

Modyfikacje/hybrydyzacje algorytmu PSO w zadaniu optymalizacji globalnej wielowymiarowej funkcji ciaglej

PSO-DE Hybrid

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ABSTRACT

Dokumentacja uzyskanych wyników hybrydy PSO-DE

Categories and Subject Descriptors

G.1.6 [Numerical Analysis]: Optimization—*global optimization, unconstrained optimization*; F.2.1 [Analysis of Algorithms and Problem Complexity]: Numerical Algorithms and Problems

General Terms

Algorithms

Keywords

Benchmarking, PSODE, Optymalizacja wielowymiarowej funkcji ciaglej

of trials that actually reached f_t [?, ?]. **Statistical significance** is tested with the rank-sum test for a given target Δf_t (10^{-8} as in Figure 1) using, for each trial, either the number of needed function evaluations to reach Δf_t (inverted and multiplied by -1), or, if the target was not reached, the best Δf -value achieved, measured only up to the smallest number of overall function evaluations for any unsuccessful trial under consideration.

1. CPU TIMING

In order to evaluate the CPU timing of the algorithm, we have run the **PSO-DE Hybrid** on the function f_8 with restarts for at least 30 seconds and until a maximum budget equal to $400(D + 2)$ is reached. The code was run on a **Mac Intel(R) Core(TM) i5-2400S CPU @ 2.50GHz** with **1** processor and **4** cores. The time per function evaluation for dimensions 2, 3, 5, 10, 20, **40** equals **$x.x$, $x.x$, $x.x$, $x.x$, xxx , and xxx** milliseconds respectively.

repeat the above for the second algorithm

2. RESULTS

Results from experiments according to [?] on the benchmark functions given in [?, ?] are presented in Figures 1, 2 and 3 and in Table 1. The **expected running time (ERT)**, used in the figures and table, depends on a given target function value, $f_t = f_{\text{opt}} + \Delta f$, and is computed over all relevant trials as the number of function evaluations executed during each trial while the best function value did not reach f_t , summed over all trials and divided by the number

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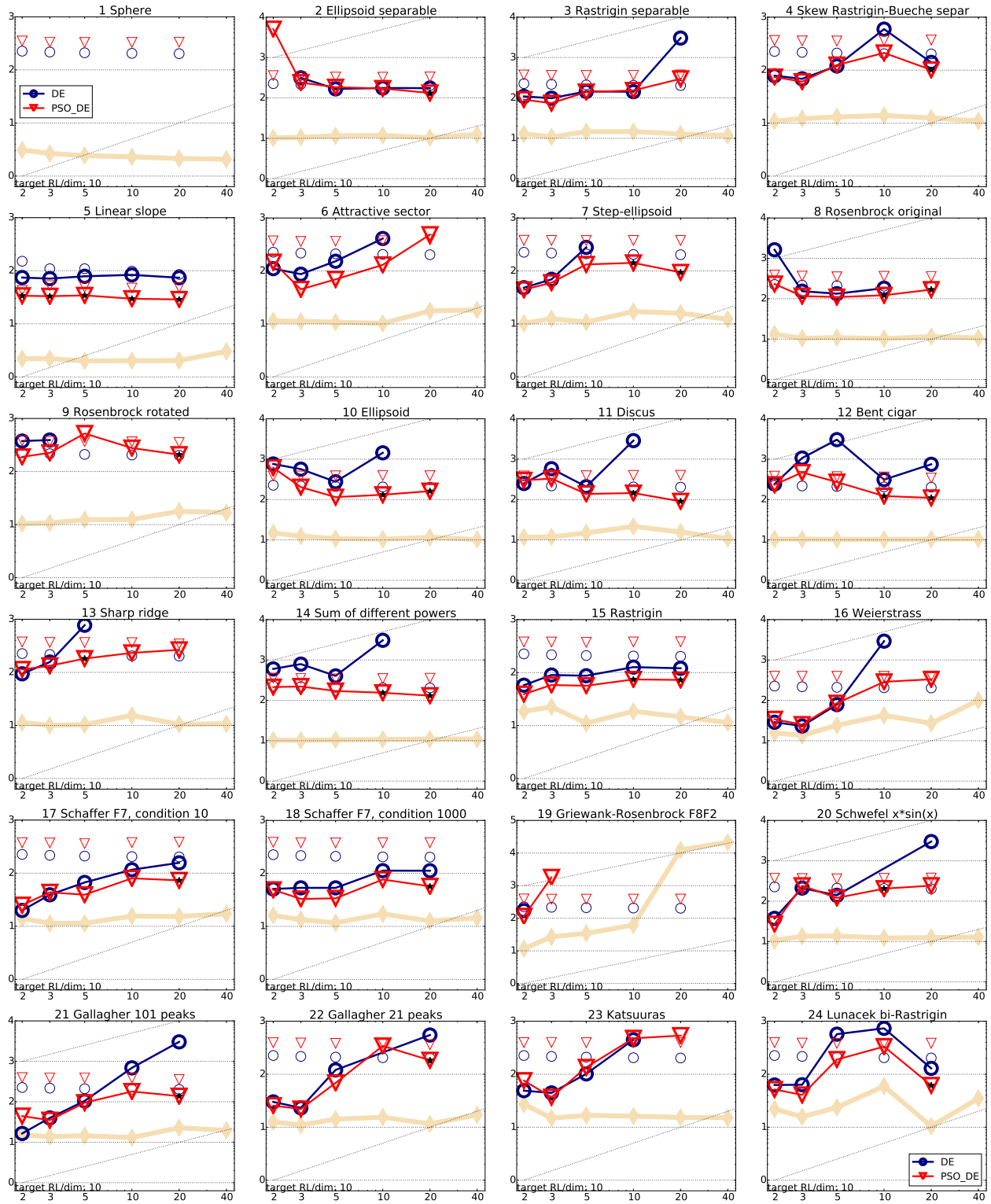


