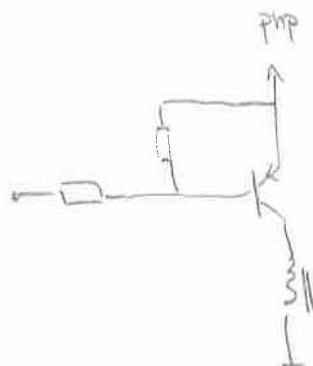
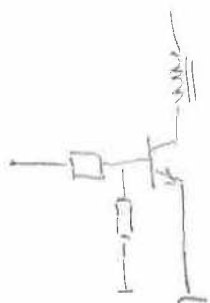


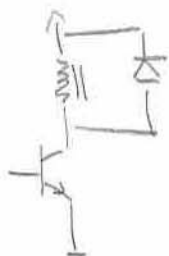
## 2 predavanie

⇒ Analýza obvodu

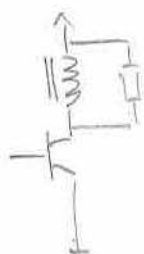
⇒ upravljanje i zaštita obkru



1) Zákida



obkru s goni sporo





bře se prací



→ odstupující režim d. složení

1) vstupní / DC

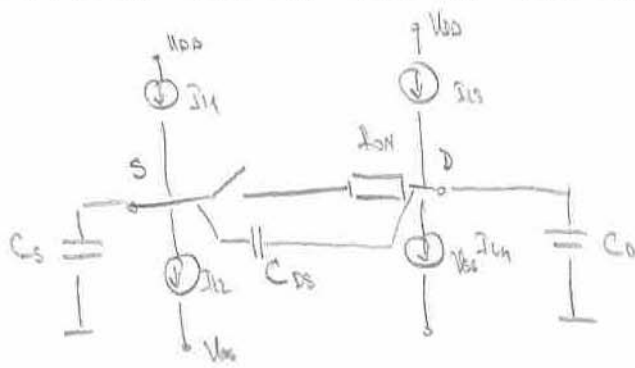
- hradlové odpory a vodivost
- šířka ověření

2) výstupní

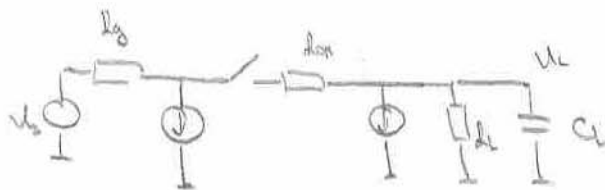
- parazitní kapacit

3) tranzistorové zpoždění

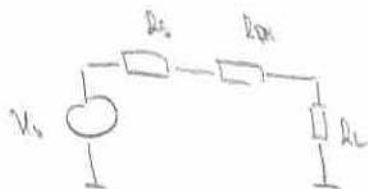
- výhledová rychlost



1) istovremena odslupanja



$$\Delta U = U \cdot R_{LH} (R_{ON} + R_S)$$



$$U_L = V_S \cdot \frac{R_L}{R_S + R_{ON} + R_L}$$

za.  $R_S = \phi$

$$U_L = V_S \cdot \frac{R_L}{R_{ON} + R_L}$$

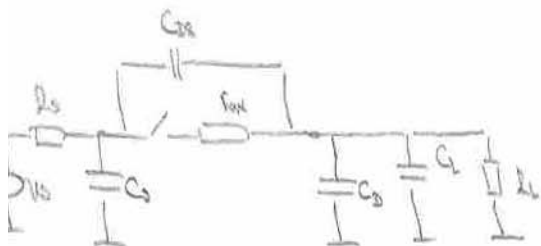
log

$$\log U = \log U_s + \log \frac{R_L}{R_{in} + R_L}$$

$20 \log \frac{R_L}{R_{in} + R_L} \leftarrow$  Uvenci gubitak (insertion loss)  
 $\downarrow$   $\Rightarrow$  veći napon napajanja ( $U \uparrow \Rightarrow R_{in} \downarrow$ ) ;  
 temperature ( $T \uparrow \Rightarrow R_{in} \uparrow$ )

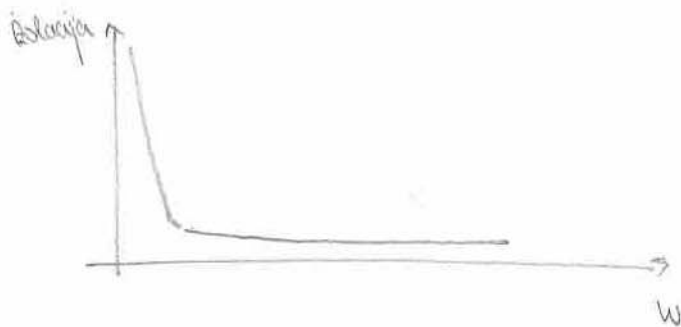
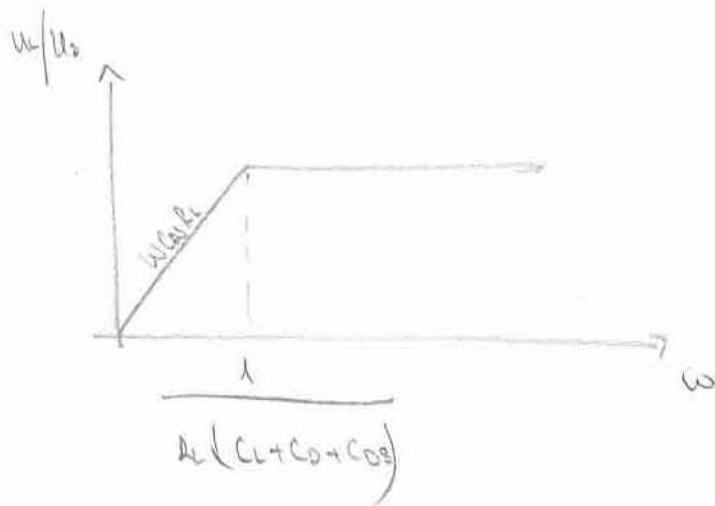
2) Izračunajte pogrešku

$\Rightarrow$  izračunajte slope



$R_s = \phi$  ;  $C_s$  zadržavajući

$$U_L = U_s \cdot \frac{R_L / [1 + j\omega(C_s + C_L)R_L]}{\frac{1}{j\omega C_s} + \frac{R_L}{1 + j\omega(C_s + C_L)R_L}} = U_s \cdot \frac{j\omega C_s R_L}{1 + j\omega R_L (C_s + C_L + C_s)}$$



Atenuacija lošija za  $\uparrow C_0$  i  $\uparrow R_0$

waye to resultu povećanju insertion loss-a

pr. 1)

A bitu

$$R_0 = 10\Omega; R_1 = 100k\Omega; R_2 = 10M\Omega$$

$$R_1 = \frac{100k\Omega}{10\Omega + 100k\Omega}$$

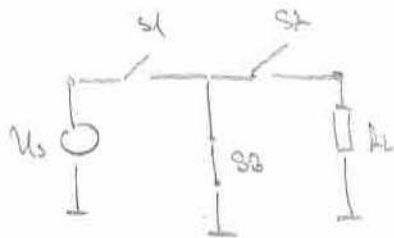
$$R_2 = \frac{10M\Omega}{10\Omega + 10M\Omega}$$

b

Atenuacija to no da bolja

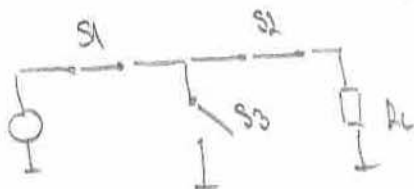
$$\cos \phi = 0,1 - 5 \text{ pF}$$

⇒ T obloga (dobro II ; dobra izolacija)



1. Zadržano s don S<sub>2</sub>

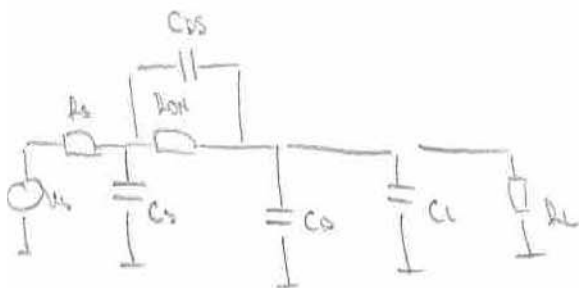
Ustav



don S1

don S2

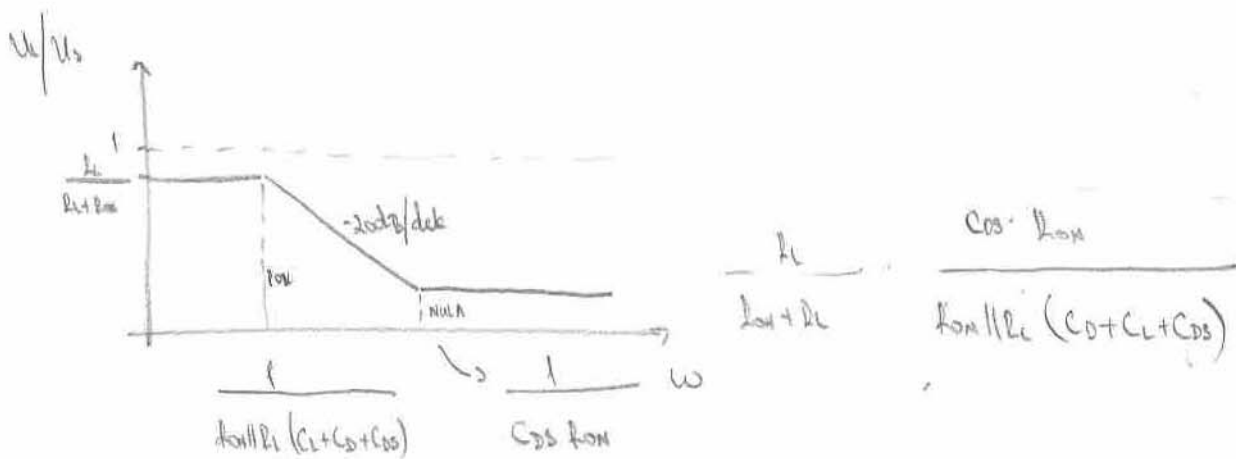
⇒ nloga obloga / impedancija obloga



$R_s \neq \phi \Rightarrow C_s$  Zadržano

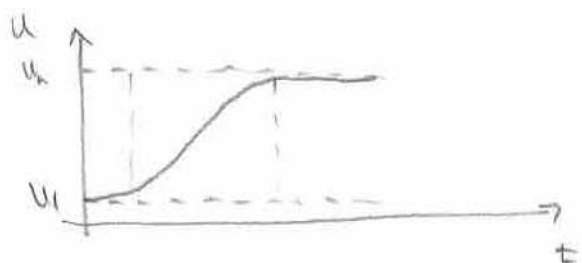
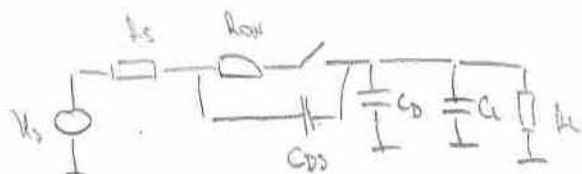
$$U_L = U_S \cdot \frac{L_L / [1 + j\omega(C_L + C_D)L_L]}{L_{on} / [1 + j\omega C_{DS}L_{on}] + L_L / [1 + j\omega(C_L + C_D)L_L]}$$

$$U_L = U_S \cdot \frac{L_L}{L_L + L_{on}} \cdot \frac{1 + j\omega C_{DS}L_{on}}{1 + j\omega L_{on} \parallel L_L \cdot (C_L + C_D + C_{DS})}$$



3) tranzijentne pogreške

3.1) preklapanje / vrijeme snimanja



$$\tau = [(L_S + L_{on}) \parallel L_L] (C_L + C_D)$$

$$u(t) = (u_1 - u_2) e^{-t/\tau} + u_2$$

$$e(t) = |u(t) - u_2| = (u_1 - u_2) e^{-t/\tau}$$

$$e \rightarrow \text{relat. prog} = \frac{e(t)}{u_1} = \left| \frac{u_1 - u_2}{u_1} \right| e^{-t/\tau}$$

$$\text{za } u_1 = 0 \quad ; \quad u_2 = U_{\text{ref}}$$

$$e = e^{-t/\tau}$$

$$\tau_E = -\tau \ln E$$

$$\tau = R(C_1 + C_0)$$

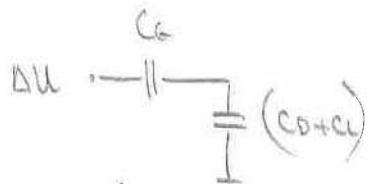
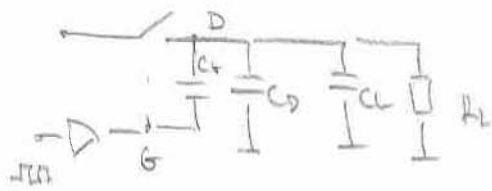
ON-OFF

Pr. 2)

$$\left| \begin{array}{l} e < \frac{\text{LSB}}{2} \\ e^{-t/\tau} < \frac{1}{2} \cdot \frac{1}{2^N} \end{array} \right|$$



## 3.2) injektiranje naboja / charge injection



$$\Delta Q = \Delta U \cdot (C_G \parallel (C_D + C_L))$$

$$= \Delta U_L \cdot (C_D + C_L)$$



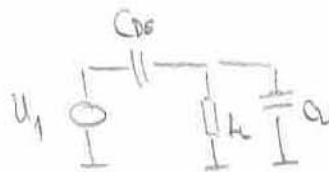
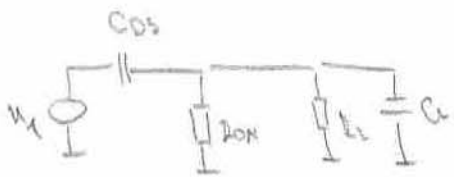
## 4) dodatne pogreške mux (prelivanja)

### 4.1) statičko prelivanje (static crosstalk)

### 4.2) dinamičko prelivanje

### 4.2) prelivanje (vraćajući) susjednih kanala

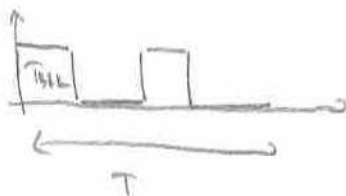
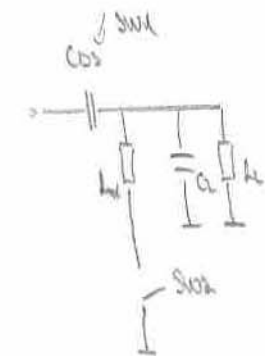
#### 4.1) statično preiskovanje



preiskovanje VH s togo sklopa

#### 4.2) dinamično preiskovanje

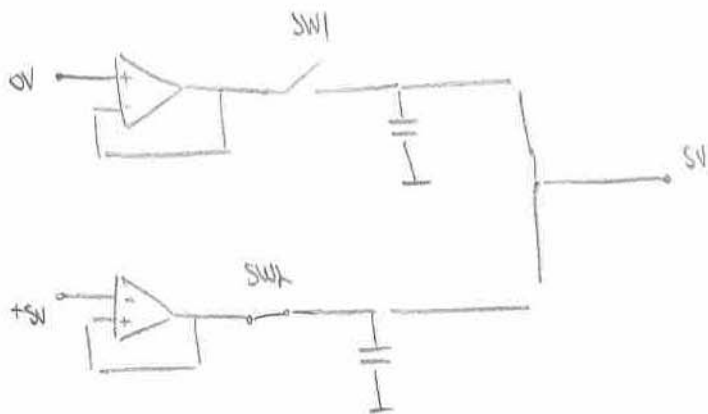
"break before make sloboje"

