODSTUPANJE U DOKJEN PODRUČJU

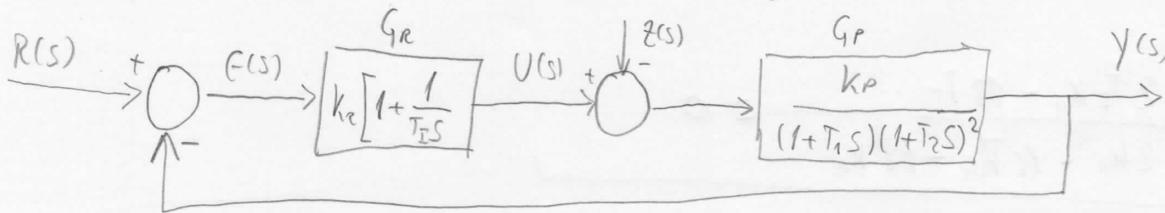
$$E(s) = \frac{C(s)}{D(s)} = \frac{c_0 + c_1 s + \dots + c_{m-1} s^{m-1}}{d_0 + d_1 s + \dots + d_m s^m}$$

② ONDA FORMIRANO I FUNKCIJU PREMA SLUŽBENOM ŠABLJU

③ TRAŽIMO PARCIALNE DERIVACIJE

### PRIMJER SKRIPTA MALBERT

ODREDI PI REGULATOR:  $k_p = 1$ ;  $T_1 = 0.5[s]$ ;  $T_2 = 1[s]$



① ODREDI REGULACIJSKO ODSTUPANJE

$$E(s) = -Y(s)$$

$$E(s) = -[(E(s) \cdot G_R - Z(s)) \cdot G_P]$$

$$E(s) = \frac{Z(s) \cdot G_P(s)}{1 + \underbrace{G_R(s) G_P(s)}_{G_0}} = \frac{k_p T_i}{T_1 T_2 T_2^2 s^3 + s^2 [T_2 T_2^2 + 2T_1 T_2 T_2] + s [2T_1 T_2 + T_1 T_1] + s [T_2 + k_p k_r T_i] + k_p k_r}$$

OČITO NĀS  $E(s)$  IZGLJEDA  $G(s) = \frac{c_0 + c_1 s + c_2 s^2 + c_3 s^3}{d_0 + d_1 s + d_2 s^2 + d_3 s^3 + d_4 s^4}$

$$c_0 = k_p T_i \quad c_1 = 0 \quad c_2 = 0 \quad c_3 = 0$$

$$d_0 = k_p k_r \quad d_1 = T_2 k_p k_r + T_1 \quad d_2 = T_1 T_2 + 2T_2 T_2 \quad d_3 = T_2^2 T_1 + 2T_1 T_2 T_2 \quad d_4 = T_1 T_2 T_2^2$$

(2) OČITANO 12 TABLICE FORMULU ZA ISC Kriterijus RGA m=4 (14)

$$T_{3,4} = \frac{(k_e T_I)^2 \left[ -T_I k_R k_p + T_I \right] \cdot (T_1 T_2 T_I)^2 + (T_1 T_I + 2T_2 T_I) (T_2^2 T_I + 2T_1 T_2 T_I) (T_1 T_I T_2^2)}{2 \cdot k_R k_p \cdot T_1 T_I T_2^2 \left[ -k_e k_p \cdot (T_2^3 T_I + 2T_1 T_2 T_I) - (T_R k_R k_p + T_I) T_1 T_2 T_I^2 + d_1 d_2 d_3 \right]} \\ \text{NE STAVI:})$$

UVRŠTINO BROJevi I SREDIMO

$$T_{3,4} = \frac{(k_e - g) T_I^2}{2 k_R \left[ k_e^2 T_I + 8 k_e T_I - 8 k_e T_I - 9 T_I \right]}$$

(3) PREGUČIMO DGRIVIRATO PO NEPOZNATICAMA I IZJEDNAČIMO SA 0

$$\frac{\partial T_{3,4}}{\partial k_R} = \frac{T_I^2 - 18 T_I}{6 k_R^2 T_I + 32 k_R - 32 k_R T_I - 18 T_I} = 0$$

$$\frac{\partial T_{3,4}}{\partial T_I} = \frac{2 T_I k_R - 18 T_I}{2 k_R^3 - 16 k_R - 18 k_R} = 0$$

