



Università degli Studi dell'Aquila

Ingegneria

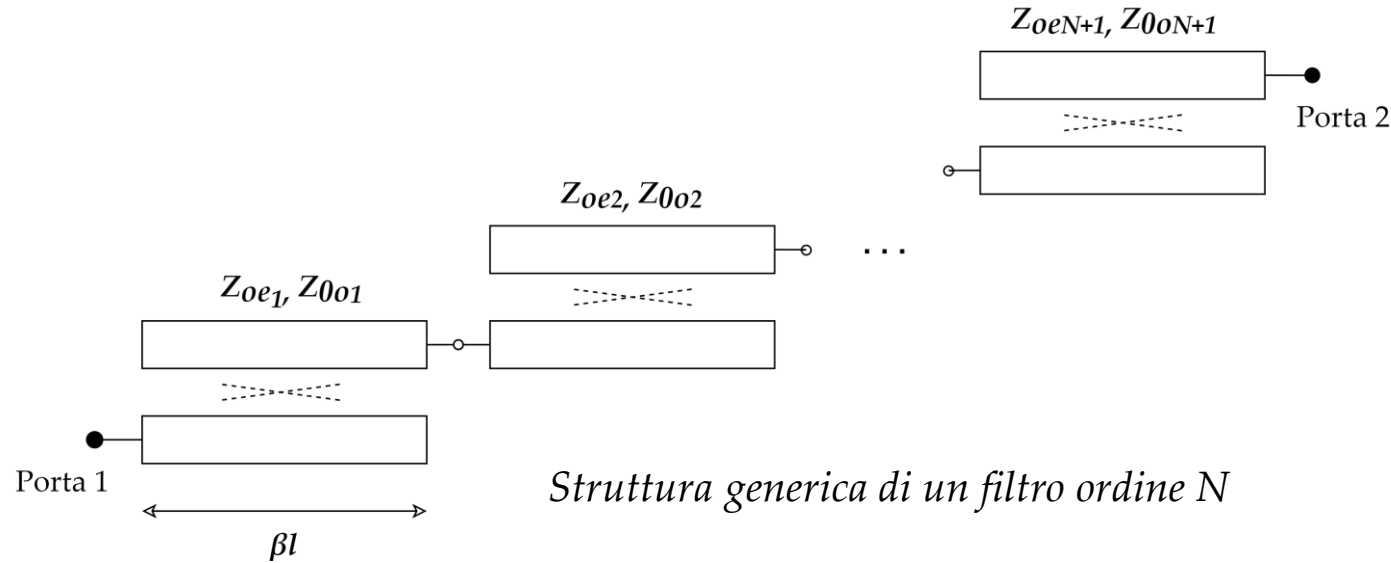
Corso di laurea Magistrale in
Ingegneria elettronica

Mattia Ragnoli

**Design, realizzazione e test di un filtro a
microstrice accoppiate**



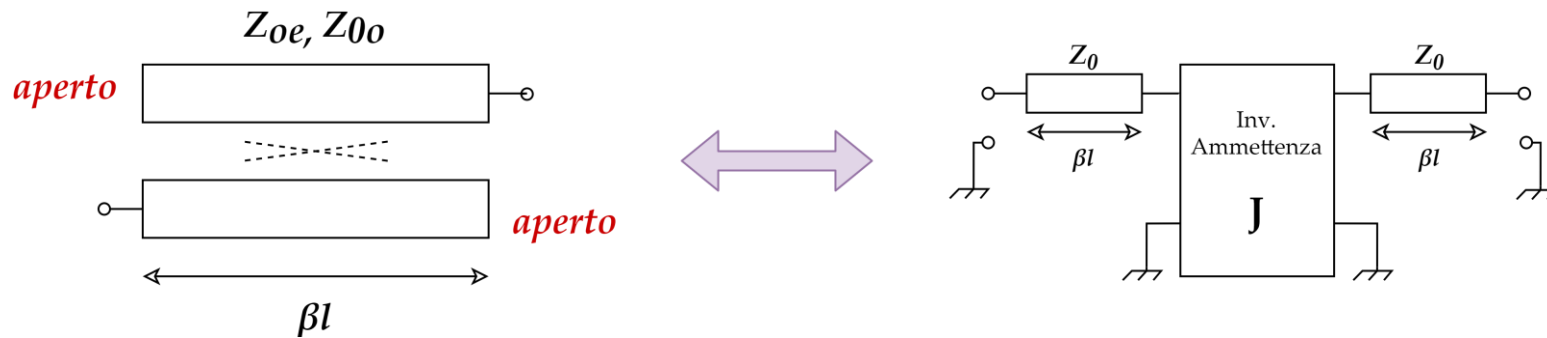
Principio di funzionamento di un filtro a linee accoppiate



- Ordine $N \rightarrow N+1$ linee accoppiate
- Valido per linee generiche

Struttura generica di un filtro ordine N

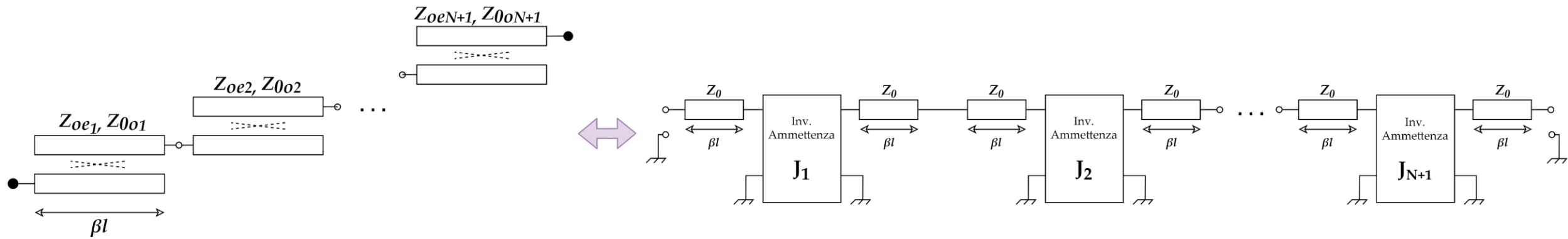
Su quale principio si basa tale struttura?