Figure 1: Expected running time (ERT in number of f -evaluations as \log_{10} value) divided by dimension versus dimension. The target function value is chosen such that the bestGECCO2009 artificial algorithm just failed to achieve an ERT of $10 \times \text{DIM}$. Different symbols correspond to different algorithms given in the legend of f_1 and f_{24} . Light symbols give the maximum number of function evaluations from the longest trial divided by dimension. Black stars indicate a statistically better result compared to all other algorithms with $p < 0.01$ and Bonferroni correction number of dimensions (six). Legend: \circ :DE, ∇ :PSO_DE.

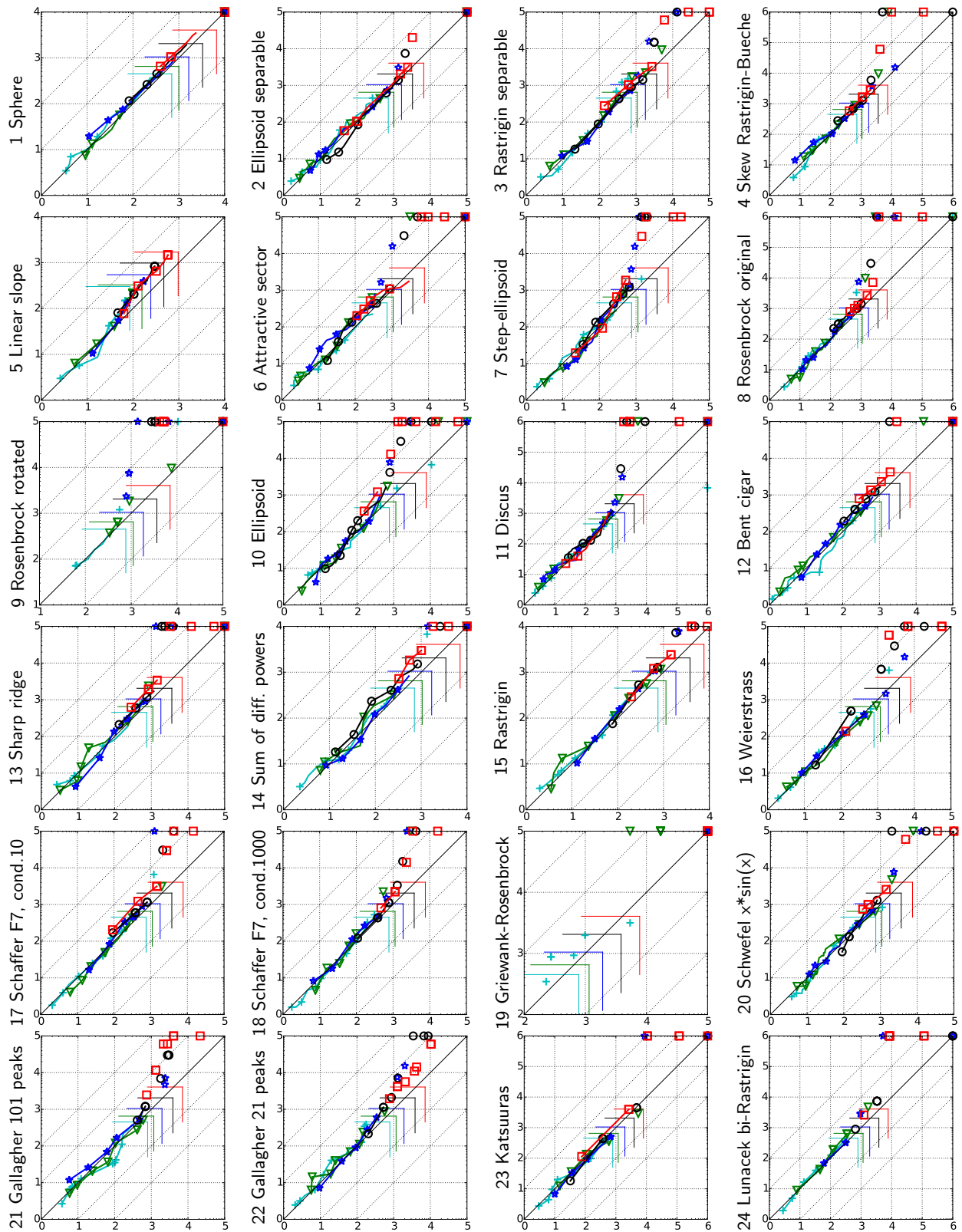


Figure 2: Expected running time (ERT in \log_{10} of number of function evaluations) of DE (y -axis) versus PSO DE (x -axis) for 8 runlength-based target function values for budgets between $0.5 \times \text{DIM}$ and $50 \times \text{DIM}$ evaluations. Each runlength-based target f -value is chosen such that the ERTs of the bestGECCO2009 artificial algorithm for the given and a slightly easier target bracket the reference budget. Markers on the upper or right edge indicate that the respective target value was never reached. Markers represent dimension: 2:+, 3:▽, 5:*, 10:○, 20:□, 40:◇.

