Sveučilište u Zagrebu Fakultet elektrotehnike i računarstva Zavod za elektrostrojarstvo i automatizaciju

# Projektiranje i konstruiranje u elektrostrojarstvu METODA KONAČNIH ELEMENATA

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# 1. OPIS MAGNETSKOG POLJA U STACIONARNOM STANJU MAXWELLOVIM JEDNADŽBAMA

Ampèreov kružni zakon (zakon protjecanja)

$$\oint_C \vec{H} d\vec{l} = \int_S \vec{J} \vec{n} dS \quad \Rightarrow \quad \nabla \times \vec{H} = \vec{J}$$

Gaussov zakon

$$\int_{S} \vec{B} \vec{n} dS = 0 \quad \Rightarrow \quad \nabla \cdot \vec{B} = 0$$

$$\vec{B} = \mu_0 \mu_r \vec{H} = \mu \vec{H}$$

Budući da je rotor divergencije vektorske funkcije uvijek jednak nuli, može se definirati vektorska funkcija  $\vec{A}$  koja će biti jednaka rotoru vektorske funkcije magnetske indukcije, tj.

$$\vec{B} = \nabla \times \vec{A} = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{vmatrix}$$

Funkcija  $\vec{A}$  predstavlja vektorski magnetski potencijal.

Pretpostavimo da struja teče samo u z osi. Onda iz  $\vec{A} = \frac{\mu_0}{4\pi} \int_{V}^{\vec{J}} \frac{\vec{J}}{R} dV$  slijedi da je jedino z komponenta vektorskog magnetskog potencijala različita od nule.

$$\vec{J} = \nabla \times \frac{1}{\mu} \vec{B} = \nabla \times \left( \frac{1}{\mu} \nabla \times \vec{A} \right) = \nabla \times \left( \frac{1}{\mu} \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & 0 & A_z \end{vmatrix} \right) = \nabla \times \left[ \frac{1}{\mu} \left( \frac{\partial A_z}{\partial y} \vec{i} - \frac{\partial A_z}{\partial x} \vec{j} \right) \right]$$

$$\vec{J} = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \frac{1}{\mu} \frac{\partial A_z}{\partial y} & -\frac{1}{\mu} \frac{\partial A_z}{\partial x} & 0 \end{vmatrix} = - \left[ \frac{\partial}{\partial x} \left( \frac{1}{\mu} \frac{\partial A_z}{\partial x} \right) + \frac{\partial}{\partial y} \left( \frac{1}{\mu} \frac{\partial A_z}{\partial y} \right) \right] \vec{k} + \frac{\partial}{\partial z} \left( \frac{1}{\mu} \frac{\partial A_z}{\partial x} \right) \vec{i} + \frac{\partial}{\partial z} \left( \frac{1}{\mu} \frac{\partial A_z}{\partial y} \right) \vec{j}$$

$$J_z = -\frac{\partial}{\partial x} \left( \frac{1}{\mu} \frac{\partial A_z}{\partial x} \right) - \frac{\partial}{\partial y} \left( \frac{1}{\mu} \frac{\partial A_z}{\partial y} \right)$$

Pišemo pojednostavljeno bez indeksa z

$$J = -\frac{\partial}{\partial x} \left( \frac{1}{\mu} \frac{\partial A}{\partial x} \right) - \frac{\partial}{\partial y} \left( \frac{1}{\mu} \frac{\partial A}{\partial y} \right)$$

Poissonova jednadžba

$$\Delta A = -\mu J$$

Područje I: područje kojim teče struja, permeabilnost zraka

$$\frac{\partial^2 A}{\partial x^2} + \frac{\partial^2 A}{\partial y^2} = -\mu_0 J$$

Područje II: područje kojim ne teče struja (zrak)

$$\frac{\partial^2 A}{\partial x^2} + \frac{\partial^2 A}{\partial y^2} = 0$$

Područje III: područje kojim ne teče struja (željezo)

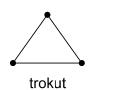
$$\frac{\partial}{\partial x} \left( \frac{1}{\mu} \frac{\partial A}{\partial x} \right) + \frac{\partial}{\partial y} \left( \frac{1}{\mu} \frac{\partial A}{\partial y} \right) = 0$$

