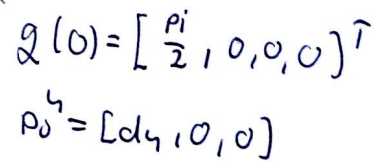


ba se kontinuier


$$Q_1 = \begin{bmatrix} -\frac{\pi}{2} & \frac{\pi}{2} \end{bmatrix}$$

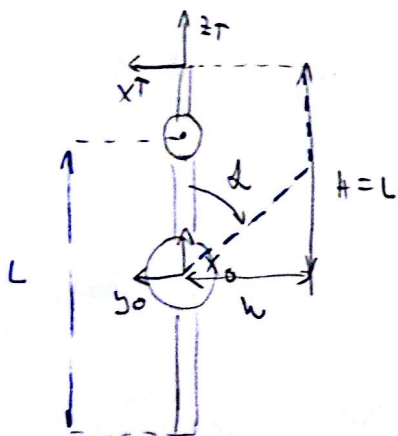
$$Q_2 = [0, 4]$$

$$Q_3 = 2$$

$$T_0^2 = \begin{bmatrix} -s_1 & -c_1 & 0 & c_1 q_2 \\ c_1 & -s_1 & 0 & s_1 q_2 \\ 0 & 0 & 1 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\vec{T}_0 = \begin{bmatrix} -s_{13} & 0 & c_{13} & c_{12}d_2 \\ c_{13} & 0 & s_{13} & s_{12}d_2 \\ 0 & 1 & 0 & d_1+d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_0^4 = \begin{bmatrix} -s_{13} & 0 & c_{13} & c_1 q_2 + c_{13} d_4 \\ c_{13} & 0 & s_{13} & s_1 q_2 + s_{13} d_4 \\ 0 & 1 & 0 & d_1 + d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \frac{\partial p_0}{\partial q_1} = m_4 \quad \begin{bmatrix} \frac{1}{3} (d_4^2 + 3 q_2 (d_4 c_3 + q_2)) & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & \frac{d_4^2}{3} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



Er
Im
Co. J.

ODREDITI Q3 DA JE ALAT KONSTANTNO OKOMIT
NA PLOŠTINU

$$\begin{aligned} \rightarrow x_0 \cdot z_0^4 &= 1 \\ y_0 \cdot z_0^4 &= 0 \end{aligned}$$

3. STUPAC 13 T₀⁴

$$C_{13} = 1$$

$$\cos(g_1 + g_3) = 1$$

$$g_1 + g_3 = 0$$

$$-\frac{\pi}{2} + g_2 = 0$$

$$Q_3 = 2\pi$$

$$\pi_1 + q_3 = 0$$

$$z_3 = -\frac{1}{4}$$

$$Q_3 = [-\frac{\pi}{4}, \frac{\pi}{4}]$$

$$\begin{bmatrix} z_0^T \cdot x_0 \\ z_0^T \cdot y_0 \\ z_0^T \cdot z_0 \end{bmatrix} = \begin{bmatrix} c_{13} \\ s_{13} \\ 0 \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}$$

1.5) Newton Euler, KUTWA BRZINA

→ ograniczenie gibanja zglobowa da robot zadrzi konstantnu orijentaciju prema statku.

$$a_0 = 0$$

$$a_1 = a_0 + \dot{q}_1 \hat{z}_0 = \begin{bmatrix} 0 \\ 0 \\ \dot{q}_1 \end{bmatrix}$$

$$a_2 = a_1 + \dot{q}_2 \hat{z}_1 = \begin{bmatrix} 0 \\ 0 \\ \dot{q}_1 \end{bmatrix}$$

0 - zglob je translacijski

$$a_3 = a_2 + \dot{q}_3 \hat{z}_2 = \begin{bmatrix} 0 \\ 0 \\ \dot{q}_1 \end{bmatrix} + \dot{q}_3 \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \dot{q}_1 + \dot{q}_3 \end{bmatrix}$$

$$a_4 = a_3 + \dot{q}_4 \hat{z}_3 = \begin{bmatrix} 0 \\ 0 \\ \dot{q}_1 + \dot{q}_3 \end{bmatrix}$$

