-> sharni pregek A=56.3 MM2

-> promjer d=9.6 mm

- apristeno naprezanje od = 100 NIMM2

- specificna lezina 3.45.10-2 N/m mm² = 10

- temp. kod naprezanja B=1.83.10-5 11K

= modul elasticusti E=7.7-104 NIMM2

-> Kled = 1.6

Omax = od; g = 10 11 132

a) fmax pri rasponu od 200 M a= 200 M

 $f_{\text{max}} = \frac{\alpha^2 T}{80}$

1) $\alpha_{KR} = ?$ $\alpha_{KR} = \sigma_{max} \sqrt{\frac{360\beta}{15^2 - 10^2}}$

TZ = To+Te = To+ 0.18.9.10 Kled = 0.0345+ 0.18.10.19.6 .1.6=

= 0.193 N/M MM2

 $Q_{KR} = 100 \cdot \sqrt{\frac{360 \cdot 1.89 \cdot 10^{-5}}{0.493^2 - 0.0345^2}} = 43.4387 \text{ M}$

arr < a -> Jimax ma -5°C +led

2) SKR = ?

J= Omax

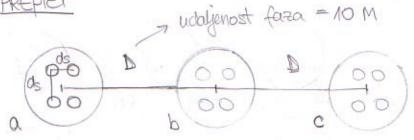
SKR = TMax (1- 10) - 5 = 100 (1- 0.0345) - 5 = 51.43°C

$$f_{\text{max}} = \frac{a^2 f_z}{8 J_{\text{max}}} = \frac{200^2 \cdot 0.493}{8.100} = \frac{9.65 \text{ M}}{9.65 \text{ M}}$$

$$\lambda = \frac{l-a}{a} \cdot 1000 \%$$

$$\lambda = \frac{\alpha^2 \sqrt{6^2}}{24 \sqrt{34^2}} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2} \cdot 1000 \% = \frac{200^2 \cdot (0.0345)^2}{24 \cdot (18.8717)^2}$$





$$D_{S} = \sqrt{(d_{S}^{2} \cdot (d_{S} \sqrt{(0.7188 r)^{4}})^{4}}$$

$$= \sqrt{(d_{S}^{3} \sqrt{2} \cdot 0.7188 r)^{4}}$$

$$= 0.1345 \text{ M}$$

r- 14 mm = 11.10⁻³ m -radigius vodica

ds=0.3 M -> rozmak vodiča u smoplu

$$\begin{array}{c|c} \alpha & \uparrow D & \downarrow \\ b & \uparrow D & \downarrow \\ \hline c & \downarrow I & \downarrow I \\ \hline 1/3 \ell & 1/3 \ell & 1/3 \ell \end{array}$$

$$1 \Big|_{L_A} = \frac{1}{3} \Big(|_{AI} + |_{AII} + |_{AII} \Big)$$

$$L_{AII} = 2.00^{-7} \text{ Im} \frac{D_{M}}{D_{S}} = 2.00^{-7} \text{ Im} \frac{1.2}{D_{S}} = 0.930 \text{ nH/km}$$

$$L_{AII} = 2.00^{-7} \text{ Im} \frac{D_{M}}{D_{S}} = 2.00^{-7} \text{ Im} \frac{10.2D}{D_{S}} = 0.930 \text{ nH/km}$$

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$$L_{BI} = 2.10^{-7} \text{ Mm} \frac{D_{M}}{D_{S}} = 2.10^{-7} \text{ Mm} \frac{\sqrt{D \cdot D}}{D_{S}} = 0.862 \text{ MH/km}$$

$$L_{BII} = 2.10^{-7} \text{ Mm} \frac{D_{M}}{D_{S}} = 2.10^{-7} \text{ Mm} \frac{\sqrt{D \cdot D}}{D_{S}} = 0.862 \text{ MH/km}$$

$$L_{BII} = 2.10^{-7} \text{ Mm} \frac{D_{M}}{D_{S}} = 2.10^{-7} \text{ Mm} \frac{\sqrt{D \cdot 2D}}{D_{S}} = 0.931 \text{ MH/km}$$

$$L_{BII} = 2.10^{-7} \text{ Mm} \frac{D_{M}}{D_{S}} = 2.10^{-7} \text{ Mm} \frac{\sqrt{D \cdot 2D}}{D_{S}} = 0.931 \text{ MH/km}$$

$$L_{CI} = 2.40^{-7} \text{ Im} \quad \frac{D_{M}}{D_{S}} = 2.40^{-7} \text{ Im} \quad \frac{10.D}{D_{S}} = 0.931 \text{ mH/km}$$

$$L_{CII} = 2.40^{-7} \text{ Im} \quad \frac{D_{M}}{D_{S}} = 2.40^{-7} \text{ Im} \quad \frac{20.D}{D_{S}} = 0.931 \text{ mH/km}$$

$$L_{CII} = 2.40^{-7} \text{ Im} \quad \frac{D_{M}}{D_{S}} = 2.40^{-7} \text{ Im} \quad \frac{10.D}{D_{S}} = 0.882 \text{ mH/km}$$

$$L_{CIII} = 2.40^{-7} \text{ Im} \quad \frac{D_{M}}{D_{S}} = 2.40^{-7} \text{ Im} \quad \frac{10.D}{D_{S}} = 0.882 \text{ mH/km}$$

· Mogli smo odnah pleati LI=LII :)

3)
$$Vad 220 \, kV$$
, during $250 \, km$.