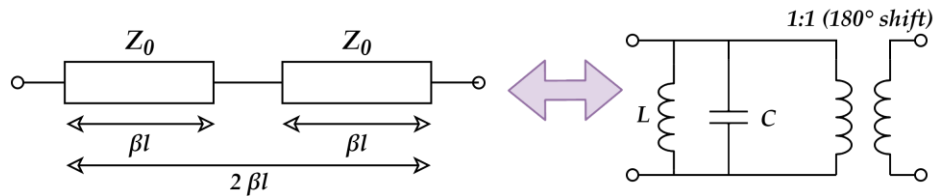
$$Z_{oe} = Z_0 [1 + J Z_0 + (J Z_0)^2]$$

$$Z_{oo} = Z_0 [1 - J Z_0 + (J Z_0)^2]$$

Se $\beta l = \frac{\pi}{2}$ (cioè $l = \lambda/2$) per entrambi i modi even e odd vale l'equivalenza



Sempre se $\beta l = \frac{\pi}{2}$ vale l'equivalenza:



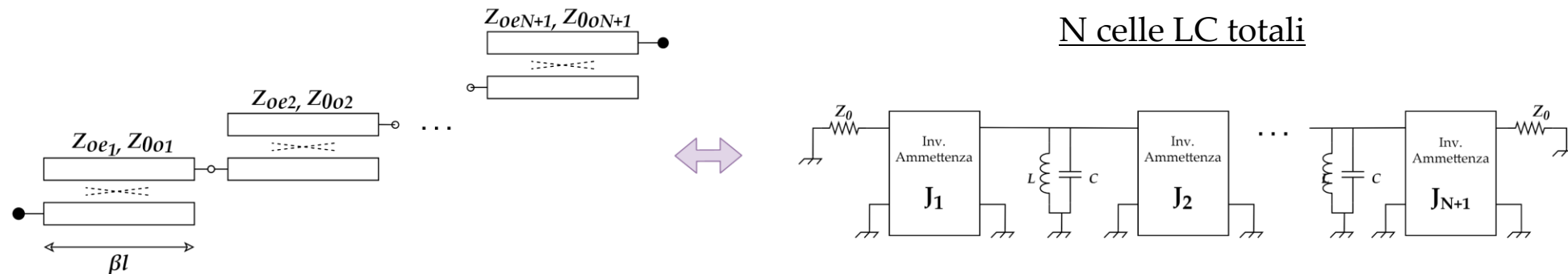
$$L = \frac{2 Z_0}{\pi \omega_0}$$

$$C = \frac{\pi}{2 Z_0 \omega_0}$$

$$\omega_0 = 2\pi f_0, \text{ freq per cui } l = \lambda/2$$

Date le precedenti equivalenze:

N celle LC totali



Ottenuti i J_n ottengo Z_{even} e Z_{odd} delle linee accoppiate \rightarrow sintesi

Per calcolare i J_n :

$$J_1 = \sqrt{\frac{\pi \Delta}{2 g_1}} \frac{1}{Z_0}$$

$$J_n = \frac{\pi \Delta}{2 \sqrt{g_{n-1} g_n}} \frac{1}{Z_0}$$

$$J_{N+1} = \sqrt{\frac{\pi \Delta}{2 g_{N+1} g_n}} \frac{1}{Z_0}$$

Δ : bw frazionale
g: parametri imp. inv.

Sviluppo del filtro

$Z_0 = 50 \, \Omega$ $\Delta = 2.5\%$ $f_0 = 4 \, \text{GHz}$ Tipologia: Butterworth, $N=4$ ed $N=5$

Dalle tabelle dei coefficienti g ottengo i parametri desiderati per la risposta Butterworth

TABLE 8.3 Element Values for Maximally Flat Low-Pass Filter Prototypes ($g_0 = 1$, $\omega_c = 1$, $N = 1$ to 10)

N	g_1	g_2	g_3	g_4	g_5	g_6	g_7	g_8	g_9	g_{10}	g_{11}
1	2.0000	1.0000									
2	1.4142	1.4142	1.0000								
3	1.0000	2.0000	1.0000	1.0000							
4	0.7654	1.8478	1.8478	0.7654	1.0000						
5	0.6180	1.6180	2.0000	1.6180	0.6180	1.0000					
6	0.5176	1.4142	1.9318	1.9318	1.4142	0.5176	1.0000				
7	0.4450	1.2470	1.8019	2.0000	1.8019	1.2470	0.4450	1.0000			
8	0.3902	1.1111	1.6629	1.9615	1.9615	1.6629	1.1111	0.3902	1.0000		
9	0.3473	1.0000	1.5321	1.8794	2.0000	1.8794	1.5321	1.0000	0.3473	1.0000	
10	0.3129	0.9080	1.4142	1.7820	1.9754	1.9754	1.7820	1.4142	0.9080	0.3129	1.0000

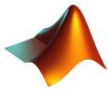
Source: Reprinted from G. L. Matthaei, L. Young, and E. M. T. Jones, *Microwave Filters, Impedance-Matching Networks, and Coupling Structures*, Artech House, Dedham, Mass., 1980, with permission.