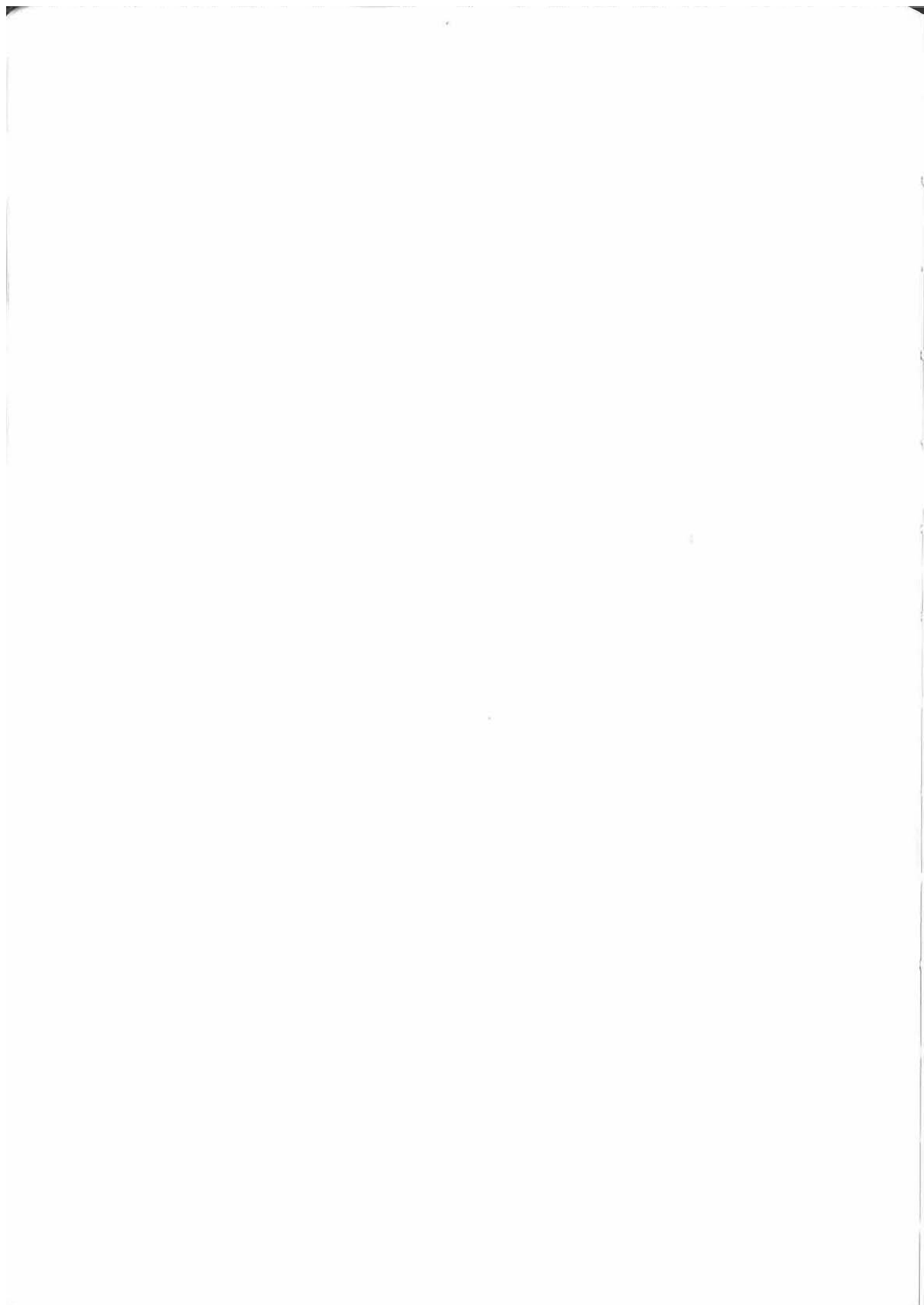


$$I_{\text{avg}} = \frac{I_L \cdot 2T_{\text{on}} + I_{\text{off}}(T - 2T_{\text{on}})}{T}$$



4.3) prečišćavanie (mimochi) uspešne kanala  
odjucet chavud chotalk  
charge injection chotalk

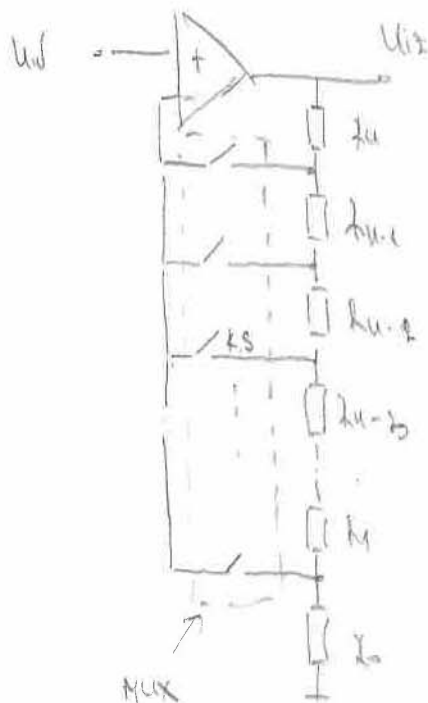




# Zadaci iz Elektroničke instrumentacije

1. dio

- 1) Nacrtajte shemu nelinearnog program. pojačala i opišite način rada. U čemu ovaj tip pojačanja takvog pojačala?



$$A = 1 + \frac{\sum_{i=1}^n Z_i}{Z_0}$$



opisna mreža (kako pojačanje tipično 1, 2, 5, 10, ..., 500, 1000)

čvrst pojačanje ovako :

1) blagotajana otpor otpornika u težišnoj mreži

2) impedancijski slopke

↳

analogne slopke u 76A

→ relativno laki spoj ima ovakvi otpor između 10  $\Omega$  i 100  $\Omega$ ; utjecaj otpora slopke u vertikalnom i horizontalnom iznosu odabira topologije ;  
na višim frekvencijama do izražaja dolaze parazitski kapaciteti slopke

proječna pojačanja

višeje potrebno da se grupni pojačanje i da se izlazi napona stabilizira p zbroj

→ manja potreba za godinama slopke

→ manja smanjenje izlaznog napona pojačala

2) Vporek tipe tehnologije analogne sheme razlikujemo po ih  
 ugraditve

	Snaga	opor u vrednosti	max. frek. prelopašnja	opor u vrednosti
Relaji	1000V / 25A	1M $\Omega$	50-250 kHz	10 <sup>10</sup> $\Omega$ (200k)
Med- relaji	200V / 50mA	1M $\Omega$ - 1k $\Omega$	1 kHz	10 <sup>12</sup> $\Omega$ (vakuum)
Poluvodnički diodni	1000V / 5A	10M $\Omega$ - 3 $\Omega$	10 MHz	10 <sup>10</sup> $\Omega$
Poluvodnički integrirani	50V / 50mA	1 $\Omega$ - 200 $\Omega$	100 MHz (do 6 Hz)	10 <sup>10</sup> $\Omega$

→ elektronika - minimalni lom, opora, velika dimenzije

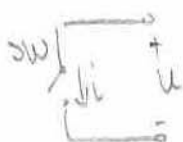
→ elektronika (silicij) - relativno veliki lom, ovise o priključnom  
 naponu i temperaturi

parazitni kapaciteti mogu utjecati na AC

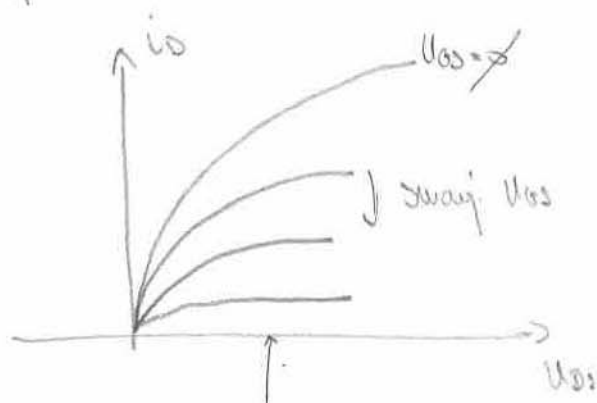
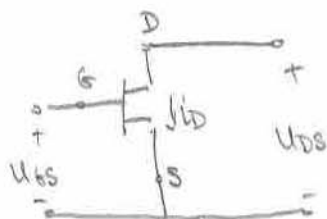
karakteristike ciklopusnog shema

3) Upotreb analognih sklopke u integriranim krugovima, tehnologije u kojima se izrade te ili usporedite!

1) Idealna analogni sklopka



2) n-kanalna JFET sklopka



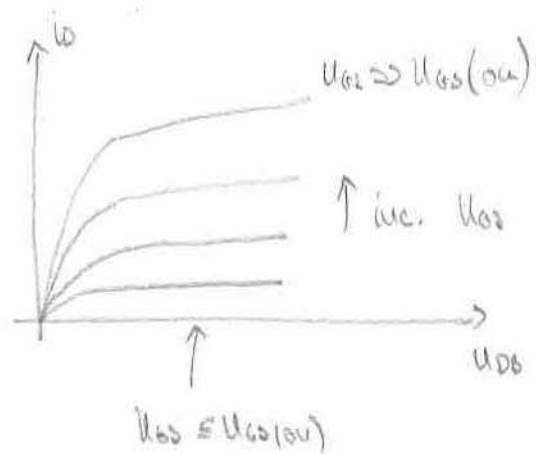
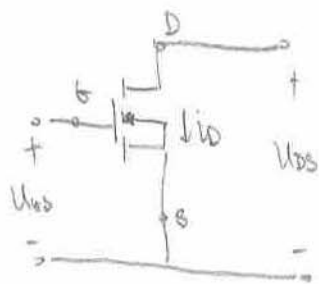
$$u_G \leq u_{GS(off)}$$

$$\frac{\Delta i_D}{\Delta u_{GS}} = \frac{1}{r_{DS(on)}}$$

3) p-kanalna JFET sklopka



#### 4) n-kanalna MOSFET sklopla

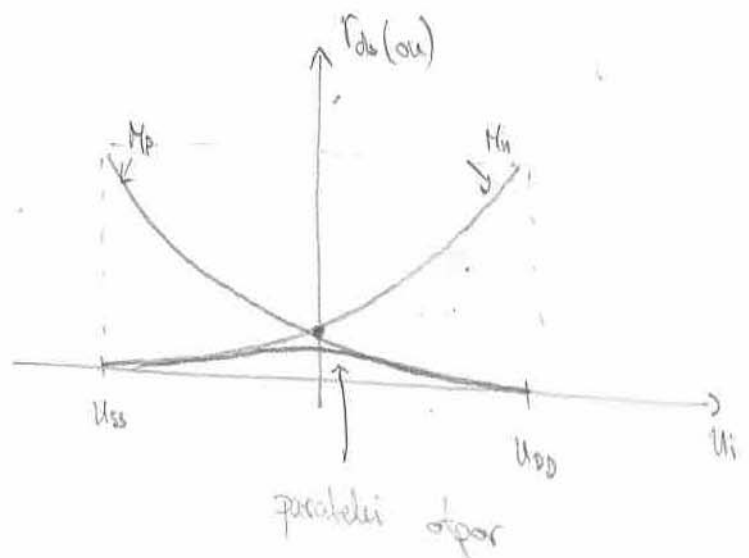
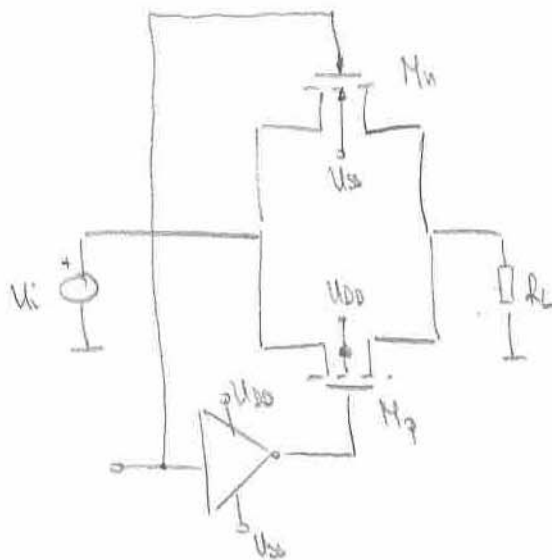


n-MOSFET :  $U_{gs(sat)} > 0$

ON:  $U_{gs} \geq U_{gs(sat)}$

OFF:  $U_{gs} = 0$

#### 5) CMOS sklopla



ON: p-MOS :  $U_{gs} \leq U_{gs(sat)} < 0$

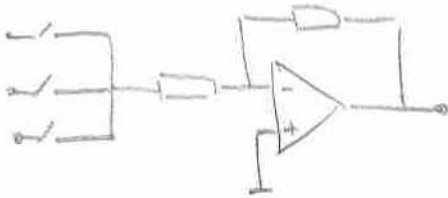
OFF: p-MOS :  $U_{gs} \geq 0$

4) Opšte ije načine rada razlikuju kod analognih stepeni  
u integriranim izgovorima

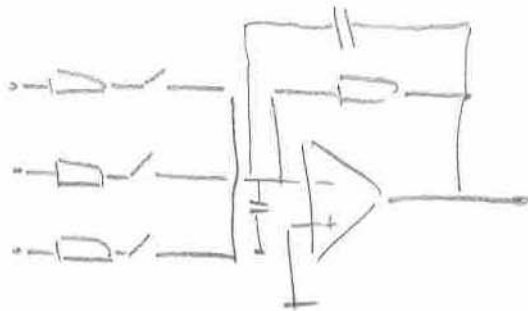
### 3. predavanje

4.4) spajanje sledila na izlaz

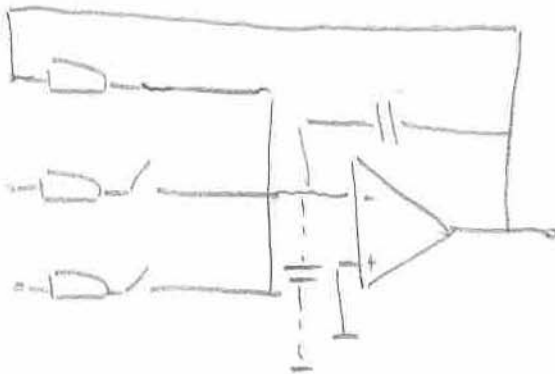
a)



b)