\* RISČIMO GOREVI SUSTAV S DVISE JED. I DVISE NEPOZNATICE

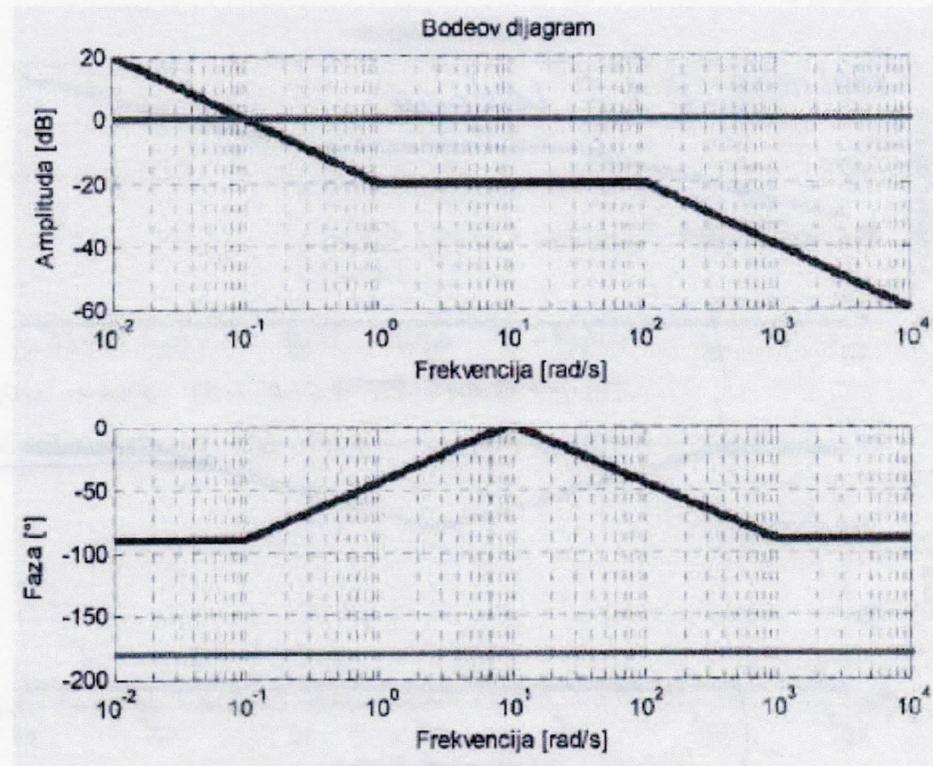
$$k_R = 1.85 \quad T_I = 1.5$$

$$G_R(s) = 1.85 \left[ 1 + \frac{1}{1.5} \right]$$

\* PARAMETRIZIRALI SMO PI REGULATORE PO ISC KRIJERIJU

6 ČITANJE PRIMJENOSNE 12 BODEA

15



1 GLEDAMO AMPLITUĐU KARAKTERISTIKU

- KOJI SVR OSNOVNI ČLAVI DJELUJU
- DJELUJE  $\frac{1}{s}$  JER BODE PADA OD BESKONAČNOSTI  $[20 \log w]$
- DJELUJE  $(1 \pm s)$  NULA JER SE U  $10^\circ$  POVIŠAVA DJELOVANJE  $\frac{1}{s}$  ČLAVA  $[20 \log \sqrt{1+w^2}]$
- DJELUJE  $(1 \pm \frac{s}{100})$  JER NAKON  $w=10^2$  BODE OPET PADA  $[20 \log \sqrt{1+\frac{w^2}{100^2}}]$
- DJELUJE POJAĆANJE OD  $-20 \text{ dB}$  JER JE CIJELI BODE SPUSTEN  $20 - 20$

PRIMJENSKA JF OBLIKA

$$G(s) = \frac{(1+s)k}{s[1 + \frac{s}{100}]}$$

$$20 \log(k) = -20 \Rightarrow k = 0.1$$

2 GLEDAMO SANO FAZU

- $\frac{1}{s}$  PRIDOKASI DA FAZA POČINJE  $12 - \frac{\pi}{2} [90^\circ]$
- NA FREKVENCII  $10^{-1}$  POČINJE DJELOVATI NULA I FAZA RASTE  $\text{arctan} \frac{1}{100}$  POSTO RASTE  $\text{arctan}$  JE POSITIVAN NAŠA NULA JE POSITIVNA +
- NA FREKVENCII  $10^1$  NULA JE GASI, ALI NAŠA FAZA JE NE IZRavnava nego počinje padati jer se upalio pol - arctan  $\frac{100}{100}$  PA ZAKLjučujemo da je pol pozitivan +

(3) NA KRAJU RAČA PRIMJERNA FUNKCIJA IZGLEDA

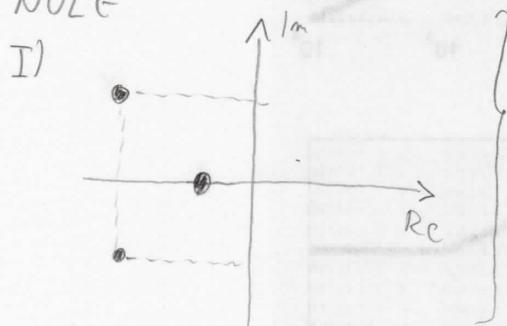
$$G(s) = \frac{0.1(s+1)}{s \left[ 1 + \frac{s}{100} \right]} = \frac{1+s}{s[100+s]} //$$