0 - virtualan

$$\dot{q}_1 + \dot{q}_3 = 0$$

ogranicenje gibanja zglobova da se zadrzi konstantna okomitost cieten na površinu koju se ispituje

1.6) NEWTON-EULER LINIJSKA BRZINA

$$v_0 = 0$$

$$\Delta S_1 = \begin{bmatrix} 0 \\ 0 \\ \dot{q}_1 \end{bmatrix}$$

$$v_1 = v_0 + \frac{d}{dt} (\Delta S_1) = v_0 + \underbrace{\bar{\omega}_1 \times \Delta S_1}_{0 - u istom smjeru vektora} + \underbrace{|\dot{\Delta S}_1| \Delta S_1}_{0 - rotacijski, konstantne dužine} = 0$$

$$v_2 = v_1 + \frac{d}{dt} (\Delta S_2) = v_1 + \bar{\omega}_2 \times \Delta S_2 + |\dot{\Delta S}_2| \Delta S_2$$

$$\Delta S_2 = \begin{bmatrix} c_1 \dot{q}_2 \\ s_1 \dot{q}_2 \\ 0 \end{bmatrix}$$

$$\bar{\omega}_2 \times \Delta S_2 = \begin{vmatrix} x & y & z \\ 0 & 0 & 1 \\ c_1 & s_1 & 0 \end{vmatrix} \dot{q}_2 = \dot{q}_2 \begin{bmatrix} -s_1 \\ c_1 \\ 0 \end{bmatrix}$$

$$\dot{\Delta S}_2 = \dot{q}_2 \hat{z}_1$$

$$V_2 = \dot{q}_1 \dot{q}_2 \begin{bmatrix} -s_1 \\ c_1 \\ 0 \end{bmatrix} + \dot{q}_2 \begin{bmatrix} c_1 \\ s_1 \\ 0 \end{bmatrix} = \begin{bmatrix} -\dot{q}_1 \dot{q}_2 s_1 + \dot{q}_2^2 c_1 \\ \dot{q}_1 \dot{q}_2 c_1 + \dot{q}_2^2 s_1 \\ 0 \end{bmatrix}$$

$$V_3 = V_2 + \frac{d}{dt} (\Delta \vec{S}_2) = V_2 + \underbrace{\vec{\omega}_3 \times \Delta \vec{S}_2}_{\text{0 - rotational}} + \underbrace{(\dot{q}_3) \cdot \hat{z}}_{\text{0 - rotational}}$$

$$\vec{\omega}_3 \times \Delta \vec{S}_2 = \begin{vmatrix} x & y & z \\ 0 & 0 & \dot{q}_1 + \dot{q}_3 \\ 0 & 0 & d_3 \end{vmatrix} = 0$$

$$\Delta \vec{S}_2 = \begin{bmatrix} 0 \\ 0 \\ d_3 \end{bmatrix}$$

$$V_3 = V_2 = \begin{bmatrix} -\dot{q}_1 \dot{q}_2 s_1 + \dot{q}_2^2 c_1 \\ \dot{q}_1 \dot{q}_2 c_1 + \dot{q}_2^2 s_1 \\ 0 \end{bmatrix}$$

$$V_4 = V_3 + \frac{d}{dt} \Delta \vec{S}_3 = V_3 + \vec{\omega}_4 \times \Delta \vec{S}_3 + \underbrace{(\dot{q}_4) \cdot \hat{z}}_{\text{0 - rotational}}$$

$$\Delta \vec{S}_3 = \begin{bmatrix} c_{13} d_4 \\ s_{13} d_4 \\ 0 \end{bmatrix}$$

$$\vec{\omega}_4 \times \Delta \vec{S}_3 = \begin{vmatrix} x & y & z \\ 0 & 0 & \dot{q}_1 + \dot{q}_3 \\ c_{13} d_4 & s_{13} d_4 & 0 \end{vmatrix}$$

$$V_4 = \begin{bmatrix} -\dot{q}_1 \dot{q}_2 s_1 + \dot{q}_2^2 c_1 - (\dot{q}_1 + \dot{q}_3) s_{13} d_4 \\ \dot{q}_1 \dot{q}_2 c_1 + \dot{q}_2^2 s_1 + (\dot{q}_1 + \dot{q}_3) c_{13} d_4 \\ 0 \end{bmatrix} = \begin{bmatrix} -(\dot{q}_1 + \dot{q}_3) s_{13} d_4 \\ (\dot{q}_1 + \dot{q}_3) c_{13} d_4 \\ 0 \end{bmatrix}$$