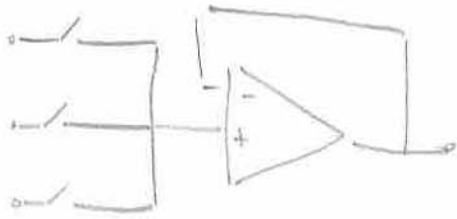


c)



neinvertirajuće razlike

2) integrator



### 3. Programabilni slopari

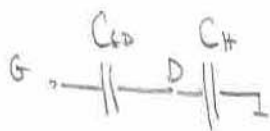
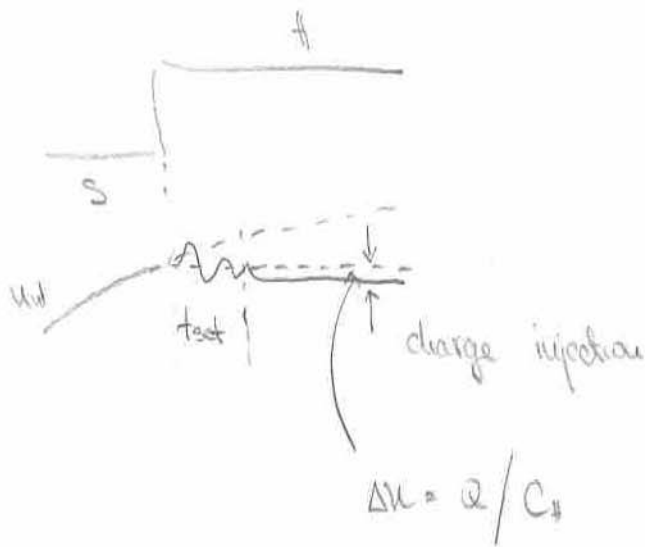
1) Sample & hold

1.1) vezovanje

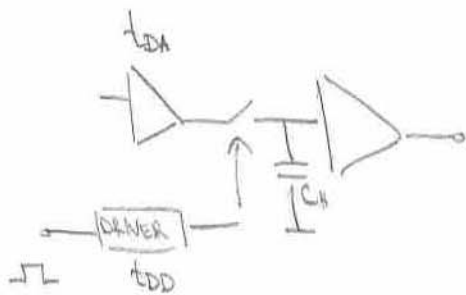
- => poroška poročanja
  - => funkcionalna karab. slopar
  - => parat nile
  - => udeležnost slopar
- } sample

- => efektivno njeve otvaranja (aperture time)
  - => njeve zadržanja (setting time)
  - => injektivna uaboga (charge injection)
- } sample -> hold

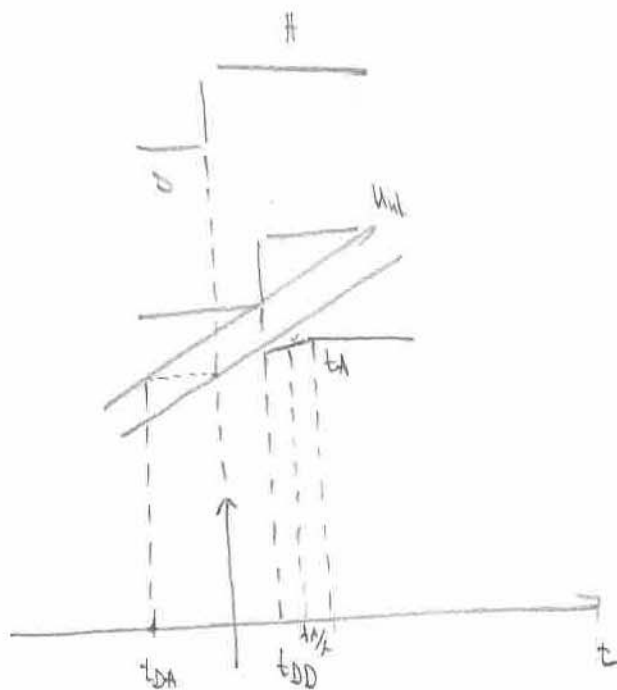
→ negative sensitivity



→ aperture noise



$$t_{ca} = t_{DD} + t_{A/2} - t_{DA}$$



→ apertura usgurust (aperture jitter)



→ kizanje zadrzaniy napru  
(drop rate)

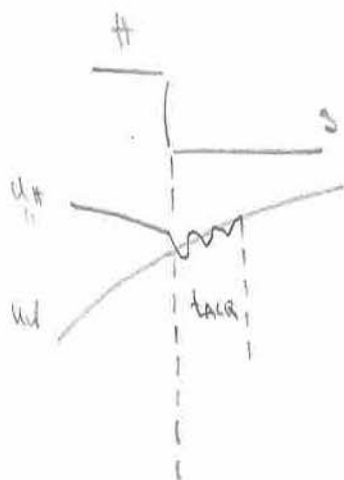
→ stuzje curuzja

$$\frac{du}{dt} = \frac{I_{x16}}{C_H}$$

} hold

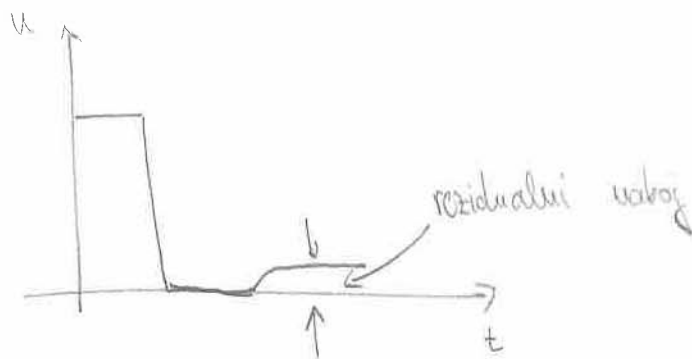
→ poslusaniye (feetthrough)

→ vijune aluzizije



} hold → sample

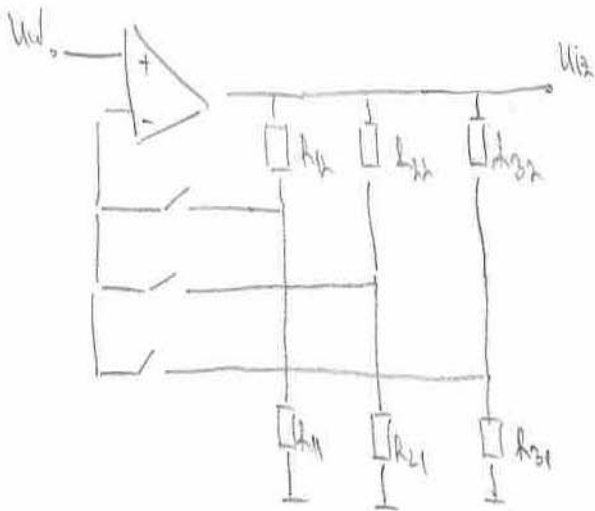
⇒ pogreška uslijed dielektrične apsorpcije





# 1. auditorske vježbe

1.



$$A_1 = 500 \quad ; \quad A_2 = 100 \quad ; \quad A_3 = 5$$

odaber.  $R_{11} = R_{22} = R_{31} = 1\text{ k}\Omega$

$$A = 1 + \frac{R_2}{R_1}$$

$$A_1 = 500 \Rightarrow R_{12} = 499\text{ k}\Omega$$

$$A_2 = 100 \Rightarrow R_{22} = 99\text{ k}\Omega$$

$$A_3 = 5 \Rightarrow R_{32} = 4\text{ k}\Omega$$

$$dA = \frac{\partial A}{\partial R_1} dR_1 + \frac{\partial A}{\partial R_2} dR_2$$

$$dA = -\frac{1}{R_1} dR_1 + \frac{1}{R_2} dR_2 \quad / : A$$

$$\frac{dA}{A} = \frac{1}{A} \left[ -\frac{R_2}{R_1} \cdot \frac{dR_1}{R_1} + \frac{R_2}{R_1} \cdot \frac{dR_2}{R_2} \right]$$

$$\frac{dA}{A} = \frac{1}{A} \cdot \frac{R_2}{R_1} \left[ -\frac{dR_1}{R_1} + \frac{dR_2}{R_2} \right]$$

1) uajgori shlyaj

$$\frac{dR_1}{R_1} = -\frac{dR_2}{R_2} = \delta$$

$$\left| \frac{dA}{A} \right| < \varepsilon$$

$$\frac{1}{A} \cdot \frac{R_2}{R_1} \cdot 2\delta < \varepsilon$$

$$\delta < \frac{\varepsilon A}{2 R_2 / R_1}$$

$$\delta < \frac{\varepsilon}{2} \left( 1 + \frac{R_2}{R_1} \right)$$

$$\delta < \frac{0,1\%}{2} \left( 1 + \frac{1k\Omega}{499k\Omega} \right) = 0,05\%$$

2.

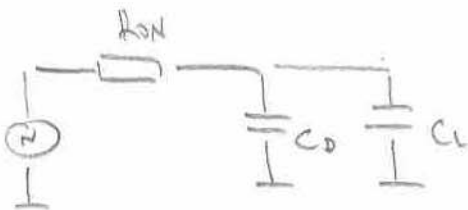
$$U_{in} = 1V$$

$$f = 100 \text{ kHz}$$

$$R_{on} = 100 \Omega$$

$$C_D = 5 \text{ pF}$$

$$C_L = 15 \text{ pF}$$

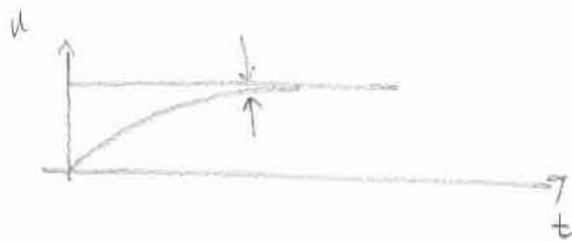


$$A = \frac{\frac{1}{j\omega(C_D + C_L)}}{R_{on} + \frac{1}{j\omega(C_D + C_L)}} \cdot \frac{1}{j\omega R_{on}(C_D + C_L) + 1}$$

$$\tau = R_{on}(C_D + C_L) = 2 \mu s$$

$$|A| = \frac{1}{\sqrt{1 + \omega^2 \tau^2}} = 1$$

$$\varphi = -\arctan(\omega \tau) = 0 \text{ p}^\circ$$



$$N \cdot e^{-t/\tau} < \frac{1.8B}{2}$$

$$t_s = -\tau \ln\left(\frac{1}{2} \cdot 1.8B\right)$$

$$t_s = -2\mu s \ln\left(\frac{1}{2} \cdot \frac{2V}{2 \cdot 1V}\right)$$

3.

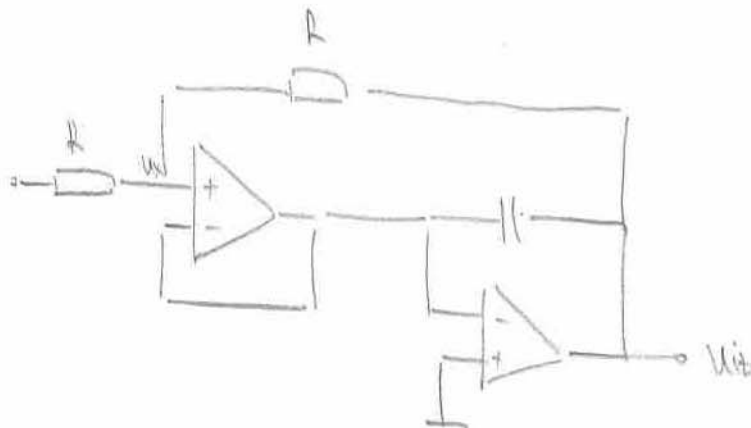
$$C_{GD} = 1 \text{ pF}$$

$$C_H = 1 \text{ nF}$$

$$I_{CCS} = 1 \text{ nA}$$

$$U_{ul} = 1 \text{ V}$$

$$t = 50 \text{ ns}$$



$$\frac{U_{ul} - U_X}{R} = \frac{U_X - U_{iz}}{R}$$

$$U_{ul} - U_X = U_X - U_{iz}$$

$$U_{ul} + U_{iz} = 2U_X$$

$$U_X = 0$$

$$U_{ul} = -U_{iz}$$

1) isjetkaja uobija



$$\Delta Q_{GD} = \Delta U_{GD} \cdot C_{GD} = -15 \text{ V} \cdot 1 \text{ pF} = -15 \text{ pC}$$

$$\Delta Q_H = \Delta Q_{GD}$$

$$\Delta U_H = \Delta Q_H \cdot \frac{1}{C_H} = -15 \text{ mV}$$

$$U_{i2} = U_{i1} - \Delta U_{\#} = -1V + 15\mu V = -985\mu V \quad \text{at } t = 0$$

$$t = 50 \mu s$$

$$C_{\#} \cdot \Delta U_{i2} = I_1 \cdot \Delta t$$

$$\Delta U_{i2} = \frac{1 \mu A \cdot 50 \mu s}{C_{\#}} = 50 \mu V$$

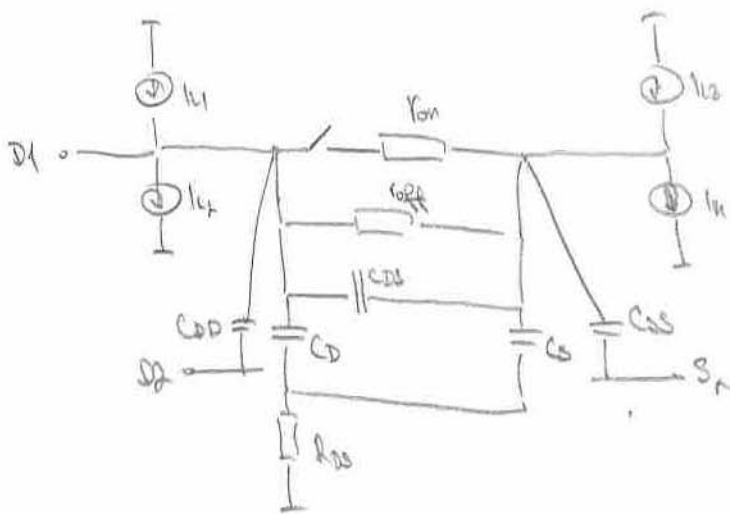
$$U_{i2} = -985\mu V + 50\mu V = -935\mu V$$