### 2. METODA KONAČNIH ELEMENATA

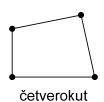
- 1. Definirati domenu na kojoj se vrši proračun
- 2. Rastaviti domenu na manja područja koristeći jednostavne oblike (trokut, četverokut...)
- 3. Kreirati mrežu
- 4. Definirati interpolacijske funkcije
- 5. Aproksimirati jednadžbu polja na svakom elementu (kreirati matricu za svaki element)
- 6. Sastaviti matričnu jednadžbu za cijelu domenu koristeći elementarne matrice
- 7. Riješiti sustav linearnih jednadžbi

#### Diskretizacija domene

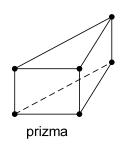
2-D



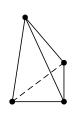
pravokutnik



3-D

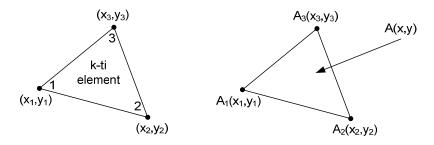


kvadar



tetraedar

#### Primjer diskretizacije 2-D domene pomoću trokuta



Uz poznavanje iznosa vektorskog magnetskog potencijala u vrhovima trokuta  $A_1(x,y)$ ,  $A_2(x,y)$  i  $A_3(x,y)$ , potencijal A(x,y) u bilo kojoj točki na površini trokuta se može interpolirati polinomom prvog, drugog ili n-tog reda. Primjena metode konačnih elemenata će biti prikazana na primjeru linearne interpolacijske funkcije.

Linearna interpolacijska funkcija

$$A = a + bx + cy$$

$$A_1 = a + bx_1 + cy_1$$

$$A_2 = a + bx_2 + cy_2$$

$$A_3 = a + bx_3 + cy_3$$

$$\begin{bmatrix} A_1 \\ A_2 \\ A_3 \end{bmatrix} = \begin{bmatrix} 1 & x_1 & y_1 \\ 1 & x_2 & y_2 \\ 1 & x_3 & y_3 \end{bmatrix} \begin{bmatrix} a \\ b \\ c \end{bmatrix}$$

$$A(x,y) = \begin{bmatrix} 1 & x & y \end{bmatrix} \begin{bmatrix} a \\ b \\ c \end{bmatrix} = \begin{bmatrix} 1 & x & y \end{bmatrix} \begin{bmatrix} 1 & x_1 & y_1 \\ 1 & x_2 & y_2 \\ 1 & x_3 & y_3 \end{bmatrix}^{-1} \begin{bmatrix} A_1 \\ A_2 \\ A_3 \end{bmatrix}$$

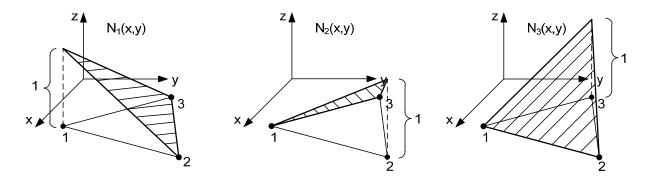
$$B^{-1} = \frac{1}{\det B} \begin{bmatrix} x_2 y_3 - x_3 y_2 & x_3 y_1 - x_1 y_3 & x_1 y_2 - x_2 y_1 \\ y_2 - y_3 & y_3 - y_1 & y_1 - y_2 \\ x_3 - x_2 & x_1 - x_3 & x_2 - x_1 \end{bmatrix} , \det B = \begin{vmatrix} 1 & x_1 & y_1 \\ 1 & x_2 & y_2 \\ 1 & x_3 & y_3 \end{vmatrix} = 2S_{\Delta}$$

$$A(x,y) = \frac{1}{2S_{\Delta}} \Big[ (x_2 y_3 - x_3 y_2) + (y_2 - y_3) x + (x_3 - x_2) y \Big] A_1 + \frac{1}{2S_{\Delta}} \Big[ (x_3 y_1 - x_1 y_3) + (y_3 - y_1) x + (x_1 - x_3) y \Big] A_2 + \frac{1}{2S_{\Delta}} \Big[ (x_1 y_2 - x_2 y_1) + (y_1 - y_2) x + (x_2 - x_1) y \Big] A_3$$

