

A time-dependent central core model and a schematic model for passive mechanism

Chanoknun Sintavanuruk

July 25, 2023

Time-dependent model

- Model equations

- Non-dimensionalization & numerical simulation

Schematic model for passive mechanism

Time-dependent model

Multiphasic medulla on the domain $(0, L)$ (superficial \rightarrow deep).

1. Central core ($k = 0$)
2. Descending tubule ($k = D$)
3. Ascending tubule ($k = A$)
4. Collecting tubule ($k = C$)

Cross-sectional areas

Cross-sectional areas α_k (cm²) satisfy

$$\sum_k \alpha_k = \alpha_* \quad (1.1)$$

where $\alpha_* : (0, L) \rightarrow \mathbb{R}_+$ is the fixed medullary cross-sectional area.

Cross-sectional areas

Cross-sectional areas α_k (cm²) satisfy

$$\sum_k \alpha_k = \alpha_* \quad (1.1)$$

where $\alpha_* : (0, L) \rightarrow \mathbb{R}_+$ is the fixed medullary cross-sectional area.

$$\frac{\partial \alpha_k}{\partial t} + \frac{\partial}{\partial x} (\alpha_k u_k) = -\beta_k w_k, \quad k = D, A, C, \quad (1.2)$$

$$\frac{\partial \alpha_0}{\partial t} + \frac{\partial}{\partial x} (\alpha_0 u_0) = \sum_{k=D,A,C} \beta_k w_k. \quad (1.3)$$

u_k : axial flow *velocity* (cm/s); w_k : transmural flux (cm/s); β_k :
total tubular circumferences (cm)

Water flow and transport

Poiseuille's equation:

$$\frac{8\pi\eta_k u_k}{\alpha_k} = -\frac{\partial p_k}{\partial x}, \quad k = 0, D, A, C, \quad (1.4)$$

η_k : viscosity (mmHg·s), p_k : pressure (mmHg).

Water flow and transport

Poiseuille's equation:

$$\frac{8\pi\eta_k u_k}{\alpha_k} = -\frac{\partial p_k}{\partial x}, \quad k = 0, D, A, C, \quad (1.4)$$

η_k : viscosity (mmHg·s), p_k : pressure (mmHg).

Water transport:

$$w_k := \zeta_k (\psi_k - \psi_0), \quad k = D, A, C \quad (1.5)$$

$$\left. \begin{aligned} \psi_k &:= p_k - \pi_k, \\ \pi_k &:= RT \left(2c_s^k + c_u^k \right), \end{aligned} \right\} \quad k = 0, D, A, C. \quad (1.6)$$

ζ_k : water permeability (mmHg·s); c_i^k : concentration (mmol/cm³)

Pressure-compliance relationship

Given tubular compliance ν_k (mmHg^{-1}), we assume

$$\nu_k(p_k - p_0) = \frac{\alpha_k}{\bar{\alpha}_k} - 1, \quad k = \text{D, A, C}. \quad (1.7)$$

Note that p_0 is determined by the medullary volume conservation (1.1).

$$\frac{\partial}{\partial t} (\alpha_k c_i^k) = -\frac{\partial}{\partial x} f_i^k - \beta_k g_i^k, \quad k = D, A, C, \quad (1.8)$$

$$\frac{\partial}{\partial t} (\alpha_0 c_i^0) = -\frac{\partial}{\partial x} f_i^0 + \sum_{k=D,A,C} \beta_k g_i^k, \quad (1.9)$$

f_i^k : Axial solute flow (mmol/s):

$$f_i^k := \alpha_k \left(-D_i^k \frac{\partial c_i^k}{\partial x} + u_k c_i^k \right), \quad k = 0, D, A, C. \quad (1.10)$$

D_i^k : diffusion coefficient (cm²/s).