2. a) TENSOR INERTIE $m_1 = m_2 = 0$

$$\Delta C_1 = \begin{bmatrix} 0 & -\frac{d_1}{2} & 0 & 1 \end{bmatrix}^T \quad \Delta C_2 = \begin{bmatrix} 0 & \frac{L}{2} & 0 & 1 \end{bmatrix}^T$$

$$\Delta C_3 = \begin{bmatrix} 0 & -\frac{d_3}{2} & 0 & 1 \end{bmatrix}^T \quad \Delta C_4 = \begin{bmatrix} 0 & 0 & -\frac{d_4}{2} & 1 \end{bmatrix}^T$$

$$D_1' = \frac{m_1 d_1^2}{12} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix} = 0$$

$$D_1 = 0$$

$$D_2' = \frac{m_2 \cdot L^2}{12} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix} \quad D_2 = R_0^T \cdot D_2' \cdot R_0$$

$$D_2 = \begin{bmatrix} -s_1 & -c_1 & 0 \\ c_1 & -s_1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} -s_1 & c_1 & 0 \\ -c_1 & -s_1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \frac{m_2 \cdot L^2}{12}$$

$$D_2 = \begin{bmatrix} -s_1 & 0 & 0 \\ c_1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} -s_1 & c_1 & 0 \\ -c_1 & -s_1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \frac{m_2 L^2}{12} = \frac{m_2 L^2}{12} \begin{bmatrix} s_1^2 & -s_1 c_1 & 0 \\ -s_1 c_1 & c_1^2 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$C_2 = H \cdot T_0^T \cdot \Delta C_2 = \begin{bmatrix} -s_1 & -c_1 & 0 & c_1 q_2 \\ c_1 & -s_1 & 0 & s_1 q_2 \\ 0 & 0 & 1 & d_1 \\ 0 & 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ \frac{L}{2} \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} -c_1 \frac{L}{2} + c_1 q_2 \\ -s_1 \frac{L}{2} + s_1 q_2 \\ d_1 \\ 0 \end{bmatrix}$$

$$J^2 = \begin{bmatrix} \frac{\partial C_2}{\partial q_1} & \frac{\partial C_2}{\partial q_2} & \frac{\partial C_2}{\partial q_3} \\ \vdots & \vdots & \vdots \\ z_0 & 0 & z_2 \end{bmatrix} = \begin{bmatrix} s_1 \frac{L}{2} - s_1 q_2 & c_1 & 0 \\ -c_1 \frac{L}{2} + c_1 q_2 & s_1 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{bmatrix}$$

$$D_2 = A_2^T \cdot m_2 \cdot A_2 + B_2^T \cdot D_2 \cdot B_2$$

$$m_2 \begin{bmatrix} s_1 (\frac{L}{2} - q_2) & -c_1 (\frac{L}{2} - q_2) & 0 \\ c_1 & s_1 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} s_1 (\frac{L}{2} - q_2) & c_1 & 0 \\ -c_1 (\frac{L}{2} - q_2) & s_1 & 0 \\ 0 & 0 & 0 \end{bmatrix} =$$

$$D_2 = m_2 \begin{bmatrix} \left(\frac{L}{2} - g_2\right)^2 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \end{bmatrix} + \begin{bmatrix} 0 & 0 & 1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} s_1^2 & -s_1 c_1 & 0 \\ -s_1 c_1 & c_1^2 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{bmatrix} \frac{m_2 L^2}{12}$$

$$D_2 = m_2 \begin{bmatrix} \left(\frac{L}{2} - g_2\right)^2 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \end{bmatrix} + \begin{bmatrix} 0 & 0 & 1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{bmatrix} \frac{m_2 L^2}{12}$$

$$D_2 = m_2 \begin{bmatrix} \left(\frac{L}{2} - g_2\right)^2 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \end{bmatrix} + \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \frac{m_2 L^2}{12}$$