N=4

Zoe1	63.8908	Zoo1	41.2399
Zoe2	51.7056	Zoo2	48.4035
Zoe3	51.0852	Zoo3	48.9600
Zoe4	51.7056	Zoo4	48.4035
Zoe5	63.8908	Zoo5	41.2399

N=5

Zoe1	65.7811	Zoo1	40.5733
Zoe2	52.0407	Zoo2	48.1135
Zoe3	51.1153	Zoo3	48.9323
Zoe4	51.1158	Zoo4	48.9319
Zoe5	52.0415	Zoo5	48.1129
Zoe6	65.7811	Zoo6	40.5733



Calcolo le impedenze caratteristiche even e odd delle linee

```
g0=1; g1=0.7654; g2=1.8478;
g3=1.8478; g4=0.7654; g5=1;
D=0.025; Zo=50;

J1= sqrt((pi*D)/(2*g1)) * (1/Zo);
Zoe1= Zo*( 1 + (J1*Zo) + (J1*Zo)^2 );
Zoo1= Zo*( 1 - (J1*Zo) + (J1*Zo)^2 );

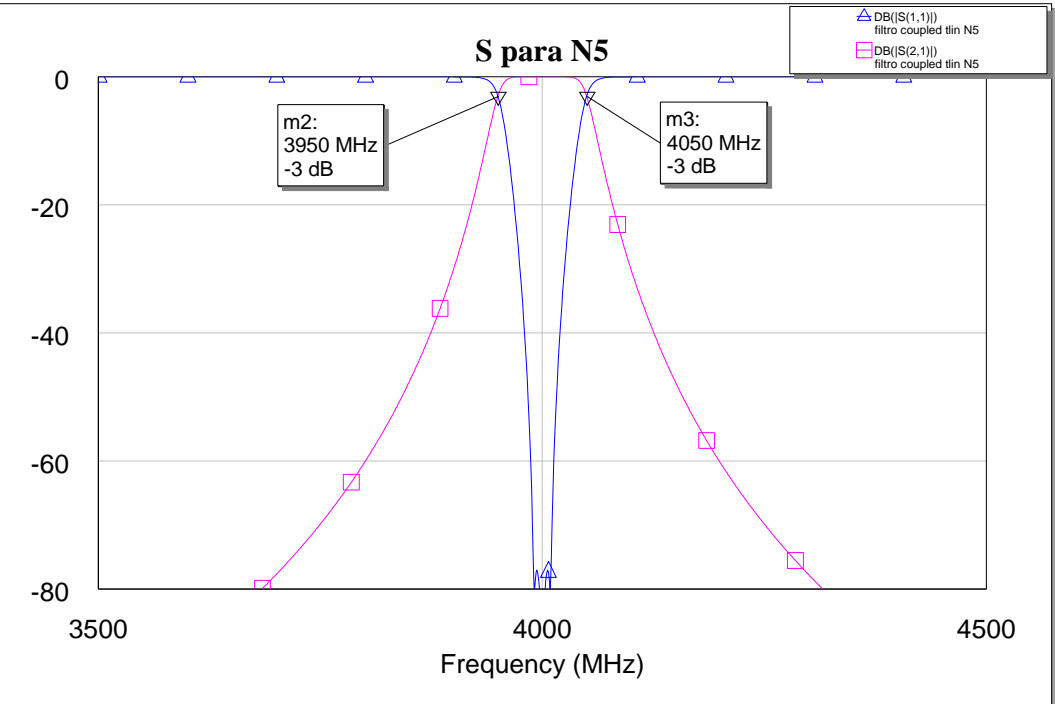