g_i^k : transmural solute flux (mmol/cm²·s),

solute transport

g_i^k : transmural solute flux (mmol/cm²·s), (adapted from Stephenson et al. [1987, 1989]):

$$g_i^k := j_i^k + h_i^k, \quad k = D, A, C, \quad (1.11)$$

$$j_i^k = \gamma_i^k \left(c_i^k - c_i^0 \right), \quad k = 0, D, A, C. \quad (1.12)$$

γ_i^k : solute permeability (cm/s).

h_i^k : active transport:

$$h_s^A = \begin{cases} \frac{h_{s,\max}^A}{1+M/c_s^A} & \text{in } (0, \frac{L}{3}) \\ 0 & \text{in } [\frac{L}{3}, L), \end{cases} \quad (1.13)$$

where M is the Michaelis-Menten constant.

Boundary condition: central core

No flux at the bottom:

$$u_0(t, L) = 0, \quad (1.14)$$

$$f_i^0(t, L) = 0, \quad i = \text{s, u}. \quad (1.15)$$

Dirichlet boundary at the cortico-medullary junction:

$$p_0(t, 0) = P_v(t), \quad (1.16)$$

$$c_i^0(t, 0) = c_i^v(t). \quad (1.17)$$

Boundary condition: descending tubule

Input from the PCT:

$$(\alpha_D u_D)(t, 0) = F_{\text{PCT}}(t), \quad (1.18)$$

$$c_i^D(t, 0) = c_i^{\text{PCT}}(t), \quad i = \text{s, u}, \quad (1.19)$$

Tip of the loop of Henle:

$$(\alpha_D u_D + \alpha_A u_A)(t, L) = 0, \quad (1.20)$$

$$\left(f_i^D + f_i^A\right)(t, L) = 0, \quad (1.21)$$

$$p_D(t, L) = p_A(t, L), \quad (1.22)$$

$$c_i^D(t, L) = c_i^A(t, L) \quad (1.23)$$

Boundary condition: modification by distal tubules

Assumption: salt from the ascending tubule is further reabsorbed so that only a fraction of $q \in (0, 1)$ are left at the collecting tubule; formally,

$$\left(f_u^A + f_u^C\right)(t, 0) = 0, \quad (1.24)$$

$$\left(qf_s^A + f_s^C\right)(t, 0) = 0. \quad (1.25)$$

Further, we assume that

$$p_A(t, 0) = p_C(t, 0), \quad (1.26)$$

$$f_i^A(t, L) = (\alpha_A u_A c_i^A)(t, L), \quad i = s, u, \quad (1.27)$$

$$(2c_s^C + c_u^C)(t, 0) = \text{osm}_{\text{cortex}}(t), \quad (1.28)$$

where the cortical osmolarity $\text{osm}_{\text{cortex}}$ is given.

Boundary condition: papillary outflow

$$p_C(t, L) = P_p(t), \quad (1.29)$$

$$f_i^C(t, L) = (\alpha_C u_C c_i^C)(t, L), \quad i = s, u, \quad (1.30)$$

where P_p is the papillary pressure.

Introduce spatial rescaling and advective timescale:

$$x = L\hat{x}, \quad t = \tau\hat{t}, \quad \tau := \frac{L}{p_*/\rho_*L} = \frac{8\pi\eta_*L^2}{\bar{\alpha}c_*RT} \quad (1.31)$$

where the subscript $*$ denotes the typical magnitude of physical quantities; here $p_* = c_*RT$ and $\rho_* = 8\pi\eta_*/\bar{\alpha}$ are those of pressure and hydraulic resistivity with $\bar{\alpha} = \frac{1}{L} \int_0^L \alpha_*(x) dx$.