$$= N_1(x,y) A_1 + N_2(x,y) A_2 + N_3(x,y) A_3$$

$$A(x, y) = \sum_{i=1}^{3} N_i(x, y) A_i$$
,  $N_i(x, y)$  - interpolacijske funkcije

$$N_{i}(x_{j}, y_{j}) = \begin{cases} 1, & i = j \\ 0, & i \neq j \end{cases}$$
$$\sum_{i=1}^{3} N_{i}(x, y) = 1$$



Na domeni  $\Omega$  je moguće naći samo približno rješenje Poissonove jednadžbe  $\tilde{A}$  pa će u jednadžbi postojati ostatak R

$$R(x, y) = \frac{1}{\mu} \frac{\partial^2 \tilde{A}}{\partial x^2} + \frac{1}{\mu} \frac{\partial^2 \tilde{A}}{\partial y^2} + J$$

Cilj je minimizirati integral tog ostatka pomnoženog nekom težinskom funkcijom W (METODA TEŽINSKIH OSTATAKA) na cijeloj domeni, tj.

$$\int_{\Omega} W(x, y)R(x, y)dxdy = 0$$

$$-\int_{\Omega} W \left( \frac{1}{\mu} \frac{\partial^2 \tilde{A}}{\partial x^2} + \frac{1}{\mu} \frac{\partial^2 \tilde{A}}{\partial y^2} \right) dx dy = \int_{\Omega} W J dx dy$$

$$\frac{\partial}{\partial x} \left( W \frac{\partial \tilde{A}}{\partial x} \right) = \frac{\partial W}{\partial x} \frac{\partial \tilde{A}}{\partial x} + W \frac{\partial^2 \tilde{A}}{\partial x^2}$$

$$\frac{\partial}{\partial y} \left( W \frac{\partial \tilde{A}}{\partial y} \right) = \frac{\partial W}{\partial y} \frac{\partial \tilde{A}}{\partial y} + W \frac{\partial^2 \tilde{A}}{\partial y^2}$$

$$-\int_{\Omega} W \left( \frac{1}{\mu} \frac{\partial^2 \tilde{A}}{\partial x^2} + \frac{1}{\mu} \frac{\partial^2 \tilde{A}}{\partial y^2} \right) dx dy = \int_{\Omega} \frac{1}{\mu} \left( \frac{\partial W}{\partial x} \frac{\partial \tilde{A}}{\partial x} + \frac{\partial W}{\partial y} \frac{\partial \tilde{A}}{\partial y} \right) dx dy - \int_{\Omega} \frac{1}{\mu} \left[ \frac{\partial}{\partial x} \left( W \frac{\partial \tilde{A}}{\partial x} \right) + \frac{\partial}{\partial y} \left( W \frac{\partial \tilde{A}}{\partial y} \right) \right] dx dy$$

Greenov teorem izražava krivuljni integral po zatvorenoj krivulji C plošnim integralom pološnim integralom po plohi  $\Omega$  omeđenoj krivuljom C.

$$\int_{\Omega} \left( \frac{\partial P}{\partial x} + \frac{\partial Q}{\partial x} \right) dx dy = \oint_{C} -Q dx + P dy$$

$$-\int_{\Omega} \frac{1}{\mu} \left| \frac{\partial}{\partial x} \left( \underbrace{W \frac{\partial \tilde{A}}{\partial x}}_{P} \right) + \frac{\partial}{\partial y} \left( \underbrace{W \frac{\partial \tilde{A}}{\partial y}}_{O} \right) \right| dx dy = -\oint_{C} \frac{1}{\mu} \left[ -W \frac{\partial \tilde{A}}{\partial y} dx + W \frac{\partial \tilde{A}}{\partial x} dy \right]$$