(16)

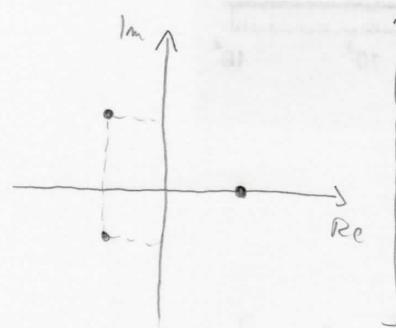
## (7) POKAZATELJI KVALITETE ZA S DOMENA

- POKAZATELJI KVALITETE NAM INDIREKTNO GOVORE O STABILNOSTI SUSTAVA UTJECAJ NULA I POLOVA NA SUSTAV  $G(s) = \frac{\text{Nula}}{\text{Polovi}}$

### I) NULE



SUSTAV KOJI IMA SVE NULE U LIJEVOJ POLURAVNINI T.J. NEIMA NIJEDNU NULU U DESNOJ POLURAVNINI ZOVE SE MINIMALNO FAZNI SUSTAV



SUSTAV KOJI POSJEDUJE BAREM JEDNU NULU U DESNOJ POLURAVNINI ZOVE SE NEMINIMALNO FAZNI SUSTAV

STABILAN NEMINIMALNO FAZNI SUSTAV IMA FAZNU KARAKTERISTIKU KOJA JE UVJEMANJA OD ODGOVARAJUĆE KARAKTERISTIKE MINIMALNO FAZNOG SUSTAVA

### II) DOMINANTNOST

- DOMINANTNE SU ONE NULE KOJE SU BLIŽE IMAGINARNIM OS-IMA, TO ZNAĆI DA JE NJIHOV UTJECAJ NA SUSTAV VRĆI

### III) UTJECAJ NA SUSTAV

NULA LIJEVO +  $PT_2$

- NULA U LIJEVOJ POLURAVNINI UBRAJAVA PRIMJERNU POSAVU, STVARA NADVIŠENJE ŠTO JE BLIŽE POLOU, NADVIŠENJE JE VRĆE, UDALJAVANjem UTJECAJA NULE ISČIĆZAVA

NULA DESNO +  $PT_2$  JE U DESNOJ POLOU

- NEPARAN BROJ NULA U DESNOJ POLURAVNINI STVARA PODBACAJ ŠTO JE NULA BLIŽE JER TO JE PODBACAJ VRĆI

## 2) POLOVI

I) - SUSTAV JE STABILAN AKO SU MU SVI POLOVI U LINIJOS POZURAVNIM

- STABILNOST SUSTAVA UVRIJEDLJIVANA JE POLOVIMA

## II) DOMINANTNOST

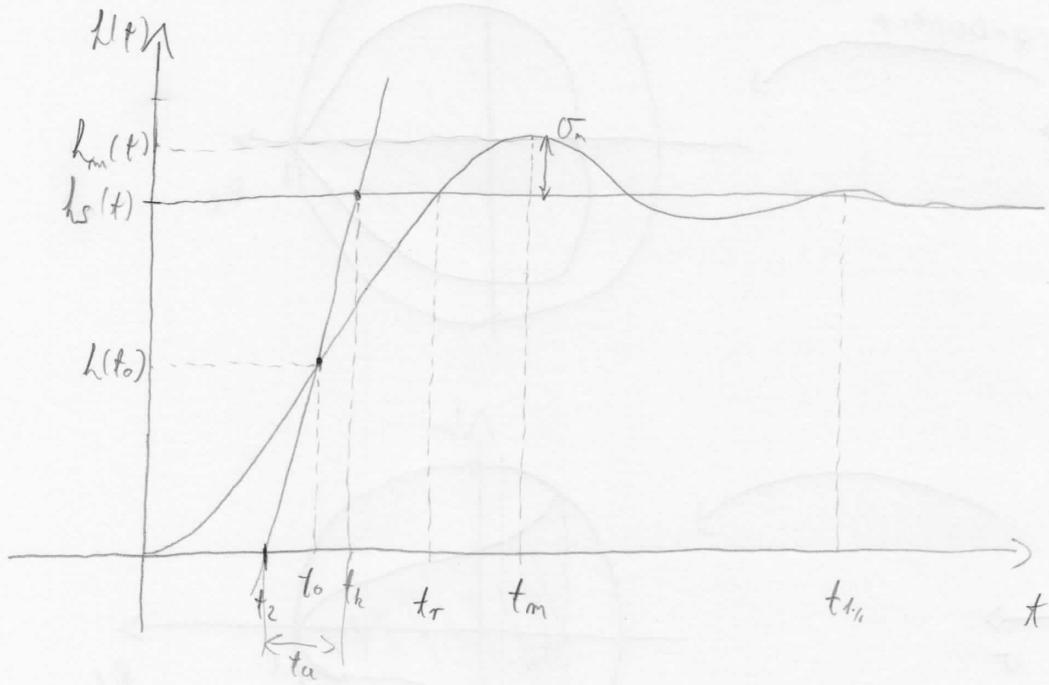
- ŠTO JE POZ BLIŽI JEDNOJ TO JAČE UTJEĆE NA SUSTAV