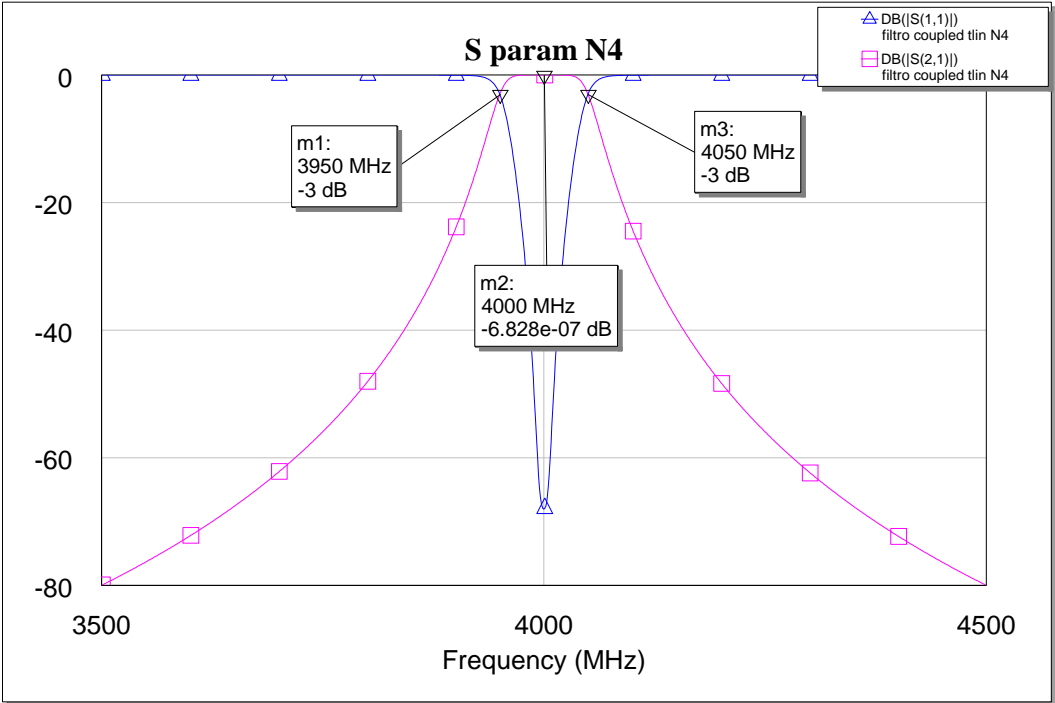
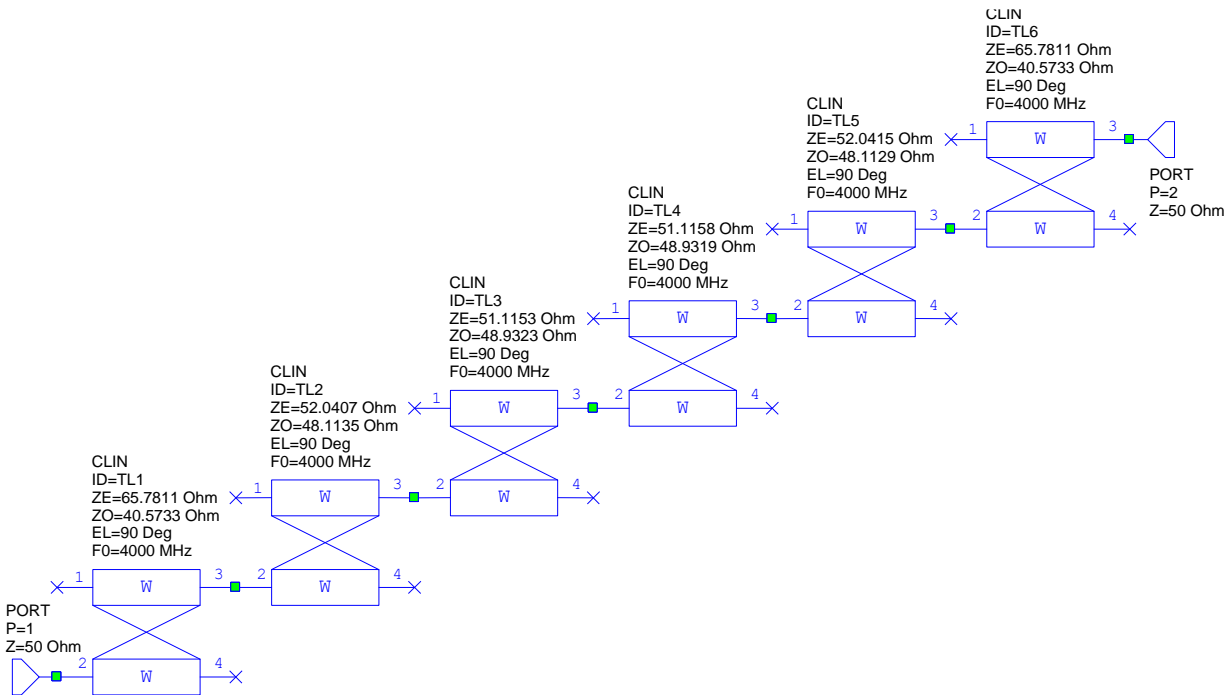
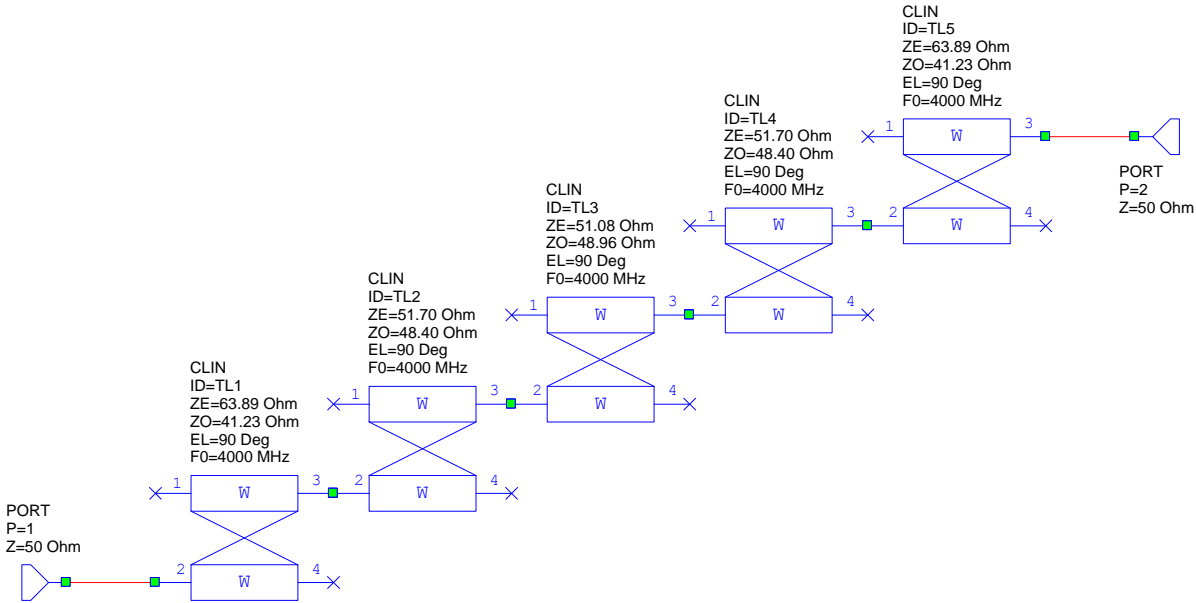
J2= ((pi*D)/(2*(sqrt(g1*g2))))*(1/Zo);
Zoe2= Zo*( 1 + (J2*Zo) + (J2*Zo)^2 );
Zoo2= Zo*( 1 - (J2*Zo) + (J2*Zo)^2 );

J3= ((pi*D)/(2*(sqrt(g2*g3))))*(1/Zo);
Zoe3= Zo*( 1 + (J3*Zo) + (J3*Zo)^2 );
Zoo3= Zo*( 1 - (J3*Zo) + (J3*Zo)^2 );

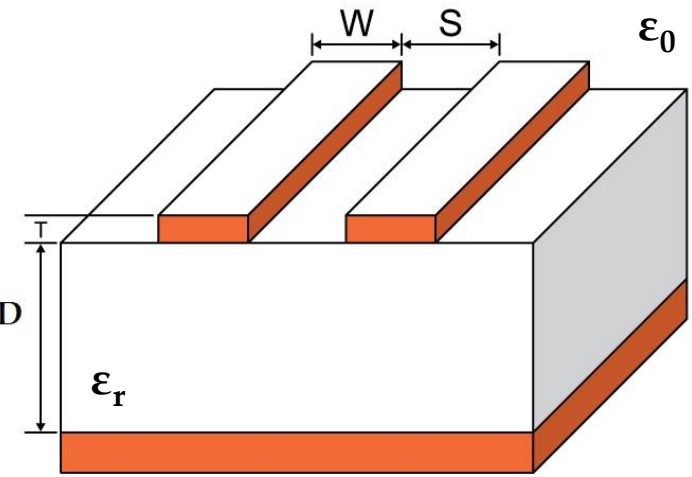
J4= ((pi*D)/(2*(sqrt(g3*g4))))*(1/Zo);
Zoe4= Zo*( 1 + (J4*Zo) + (J4*Zo)^2 );
Zoo4= Zo*( 1 - (J4*Zo) + (J4*Zo)^2 );

J5= sqrt((pi*D)/(2*g5*g4))*(1/Zo);
Zoe5= Zo*( 1 + (J5*Zo) + (J5*Zo)^2 );
Zoo5= Zo*( 1 - (J5*Zo) + (J5*Zo)^2 );
```