Vektor normale na krivulju C je jedinični vektor koji se definira kao

$$\vec{n} = \frac{1}{\sqrt{dx^2 + dy^2}} \left( dy\vec{i} - dx\vec{j} \right)$$

Usmjerena derivacija funkcije  $\tilde{A}$  u smjeru vektora  $\vec{n}$  je jednaka

$$\frac{\partial \tilde{A}}{\partial \vec{n}} = \vec{n} \cdot \nabla \tilde{A} = \frac{1}{\sqrt{dx^2 + dy^2}} \left( \frac{\partial \tilde{A}}{\partial x} dy - \frac{\partial \tilde{A}}{\partial y} dx \right)$$

Duljina infinitenzimalnog dijela krivulje C iznosi  $dl = \sqrt{dx^2 + dy^2}$ .

Odatle slijedi da je

$$-\oint_{C} \frac{1}{\mu} \left[ -W \frac{\partial \tilde{A}}{\partial y} dx + W \frac{\partial \tilde{A}}{\partial x} dy \right] = -\oint_{C} \frac{1}{\mu} W \frac{\partial \tilde{A}}{\partial \vec{n}} dl$$

Na kraju se dobiva

$$\int_{\Omega} \frac{1}{\mu} \left( \frac{\partial W}{\partial x} \frac{\partial \tilde{A}}{\partial x} + \frac{\partial W}{\partial y} \frac{\partial \tilde{A}}{\partial y} \right) dx dy - \oint_{C} \frac{1}{\mu} W \frac{\partial \tilde{A}}{\partial \vec{n}} dl = \int_{\Omega} W J dx dy$$

Integral na cijeloj domeni se prikazuje kao suma integrala na pojedinačnim elementima

$$\sum_{e=1}^{N} \left\{ \frac{1}{\mu^{e}} \int_{\mathcal{O}_{e}} \left( \frac{\partial W^{e}}{\partial x} \frac{\partial \tilde{A}^{e}}{\partial x} + \frac{\partial W^{e}}{\partial y} \frac{\partial \tilde{A}^{e}}{\partial y} \right) dx dy - \frac{1}{\mu^{e}} \frac{\partial \tilde{A}^{e}}{\partial \vec{n}} \oint_{\mathcal{C}} W^{e} dl \right\} = J \int_{\mathcal{O}_{e}} W^{e} dx dy$$

Član  $\frac{1}{\mu^e} \frac{\partial \tilde{A}^e}{\partial \vec{n}} \oint_C W^e dl$  definira uvjete na granici. Ako se postavi  $\frac{\partial \tilde{A}^e}{\partial \vec{n}} = 0$ , onda se nameću tzv.

prirodnu rubni uvjeti, tj. polje je okomito na granicu domene.

$$\tilde{A}^e = \begin{bmatrix} N_1^e & N_2^e & N_3^e \end{bmatrix} \begin{bmatrix} \tilde{A}_1^e \\ \tilde{A}_2^e \\ \tilde{A}_3^e \end{bmatrix}$$

$$N_{1}^{e} = \frac{1}{2S_{\Lambda}} \left( a_{1}^{e} + b_{1}^{e} x + c_{1}^{e} y \right)$$

$$N_2^e = \frac{1}{2S_{\Lambda}} \left( a_2^e + b_2^e x + c_2^e y \right)$$

$$N_3^e = \frac{1}{2S_{\Lambda}} \left( a_3^e + b_3^e x + c_3^e y \right)$$

Potrebno je definirati težinsku funkciju  $W^e$ . Najčešće se koristi Galerkinova metoda kod koje su težinske funkcije jednake interpolacijskim funkcijama.