Unknowns:

$$\alpha_k = \bar{\alpha}\hat{\alpha}, \quad c_i^k = c_*\hat{c}_i^k, \quad p_k = p_*\hat{p}_k = c_*RT\hat{p}_k. \quad (1.32)$$

$$\frac{\partial \hat{\alpha}_k}{\partial \hat{t}} + \frac{\partial}{\partial \hat{x}} (\hat{\alpha}_k \hat{u}_k) = -\hat{w}_k, \quad (1.33)$$

$$\frac{\partial \hat{\alpha}_0}{\partial \hat{t}} + \frac{\partial}{\partial \hat{x}} (\hat{\alpha}_0 \hat{u}_0) = \sum_k \hat{w}_k, \quad (1.34)$$

$$\hat{\nu}_k (\hat{p}_k - \hat{p}_0) = \frac{\hat{\alpha}_k}{\hat{\hat{\alpha}}_k} - 1, \quad (1.35)$$

$$\hat{\alpha}_0 + \sum_k \hat{\alpha}_k = \hat{\alpha}_*, \quad (1.36)$$

$$\frac{\partial}{\partial \hat{t}} (\hat{\alpha}_k \hat{c}_i^k) = -\frac{\partial}{\partial \hat{x}} \hat{f}_i^k - \hat{g}_i^k, \quad (1.37)$$

$$\frac{\partial}{\partial \hat{t}} (\hat{\alpha}_0 \hat{c}_i^0) = -\frac{\partial}{\partial \hat{x}} \hat{f}_i^0 + \sum_k \hat{g}_i^k, \quad (1.38)$$

$$\hat{u}_k := -\frac{\hat{\alpha}_k}{\hat{\rho}_k} \frac{\partial \hat{p}_k}{\partial \hat{x}}, \quad (1.39)$$

$$\hat{f}_i^k := \hat{\alpha}_k \left(-\hat{D}_i^k \frac{\partial \hat{c}_i^k}{\partial \hat{x}} + \hat{u}_k \hat{c}_i^k \right), \quad (1.40)$$

$$\hat{w}_k := \hat{\zeta}_k \left(\hat{\psi}_k - \hat{\psi}_0 \right), \quad \hat{\psi}_k := \hat{p}_k - \left(2\hat{c}_s^k + \hat{c}_u^k \right), \quad (1.41)$$

$$\hat{g}_i^k := \hat{j}_i^k + \hat{h}_i^k, \quad \hat{j}_i^k = \hat{\gamma}_i^k (\hat{c}_i^k - \hat{c}_i^0). \quad (1.42)$$

$$\hat{h}_s^A = \begin{cases} \frac{\hat{h}_{s,\max}^A}{1 + \hat{M}/\hat{c}_s^A} & \text{in } (0, \frac{1}{3}) \\ 0 & \text{in } [\frac{1}{3}, 1) \end{cases} \quad (1.43)$$

Parameters and boundary conditions

Parameters (note that β_k is absorbed into $\hat{\zeta}_i^k, \hat{\zeta}_w^k$):

$$\begin{aligned}\hat{\rho}_k &= \frac{8\pi\eta_k}{\rho_*}, & \hat{\nu}_k &= p_*\nu_k, & \hat{\bar{\alpha}}_k &= \frac{\bar{\alpha}_k}{\bar{\alpha}}, & \hat{\alpha}_* &= \frac{\alpha_*}{\bar{\alpha}} \\ \hat{D}_i^k &= \frac{\tau}{L^2}D_i^k, & \hat{\zeta}_k &= \frac{\beta_k p_* \tau}{\bar{\alpha}}\zeta_k, & \hat{\gamma}_i^k &= \frac{\beta_k p_* \tau}{\bar{\alpha}c_*^2}\gamma_i^k, \\ \hat{h}_s^A &= \frac{\beta_A \tau}{\bar{\alpha}c_*}h_s^A, & \hat{M} &= \frac{M}{c_*}.\end{aligned}$$

Boundary conditions are the same but with $\hat{\cdot}$ notation where

$$\begin{aligned}F_{\text{PCT}} &= \frac{\bar{\alpha}L}{\tau}\hat{F}_{\text{PCT}}, & P_p &= p_*\hat{P}_p, & P_v &= p_*\hat{P}_v, \\ c_i^v &= c_*\hat{c}_i^v, & \text{osm}_{\text{cortex}} &= c_*\widehat{\text{osm}}_{\text{cortex}}.\end{aligned}$$

Numerical simulation

- Approximation: backward difference for time derivatives and central difference for spatial derivatives. Then, use an iterative method.
- Most parameters except for D_i^k when $k \neq 0$, η_k , P_v , P_p , ν_k , q are available in [Stephenson et al. \[1987, 1989\]](#) which uses transfusion data in rabbit; these 6 will be chosen empirically.
- The simulated solution appears to converge to a steady state.