Simulazione filtro prototipo a linee accoppiate generiche



Passaggio a linee a microstrisce



Come passare da linee generiche a microstrisce?

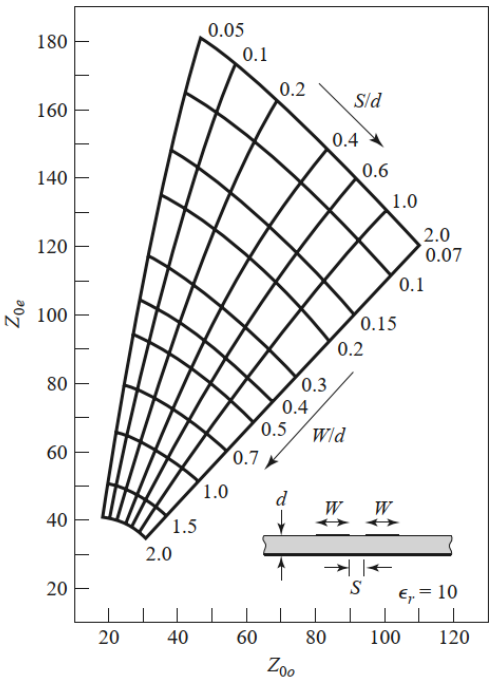
Le impedenze even e odd dipendono dai *parametri* delle microstrisce accoppiate → posso trovarli dal grafico o tramite il *sintetizzatore* di AWR

Synthesize	Name	Value	Unit	Description
<input type="checkbox"/>	Freq	4000	MHz	Evaluation Frequency
<input checked="" type="checkbox"/>	W	1.74144	mm	Conductor Width
<input checked="" type="checkbox"/>	S	0.292865	mm	Gap Width
<input checked="" type="checkbox"/>	L	12.6566	mm	Conductor length
<input type="checkbox"/>	Er	2.55		Relative dielectric constant
<input type="checkbox"/>	H	0.76	mm	Substrate thickness
<input type="checkbox"/>	T	0.035	mm	Conductor thickness
<input type="checkbox"/>	Rho	0		Metal resistivity normalized to gold
<input type="checkbox"/>	Tand	0		Loss tangent of dielectric

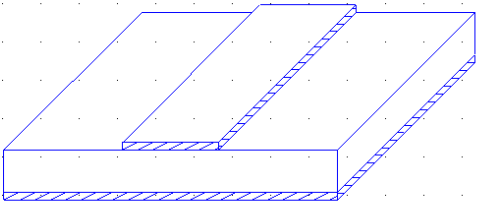
→

←

Target	Name	Value	Unit	Description
<input checked="" type="checkbox"/>	Z0 re (even)	63.8908	Ohms	Characteristic Impedance (real)
<input type="checkbox"/>	Z0 im (even)	0	Ohms	Characteristic Impedance (imag)
<input type="checkbox"/>	Alpha (even)	0	dB/m	Attenuation Constant
<input type="checkbox"/>	Loss (even)	0	dB	Loss
<input type="checkbox"/>	Beta (even)	7160.29	deg/m	Phase Constant
<input type="checkbox"/>	EL (even)	90	deg	Electrical Length
<input checked="" type="checkbox"/>	Z0 re (odd)	41.2399	Ohms	Characteristic Impedance (real)
<input type="checkbox"/>	Z0 im (odd)	0	Ohms	Characteristic Impedance (imag)
<input type="checkbox"/>	Alpha (odd)	0	dB/m	Attenuation Constant
<input type="checkbox"/>	Loss (odd)	0	dB	Loss
<input type="checkbox"/>	Beta (odd)	6625.09	deg/m	Phase Constant
<input checked="" type="checkbox"/>	EL (odd)	90	deg	Electrical Length