# Zadaci iz Elektronike instrumentacije

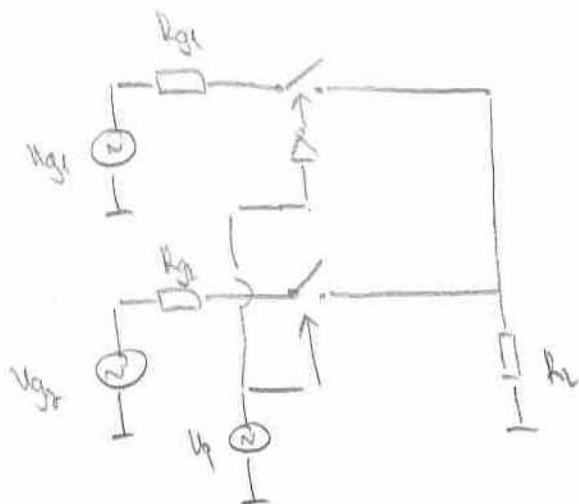
1. dio

→ nastavak

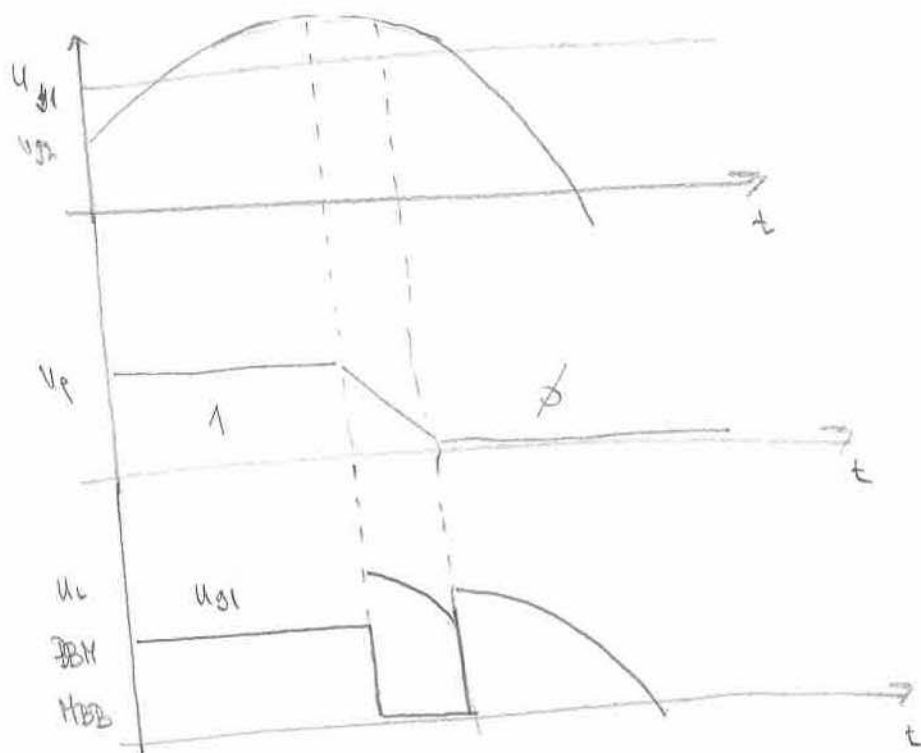
- 4) Pošte koje rade u području različitih analognih slopki  
u integriranim kugovima



- 1) BBM (Break before make) - kod. vjerojatnije slopki prikladan  
promjene položaja događa se. prvo se stari kontakt (tj. signal)  
prekinu, pa se spoji novi (otvorena petlja pos. vese,  
stabilizacija pojicata, oscilacije slopova)
- 2) HBB (Make before break) - prvo se spoji novi signal,  
pa se odspoji stari (kratki spigori, veliki različitih suaga)



verwende diagram





1 audiotone

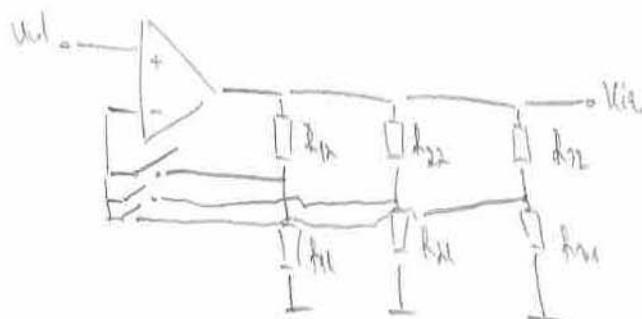
→ downaci 100

$$A_1 = 500$$

$$A_2 = 100$$

$$A_3 = 5$$

$$\varepsilon = 0,1\%$$



$$R_{11} = R_{21} = R_{31} = 1 \text{ k}\Omega$$

$$A = 1 + \frac{R_{12}}{R_{11}}$$

$$A_1 = 1 + \frac{R_{12}}{R_{11}} \Rightarrow$$

$$A_1 - 1 = \frac{R_{12}}{R_{11}} \Rightarrow R_{12} = (A_1 - 1) \cdot R_{11} = 499 \text{ k}\Omega$$

$$R_{22} = 20 \text{ k}\Omega$$

$$R_{32} = 4 \text{ k}\Omega$$

$$A = 1 + \frac{R_{12}}{R_{11}}$$

$$dA = \frac{\partial A}{\partial R_{11}} dR_{11} + \frac{\partial A}{\partial R_{12}} dR_{12}$$

$$dA = \frac{-R_{12}}{R_{11}^2} dR_{11} + \frac{1}{R_{11}} dR_{12}$$

$$dA = \frac{-R_2}{R_1} \frac{dR_1}{R_1} + \frac{R_2}{R_1} \cdot \frac{dR_2}{R_2} : A$$

$$\frac{dA}{A} = \frac{1}{A} \left[ -\frac{R_2}{R_1} \frac{dR_1}{R_1} + \frac{R_2}{R_1} \frac{dR_2}{R_2} \right]$$

$$\frac{dA}{A} = \frac{1}{A} \cdot \frac{R_2}{R_1} \left[ -\frac{dR_1}{R_1} + \frac{dR_2}{R_2} \right]$$

najgori slučaj

$$\frac{dR_2}{R_2} = \delta = -\frac{dR_1}{R_1}$$

$$\frac{dA}{A} = \frac{1}{A} \cdot \frac{R_2}{R_1} \cdot 2\delta$$

pogreška proračuna manja od 0,1%

$$\left| \frac{dA}{A} \right| < \varepsilon$$

$$\left| \frac{1}{A} \cdot \frac{R_2}{R_1} \cdot 2\delta \right| < \varepsilon$$

$$\Delta < \frac{\epsilon \cdot A \cdot R_1}{R_2}$$

$$\left| \Delta < \frac{\epsilon \cdot A \cdot R_1}{2 R_2} = \epsilon \cdot \frac{\lambda}{2} \left( 1 + \frac{R_2}{R_1} \right) \frac{R_1}{R_2} \right.$$

$$\Delta < \epsilon \frac{\lambda}{2} \left( 1 + \frac{R_2}{R_1} \right)$$

$$\Delta A = 500$$

$$R_1 = 1 \text{ km}$$

$$R_2 = 400 \text{ km}$$

$$\Delta < 5,01 \cdot 10^{-4}$$

2.

$$U_{in} = 1V$$

$$f = 100kHz$$

$$R_{on} = 100\Omega$$

$$C_D = 5pF$$

$$C_L = 15pF$$

1/2 LSB

16-bitni ADP

 $\pm 1V$  ulazni opseg

$C_D$  ne igra nikakvu ulogu, bez unutarnjeg  
 otpora generatora; a  $C_{SS}$  zamenjuje se u

ON načinu rada

$$C = C_D + C_L$$

$$\tau = R_{on}C = R_{on}(C_D + C_L) = 100\Omega \cdot 20pF = 2ns$$

$$U_{iz} = U_{ul} \cdot \frac{\frac{1}{j\omega C}}{R_{on} + \frac{1}{j\omega C}} = U_{ul} \cdot \frac{\frac{1}{j\omega C}}{\frac{R_{on}j\omega C + 1}{j\omega C}}$$

$$= U_{ul} \cdot \frac{1}{1 + j\omega R_{on}C} = U_{ul} \cdot \frac{1}{1 + j\omega\tau}$$

$$|u_2| = |u_1| \frac{1}{\sqrt{1 - \omega^2 \tau^2}} \approx |u_1|$$

$$\varphi = 0 - \arctan(\omega \tau) \approx -0,072^\circ$$

$$IV. \quad e^{-\frac{t_s}{\tau}} < \frac{1}{2} \text{ LSB} \quad / \quad \ln$$

$$-\frac{t_s}{\tau} < \ln \left[ \frac{1}{2} \text{ LSB} \right]$$

$$t_s > -\tau \ln \left[ \frac{1}{2} \text{ LSB} \right]$$

$$\text{LSB} = \frac{U_{FS}}{2^{16}} = 30,52 \mu\text{V} \quad \curvearrowright$$

B.

$$C_{GD} = 1 \text{ pF}$$

$$C_H = 1 \text{ nF}$$

$$I_L = 1 \text{ nA}$$

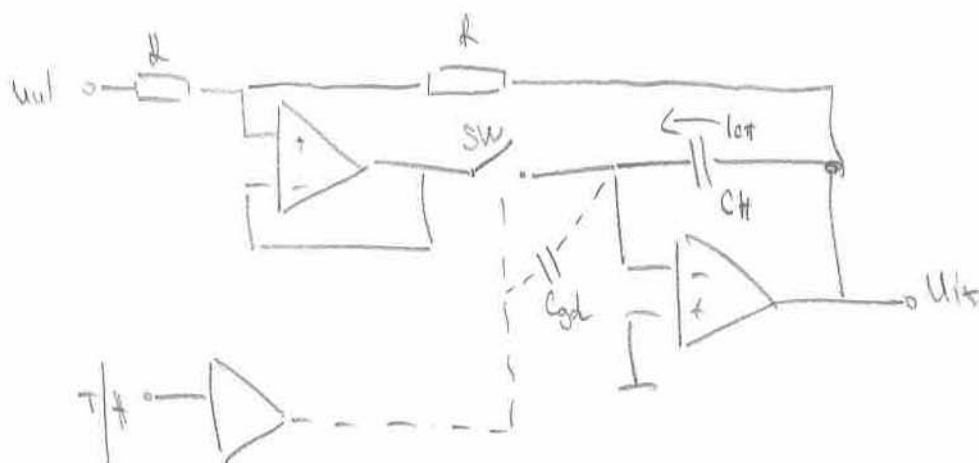
$$U_{in} = 1 \text{ V}$$

$$U_{i2} = 0$$

$$t = 50 \text{ ns}$$

N-JFET

$$0 \text{ V} - 15 \text{ V}$$



$$\frac{U_{in} - U_x}{R} = \frac{U_x - U_{i2}}{R} \quad \text{---} \cdot R$$

$$U_{in} - U_x = U_x - U_{i2}$$

$$\underline{U_x = 0}$$

$$U_{in} = -U_{i2}$$

$$\Delta Q_{GD} = -15 \text{ V} \cdot C_{GD} = -15 \text{ pC}$$

↓ naboj koji je dano do CH

$$\Delta U_{i2} = \frac{-\Delta Q_{GD}}{C_H} = 0,015 \text{ V}$$

$$U_{i2} = -U_{in} + \Delta U_{i2} = -0,975 \text{ V}$$

$$T = 50 \text{ ns}$$

$$C_H \cdot \Delta U_{i2} = I_L \cdot T \Rightarrow \Delta U_{i2} = \frac{I_L \cdot T}{C_H}$$

$$U_{i2} = U_{i2} + \Delta U_{i2} = 0,935 \text{ V}$$

1.

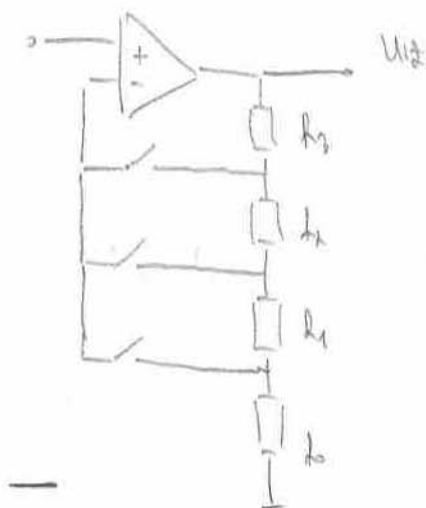
$$A_1 = 5$$

$$A_2 = 100$$

$$A_3 = 500$$

$$\varepsilon = 0,1\%$$

$$R_0 = 1 \text{ k}\Omega$$



$$A_1 = 1 + \frac{R_2}{R_1 + R_0}$$

$$A_1 = \frac{R_2}{R_1 + R_0} \Rightarrow \boxed{R_0 = 4R_2 + 4R_1 + 4R_0}$$

$$A_2 = 1 + \frac{R_3 + R_4}{R_1 + R_0}$$

$$A_2 = \frac{R_3 + R_4}{R_1 + R_0} \Rightarrow R_3 + R_4 = 99R_1 + 99R_0$$

$$\boxed{R_0 = 99R_1 + 99R_0 - R_2}$$

$$A_3 = 1 + \frac{R_1 + R_2 + R_3}{R_0}$$

$$499 = \frac{R_1 + R_2 + R_3}{R_0} \Rightarrow$$

$$\boxed{499 R_0 = R_1 + R_2 + R_3}$$

$$4R_2 + 4R_1 + 4R_0 = 99R_1 + 99R_0 - R_2$$

$$5R_1 + 95R_0 - 5R_2 = 0$$

$$\boxed{5R_1 - 5R_2 = -95R_0}$$

$$4R_2 + 4R_1 + 4R_0 = -R_2 - R_1 + 499R_0$$

$$\boxed{5R_2 + 5R_1 = 495R_0}$$

$$\begin{array}{r|l} 95R_1 - 5R_2 = -95R_0 & \\ 5R_1 + 5R_2 = 495R_0 & + \end{array}$$

$$100R_1 = 400R_0$$

$$\boxed{R_1 = 4R_0}$$

$$5R_2 + 5R_1 = 495R_0$$

$$5R_2 = 475R_0 \Rightarrow \boxed{R_2 = 95R_0}$$

$$R_3 = 4R_2 + 4R_1 + 4R_0$$

$$\boxed{R_3 = 400R_0}$$



$$E = 0,1 \%$$

$$A = 1 + \frac{R_1 + R_2 + R_3}{R_0}$$

$$R_x = R_1 + R_2 + R_3 = 499,1 \text{ €}$$

$$A_3(1+E) = 1 + \frac{R_x(1+\delta)}{R_0(1-\delta)}$$

$$\frac{R_x(1+\delta)}{R_0(1-\delta)} = 499,5$$

$$R_x(1+\delta) = 499,5 R_0(1-\delta)$$

$$R_x + R_x \delta = 499,5 R_0 - 499,5 R_0 \delta$$

$$\delta(R_x + 499,5 R_0) = 499,5 R_0 - R_x$$

$$\delta < \frac{499,5 R_0 - R_x}{R_x + 499,5 R_0}$$

$$\delta < 5,007 \cdot 10^{-4}$$

2.