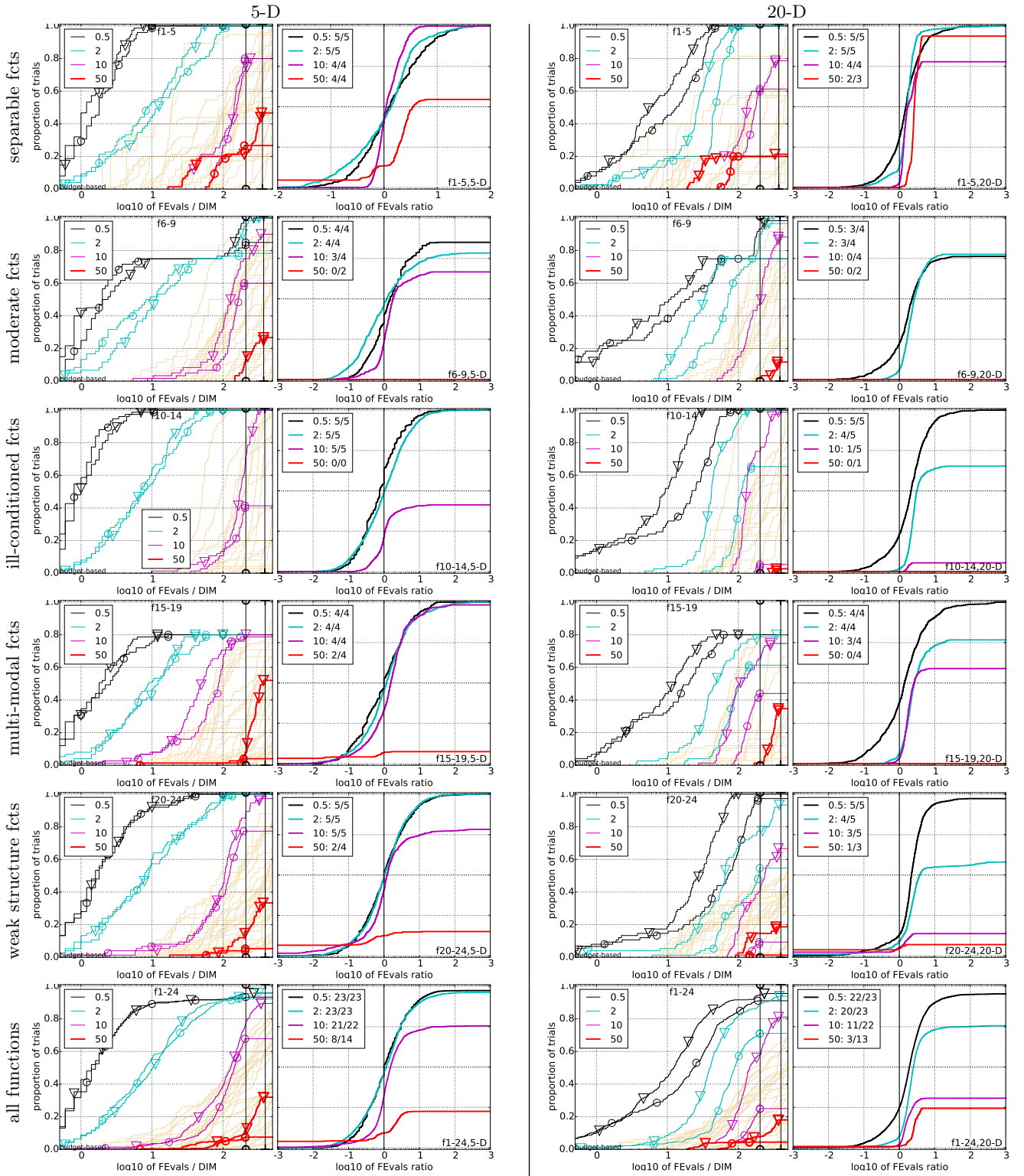


Figure 3: Empirical cumulative distributions (ECDF) of run lengths and speed-up ratios in 5-D (left) and 20-D (right). Left sub-columns: ECDF of the number of function evaluations divided by dimension D (FEvals/ D) to fall below $f_{\text{opt}} + \Delta f$ for DE (\circ) and PSO DE (∇) where Δf is the target just not reached by the GECCO-BBOB-2009 best algorithm within a budget of $k \times \text{DIM}$ evaluations, with k being the value in the legend. Right sub-columns: ECDF of FEval ratios of DE divided by PSO DE for run-length-based targets; all trial pairs for each function. Pairs where both trials failed are disregarded, pairs where one trial failed in the limits being > 0 or < 1 . The legends indicate the target budget of $k \times \text{DIM}$ evaluations and, after the colon, the number of functions that were solved in at least one trial (DE first).