## III) UTJEĆAJ NA SUSTAV

- AKO JE POZ REALAN OUDA UTJEĆE NA VRIJEME DOSTIGAMO USTALJENOG STANJA [ŠTO JE BLIŽI JEDNOJ TO ODZIV SPORIJE RASJE]

- AKO SUSTAVIMA IMA KONJUGIRANO-KOMPLEKSNI PAR POZOVA OUDA JE SUSTAV OSCILATORAN TJ. ODZIV MU IMA HARMONIČKA TITRANJA [ $\tilde{P}_2(5)$ ]

POKAZATELJI KVALITETE  $\tilde{P}_2(5)$  ČLARA



$O_m$  - MAKSIMALNO NADVJESENJE

$t_m$  - VRIJEME PRVOG MAKSIMUMA

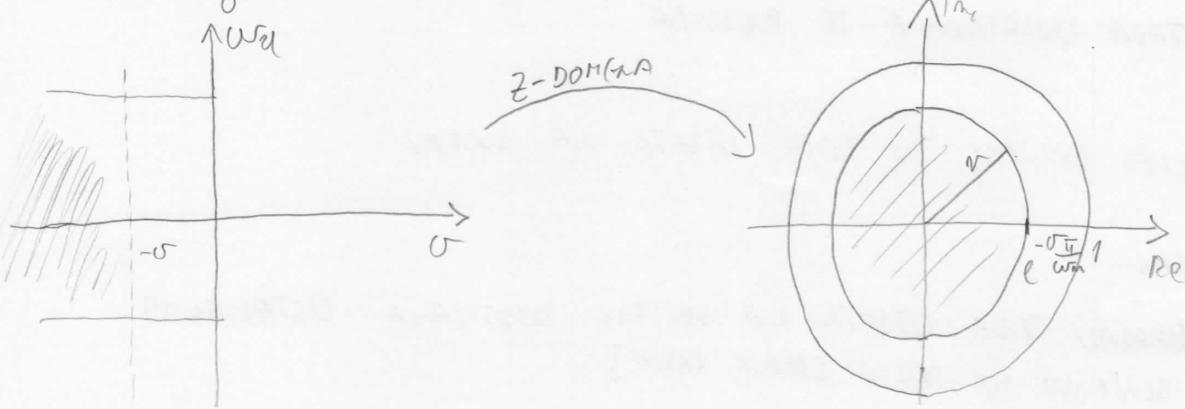