$$W^e = \begin{bmatrix} N_1^e \\ N_2^e \\ N_3^e \end{bmatrix}$$

$$\begin{split} &\frac{\partial \tilde{A}^e}{\partial x} = \frac{1}{2S_{\Delta}} \left[ b_1^e \quad b_2^e \quad b_3^e \right] \left[ \begin{array}{c} \tilde{A}_1^e \\ \tilde{A}_2^e \\ \tilde{A}_3^e \end{array} \right] \quad , \quad \frac{\partial \tilde{A}^e}{\partial y} = \frac{1}{2S_{\Delta}} \left[ c_1^e \quad c_2^e \quad c_3^e \right] \left[ \begin{array}{c} \tilde{A}_1^e \\ \tilde{A}_2^e \\ \tilde{A}_3^e \end{array} \right] \\ &\frac{\partial W^e}{\partial x} = \frac{1}{2S_{\Delta}} \left[ \begin{array}{c} b_1^e \\ b_2^e \\ b_3^e \end{array} \right] \quad , \quad \frac{\partial W^e}{\partial y} = \frac{1}{2S_{\Delta}} \left[ \begin{array}{c} c_1^e \\ c_2^e \\ c_3^e \end{array} \right] \\ &\frac{1}{\mu^e} \left( \begin{array}{c} \frac{\partial W^e}{\partial x} \frac{\partial \tilde{A}^e}{\partial x} + \frac{\partial W^e}{\partial y} \frac{\partial \tilde{A}^e}{\partial y} \\ \frac{\partial \tilde{A}^e}{\partial y} \end{array} \right) \int_{\Omega^e} dx dy = J \int_{\Omega^e} W^e dx dy \\ &\int_{\Omega^e} dx dy = S_{\Delta} \end{split}$$

Uvrštavanjem parcijalnih derivacija u integral dobiva se

$$\frac{1}{\mu^{e}} \left( \frac{\partial W^{e}}{\partial x} \frac{\partial \tilde{A}^{e}}{\partial x} + \frac{\partial W^{e}}{\partial y} \frac{\partial \tilde{A}^{e}}{\partial y} \right) \int_{\Omega^{e}} dx dy = \frac{1}{4\mu^{e} S_{\Delta}} \begin{bmatrix} \left( b_{1}^{e} \right)^{2} + \left( c_{1}^{e} \right)^{2} & b_{1}^{e} b_{2}^{e} + c_{1}^{e} c_{2}^{e} & b_{1}^{e} b_{3}^{e} + c_{1}^{e} c_{3}^{e} \\ b_{1}^{e} b_{2}^{e} + c_{1}^{e} c_{2}^{e} & \left( b_{2}^{e} \right)^{2} + \left( c_{2}^{e} \right)^{2} & b_{2}^{e} b_{3}^{e} + c_{1}^{e} c_{3}^{e} \\ b_{1}^{e} b_{3}^{e} + c_{1}^{e} c_{3}^{e} & \left( b_{2}^{e} \right)^{2} + \left( c_{2}^{e} \right)^{2} & b_{2}^{e} b_{3}^{e} + c_{2}^{e} c_{3}^{e} \\ b_{1}^{e} b_{3}^{e} + c_{1}^{e} c_{3}^{e} & \left( b_{2}^{e} \right)^{2} + \left( c_{2}^{e} \right)^{2} & b_{2}^{e} b_{3}^{e} + c_{2}^{e} c_{3}^{e} \\ b_{1}^{e} b_{3}^{e} + c_{1}^{e} c_{3}^{e} & b_{2}^{e} b_{3}^{e} + c_{2}^{e} c_{3}^{e} & \left( b_{3}^{e} \right)^{2} + \left( c_{3}^{e} \right)^{2} \end{bmatrix} \begin{bmatrix} \tilde{A}_{1}^{e} \\ \tilde{A}_{2}^{e} \\ \tilde{A}_{3}^{e} \end{bmatrix}$$

$$= \begin{bmatrix} S_{11}^{e} & S_{12}^{e} & S_{13}^{e} \\ S_{21}^{e} & S_{22}^{e} & S_{23}^{e} \\ S_{31}^{e} & S_{32}^{e} & S_{33}^{e} \end{bmatrix} \begin{bmatrix} \tilde{A}_{1}^{e} \\ \tilde{A}_{2}^{e} \\ \tilde{A}_{3}^{e} \end{bmatrix}$$

$$= \begin{bmatrix} \int_{\Omega^{e}} \left( a_{1}^{e} + b_{1}^{e} x + c_{1}^{e} y \right) dx dy \\ \int_{\Omega^{e}} \left( a_{2}^{e} + b_{2}^{e} x + c_{2}^{e} y \right) dx dy \\ \int_{\Omega^{e}} \left( a_{3}^{e} + b_{3}^{e} x + c_{3}^{e} y \right) dx dy \end{bmatrix}$$