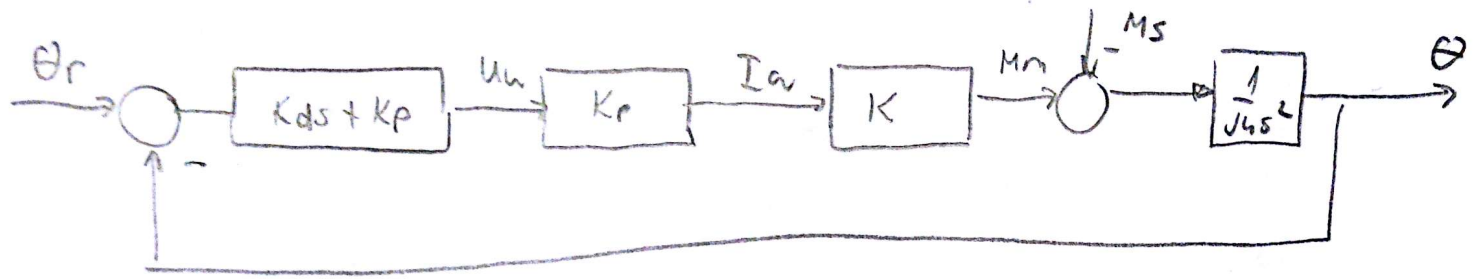
$$D_2 = m_2 \begin{bmatrix} \frac{L^2}{12} + \left(\frac{L}{2} - g_2\right)^2 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\underline{D_3 = 0 \quad m_3 = 0}$$

$$D_4 = \text{Miro izračunao}$$

$$D_{uk} = D_2 + D_4 = \begin{bmatrix} m_2 \left(\frac{L^2}{12} + \left(\frac{L}{2} - g_2 \right)^2 \right) + \frac{m_4}{3} (d_4^2 + 3g_2(d_4 c_3 + g_2)) & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & \frac{d_4^2}{3} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

2.b) REGULACIJSKA PETLJA POLUŽAJA ZGLOBA UZ UPRAVLJANJE MOMENTOM, 2c) UZ KOMPENZACIJSKO PROŠIRENJE



MIN MAX METOD

$$K_p \cdot K = 1 \quad m_2 = m_4 \quad d_4 = \frac{L}{2}$$

$$D_{11} = m_2 \left(\frac{L^2}{12} + \left(\frac{L}{2} - g_2 \right)^2 \right) + \frac{m_4}{3} \left(d_4^2 + 3g_2(d_4 c_3 + g_2) \right)$$

$$\omega_n = \sqrt{\frac{K_p \cdot J_{ue}}{J_h}}$$

$$K_p = \omega_n^2 \cdot \frac{J_{max}}{J_{min}}$$

$$J_{ue} = J_{min}$$

$$J_h = J_{max}$$

$$K_d = \frac{\varepsilon \cdot 2}{\sqrt{\frac{J_{min}}{K_p \cdot J_{max}}}}$$

$$g_{2min} = 0 \quad g_{2max} = L$$

$$g_{3min} = \frac{\pi}{4} \quad g_{3max} = 0 \Rightarrow \cos 0 = 1$$

$$J_{min}^1 = J_r + \frac{D_{11}}{i^2} = m_2 L^2 + D_{11min} = m_2 L^2 + \frac{5}{12} m_2 L^2 = \frac{17}{12} m_2 L^2$$

$$D_{11}(g_{2min}, g_{3min}) = m_2 \frac{L^2}{12} + m_2 \frac{L^2}{4} + \frac{m_4}{3} \left(\frac{L}{2} \right)^2 \quad m_2 = m_4$$

$$D_{11min} = \frac{m_2 L^2}{12} + m_2 \frac{L^2}{4} + \frac{m_4 L^2}{12} = \frac{5}{12} m_2 L^2$$

$$D_{11max} = m_2 \left(\frac{L^2}{12} + \left(\frac{L}{2} - L \right)^2 \right) + \frac{m_4}{3} \left(\left(\frac{L}{2} \right)^2 + 3L \left(\frac{L}{2} + L \right) \right) \quad \boxed{m_4 = m_2}$$