$t_r$  - VRIJEME RASTA

$t_{1,1}$  - VRIJEME USTALJIVANJA

$t_a$  - VRIJEME PONASTA

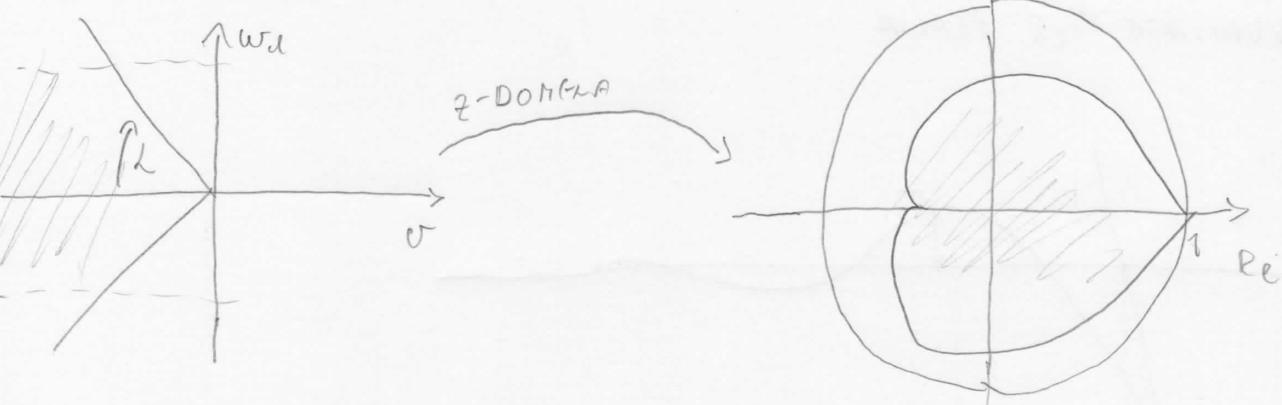
$t_z$  - VRIJEME ZADRŽAVANJA

$t_{1y} = \frac{4.6}{\sigma}$  I) VRISNA USTAVLJAVSA

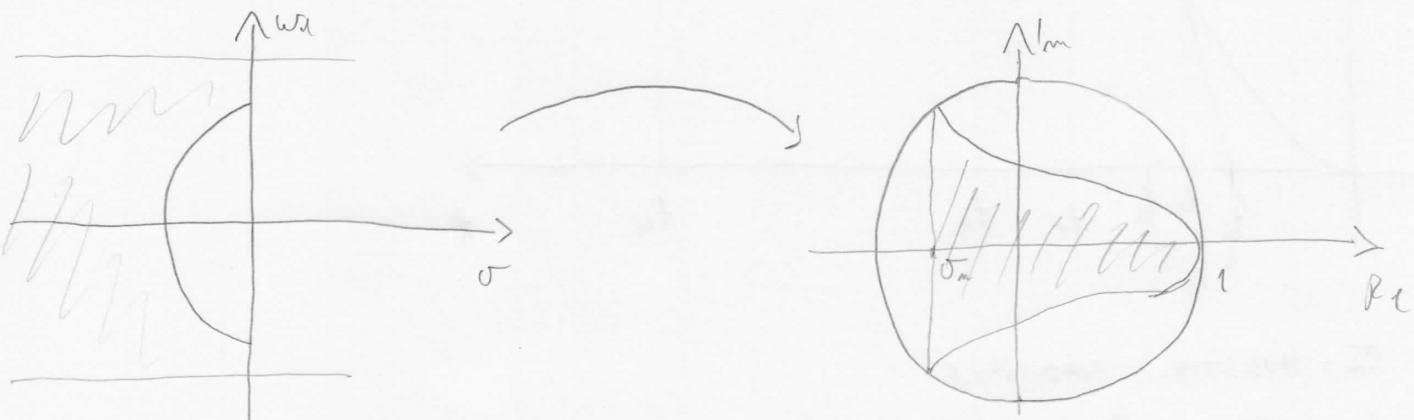


2) NADVIŠENJE

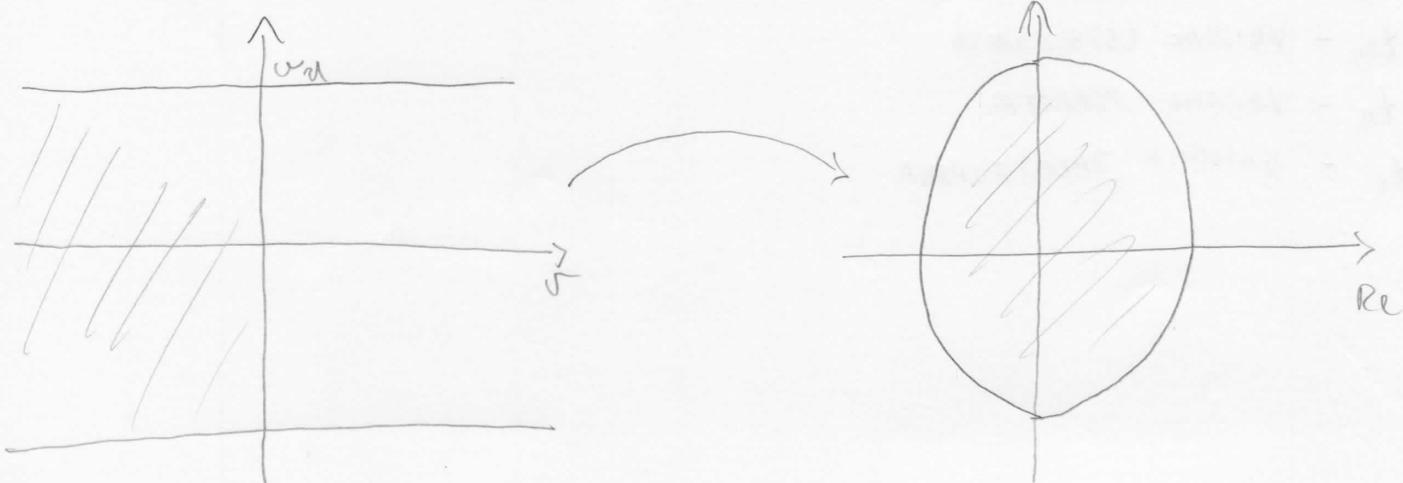
$$O_m = 100 \quad \underline{\underline{E}} = \frac{\underline{\underline{E}}_0}{1 - \zeta^2}$$