$$R_L = 100 \Omega$$

$$C_L = 8 \text{ pF}$$

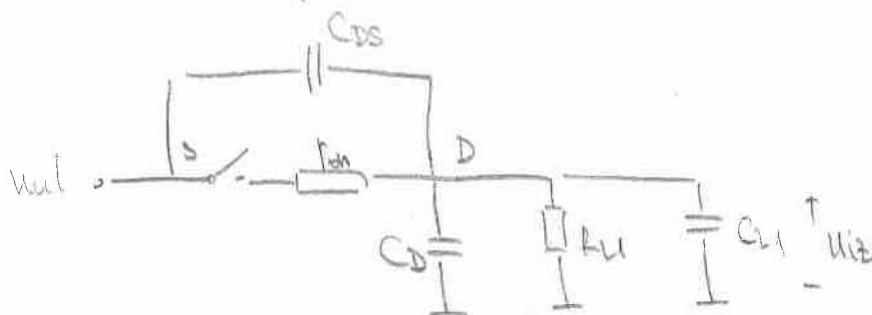
$$p_{ro} = 50 \text{ dB na } f = 5 \text{ MHz}$$

$$C_D = 8 \text{ pF}$$

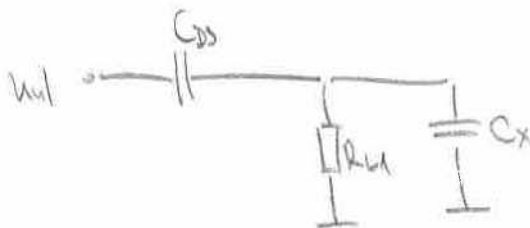
$$C_{DS} = ?$$

$$p_{ro} = ? \text{ na } f = 50 \text{ kHz}$$

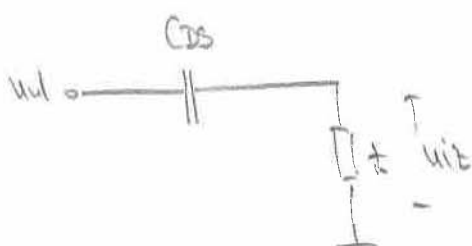
$$\text{na } R_L = 10 \text{ k}\Omega \text{ i } C_L = 10 \text{ pF}$$



poniżej zamieniamy na składowe tworzenia



$$C_X = C_D + C_L = 16 \text{ pF}$$



$$\frac{1}{Z} = R_L \parallel C_X$$

$$= \frac{R_L \cdot \frac{1}{sC_X}}{R_L + \frac{1}{sC_X}}$$

$$\underline{z} = \frac{R_L \cdot \frac{1}{sC_x}}{\frac{sR_L C_x + 1}{sC_x}} = \frac{R_L}{1 + sR_L C_x}$$

$$s = j\omega$$

$$\underline{z} = \frac{R_L}{1 + j\omega R_L C_x} = \frac{100 \Omega}{1 + j2\pi \cdot 5 \cdot 10^6 \cdot 100 \cdot 16 \text{ pF}} = \frac{100}{1 + j0,0502}$$

$$= 99,874 \angle -2,8738^\circ$$

$$F_1 = 20 \log |A| = -50 \text{ dB}$$

$$A = \frac{u_z}{u_{in}}$$

$$u_z \left( \frac{1}{z} + sC_D \right) = u_{in} \cdot sC_D$$

$$\frac{u_z}{u_{in}} = A = \frac{sC_D}{\frac{1}{z} + sC_D} = \frac{sC_D}{1 + s z C_D}$$

$$A = \frac{s^2 \cos}{1 + s^2 \cos} = \frac{j\omega^2 \cos}{1 + j\omega^2 \cos}$$

$$|A| = \frac{1 \cdot \cos \cdot \omega^2}{\sqrt{1 + \omega^4 \cos^2}}$$

$$-50 \text{ dB} = 20 \log |A|$$

$$-\frac{5}{2} = \log |A|$$

$$|A| = 10^{-5/2}$$

$$\frac{1 \cdot \cos \omega}{\sqrt{1 + \omega^4 \cos^2}} = 10^{-5/2}$$

$$\frac{1^2 \cos^2 \omega^2}{1 + \omega^4 \cos^2} = 10^{-5}$$

$$\frac{1}{2} C D^2 W^2 = 10^{-5} + 10^{-5} W^2 \frac{1}{2} C D^2$$

$$C D^2 \left( \frac{1}{2} W^2 - 10^{-5} W^2 \right) = 10^{-5}$$

$$C D^2 \frac{1}{2} W^2 (1 - 10^{-5}) = 10^{-5}$$

$$C D = \sqrt{\frac{10^{-5}}{\frac{1}{2} W^2 (1 - 10^{-5})}}$$

$$= \frac{10^{-5/2}}{\frac{1}{2} W \sqrt{1 - 10^{-5}}}$$

$$= 1.0076 \text{ pF}$$

$$3. \quad t_{ap} = 200 \text{ ns}$$

$$I_L = 1 \text{ nA}$$

$$\Delta u = \frac{du}{dt} t_{ap}$$

$$du \leq \frac{LSB}{8}$$

2 bitni ADP

$$\frac{du}{dt} = \frac{I_L}{C_H} = 2\pi f \cdot U_A$$

$f_{max} = ?$

$C_{min} = ?$

$$e < LSB/8$$

$$u_{in} = U_A \sin(2\pi f t)$$

$$LSB = \frac{2U_A}{2^n} = \frac{2U_A}{2^{12}}$$

$$\frac{du}{dt} \cdot t_{ap} \leq \frac{LSB}{8}$$

$$2\pi f \cdot U_A \cdot t_{ap} < \frac{2U_A}{2^{12}} \quad / : U_A$$

$$2\pi f t_{ap} < \frac{2}{2^{12} \cdot 8} \quad / \quad \frac{1}{2\pi f t_{ap}}$$

$$f < \frac{1}{2\pi t_{ap} 2^{14} \cdot 2^3} = \frac{1}{2^{15} \pi t_{ap}} = 48,57 \text{ Hz}$$

$$\frac{I_L}{C_H} = 2\pi f U_A \Rightarrow C_H = \frac{I_L}{2\pi f U_A}$$

1. Audíone výřka

2. do

břka aktivita

maže  $C_+$

břka klíauje

břka přetřavauje (veče)

4.

$$C_+ = 1 \mu F$$

$$t_{ak} = 4,5 \mu s$$

$$\pm 0,1\% \text{ } U_d = 20V$$

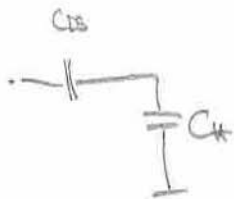
$$\frac{du}{dt} = \frac{I_L}{C_+}$$

$I = \text{konst.}$

$$C_+ = 100 \text{ pF}$$

$$C_+ = 100 \text{ pF}$$

$$\frac{du}{dt} = 10 \frac{du}{dt} = 10 \cdot 30 \text{ V/s} = 300 \text{ V/s}$$



$$F = 20 \log \frac{C_{DS}}{C_+ + C_{DS}} = -70 \text{ dB}$$

$$\frac{C_{DS}}{C_+ + C_{DS}} = 10^{-7/2}$$

$$C_{DS} (1 - 10^{-7/2}) = 10^{-7/2} C_+$$

$$C_{DS} = \frac{10^{-7/2} C_+}{1 - 10^{-7/2}}$$

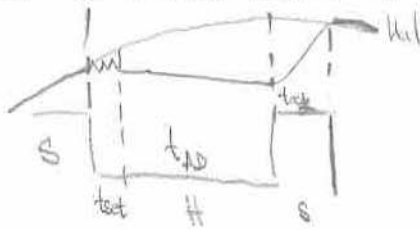
$$= 0,816 \text{ pF}$$

$$F = 20 \log \frac{C_{DS}}{C_+ + C_{DS}}$$

$$= -50 \text{ dB}$$

$$\text{do } C_+ = 100 \text{ pF}$$

5.



$$T_{min} = t_{set} + t_{AD} + t_{aog}$$

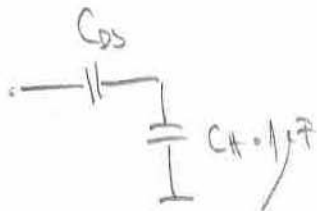
$$f = 1/T_{min} = 250 \text{ kHz} \rightarrow T_{min} = 1/250 \text{ kHz}$$

$$t_{AD} \leq \frac{1}{f_{max}} - t_{set} - t_{aog}$$

$$t_{AD} \leq 4000 \text{ ns} - 500 \text{ ns} - 2000 \text{ ns}$$

$$t_{AD} \leq 1500 \text{ ns}$$

$$t_{AD} \leq 1,5 \text{ } \mu\text{s}$$



$$f = 20 \log \frac{C_{DS}}{C_{DS} + C_H} \Rightarrow C_{DS} = 0,1 \text{ pF}$$



c.

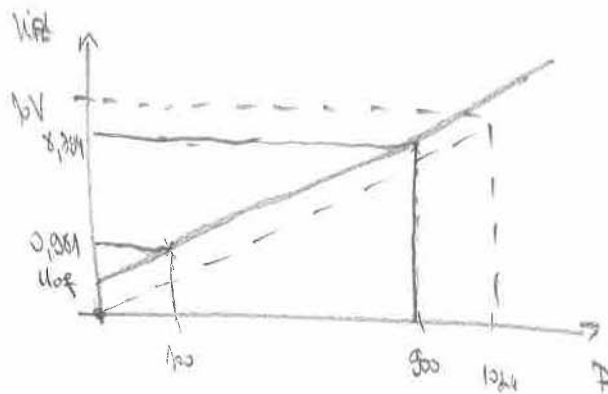
10 bit DAC

$$U_{ref} = 10V$$

$$U_{a1} = 0,981V$$

$$U_{a2} = 8,794V$$

$$A_{ideal} = \frac{10V}{128} = 9,765625 \text{ mV/bit}$$



$$A_{sw} = \frac{8,794 - 0,981}{300 - 100} = 9,76625 \text{ mV/bit}$$

$$\varepsilon = \left| \frac{A_{sw} - A_{ideal}}{A_{ideal}} \right| = 6,4 \cdot 10^{-7}$$

$$U_{sg} = 0,981 - A_{sw} \cdot 100 = 4,295 \text{ mV}$$

4. predavanje

3. prezentacija / 2. dio

1) Digitalni - Analogni pretvarači

1.1) vanjska referenca

~ interna

- eksterna

⇒ s doznom na opseg napona refer. izvora

~ DA s fiksne napona

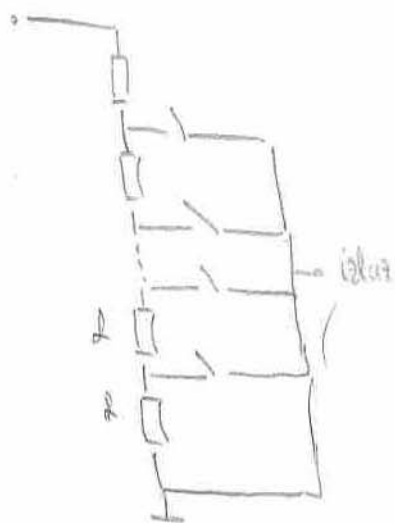
~ DA s promjenjivom iznosu referenca (množiteljici DA pretvarači)

⇒ Razni stupanj DAP

~ strujni

~ naponski

## 1.2) 2<sup>n</sup> (string DAC, Leibnizovo deljenje)

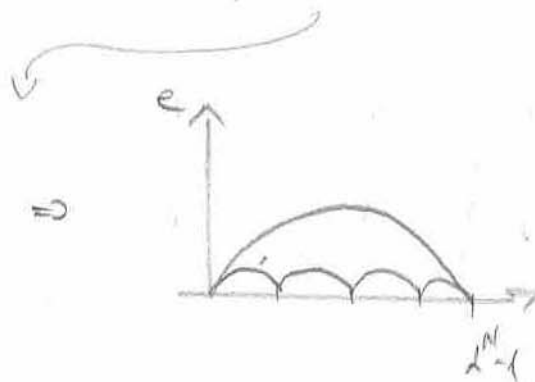
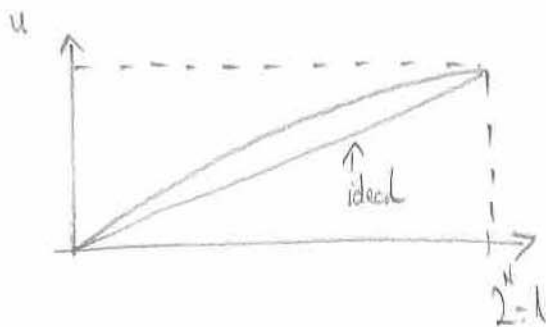


velikodužni napor → (poveć. digit.)

kipči napori na izlazu su mala  
⇒ povećava R

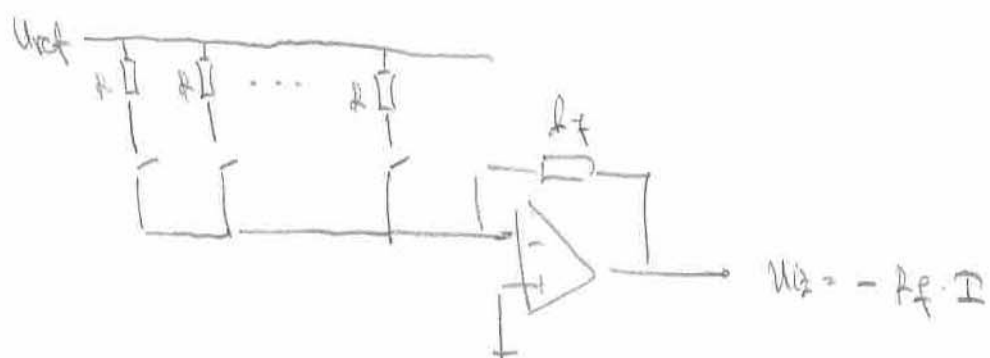
veliki broj otpornika ⇒ nedostatak

počasno napredak znake  $2^n$  ⇒ da bi se došlo doja linearnost

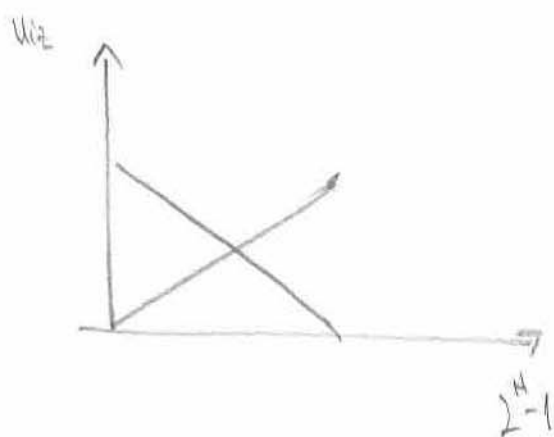
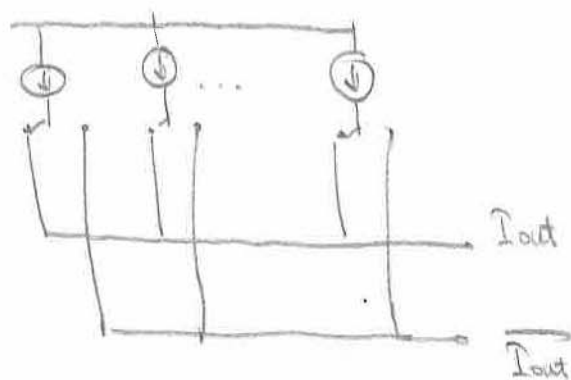


povećavaju otpornika na četvrtinano opsega

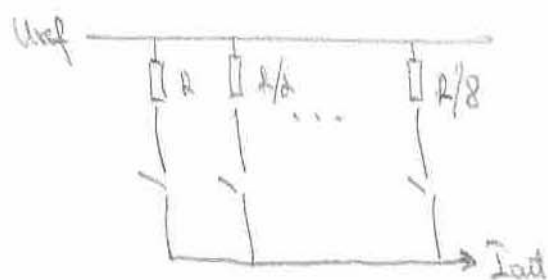
1.2)  $U_{iz}$  stajigulu izoqa



1.3.1) peshirpawaye stajye (current steering DAC)