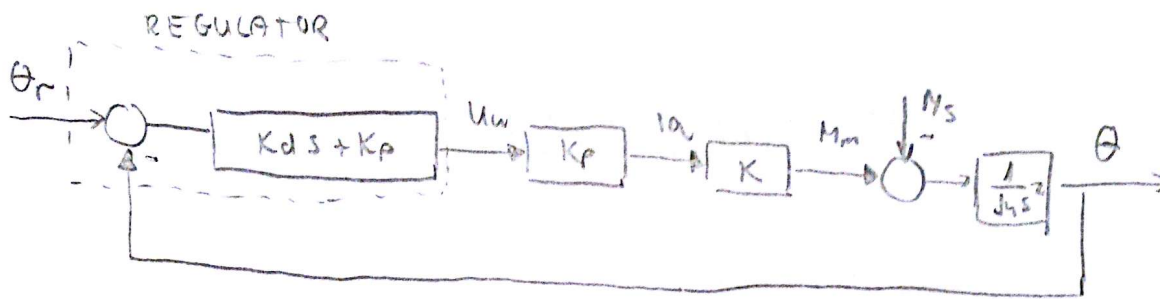
$$= \frac{m_2 L^2}{3} + \frac{m_2}{3} \left[\frac{L^2}{4} + \frac{9}{2} L^2 \right] = \frac{23}{12} m_2 L^2$$

$$J_{max}' = \frac{D_{11max}}{1} + m_2 L^2 = \frac{35}{12} L^2 m_2$$

$$K_p = \omega_n^2 \cdot \frac{J_{max}}{J_{min}} = \frac{\frac{35}{12}}{\frac{5}{12}} = 7 \omega_n^2$$

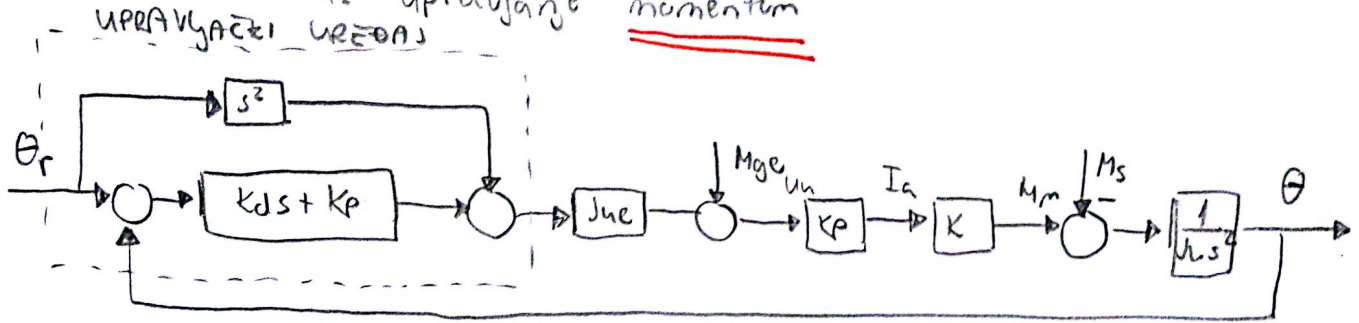
$$K_d = \frac{2 \cdot \zeta_{min}}{\sqrt{\frac{J_{min}}{K_p \cdot J_{max}}}} = \frac{2 \cdot \zeta_{min}}{\sqrt{\frac{5}{7 \cdot \frac{35}{12}}}} = 14 \zeta_{min}$$