3) VRISNE RASTA  $t_r$



4) VRISNE PRVOG MAXIMA

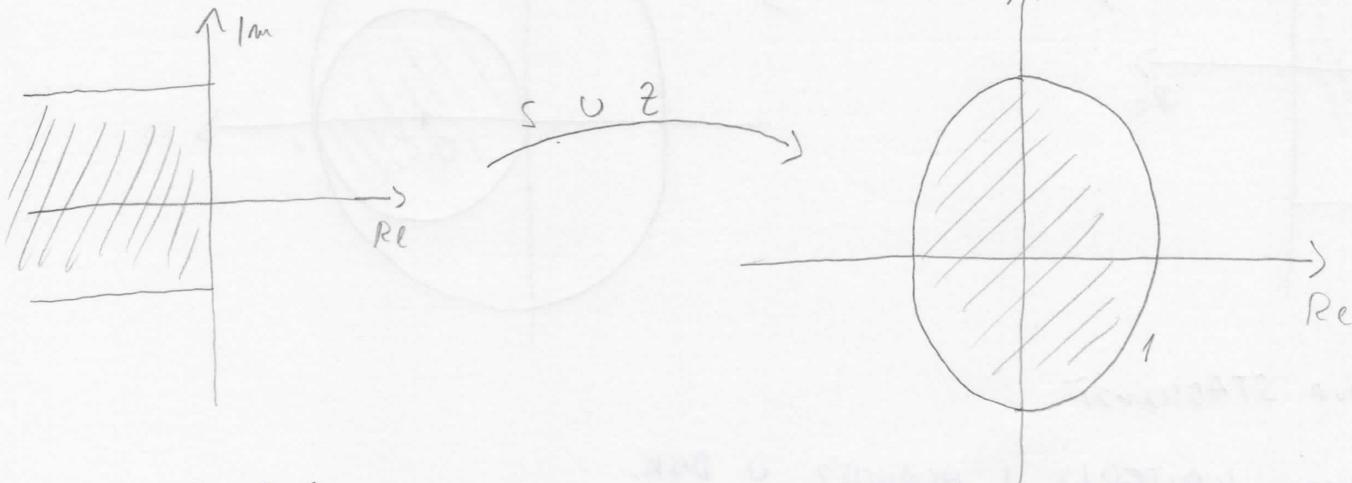


## (8) DISKRETIZACIJA

- SAMO ĆU POKAZATI KAKO SE PRESLIKAVAJU POLOVI S ODRŽAVIM DISKRETIZACIJOM

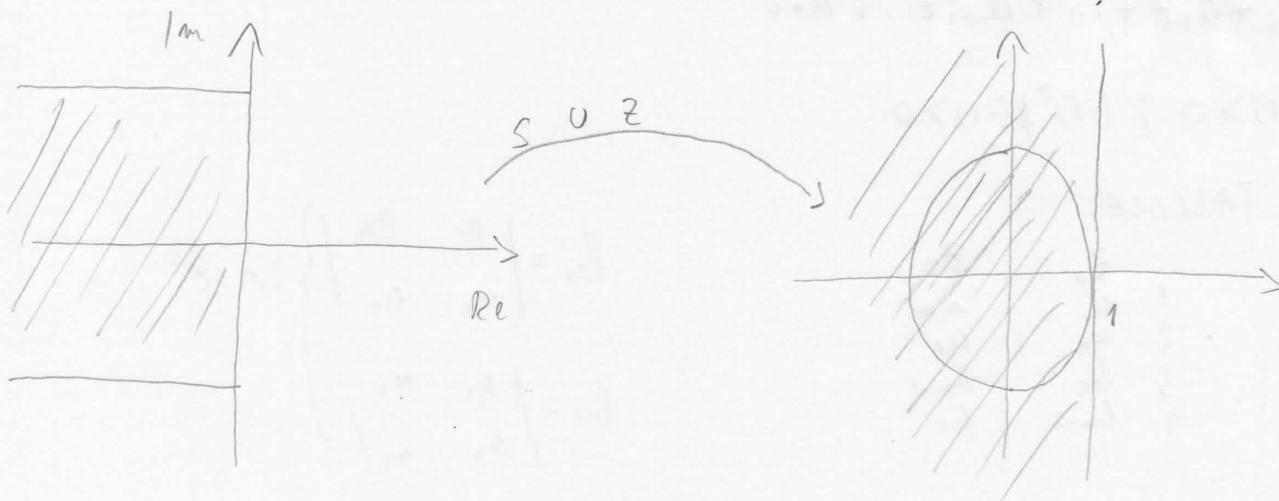
(19)