## 1.4) Težinska mreža



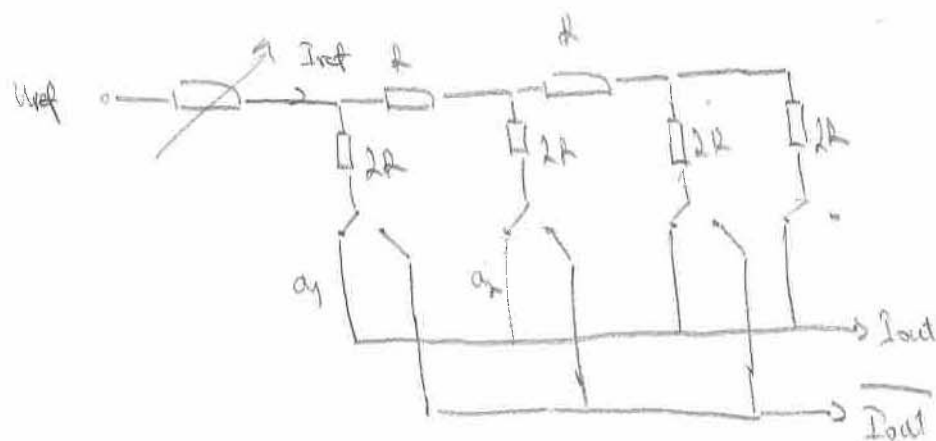
Zaključna precizna opornika i  
precizne strujne izlaze

## 1.5) R-2R ljestnica

1.5.1) strujni izlaz

1.5.2) naponski izlaz

### 1.5.1) strujni izlaz



$$I_{ref} = \frac{U_{ref}}{R}$$

$$I_1 = \frac{I_{ref}}{2} \quad ; \quad I_2 = \frac{I_1}{2} = \frac{I_{ref}}{4}$$

$$U_{ref} = -R_f \cdot I_{ref} = -R_f \cdot \sum_{i=1}^n a_i \cdot \frac{I_{ref}}{2^i}$$

$$= -R_f \cdot I_{ref} \cdot \sum_{i=1}^n a_i \frac{1}{2^i}$$

$$= -R_f \cdot I_{ref} \cdot \frac{1}{2^n} \left( a_1 \cdot 2^{n-1} + a_2 \cdot 2^{n-2} + \dots + a_n \right)$$

$$R_f = R$$

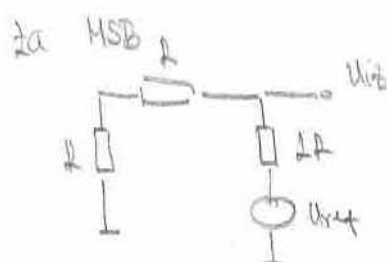
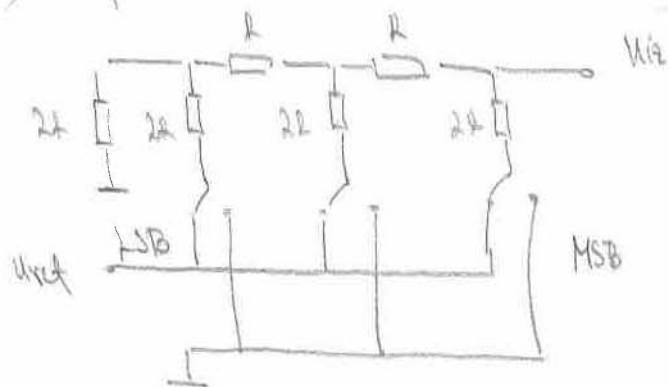
$$= -R \cdot \frac{U_{ref}}{R} \left( a_1 \cdot 2^{n-1} + a_2 \cdot 2^{n-2} + \dots + a_n \right)$$

$$= -U_{ref} \cdot \frac{1}{2^n}$$

last. optoizolacija  $U_{ref}$  ( $U_{ref}$  ovini o ferdnu)

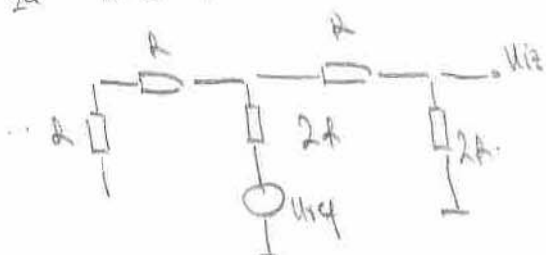
slabije status na visoku potenc. (virtuelni spoj ili nasa)

1.5.2) upovršni izlaz



$$U_{iz} = U_{ref} / 2$$

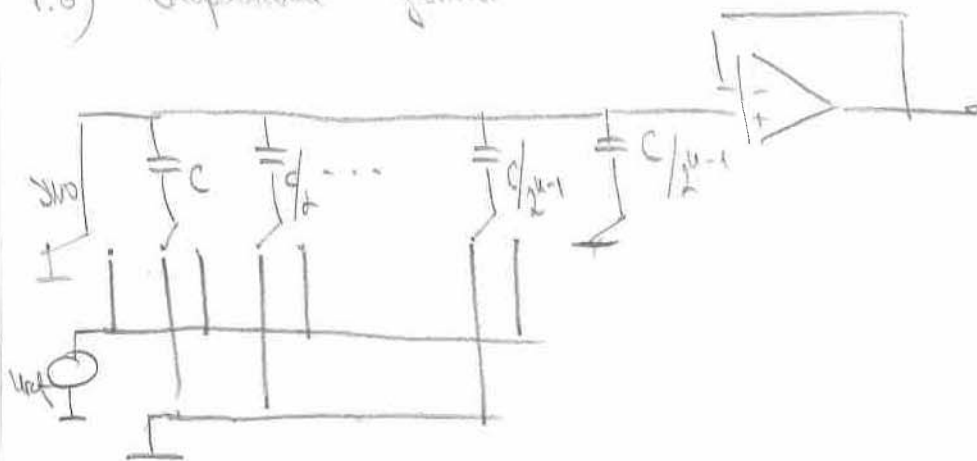
za MSB-1



$$U_{iz} = \frac{3R \parallel 2R}{3R \parallel 2R + 2R} \cdot \frac{2R}{3R} U_{ref} = \frac{6/5 R}{11/5 R} \cdot \frac{1}{3} U_{ref} = U_{ref} / 4$$

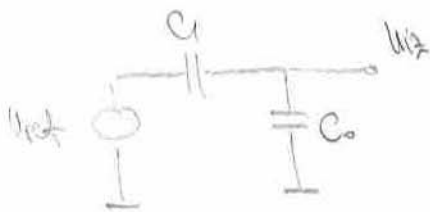
izlazni otpor ne ovisi o kod

# 1.6) Kopiermaschine hydraulica



$SW \rightarrow 1$  test

$SW \rightarrow 2$  sample



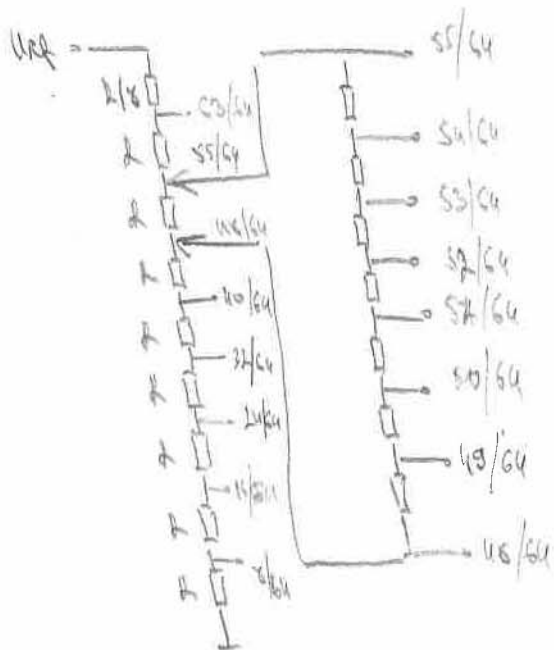
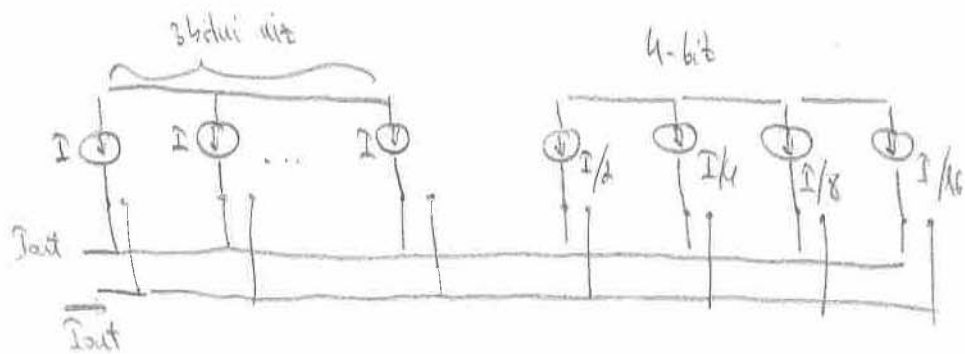
$$U_x = U_{ref} \cdot \frac{C_1}{C_1 + C_0} = U_{ref} \cdot \frac{C_1}{C_{tot}} = U_{ref} \cdot \frac{a_{n-1} \cdot C + a_{n-2} \cdot \frac{C}{2} + \dots + a_0 \cdot \frac{C}{2^{n-1}}}{C + \frac{C}{2} + \dots + \frac{C}{2^{n-1}} + \frac{C}{2^{n-1}}}$$

$$U_x = U_{ref} \cdot \frac{a_{n-1} \cdot C + \dots + a_0 \cdot \frac{C}{2^{n-1}}}{2C}$$

$$U_x = U_{ref} / 2^n \quad (a_{n-1} \cdot 2^{n-1} + \dots + a_0)$$



# 1.7) Sigma-Delta DAC



$$\frac{2+7+1}{2+7+1} = 7/8$$

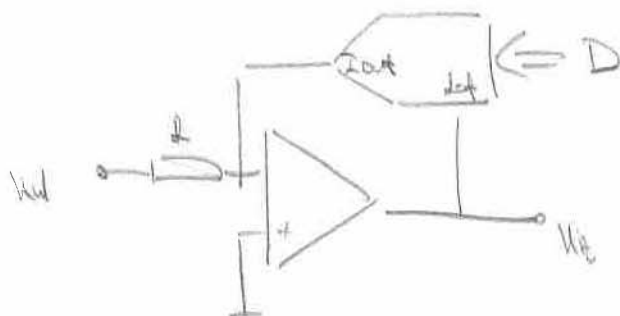
6. predavanje  
3. predavanja / 3. dio

1.8) Multiplikativni DAP

- ⇒ ilustrativni
- ⇒ ilustrativni

1.8.1) Izotaba MOAP-a

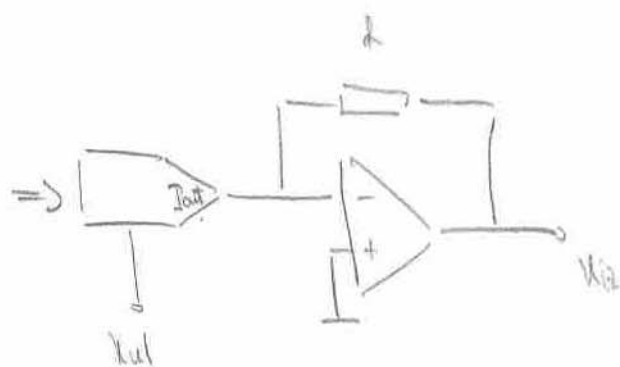
⇒ PBA s multiplikativnim DAP-ovima



$$I_{out} = I_{ref} \cdot \frac{2^n}{2^N}$$

$$\frac{u_{in}}{R} = -I_{ref} \cdot \frac{2^n}{2^N} = -\frac{U_{ref}}{R} \cdot \frac{2^n}{2^N} \quad / \cdot R$$

$$\frac{u_{in}}{u_{ref}} = -\frac{2^n}{2^N} \quad \text{razlučivost}$$



$$\frac{u_{kz}}{u_d} = - \frac{2^n}{2^N}$$

1.8.2) Pogreške priručanja uslijed

1) integrativne nelinearnosti MOAP-a

2) pogreška priručanja DAP-a

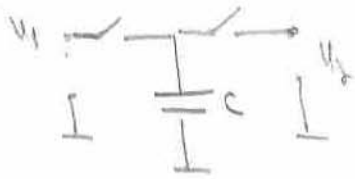
$$u_{kz} = u_{ref} \cdot D$$

↑  
dovodi grešku

$$\frac{u_{kz}}{u_d} = - \frac{2^N}{(2^n + x) \cdot (1 + x)}$$

1.8.3) svi otpornici relativno male / može se postići veće pojačanje

2) Shlissli o parallelnu kapacitivna



$$U_1 > U_2$$

$$\Delta Q = C \cdot (U_1 - U_2)$$

$$I_{sr} = \Delta Q \cdot f_{dk} = \Delta Q \cdot \frac{1}{T} = C \cdot \Delta U \cdot f_{dk}$$