$$M_{ge} = ?$$



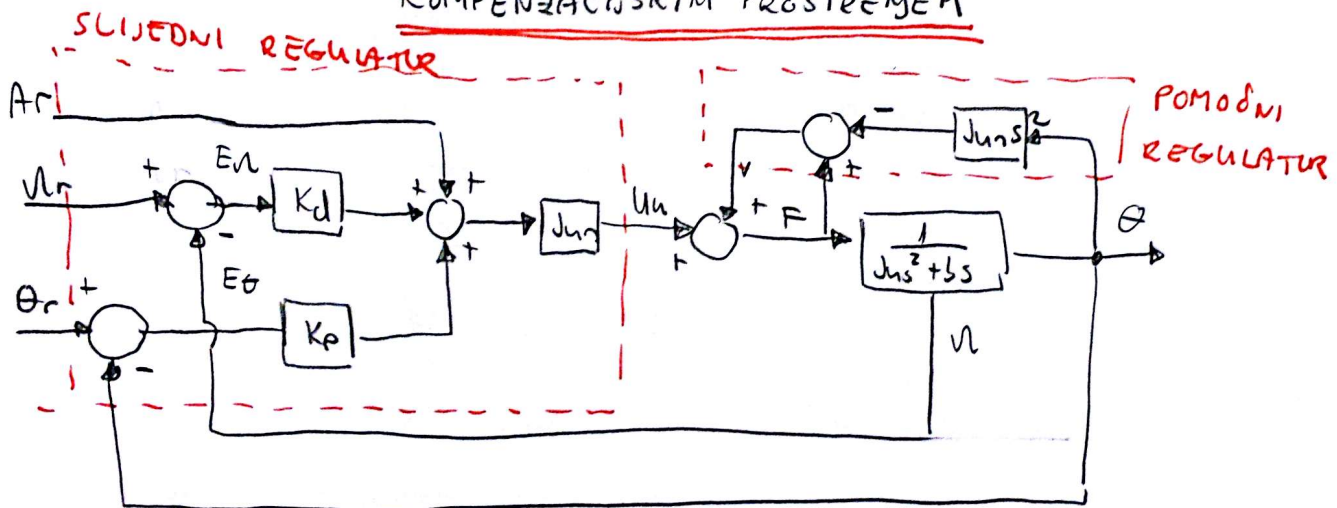
→ Blokova shema regulacijske petlje položaja

uz upravljanje momentom

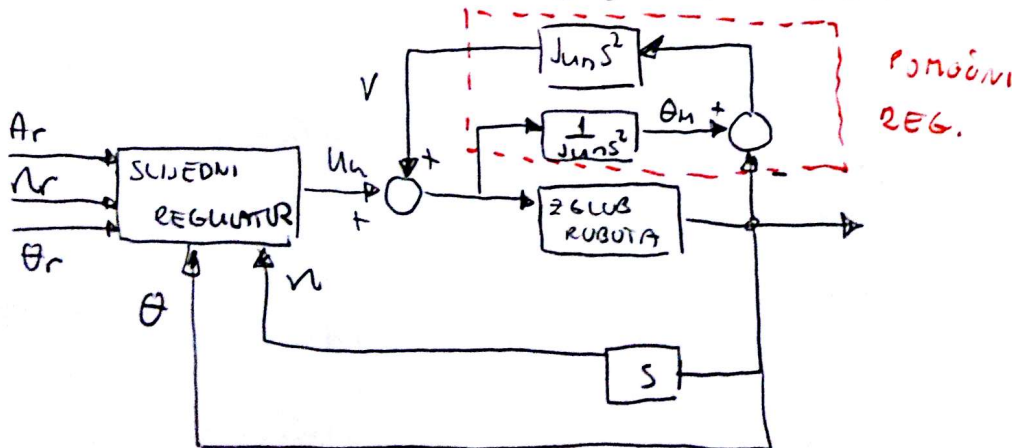


→ ISTA shema po upravljanju momentom, ali s

KOMPENZACIJSKIM PROŠIRENEM



- shema robustnog upravljanja položajem po Hsiaowu metodu
uz upravljanje po momentu



shema ADAPTIVNOG upravljanja položajem

po Hsiaowu metodu uz upravljanje po momentu