### 1) TUSTINOVА SUPSTITUCIJA



$$S = \frac{2}{T} \frac{z-1}{z+1}$$

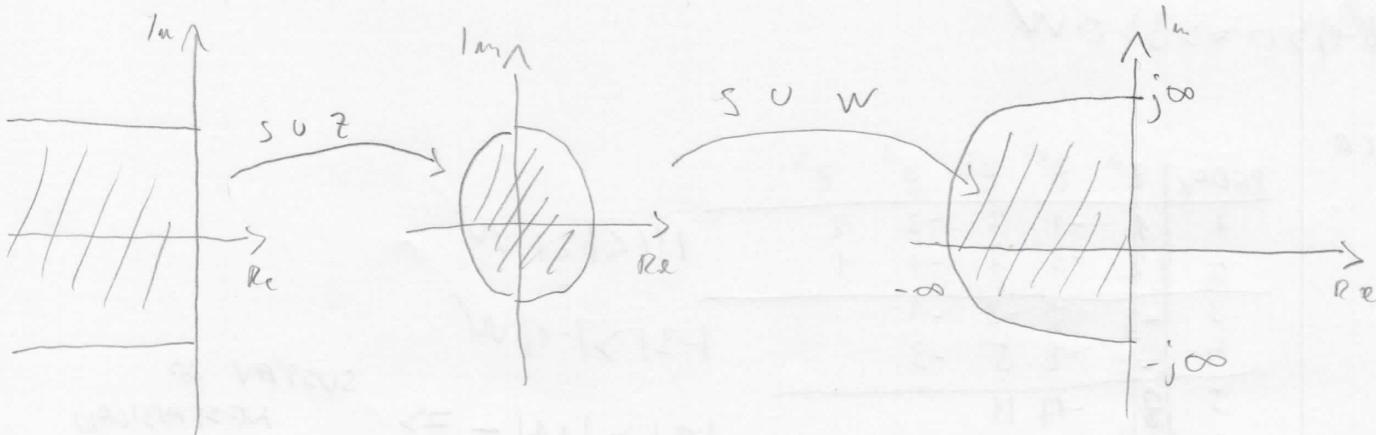
### 2) GULFOVA UNAPRISEDNA DIFFERENCIJA



$$S = \frac{z-1}{T}$$

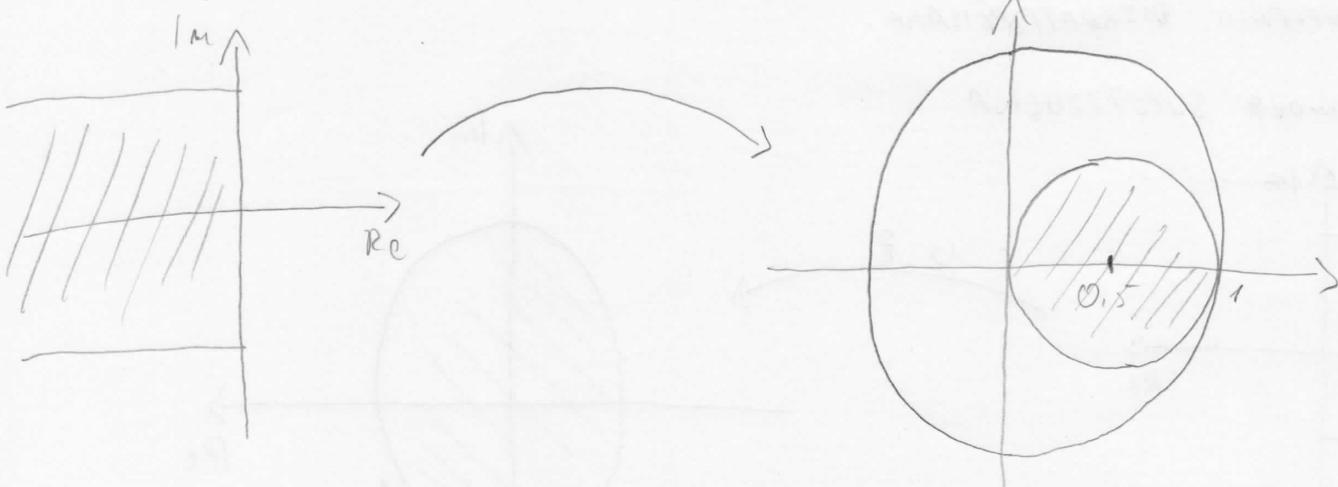
- NE ĆUVA STABILNOST SUSJAVA

### 3) BILINEARNA TRANSFORMACIJA



### 4) EULEROVA UNARADNA

$$S = \frac{1 - e^{-T}}{T}$$



- ZADRŽAVA STABILNOST

### ⑨ JURYEV KRITERIJ I HURWITZ U DISK.

1)  $f(z) = 1 + g_0 = 0$ ; kao kod Hurwitza samo sa z-vlina

$$f(z) = a_0 + a_1 z + \dots + a_{m-1} z^{m-1} + a_m z^m$$

$$\text{UVJETI: } f(1) > 0; (-1)^m f(-1) > 0$$

### 2) JURYEVA TABLICA

	$z_0$	$\dots$	$z_n$
1	$a_0$	$\dots$	$a_m$
2	$a_m$		$a_0$
3	$b_0$		$b_{m-1}$
4	$b_{m-1}$		$b_0$
		$\vdots$	