Integral linearne funkcije oblika  $a_1^e + b_1^e x + c_1^e y$  po površini trokuta se može izračunati iz koordinata težišta trokuta na sljedeći način:

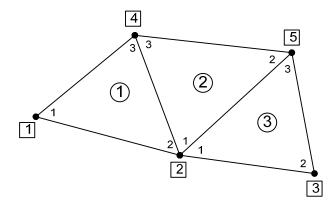
$$\int_{\Omega^e} \left( a_1^e + b_1^e x + c_1^e y \right) dx dy = \int_{\Omega^e} \left( a_1^e + b_1^e \overline{x} + c_1^e \overline{y} \right) dx dy$$

$$\overline{x} = \frac{x_1 + x_2 + x_3}{3} \quad , \quad \overline{y} = \frac{y_1 + y_2 + y_3}{3} \quad - \text{koordinate te} \\ \text{te} \\ \text{ista trokuta}$$

$$\begin{split} \frac{J}{2S_{\Delta}} & \int_{\Omega^{e}} \left( a_{1}^{e} + b_{1}^{e} x + c_{1}^{e} y \right) dx dy = \frac{J}{2S_{\Delta}} \int_{\Omega^{e}} \left[ \left( x_{2} y_{3} - x_{3} y_{2} \right) + \left( y_{2} - y_{3} \right) \frac{x_{1} + x_{2} + x_{3}}{3} + \left( x_{3} - x_{2} \right) \frac{y_{1} + y_{2} + y_{3}}{3} \right] dx dy \\ & = \frac{J}{2S_{\Delta}} \frac{1}{3} \left[ x_{2} y_{3} - x_{3} y_{2} + x_{1} (y_{2} - y_{3}) + y_{1} (x_{3} - x_{2}) \right] \int_{\Omega^{e}} dx dy \\ & = \frac{J}{2S_{\Delta}} \frac{1}{3} 2S_{\Delta} S_{\Delta} = \frac{JS_{\Delta}}{3} \\ & \frac{J}{2S_{\Delta}} \int_{\Omega^{e}} \left( a_{2}^{e} + b_{2}^{e} x + c_{2}^{e} y \right) dx dy = \frac{JS_{\Delta}}{3} \\ & J \int_{\Omega^{e}} W^{e} dx dy = \frac{JS_{\Delta}}{3} \begin{bmatrix} 1 \\ 1 \end{bmatrix} \\ & \begin{bmatrix} S_{11}^{e} & S_{12}^{e} & S_{13}^{e} \\ S_{21}^{e} & S_{22}^{e} & S_{23}^{e} \\ S_{21}^{e} & S_{22}^{e} & S_{23}^{e} \end{bmatrix} \begin{bmatrix} \tilde{A}_{1}^{e} \\ \tilde{A}_{2}^{e} \end{bmatrix} = \frac{JS_{\Delta}}{3} \begin{bmatrix} 1 \\ 1 \end{bmatrix} \end{split}$$

#### Kreiranje globalne "Stiffness" matrice

Primjer: N=3 (broj elemenata), n=5 (broj čvorova), dimenzije matrice n×n Element 1 je vodič s gustoćom struje J<sub>0</sub>. Na čvorovima 3 i 5 su postavljeni Dirichletovi rubni uvjeti (A=0)



 $S_{mn}$  – suma svih  $S_{ij}^e$  za sve elemente e koji imaju zajedničke čvorove m i n

 $S_{11} = S_{11}^1$  - zato što globalni čvor 🗓 pripada samo elementu 1

$$S_{22} = S_{22}^1 + S_{11}^2 + S_{11}^3$$

$$S_{33} = S_{22}^3$$

$$S_{44} = S_{33}^1 + S_{33}^2$$

$$S_{55} = S_{22}^2 + S_{33}^3$$

$$S_{12} = S_{21} = S_{12}^1$$

$$S_{13} = S_{31} = 0$$

$$S_{14} = S_{41} = S_{13}^1$$

$$S_{15} = S_{51} = 0$$

$$S_{23} = S_{32} = S_{12}^3$$

$$S_{24} = S_{42} = S_{23}^1 + S_{13}^2$$

$$S_{25} = S_{52} = S_{12}^2 + S_{13}^3$$

$$S_{35} = S_{53} = S_{23}^3$$

$$S_{34} = S_{43} = 0$$

$$S_{45} = S_{54} = S_{32}^2$$

Matrica *S* je simetrična, singularna i rijetko popunjena.