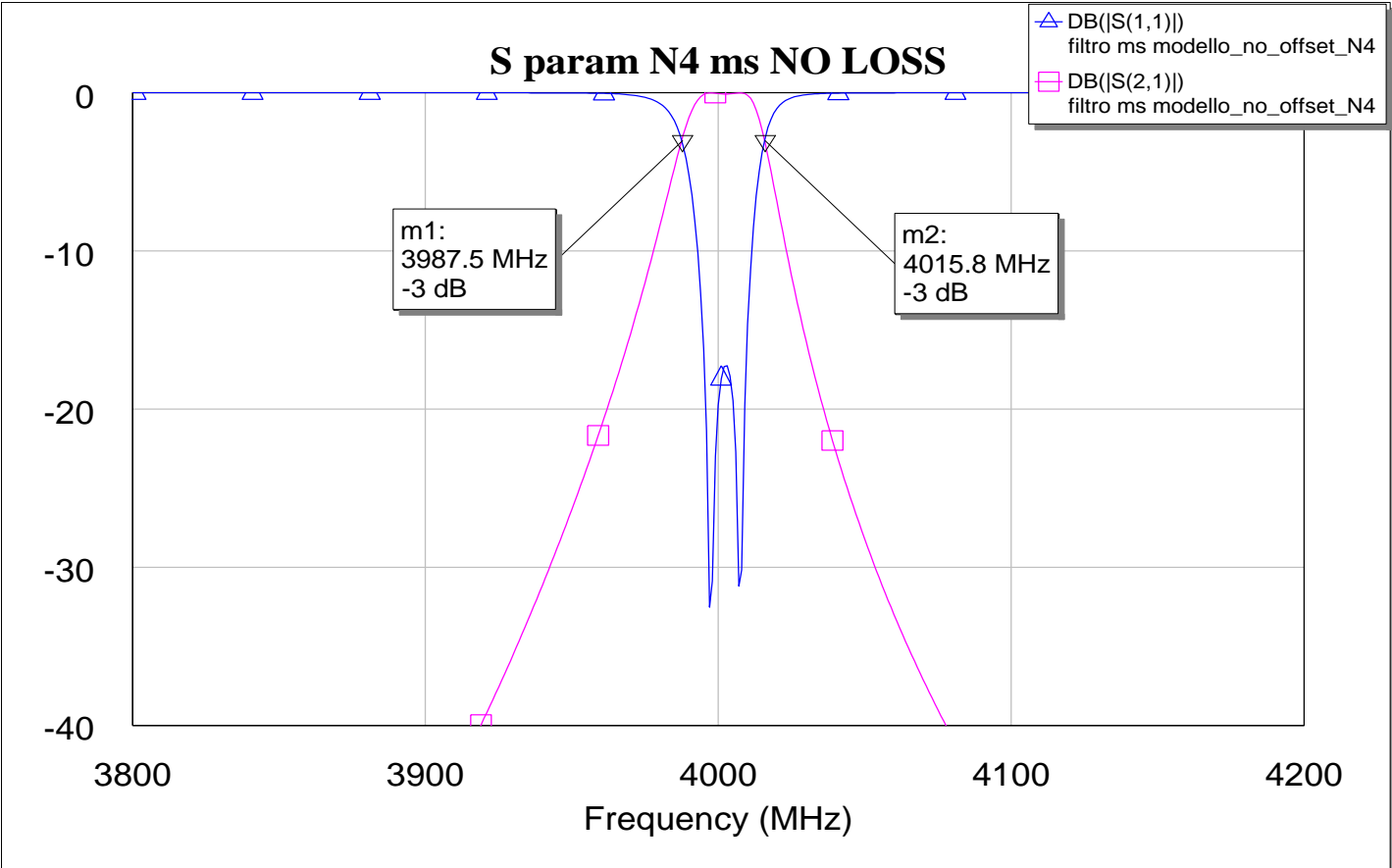
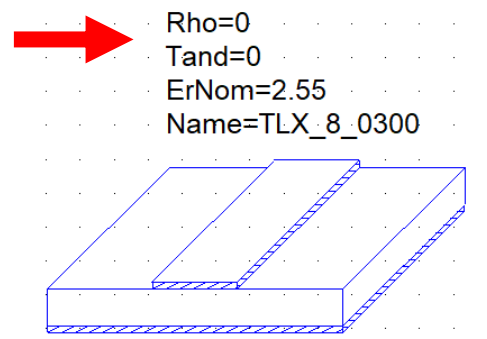
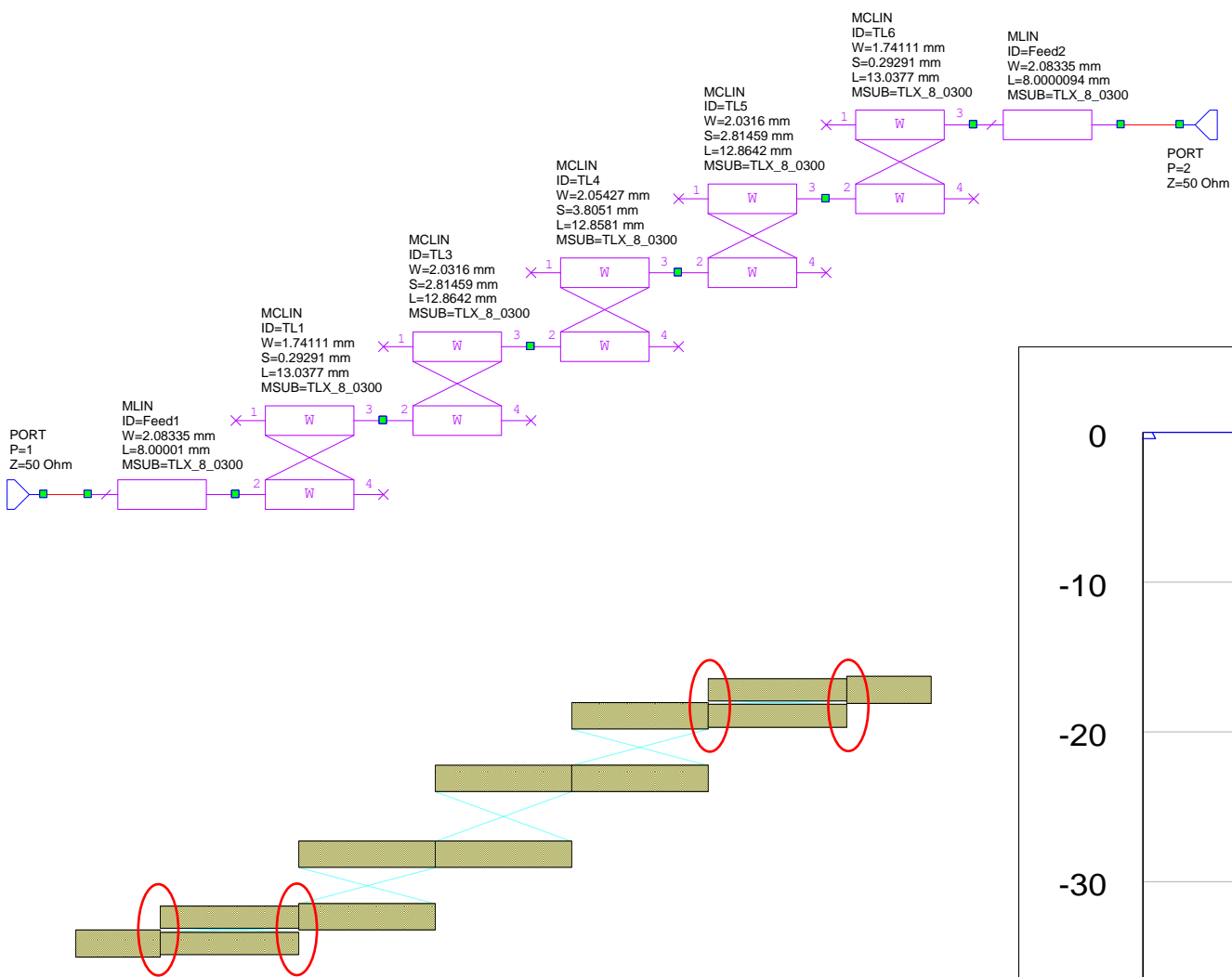
MSUB
Er=2.55
H=0.76 mm
T=0.035 mm
Rho=0.7118
Tand=0.0019
ErNom=2.55
Name=TLX_8_01