Parameters

Physical and geometric parameters (take $\bar{\alpha}_k = \pi r^2$, $\beta_k = 2\pi r_k$, $\alpha_* = \sum_k \bar{\alpha}_k$):

D_s^0	D_u^0	$D_i^k, k \neq 0$	η_k	ν_k	r_0	r_D	r_A	r_C
$(\times 10^{-4} \text{ cm}^2/\text{s})$			$(\text{cP} \approx 7.5 \times 10^{-6} \text{ mmHg}\cdot\text{s})$	(mmHg^{-1})	$(\times 10^{-3} \text{ cm})$			
2.5	2	0.15	0.6915	0.0517	2.5	0.8	1	1.2

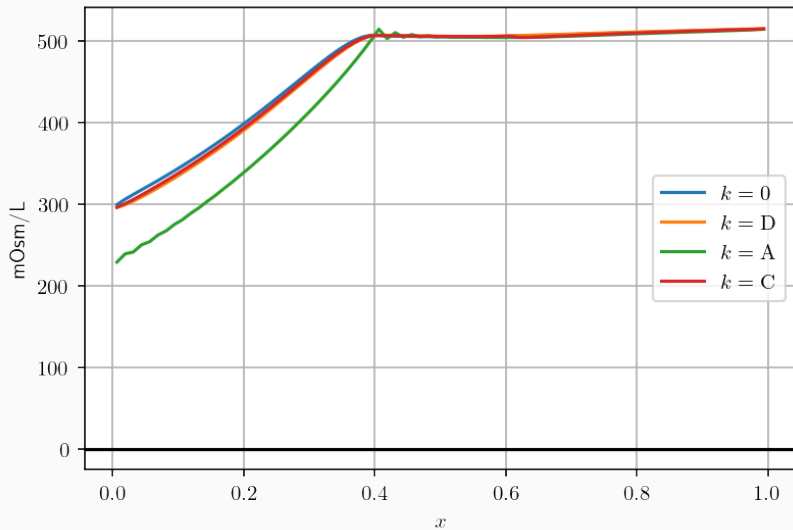
Transport parameters:

ζ_D	ζ_A	ζ_C	γ_s^D	γ_s^A	γ_s^C	γ_u^D	γ_u^A	γ_u^C	$h_{s,\max}^A$	M
$(\times 10^{-8} \text{ cm/mmHg}\cdot\text{s})$			$(\times 10^{-5} \text{ cm/s})$						$(\frac{10^{-6} \text{ mmol}}{\text{cm}^2 \cdot \text{s}})$	$(\frac{\text{mmol}}{\text{cm}^3})$
22.5	0	3.95	1.61	6.27	0.04	1.5	0.86	0	14.2	0.15
33.8	0	3.95	1.61	26.0	0.04	1.5	6.70	0	0	
26.4	0	3.95	1.61	26.0	0.04	1.5	6.70	1.5	0	

Boundary data

F_{PCT}	P_p	P_v	c_s^v	c_u^v	$\text{osm}_{\text{cortex}}$
$(\times 10^{-7} \text{ cm}^3/\text{s})$	(mmHg)		(mmol/L)		
1.67	6.4	0	145	5	295

Result



Schematic model for passive mechanism

- We want to have a clean picture of what makes passive mechanism working.
- Derive a schematic model of *inner medulla* based on the common explanation of passive mechanism:

Concept of passive mechanism

The net water and NaCl reabsorption preceding the inner medulla collecting tubules concentrate the urea enough that it diffuses out in the inner medulla. This in turn increases osmolality in the interstitium that drives the water reabsorption from the thin descending limbs, concentrating NaCl in the process. NaCl is then passively reabsorbed at the ascending tubule.