$$b_0 = \begin{vmatrix} a_0 & a_1 \\ a_m & a_0 \end{vmatrix} \quad 2) \quad z^2$$

$$b_1 = \begin{vmatrix} a_0 & a_2 \\ a_m & a_1 \end{vmatrix}$$

PRIMJER

$$f(z) = 1 - z + 2z^2 - 3z^3 + 2z^4$$

$$1) f(1) > 0 \Rightarrow 1 > 0 \checkmark$$

$$(-1)^4 \cdot f(-1) > 0 \Rightarrow 3 > 0 \checkmark$$

### 3) TABLICA

PGDAN	$z^0$	$z^1$	$z^2$	$z^3$	$z^4$
1	1	-1	2	-3	2
2	2	-3	2	-1	1
3	-3	5	-2	-1	
4	-1	-2	5	-3	
5	8	-17	11		
6	11	-17	8		

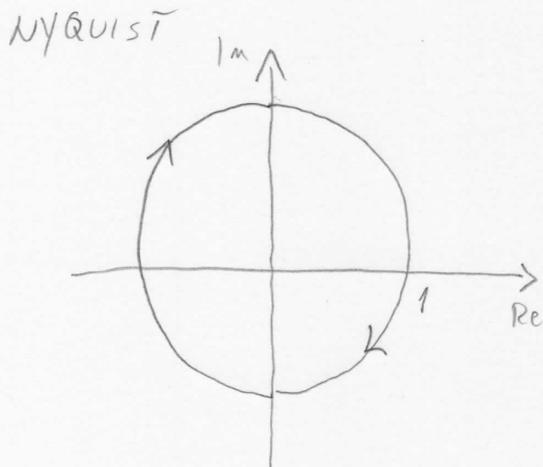
$$|1| < |2| \checkmark$$

$$|-3| > |-1| \checkmark$$

$$|8| > |11| \Rightarrow$$

SUSTAV JE  
NESTABILAN

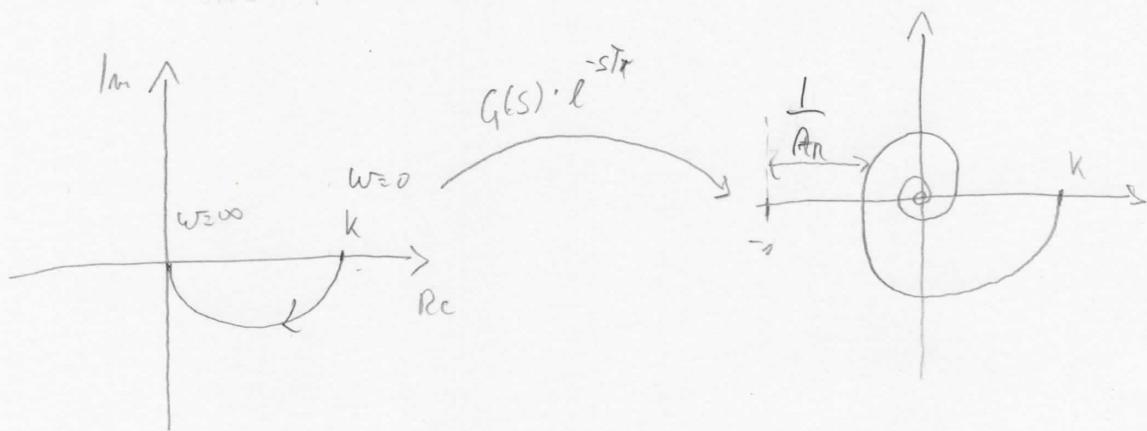
(10) VRIJSCHE KAŠLJENSA  
sít



VRIJSCHE KAŠLJENJA POKUŠAVA NYQUISTA ZAVRITI U KRUG

$$G(s) = k_e \frac{1}{Ts + 1}$$

$$G(s) = k_e \frac{e^{-sT_p}}{Ts + 1}$$



(11) STATIČKO POSAĆAMJE DISKRETEH SUSTAVA

$$\lim_{z \rightarrow 1} \frac{z-1}{z} \cdot H(z) = \lim_{z \rightarrow 1} G(z) \quad \left. \right\} \text{STATIČKO POSAĆAMJE}$$

OOSTUPAJJC

$$E(\bar{z}) = \lim_{z \rightarrow 1} \frac{z-1}{z} E(z)$$

(21)

\* KRES

(22)

SITNICE