5-D

#FEs/D	0.5	1.2	3	10	50	#succ
f₁	<i>2.5e+1:4.8</i>	<i>1.6e+1:7.6</i>	<i>1.0e-8:12</i>	<i>1.0e-8:12</i>	<i>1.0e-8:12</i>	15/15
1: DE	4.1(3)	5.8(5)	∞	∞	∞1100	0/15
2: PSO	2.3(3)	3.8(6)	∞	∞	∞1600	0/15
f₂	<i>1.6e+6:2.9</i>	<i>4.0e+5:11</i>	<i>4.0e+4:15</i>	<i>6.3e+2:58</i>	<i>1.0e-8:95</i>	15/15
1: DE	1.7(1)	1.5(2)	10(9)	15(4)	∞1100	0/15
2: PSO	1.9(1)	1.2(0.7)	9.3(7)	16(3)	∞1600	0/15
f₃	<i>1.6e+2:4.1</i>	<i>1.0e+2:15</i>	<i>6.3e+1:23</i>	<i>2.5e+1:73</i>	<i>1.0e+1:716</i>	15/15
1: DE	2.9(3)	2.0(1.0)	8.1(6)	10(2)	22(18)	1/15
2: PSO	2.3(2)	3.2(3)	7.7(4)	10(3)	3.2(3)	10/15
f₄	<i>2.5e+2:2.6</i>	<i>1.6e+2:10</i>	<i>1.0e+2:19</i>	<i>4.0e+1:65</i>	<i>1.6e+1:434</i>	15/15
1: DE	5.4(6)	5.6(7)	5.6(6)	9.2(3)	8.5(7)	4/15
2: PSO	2.6(2)	2.9(4)	5.9(6)	10(3)	5.4(5)	10/15
f₅	<i>6.3e+1:4.0</i>	<i>4.0e+1:10</i>	<i>1.0e-8:10</i>	<i>1.0e-8:10</i>	<i>1.0e-8:10</i>	15/15
1: DE	2.6(2)	5.6(7)	39(9)	39(10)	39(9)	15/15
2: PSO	3.3(2)	4.9(4)	17(4)*³	17(5)*³	17(6)*³	15/15
f₆	<i>1.0e+5:3.0</i>	<i>2.5e+4:8.4</i>	<i>1.0e+2:16</i>	<i>2.5e+1:54</i>	<i>2.5e-1:254</i>	15/15
1: DE	2.5(3)	5.2(6)	7.1(3)	14(11)	∞1100	0/15
2: PSO	1.9(0.4)	2.0(0.7)	5.1(4)	6.4(6)	∞1800	0/15
f₇	<i>1.6e+2:4.2</i>	<i>1.0e+2:6.2</i>	<i>2.5e+1:20</i>	<i>4.0e+0:54</i>	<i>1.0e+0:324</i>	15/15
1: DE	2.0(2)	2.1(2)	7.7(7)	26(21)	∞1100	0/15
2: PSO	3.1(2)	3.7(3)	5.3(3)	12(4)	3.8(2)	14/15
f₈	<i>1.0e+4:4.6</i>	<i>6.3e+3:6.8</i>	<i>6.3e+3:18</i>	<i>6.3e+1:54</i>	<i>1.6e+0:258</i>	15/15
1: DE	2.3(2)	3.0(2)	6.2(4)	12(6)	∞1100	0/15
2: PSO	2.6(2)	2.3(2)	6.3(5)	10(4)	49(47)	2/15