 $Z_1 = 0.06 + j 0.32$ $-21 \, km = 0.3256 \, [+9.38^{\circ}] S^2 \, km$
 $V_1 = j3.5 \, \mu S \, km = 3.5 \cdot ho^{-6} \, [-90^{\circ}] \, S \, km$
 $S_1 = 80 - j45 \, MVA$
 $U_1 = U_1 - 920 \, kV - 7 \quad V_2 = \frac{220}{3} = 127 \cdot 0.047 \, kV$
 $AS = ?$
 $AS = S_1 - S_2$
 $Z_2 = \sqrt{\frac{Z_1}{V_1}} = 305 \cdot [-5.31^{\circ}] \, SZ$
 $I_1 - \left(\frac{S_1}{3V_1}\right)^* = 0.2089 + j0.0894 \, kA$
 $I_2 = 0.2469 + j0.2656$
 $I_3 = \frac{S_1}{3V_2} = \frac{S_1}{2} \cdot \frac{S_2}{2}$
 $I_4 = \frac{S_1}{2} = \frac{S_1}{2} \cdot \frac{S_2}{2} \cdot \frac{S_2}{2}$
 $I_5 = \frac{S_1}{2} = \frac{S_1}{2} \cdot \frac{S_2}{2} \cdot \frac{$

 $S_z = 3 \cdot (122.611 - j16.37)(0.2025 + j0.0706) =$ = 77.95 + j16.024 MVA

AS=S1-Sz = 2.05-j31.024 MVA

$$Z_{\Lambda} = 0.12 + j0.42$$
 $S_{2}|_{KM} = 0.437 [74.05^{\circ}]_{S_{2}|_{KM}}$
 $Y_{\Lambda} = j2.7 \,\mu_{S}|_{KM} = 2.7 \cdot 10^{-6} [90^{\circ}]_{S}|_{KM}$
 $Z_{C} = \sqrt{\frac{Z_{1}}{Y_{1}}} = 402.31 [-7.975^{\circ}]_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_{2}|_{S_$

$$\gamma = \sqrt{2} \sqrt{10^{-3}} = 1.086 \cdot 10^{-3} = 1.086$$

(5)

$$U_{N}=$$
 $100 \, \text{KV}$
 $300 \, \text{km}$
 $100 \, \text{KV}$
 $100 \, \text{KV}$
 $100 \, \text{KM}$
 $100 \, \text{K$

$$t_{VA} = \frac{l_1}{C_1} = \frac{l_2}{\sqrt{l_1 C_1}} = l_1 \sqrt{l_1 C_1} = 1.006 \text{ ms}$$

a) Mapon u X M 2ms

$$\alpha_2 = \frac{2 \cdot 2v_2}{2v_1 + 2v_2} = 1.007$$
 $\beta = x - 1 = 0.07$

$$U_{p_2} = U_1 \cdot \alpha_2 \cdot e^{-\frac{R_1}{L_1} \cdot t_{M_2}} = 95.953 \text{ kV}$$

$$N_3 = \frac{2R}{R + 242} = 0.692$$
 $\beta = -0.308$

Ux4ms (od reflekthranog vala u3) =
$$03r \cdot e^{-\frac{Rz}{L_2} \cdot \frac{tvz}{Z}} = -26.02 \text{ kV}$$

-prolazni val uz

= reflethrami M3

$$U_{N\Gamma} = U_{2\Gamma} \cdot \beta \cdot e^{-\frac{Rn}{Ln} \cdot t_{N\Gamma}} = -0.6356 \text{ kV}$$

$$U_{2\rho_{2}} = U_{N\Gamma} \cdot k_{2} e^{-\frac{Rn}{Ln} t_{N\Gamma}} = -0.6089 \text{ kV}$$

$$U_{X_{4MC}} = U_{2\rho_{2}} \cdot e^{-\frac{R^{2}}{L^{2}} \cdot \frac{t_{V2}}{2}} = -0.585 \text{ kV}$$

$$\downarrow \rightarrow \text{reflekhiami val } L 2$$

$$\Rightarrow \text{reflekhiami val } L 1$$