$$\frac{\Delta U}{I_{sr}} = \frac{1}{C \cdot f_{dk}} = R_{ekv}$$

4. prezentacija / Diferencijalna, instrumentaciona  
i izlazišna pogreška

1) Pogreška

⇒ diferencijalna

⇒ instrumentaciona

~ sum

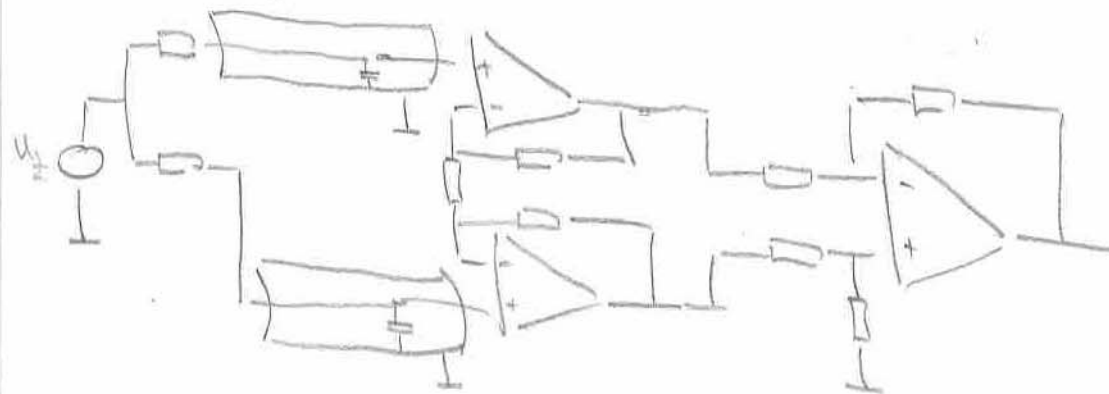
⇒ otklapanje / zaštitna dioda

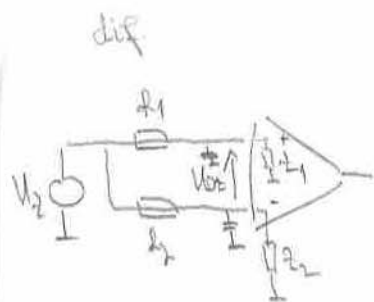
⇒ izlazišna pg

⇒ disperziona pg

⇒ auto-zero pg

1.1) Otklapanje i zaštitna dioda





$$U_{02} = U_2 \cdot \left( \frac{z_1}{R_1 + z_1} - \frac{z_2}{R_2 + z_2} \right)$$

zajed. smetnja  $U_2$   $z_1 = z_2 = z$

$$z \gg R_1, R_2$$

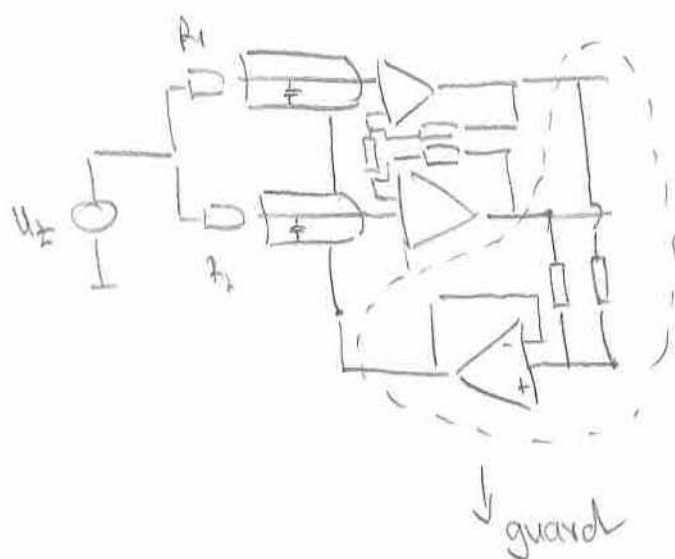
$$U_{02} = U_2 \frac{\Delta I}{I}$$

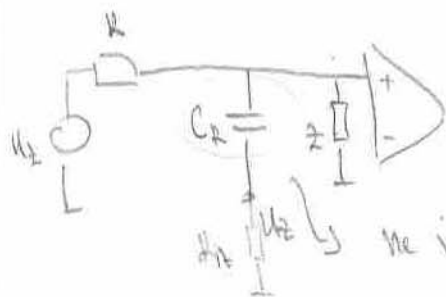
↓ difer. napon kao posljedica zajedničke struje

slapanje se dolje rasipni kapacitet ali smanjuje  
vlastitu imped. pojačala  $\Rightarrow$  povećava se  $U_{02}$



negativna strava slapanja (izbjegava se korištenje  
zastitne elektode ~ guard)

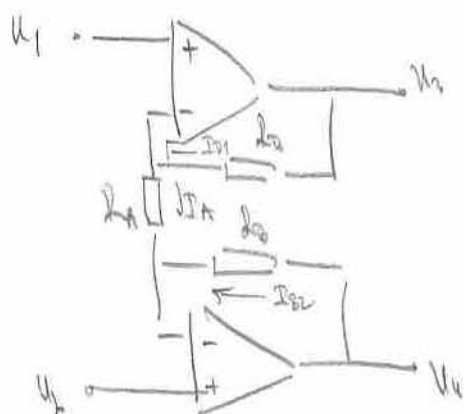




ne igra uloge (braklo spojeu)  $\Rightarrow$  guarding



$R_2 \ll$   $C_2$  preko nuped. izolirnog elektrolita spojeu na masu



$$I_{B1} = I_A$$

$$\frac{U_2 - U_1}{R_B} = \frac{U_1 - U_2}{R_A}$$

$$I_A = -I_{B2}$$

$$\frac{U_1 - U_2}{R_A} = \frac{U_2 - U_1}{R_B}$$

$$\begin{aligned} U_3 &= -\frac{R_B}{R_A} U_2 + \left(1 + \frac{R_B}{R_A}\right) U_1 \\ U_4 &= \left(1 + \frac{R_B}{R_A}\right) U_2 - \frac{R_B}{R_A} U_1 \end{aligned}$$

$$U_4 - U_3 = \left(1 + \frac{2R_B}{R_A}\right) U_2 - \left(1 + 2\frac{R_B}{R_A}\right) U_1$$

$$U_4 - U_3 = \left(1 + 2\frac{R_B}{R_A}\right) (U_2 - U_1)$$

$$\frac{u_1 + u_2}{2} = \frac{u_2 + u_1}{2}$$

$$u_{D,ul} = u_2 - u_1$$

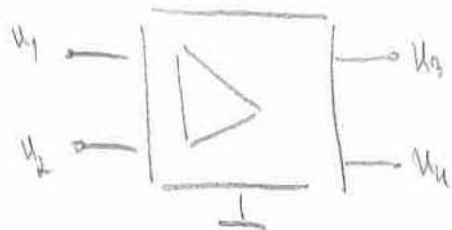
$$u_{D,i2} = \left(1 + 2R_2/R_1\right) u_{D,ul}$$

$$u_{2,i2} = u_{2,ul}$$



## 2. auditorska vježba / 1. dio

1. dif. poj. / simetrično



$$u_3 = C_{11} u_1 + C_{12} u_2$$

$$u_4 = C_{21} u_1 + C_{22} u_2$$

$$u_{D,ul} = u_1 - u_2$$

$$u_{D,iz} = u_3 - u_4$$

$$u_{Z,ul} = \frac{1}{2} (u_1 + u_2)$$

$$u_{Z,iz} = \frac{1}{2} (u_3 + u_4)$$

$$\begin{bmatrix} u_{D,iz} \\ u_{Z,iz} \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \begin{bmatrix} u_{D,ul} \\ u_{Z,ul} \end{bmatrix}$$

$$\begin{bmatrix} u_{D,iz} \\ u_{Z,iz} \end{bmatrix} = \begin{bmatrix} A_D & A_Z \\ a_{21} & a_{22} \end{bmatrix} \begin{bmatrix} u_{D,ul} \\ u_{Z,ul} \end{bmatrix}$$

$$A_D = \left. \frac{u_{D,iz}}{u_{D,ul}} \right|_{u_{Z,ul}=0}$$

$$A_Z = \left. \frac{u_{D,iz}}{u_{Z,ul}} \right|_{u_{D,ul}=0}$$

faktor pojačavanja / rejekcije (CMRR)

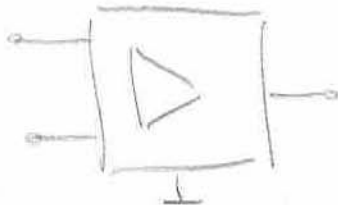
$$CMRR = C = \left| \frac{A_D}{A_Z} \right| \cdot H = T = \left| \frac{\frac{u_{D,iz}}{u_{D,ul}} \big|_{u_{Z,ul}=0}}{\frac{u_{D,iz}}{u_{Z,ul}} \big|_{u_{D,ul}=0}} \right|$$

faktor diskriminacije

$$\overline{F_D} = \frac{A_D}{\left. \frac{U_{z,iz}}{U_{z,ul}} \right|_{U_{D,ul} = \phi}} = \frac{A_D}{a_{zz}}$$

$$a_{zu} = \phi$$

osimbenici poj. / dif.



$$U_z = \begin{bmatrix} A_D & A_z \end{bmatrix} \begin{bmatrix} U_{D,ul} \\ U_{z,ul} \end{bmatrix}$$

$$U_{D,ul} = 1V ; U_{z,ul} = 2V$$

$$P = 80dB = 10^4$$

$$\overline{F_D} = 80dB = 10^4$$

$$A_D = 1000$$

$$U_{D,iz} = A_D \cdot U_{D,ul} \pm A_z \cdot U_{z,ul}$$

$$= 1000 \cdot 1mV \pm 0,1 \cdot 2V$$

$$= 1V \pm 0,2V$$

$$A_z = \frac{A_D}{P} = 0,1$$

$$a_{zz} = \frac{A_D}{\overline{F_D}} = 0,1$$

$$a_{zu} = \phi$$

$$U_{z,iz} = a_{zz} U_{z,ul}$$

$$= 0,1 \cdot 2V$$

$$= 0,2V$$

čistá síť / 2. stupňů



$$U_{12} = \begin{bmatrix} A_{02} & A_{22} \end{bmatrix} \begin{bmatrix} A_{01} & A_{21} \\ \phi & a_{22} \end{bmatrix} \begin{bmatrix} U_{0,ul} \\ U_{2,ul} \end{bmatrix}$$

$$U_{12} = \begin{bmatrix} A_{02}A_{01} & A_{02}A_{21} + A_{22}a_{22} \end{bmatrix} \begin{bmatrix} U_{0,ul} \\ U_{2,ul} \end{bmatrix}$$

$$P = \left| \frac{A_{0,uk}}{A_{2,uk}} \right| = \left| \frac{A_{02}A_{01}}{A_{02}A_{21} + A_{22}a_{22}} \right| = \left| \frac{1}{\frac{A_{21}}{A_{01}} + \frac{A_{22}}{A_{02}} \frac{a_{22}}{A_{01}}} \right|$$

$$1/P = \frac{1}{\frac{A_{01}}{A_{21}}} + \frac{1}{\frac{A_{02}}{A_{22}}} \cdot \frac{1}{\frac{A_{01}}{a_{22}}}$$

$$1/P = \frac{1}{P_1} + \frac{1}{P_2} \cdot \frac{1}{P_{01}}$$

2.

dif. pp. 8 asimetri. intrazare

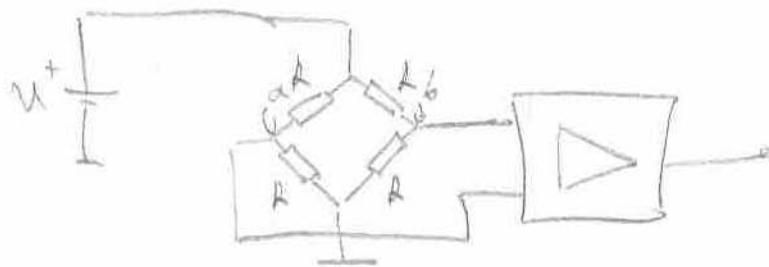
$$A_D = 1000$$

$$U_{D,ul} = 1\text{mV}$$

$$U = 10\text{V}$$

$$\rho = 10000 = 10^4$$

$$U_{D,iz} = ?$$



$$U_{D,ul} = U_A - U_B$$

$$U_A = \frac{1}{2} (U + U_{D,ul}) = 5,0005\text{V}$$

$$U_B = \frac{1}{2} (U - U_{D,ul}) = 4,9995\text{V}$$

$$U_{Z,ul} = \frac{1}{2} (U_A + U_B) = 5\text{V}$$

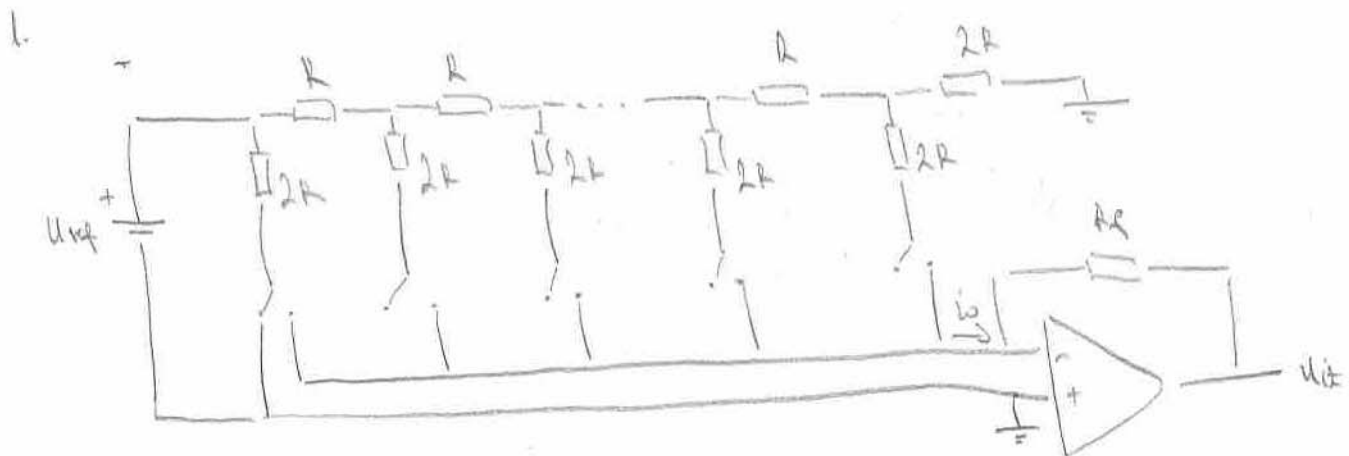
$$U_{iz} = \begin{bmatrix} A_D & A_Z \end{bmatrix} \begin{bmatrix} U_{D,ul} \\ U_{Z,ul} \end{bmatrix}$$

$$U_{iz} = A_D U_{D,ul} \pm A_Z U_{Z,ul}$$

$$\left( \rho = \frac{A_D}{A_Z} \Rightarrow A_Z = A_D / \rho = 0,1 \right)$$

$$U_{D,iz} = (1 \pm 0,5)\text{V}$$

## 2. Kratka prijava znanja



u stvarnom ucinu

$$R = R_f = 15 \text{ k}\Omega$$

$$U_{ref} = 5V$$

4-bitni pretvornik

$$a_1 a_2 a_3 a_4 = 1010$$

$$U_{iz} = ?$$

$$U_{iz} = -R_f \cdot i_o$$

$$i_o = \frac{U_{ref}}{R} \cdot D$$

$$U_{iz} = - \frac{R_f}{R} \cdot U_{ref} \left( \frac{a_1}{2^1} + \frac{a_2}{2^2} + \frac{a_3}{2^3} + \dots + \frac{a_n}{2^n} \right)$$

$$U_{iz} = -U_{ref} \left( \frac{1}{2} + \frac{1}{4} + \frac{1}{16} \right)$$

$$U_{iz} = -U_{ref} \left( \frac{8 + 4 + 1}{16} \right)$$

$$U_{iz} = -U_{ref} \left( \frac{13}{16} \right)$$

$$U_{iz} = -4,0625V$$

2.