f₉	<i>2.5e+1:20</i>	<i>1.6e+1:26</i>	<i>1.0e+1:35</i>	<i>4.0e+0:62</i>	<i>1.6e-2:256</i>	15/15
1: DE	119(207)	290(292)	∞	∞	∞1100	0/15
2: PSO	39(14)	35(8)	32(22)*²	42(101)	∞1700	0/15
f₁₀	<i>2.5e+6:2.9</i>	<i>6.3e+5:7.0</i>	<i>2.5e+5:17</i>	<i>6.3e+3:54</i>	<i>2.5e+1:297</i>	15/15
1: DE	1.5(1)	2.6(3)	2.1(2)	26(38)	∞1100	0/15
2: PSO	2.6(4)	2.3(1)	2.2(1)	11(5)	∞1900	0/15
f₁₁	<i>1.0e+6:3.0</i>	<i>6.3e+4:6.2</i>	<i>6.3e+2:16</i>	<i>6.3e-1:74</i>	<i>6.3e-1:298</i>	15/15
1: DE	2.3(5)	4.5(7)	10(8)	14(8)	∞1100	0/15
2: PSO	1.4(1)	4.8(6)	11(11)	9.3(6)	∞1900	0/15
f₁₂	<i>4.0e+7:3.6</i>	<i>1.6e+7:7.6</i>	<i>4.0e+6:19</i>	<i>1.6e+4:52</i>	<i>1.0e+0:268</i>	15/15
1: DE	1.6(1)	3.2(3)	8.0(7)	295(458)	∞1100	0/15
2: PSO	2.1(0.9)	2.6(3)	4.5(2)	26(4)	∞1800	0/15
f₁₃	<i>1.0e+3:2.8</i>	<i>6.3e+2:8.4</i>	<i>4.0e+2:17</i>	<i>6.3e+1:52</i>	<i>6.3e-2:264</i>	15/15
1: DE	1.5(1)	3.1(3)	8.1(6)	74(96)	∞1100	0/15
2: PSO	3.1(2)	4.7(4)	5.8(4)	17(3)	∞1800	0/15
f₁₄	<i>1.6e+1:3.0</i>	<i>1.0e+1:10</i>	<i>6.3e+0:15</i>	<i>2.5e-1:53</i>	<i>1.0e-5:251</i>	15/15
1: DE	3.1(4)	1.3(0.8)	2.2(0.9)	38(19)	∞1100	0/15
2: PSO	2.8(4)	2.0(1)	3.1(4)	16(3)	∞1700	0/15
f₁₅	<i>1.6e+2:3.0</i>	<i>1.0e+2:13</i>	<i>6.3e+1:24</i>	<i>4.0e+1:55</i>	<i>1.6e+1:289</i>	5/5
1: DE	3.5(3)	2.7(3)	6.4(6)	7.9(3)	27(68)	2/15
2: PSO	4.3(9)	2.5(1)	4.5(5)	5.1(3)	7.4(4)	10/15
f₁₆	<i>4.0e+1:4.8</i>	<i>2.5e+1:16</i>	<i>1.6e+1:46</i>	<i>1.0e+1:120</i>	<i>4.0e+0:334</i>	15/15
1: DE	2.1(3)	1.8(1)	2.6(4)	3.3(3)	44(72)	1/15
2: PSO	1.8(2)	1.4(0.5)	2.4(4)	3.5(2)	16(17)	5/15