$$\begin{bmatrix} S_{11}^{1} & S_{12}^{1} & 0 & S_{13}^{1} & 0 \\ S_{12}^{1} & S_{22}^{1} + S_{11}^{2} + S_{13}^{3} & S_{12}^{3} & S_{23}^{1} + S_{13}^{2} & S_{12}^{2} + S_{13}^{3} \\ 0 & S_{12}^{3} & S_{22}^{1} & 0 & S_{33}^{1} + S_{33}^{2} & S_{22}^{2} \\ S_{13}^{1} & S_{12}^{1} + S_{13}^{2} & 0 & S_{33}^{1} + S_{33}^{2} & S_{32}^{2} \\ 0 & S_{12}^{2} + S_{13}^{3} & S_{23}^{3} & S_{32}^{2} & S_{22}^{2} + S_{33}^{3} \end{bmatrix} \begin{bmatrix} A_{1} \\ A_{2} \\ A_{3} \\ A_{4} \\ A_{5} \end{bmatrix} = \begin{bmatrix} \frac{J_{0}S_{\Delta}^{1}}{3} \\ \frac{J_{0}S_{\Delta}^{1}}{3} \\ 0 \\ \frac{J_{0}S_{\Delta}^{1}}{3} \\ 0 \\ \frac{J_{0}S_{\Delta}^{1}}{3} \\ 0 \\ 0 \end{bmatrix}$$

Nakon primjene Dirichletovih rubnih uvjeta dobiva se

$$\begin{bmatrix} S_{11}^{1} & S_{12}^{1} & 0 & S_{13}^{1} & 0 \\ S_{12}^{1} & S_{22}^{1} + S_{11}^{2} + S_{11}^{3} & S_{12}^{3} & S_{23}^{1} + S_{13}^{2} & S_{12}^{2} + S_{13}^{3} \\ 0 & 0 & 1 & 0 & 0 \\ S_{13}^{1} & S_{23}^{1} + S_{13}^{2} & 0 & S_{33}^{1} + S_{33}^{2} & S_{32}^{2} \\ 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} A_{1} \\ A_{2} \\ A_{3} \\ A_{4} \\ A_{5} \end{bmatrix} = \begin{bmatrix} \frac{J_{0}S_{\Delta}^{1}}{3} \\ \frac{J_{0}S_{\Delta}^{1}}{3} \\ 0 \\ \frac{J_{0}S_{\Delta}^{1}}{3} \\ 0 \\ \frac{J_{0}S_{\Delta}^{1}}{3} \\ 0 \\ 0 \end{bmatrix}$$

Proračun magnetske indukcije

$$\vec{B} = \nabla \times \vec{A} = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & 0 & A_z \end{vmatrix} = \vec{i} \frac{\partial A_z}{\partial y} - \vec{j} \frac{\partial A_z}{\partial x} \quad \Rightarrow \quad B_x = \frac{\partial A_z}{\partial y} \quad , \quad B_y = -\frac{\partial A_z}{\partial x}$$

$$B_{x} = \frac{1}{2S_{\Delta}} \left( c_{1}^{e} \tilde{A}_{1}^{e} + c_{2}^{e} \tilde{A}_{2}^{e} + c_{3}^{e} \tilde{A}_{3}^{e} \right)$$

$$B_{y} = -\frac{1}{2S_{\Lambda}} \Big( b_{1}^{e} \tilde{A}_{1}^{e} + b_{2}^{e} \tilde{A}_{2}^{e} + b_{3}^{e} \tilde{A}_{3}^{e} \Big)$$

Magnetska indukcija je konstantna na cijeloj površini elementa.

#### 3. LITERATURA

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