diff. pg. sa birod. izlazu

$$A_D = 1000$$

$$F = 100 \text{ dB}$$

$$F_D = 120 \text{ dB}$$

$$U_{iz} = 5 \text{ V}$$

$$U_{pul} = 2 \text{ mV}$$

$$U_{iz} = ?$$

$$\begin{bmatrix} U_{piz} \\ U_{ziz} \end{bmatrix} = \begin{bmatrix} A_D & A_z \\ a_{21} & a_{22} \end{bmatrix} \begin{bmatrix} U_{pul} \\ U_{zpl} \end{bmatrix}$$

$$F = 20 \log \left| \frac{A_D}{A_z} \right|$$

$$5 = \log \left| \frac{A_D}{A_z} \right| \Rightarrow \frac{A_D}{A_z} = 10^5 \Rightarrow$$

$$A_z = \frac{A_D}{10^5}$$

$$a_{21} = \phi$$

$$F_D = \frac{A_D}{\frac{U_{ziz}}{U_{zpl} | U_{zpl} = \phi}} = \frac{A_D}{a_{22}}$$

$$120 \text{ dB} = 20 \log \left| \frac{A_D}{a_{22}} \right|$$

$$6 = \log \left| \frac{A_D}{a_{22}} \right| \Rightarrow \frac{A_D}{a_{22}} = 10^6 \Rightarrow a_{22} = \frac{A_D}{10^6}$$

$$\begin{array}{ccc}
 & 2 \times 2 & 2 \times 1 \Rightarrow 2 \times 1 \\
 \begin{bmatrix} U_{D,12} \\ U_{Z,12} \end{bmatrix} & = \begin{bmatrix} A_0 & A_z \\ \phi & a_z \end{bmatrix} \begin{bmatrix} U_{D,ul} \\ U_{Z,ul} \end{bmatrix}
 \end{array}$$

$$\begin{bmatrix} U_{D,12} \\ U_{Z,12} \end{bmatrix} = \begin{bmatrix} A_0 U_{D,ul} \pm A_z U_{Z,ul} \\ a_z U_{Z,ul} \end{bmatrix}$$

$$U_{D,12} = A_0 U_{D,ul} \pm A_z U_{Z,ul}$$

$$= (2 \pm 0.05) V$$

$$U_{Z,12} = A_0 / 10^6 U_{Z,ul}$$

$$= 5 \mu V$$

6 predavaja

4. predavaja /

1) Izmerilni priključki

2) Auto-zero priključki

3) Izmerilni priključki

Natani signal  $\Rightarrow$  male amplitude; spro. priravnitev (intergr.)

upr. temperaturni most ( $0,4 \text{ V/g}$ )

1-tip termopar ( $40,7 \text{ } \mu\text{V/}^\circ\text{C}$ )

$< 10 \text{ } \mu\text{V}$

Nizki tona

$\sim$  zelo mali napor pomba

$\sim$  zelo mali temperaturni i. mehanični posuni

$\sim$  zelo mali  $1/f$  šum

Izmerilni i. auto-zero priključki tipično:

$\sim 1 \text{ nV}$  pomba

$\sim 20 \text{ } \mu\text{V/}^\circ\text{C}$

$\sim 20 \text{ } \mu\text{V/}$  upreza

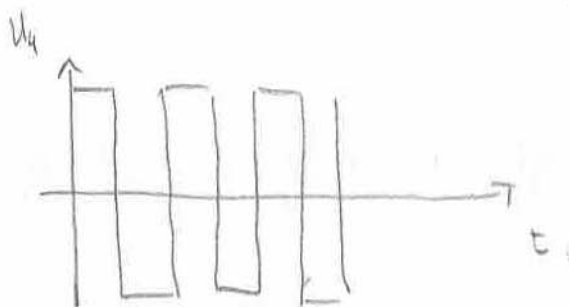
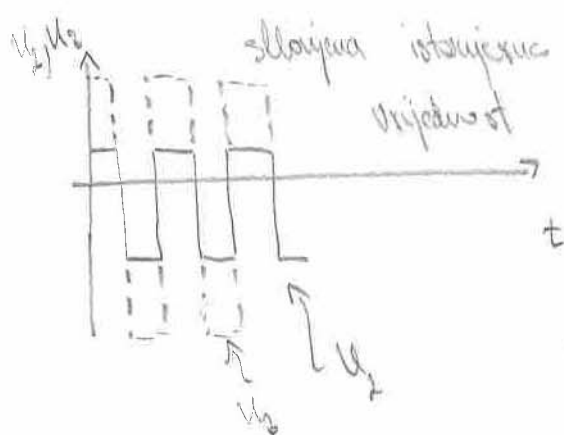
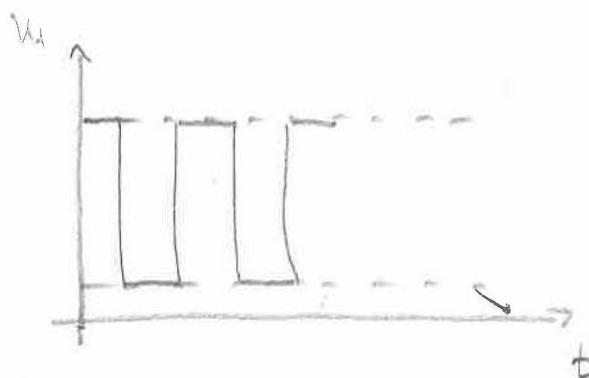
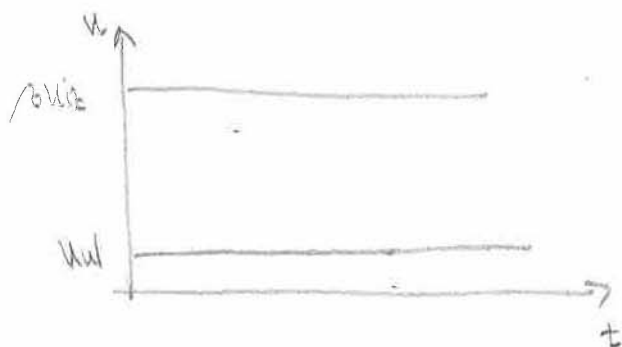


# 1) Čepasto - pojačalo

$C1$  ~ slaba izlazi komponenta

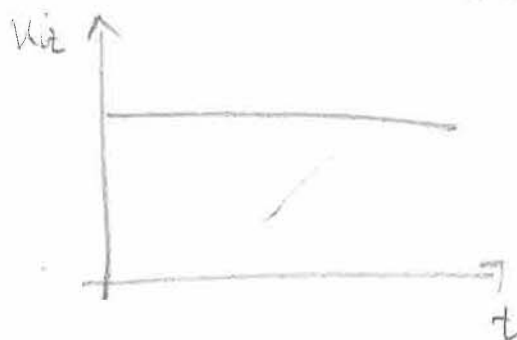
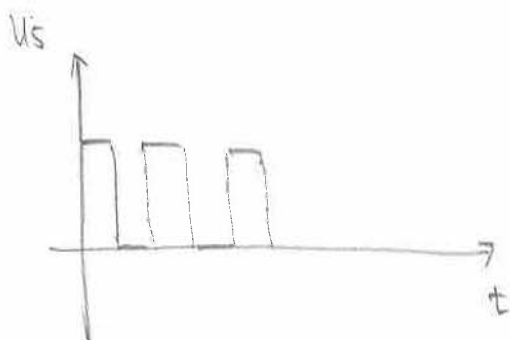
$C2$  ~ izlazi pojačalo (AI)

AI ~ integrator

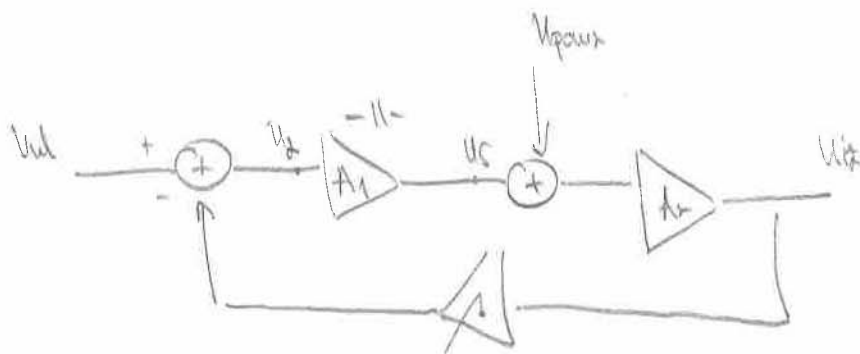


$$u_4 = u_2$$

na prvu koju uvr. AI



integracijom  $u_5$  dobiva se  $u_{iz}$



$$u_2 = u_{in} - \beta u_{out}$$

$$u_5 = A_1 u_2 = A_1 (u_{in} - \beta u_{out})$$

$$u_{out} = A_2 (u_5 + u_{pout}) = A_2 (A_1 (u_{in} - \beta u_{out}) + u_{pout})$$

$$u_{out} = A_2 A_1 u_{in} - A_2 A_1 \beta u_{out} + A_2 u_{pout}$$

$$u_{out} (1 + A_2 A_1 \beta) = A_2 A_1 u_{in} + A_2 u_{pout}$$

$$u_{out} = \frac{A_2 A_1 u_{in} + A_2 u_{pout}}{1 + A_2 A_1 \beta}$$

$$u_{out} = \frac{A_2 A_1}{1 + \beta A_1 A_2} u_{in} + \frac{A_2}{1 + A_1 A_2 \beta} u_{pout}$$

$$A_1 A_2 \gg \beta \quad ; \quad A_1 \gg A_2$$

$$\beta = A_1 / (r_1 + R_2)$$

$$U_{iz} = \frac{1}{\beta} U_{ul} + \frac{1}{\beta A_1} U_{puz}$$

$$1/\beta = 1 + R_2/r_1$$

frekv. davanja

2. mixera

- 1) signal se poslati na freg. predlozaj (harmonike)  
poučakati suo signal iz područja  $\sim 0$  Hz na više frekvencije  
(spektar)
- 2) pojačalo pojačava signal / koristi pogreške (bijeli šum i  $1/f$  pogreške)
- 3) 2. mixanje vraća signal u osnovne frekvencije ; a  
još neke priče na frekvencije harmonika
- 4) filtriranje signala  
  - šum se 1. put  
vix-a
  - uporedio s  
matricom  
signalom

2) Auto-zero fizičalo

2.1) sub-zero faza (određuje se uopu punkto)

S1 na "a"

S2 na "a"

$$U_{iz1}^a = U_{pau2} \cdot A_1 - B_2 \cdot U_{iz1}^a$$

$$U_{iz1}^a (1 + B_2) = U_{pau2} \cdot A_1$$

$$U_{iz1}^a = \frac{U_{pau2} \cdot A_1}{1 + B_2} = \frac{A_1}{1 + B_2} U_{pau2}$$

2.2) fizičavanje signala

S1 na "b"

S2 na "b"

$$U_{iz1}^b = (U_{ul} + U_{pau2}) A_1 - B_2 \cdot U_{iz1}^a$$

$$U_{iz1}^b = (U_{ul} + U_{pau2}) A_1 - B_2 \cdot \frac{A_1}{1 + B_2} U_{pau2}$$

$$U_{iz1}^b = U_{ul} A_1 + \frac{A_1}{1 + B_2} U_{pau2}$$

$$V_{in1} = (U_{in1} + U_{pau1}) A_1 + B_1 V_{in2}$$

$$V_{in1} = (U_{in1} + U_{pau1}) A_1 + B_1 \left\{ U_{in2} + \frac{A_2}{1+B_2} U_{pau2} \right\}$$

$$V_{in1} = (A_1 + A_2 B_1) U_{in1} + A_1 U_{pau1} + \frac{B_1 A_2}{1+B_2} U_{pau2}$$

za  $A_1 = A_2$  ;  $B_2 = B_1 \gg 1$

$$V_{in1} = A \cdot B U_{in1} + A U_{pau1} + A U_{pau2}$$

$$V_{in1}^a = V_{in1}^b$$

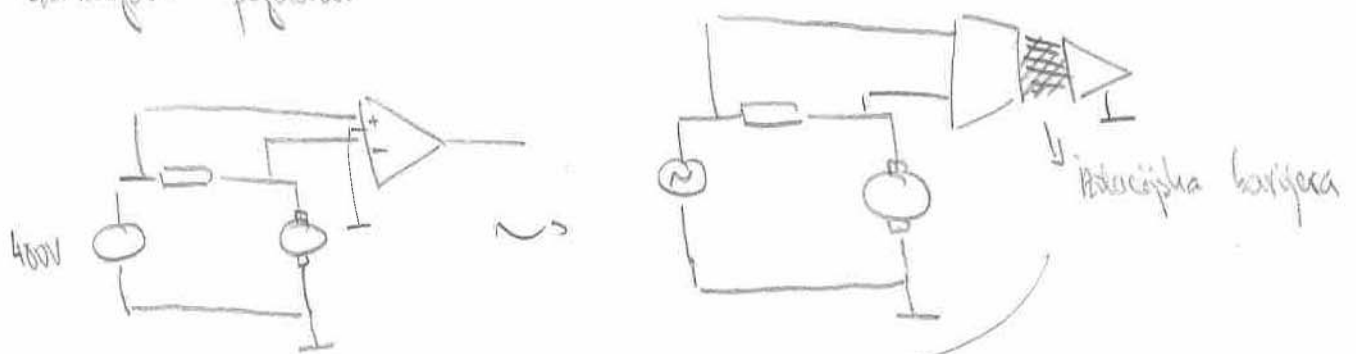
2.2) vedlostadi.

niznifrekvencija

vr. signal 200kHz } u spektru geok. svi na  
 $f_s = 44kHz$  } 300kHz; 400kHz, ...

### 3) Inducijsko pojačalo

napr.



- ~ optični spregnito
- ~ elektromagnetni spregnito (induktivno)
- ~ kapacitivno

#### 3.1) Optični spregnito

$$i_2 + \frac{u_c}{R_4} = - \frac{u_1}{R_1}$$

$$i_2 = f(u_1); \quad u_2 = f^{-1}(i_2)$$

$$\frac{u_c}{R_4} + i_2' + i_3 = 0$$

$$u_c = 0; \quad AC \rightarrow analiza$$

$$i_2' = -i_3 = u_3 / R_3$$

$$i_2' = f(u_1)$$

$$u_3/r_3 = f(u_2) = f(f'(u_1/r_1))$$

$$u_3/r_3 = u_1/r_1$$