f₁₇	<i>1.0e+1:5.2</i>	<i>6.3e+0:26</i>	<i>4.0e+0:57</i>	<i>2.5e+0:110</i>	<i>6.3e-1:412</i>	15/15
1: DE	3.2(8)	3.2(4)	5.9(4)	4.2(2)	∞1100	0/15
2: PSO	4.0(5)	2.9(3)	3.5(1)	3.2(0.8)	3.1(2)	14/15
f₁₈	<i>6.3e+1:3.4</i>	<i>4.0e+1:7.2</i>	<i>2.5e+1:20</i>	<i>1.6e+1:58</i>	<i>1.6e+0:318</i>	15/15
1: DE	2.4(3)	2.5(2)	5.6(6)	4.6(3)	∞1100	0/15
2: PSO	2.0(1)	3.1(4)	3.9(2)	2.9(3)	7.6(8)	10/15
f₁₉	<i>1.6e-1:172</i>	<i>1.0e-1:242</i>	<i>6.3e-2:675</i>	<i>4.0e-2:3078</i>	<i>2.5e-2:4946</i>	15/15
1: DE	∞	∞	∞1100	∞	∞1900	0/15
2: PSO	∞	∞	∞	∞	∞	0/15
f₂₀	<i>6.3e+3:5.1</i>	<i>4.0e+3:8.4</i>	<i>4.0e+1:15</i>	<i>2.5e+0:69</i>	<i>1.0e+0:851</i>	15/15
1: DE	2.4(2)	2.6(2)	12(6)	10(6)	∞1100	0/15
2: PSO	2.2(2)	2.0(1)	8.9(7)	8.8(5)	15(10)	2/15
f₂₁	<i>4.0e+1:3.9</i>	<i>2.5e+1:11</i>	<i>1.6e+1:31</i>	<i>6.3e+0:73</i>	<i>1.6e+0:347</i>	5/5
1: DE	3.0(3)	2.5(2)	2.2(2)	7.2(10)	14(9)	3/15
2: PSO	1.5(1)	1.8(2)	2.0(3)	6.5(4)	6.8(17)	8/15
f₂₂	<i>6.3e+1:3.6</i>	<i>4.0e+1:15</i>	<i>2.5e+1:32</i>	<i>1.0e+1:71</i>	<i>1.6e+0:341</i>	5/5
1: DE	2.0(1)	2.6(3)	2.8(2)	8.5(7)	45(71)	1/15
2: PSO	2.6(3)	2.6(3)	2.9(5)	4.8(4)	5.9(8)	10/15
f₂₃	<i>1.0e+1:3.0</i>	<i>6.3e+0:9.0</i>	<i>4.0e+0:33</i>	<i>2.5e+0:84</i>	<i>1.0e+0:518</i>	15/15
1: DE	2.2(2)	3.6(6)	2.8(3)	6.1(4)	∞1100	0/15
2: PSO	3.3(3)	4.1(6)	3.4(6)	8.1(14)	∞2000	0/15
f₂₄	<i>6.3e+1:15</i>	<i>4.0e+1:37</i>	<i>4.0e+1:37</i>	<i>2.5e+1:118</i>	<i>1.6e+1:692</i>	15/15
1: DE	4.7(4)	8.8(9)	8.8(6)	24(29)	∞1100	0/15
2: PSO	4.2(5)	8.6(4)	8.6(4)	8.0(7)	7.5(4)	5/15