Consider a steady state of the previous dimensionless model but rescale $\hat{x} \in (0, 1)$ to be the *inner medulla* instead (from now on, we omit the $\hat{\cdot}$ notation). We further make simplifying assumptions that

- The descending and ascending tubule urea concentration and the collecting tubule salt concentration are negligible.
- Zero salt permeability in the descending tubule.

Rewriting $q_k = \alpha_k u_k$, $s_k = c_s^k$, $u_k = c_u^k$, $\gamma_s = \gamma_s^A$, $\gamma_u = \gamma_u^C$, and assuming that $1/\nu_k$ and D_i^k are small, we arrive at the leading order equations:

$$\frac{dq_D}{dx} = -\zeta_D (2s_0 + u_0 - 2s_D) = -w_D, \quad \frac{d}{dx}(s_D q_D) = 0, \quad (2.5)$$

(2.1)

$$\frac{d}{dx}(s_A q_A) = -\gamma_s(s_A - s_0), \quad (2.6)$$

$$\frac{dq_A}{dx} = 0, \quad (2.2)$$

$$\frac{dq_C}{dx} = -\zeta_C (2s_0 + u_0 - u_C) = -w_C, \quad \frac{d}{dx}(s_0 q_0) = \gamma_s(s_A - s_0), \quad (2.7)$$

(2.3)

$$\frac{d}{dx}(u_C q_C) = -\gamma_u(u_C - u_0), \quad (2.8)$$

$$\frac{dq_0}{dx} = w_D + w_C, \quad (2.4)$$

$$\frac{d}{dx}(u_0 q_0) = \gamma_u(u_C - u_0). \quad (2.9)$$

9 unknowns: the water flow q_D, q_A, q_C, q_0 and the solute concentrations s_D, s_A, s_0, u_C, u_0 . (Note that in the limit as $1/\nu_k \searrow 0$, p_k are identical.)

The ODEs are completed with 9 boundary conditions:

$$q_D(0) = \frac{2S}{C}, \quad q_A(1) = -q_D(1), \quad q_C(0) = \frac{U}{C}, \quad q(1) = 0. \quad (2.10)$$

$$2s_D(0) = u_C(0) = C, \quad (2.11)$$

$$\frac{2S}{C} + q_0(0) + q_A + \frac{U}{C} = q_C(1), \quad (2.12)$$

$$S + q_A(0)s_A(0) + s_0(0)q_0(0) = 0, \quad (2.13)$$

$$U + u_0(0)q_0(0) = u_C(1)q_C(1). \quad (2.14)$$

The problem can be reduced even further!

After some tedious calculation, we can explicitly solve for q_A , q_0 , s_D , s_0 , u_0 in terms of q_D , q_C , s_A , u_C . Hence, this problem is equivalent to

$$\frac{dq_D}{dx} = -\zeta_D \left(2s_0 + u_0 - \frac{2S}{q_D} \right) \quad (2.15)$$

$$\frac{ds_A}{dx} = -\frac{\gamma_s}{q_A} (s_A - s_0), \quad (2.16)$$

$$\frac{dq_C}{dx} = -\zeta_C (2s_0 + u_0 - u_C), \quad (2.17)$$

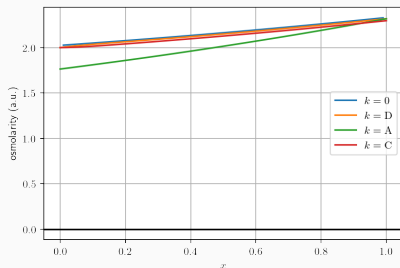
$$\frac{du_C}{dx} = \frac{1}{q_C} (\zeta_C u_C (2s_0 + u_0 - u_C) - \gamma_u (u_C - u_0)), \quad (2.18)$$

with boundary conditions

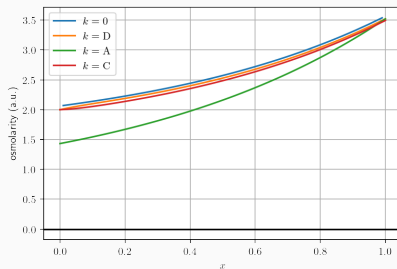
$$q_D(0) = \frac{2S}{C}, \quad s_A(1) = S/q_D(1), \quad q_C(0) = \frac{U}{C}, \quad u_C(0) = C. \quad (2.19)$$