Discontinuità di dielettrico: β_{even} e β_{odd} sono diversi in linee a microstrisce

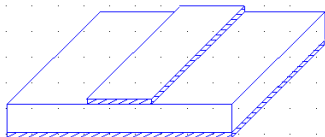
Per questo lavoro è stato usato il substrato TLX_8 0300 di Taconic.

Modello 1: modello MCLIN AWR – no perdite



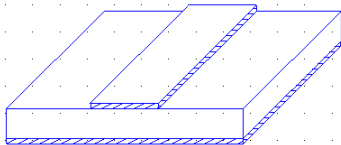
Solo perdite rame

MSUB
Er=2.55
H=0.76 mm
T=0.035 mm
Rho=0.7118
Tand=0
ErNom=2.55
Name=TLX_8_0300



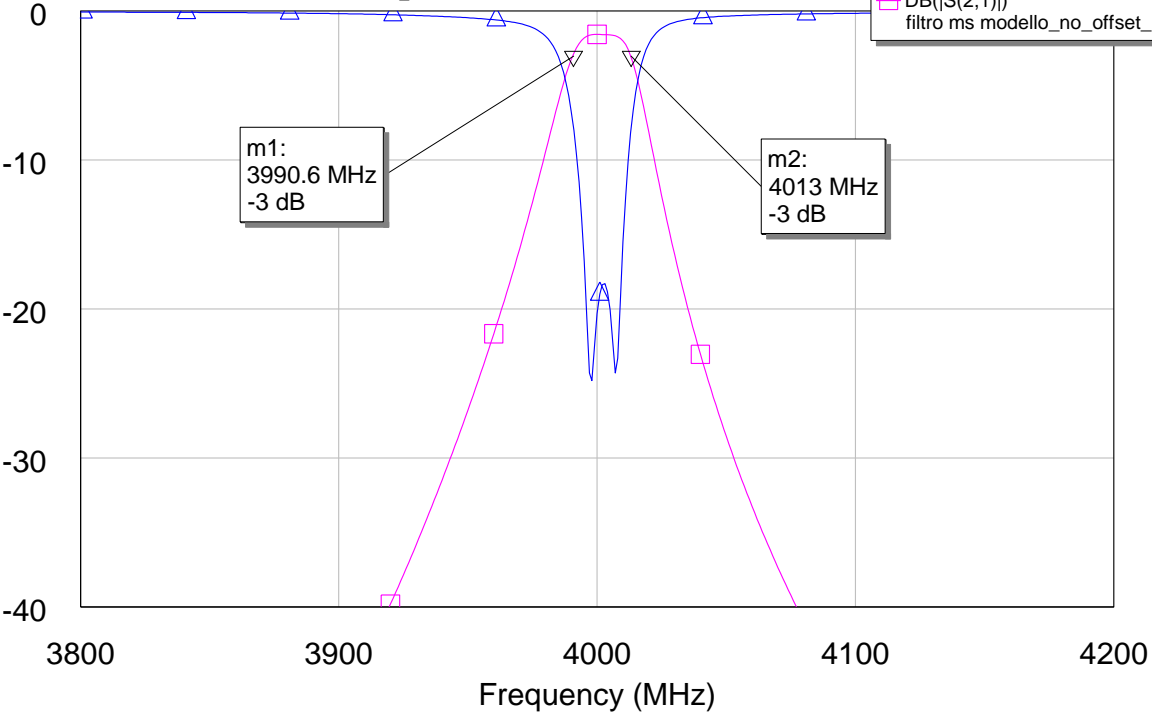
Perdite rame + dielettrico

MSUB
Er=2.55
H=0.76 mm
T=0.035 mm
Rho=0.7118
Tand=0.0019
ErNom=2.55
Name=TLX_8_0300