20-D

#FEs/D	0.5	1.2	3	10	50	#succ
f₁	6.3e+1:24	4.0e+1:42	1.0e-8:43	1.0e-8:43	1.0e-8:43	15/15
1: DE	27(5)	25(7)	∞	∞	∞4100	0/15
2: PSO	16(3)*²	16(2)*²	∞	∞	∞6600	0/15
f₂	4.0e+6:29	2.5e+6:42	1.0e+5:65	1.0e+4:207	1.0e-8:412	15/15
1: DE	2.0(4)	2.5(2)	25(3)	17(1.0)	∞4100	0/15
2: PSO	1.6(2)	2.4(3)	21(5)*	13(1)*³	∞6500	0/15
f₃	6.3e+2:33	4.0e+2:44	1.6e+2:109	1.0e+2:255	2.5e+1:3277	15/15
1: DE	8.5(5)	24(3)	30(5)	239(247)	∞4100	0/15
2: PSO	4.2(2)	14(4)*³	25(6)	23(10)	∞7400	0/15
f₄	6.3e+2:22	4.0e+2:91	2.5e+2:250	1.6e+2:332	6.3e+1:1927	15/15
1: DE	27(12)	18(4)	11(0.8)	183(67)	∞4100	0/15
2: PSO	19(11)	12(5)*²	8.1(2)*³	13(0.9)	57(80)	1/15
f₅	2.5e+2:19	1.6e+2:34	1.0e-8:41	1.0e-8:41	1.0e-8:41	15/15
1: DE	4.1(4)	9.1(2)	36(3)	36(5)	36(3)	15/15
2: PSO	3.3(2)	3.8(2)*³	14(7)*³	14(3)*³	14(4)*³	15/15
f₆	2.5e+5:16	6.3e+4:43	1.6e+4:62	1.6e+2:353	1.6e+1:1078	15/15
1: DE	13(10)	12(7)	12(3)	∞	∞4100	0/15
2: PSO	7.0(6)	6.0(3)*	6.1(2)*	27(25)	∞7500	0/15
f₇	1.0e+3:11	4.0e+2:39	2.5e+2:74	6.3e+1:319	1.0e+1:1351	15/15
1: DE	1.8(0.3)	17(16)	25(12)	∞	∞4100	0/15
2: PSO	2.1(2)	7.6(7)	7.1(3)*³	5.9(2)*³	13(11)	6/15
f₈	4.0e+4:19	2.5e+4:35	4.0e+3:67	2.5e+2:231	1.6e+1:1470	15/15
1: DE	42(17)	29(11)	34(5)	∞	∞4100	0/15
2: PSO	23(12)*	17(4)*	21(4)*³	15(8)*³	69(54)	1/15
f₉	1.0e+2:357	6.3e+1:560	4.0e+1:684	2.5e+1:756	1.0e+1:1716	15/15
1: DE	∞	∞	∞	∞	∞4100	0/15
2: PSO	12(6)*³	9.2(6)	8.2(3)	8.4(5)	∞6800	0/15
f₁₀	1.6e+6:15	1.0e+6:27	4.0e+5:70	6.3e+4:231	4.0e+3:1015	15/15
1: DE	24(30)	44(77)	184(209)	∞	∞4100	0/15
2: PSO	10(8)	13(10)	12(4)*²	14(13)*³	56(78)	2/15
f₁₁	4.0e+4:11	2.5e+3:27	1.6e+2:313	1.0e+2:481	1.0e+1:1002	15/15
1: DE	2.0(4)	2.5(3)	∞	∞	∞4100	0/15
2: PSO	2.0(3)	3.9(3)	5.8(3)*³	6.0(3)*³	∞8000	0/15
f₁₂	1.0e+8:23	6.3e+7:39	2.5e+7:76	4.0e+6:209	1.0e+1:1042	15/15
1: DE	34(11)	35(10)	30(4)	72(121)	∞4100	0/15
2: PSO	12(8)*³	15(6)*³	15(3)*³	11(2)*³	∞6700	0/15