Exploring passive mechanism

The system of ODEs is approximated using central difference scheme, then solved using an iterative method.

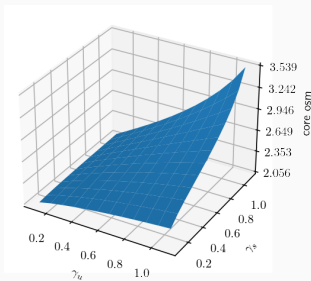


(a) $\gamma_u = \gamma_s = 0.1$

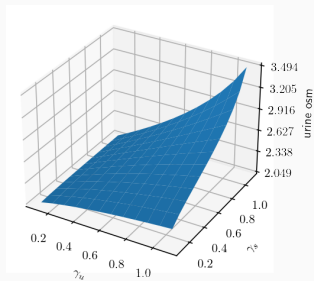


(b) $\gamma_u = \gamma_s = 1.2$

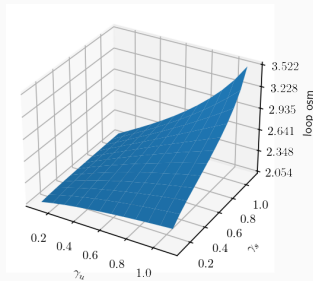
Figure 1: $\zeta_D = \zeta_C = 10$, $S = 1$, $U = 2$, $C = 2$



(a) papillary core osmolarity



(b) urine osmolarity



(c) osmolarity at the turning of Henle's loop

Conclusion #1: urea is an 'enabler' of salt reabsorption, while both salt and urea act as sources of osmotic drive.

Long-short loop proportion

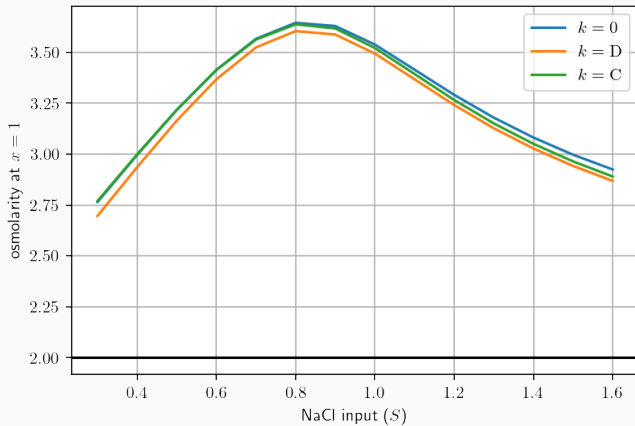


Figure 3: $\zeta_D = \zeta_C = 10$, $\gamma_u = \gamma_s = 1.2$, $U = 2$, $C = 2$

References

- J. L. Stephenson, Y. Zhang, A. Eftekhari, and R. Tewarson. Electrolyte transport in a central core model of the renal medulla. *American Journal of Physiology-Renal Physiology*, 253(5):F982–F997, November 1987. doi: 10.1152/ajprenal.1987.253.5.f982. URL <https://doi.org/10.1152/ajprenal.1987.253.5.f982>.
- J. L. Stephenson, Y. Zhang, and R. Tewarson. Electrolyte, urea, and water transport in a two-nephron central core model of the renal medulla. *American Journal of Physiology-Renal Physiology*, 257(3):F399–F413, September 1989. doi: 10.1152/ajprenal.1989.257.3.f399. URL <https://doi.org/10.1152/ajprenal.1989.257.3.f399>.