f₁₃	1.6e+3:28	1.0e+3:64	6.3e+2:79	4.0e+1:211	2.5e+0:1724	15/15
1: DE	23(8)	30(5)	43(28)	25(2)	∞4100	0/15
2: PSO	10(4)*²	13(2)*³	18(3)*³	25(2)	∞6800	0/15
f₁₄	2.5e+1:15	1.6e+1:42	1.0e+1:75	1.6e+0:219	6.3e-4:1106	15/15
1: DE	50(33)	43(20)	40(11)	∞	∞4100	0/15
2: PSO	22(15)	13(6)*³	13(3)*³	12(1)*³	∞7000	0/15
f₁₅	6.3e+2:15	4.0e+2:67	2.5e+2:292	1.6e+2:846	1.0e+2:1671	15/15
1: DE	19(9)	18(5)	8.3(2)	∞	∞4100	0/15
2: PSO	13(8)	9.0(4)*³	5.0(1.0)*³	4.8(0.7)	5.4(2)	11/15
f₁₆	4.0e+1:26	2.5e+1:127	1.6e+1:540	1.6e+1:540	1.0e+1:1384	15/15
1: DE	5.2(8)	457(792)	∞	∞	∞4100	0/15
2: PSO	5.1(5)	16(8)*²	12(9)	12(10)	41(55)	2/15
f₁₇	1.6e+1:11	1.0e+1:63	6.3e+0:305	4.0e+0:468	1.0e+0:1030	15/15
1: DE	19(47)	19(10)	10(2)	63(71)	∞4100	0/15
2: PSO	8.6(6)	7.1(5)*	4.8(3)*³	5.8(3)*²	14(13)	7/15
f₁₈	4.0e+1:116	2.5e+1:252	1.6e+1:430	1.0e+1:621	4.0e+0:1090	15/15
1: DE	7.0(4)	8.9(2)	33(35)	∞	∞4100	0/15
2: PSO	4.1(2)	4.5(3)*²	5.4(2)*	5.5(2)*²	15(13)	6/15
f₁₉	1.6e-1:2.5e5	1.0e-1:3.4e5	6.3e-2:3.4e5	4.0e-2:3.4e5	2.5e-2:3.4e5	3/15
1: DE	∞	∞	∞	∞	∞4100	0/15
2: PSO	∞	∞	∞	∞	∞7700	0/15
f₂₀	1.6e+4:38	1.0e+4:42	2.5e+2:62	2.5e+0:250	1.6e+0:2536	15/15
1: DE	19(6)	24(4)	38(5)	239(186)	∞4100	0/15
2: PSO	8.6(4)*³	11(3)*³	21(6)*³	19(10)	14(12)	3/15
f₂₁	6.3e+1:36	4.0e+1:77	4.0e+1:77	1.6e+1:456	4.0e+0:1094	15/15
1: DE	69(43)	152(83)	152(80)	133(84)	∞4100	0/15
2: PSO	21(10)*²	17(8)*³	17(3)*³	6.0(9)*³	20(33)	4/15
f₂₂	6.3e+1:45	4.0e+1:68	4.0e+1:68	1.6e+1:231	6.3e+0:1219	15/15
1: DE	43(18)	62(66)*	62(36)	48(37)	49(37)	1/15
2: PSO	17(9)*³	19(9)*²	19(6)*²	16(29)*	8.4(7)	7/15
f₂₃	6.3e+0:29	4.0e+0:118	2.5e+0:306	2.5e+0:306	1.0e+0:1614	15/15
1: DE	4.0(6)	34(42)	∞	∞	∞4100	0/15
2: PSO	2.7(2)	22(20)	35(45)	35(15)	∞7900	0/15
f₂₄	2.5e+2:208	1.6e+2:918	1.0e+2:6628	6.3e+1:9885	4.0e+1:31629	15/15
1: DE	12(3)	∞	∞	∞	∞4100	0/15
2: PSO	5.9(2)*³	9.2(9)	17(14)	∞	∞7700	0/15