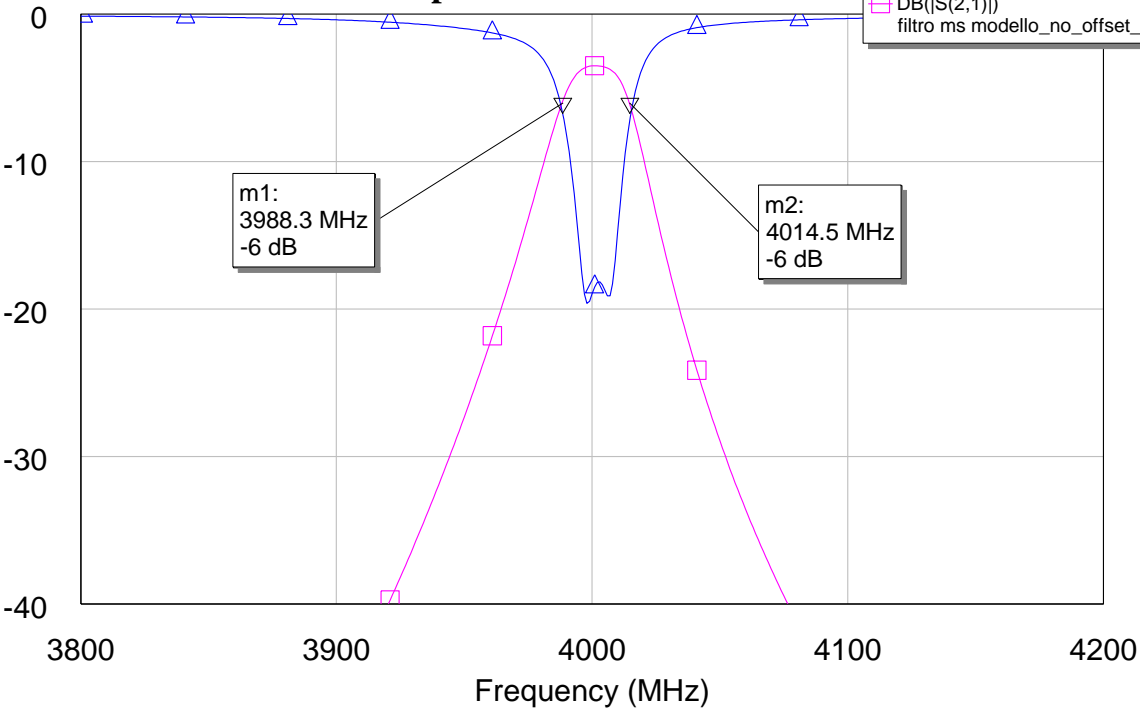
S param N4 ms COND LOSS

△ DB(|S(1,1)|)
filtro ms modello_no_offset_N4
□ DB(|S(2,1)|)
filtro ms modello_no_offset_N4



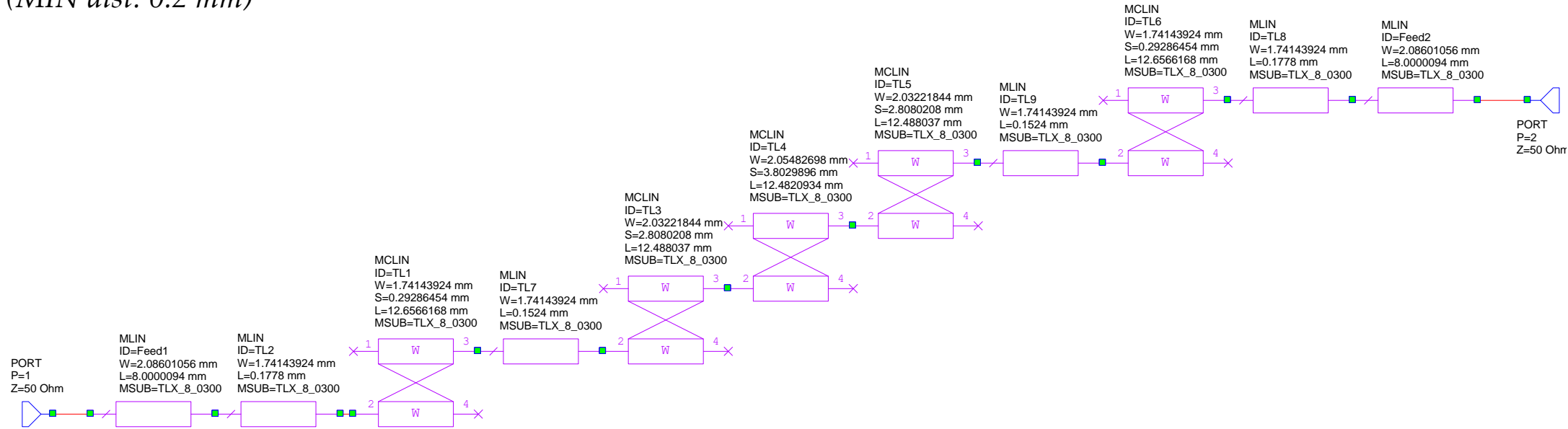
S param N4 ms LOSSES

△ DB(|S(1,1)|)
filtro ms modello_no_offset_N4
□ DB(|S(2,1)|)
filtro ms modello_no_offset_N4



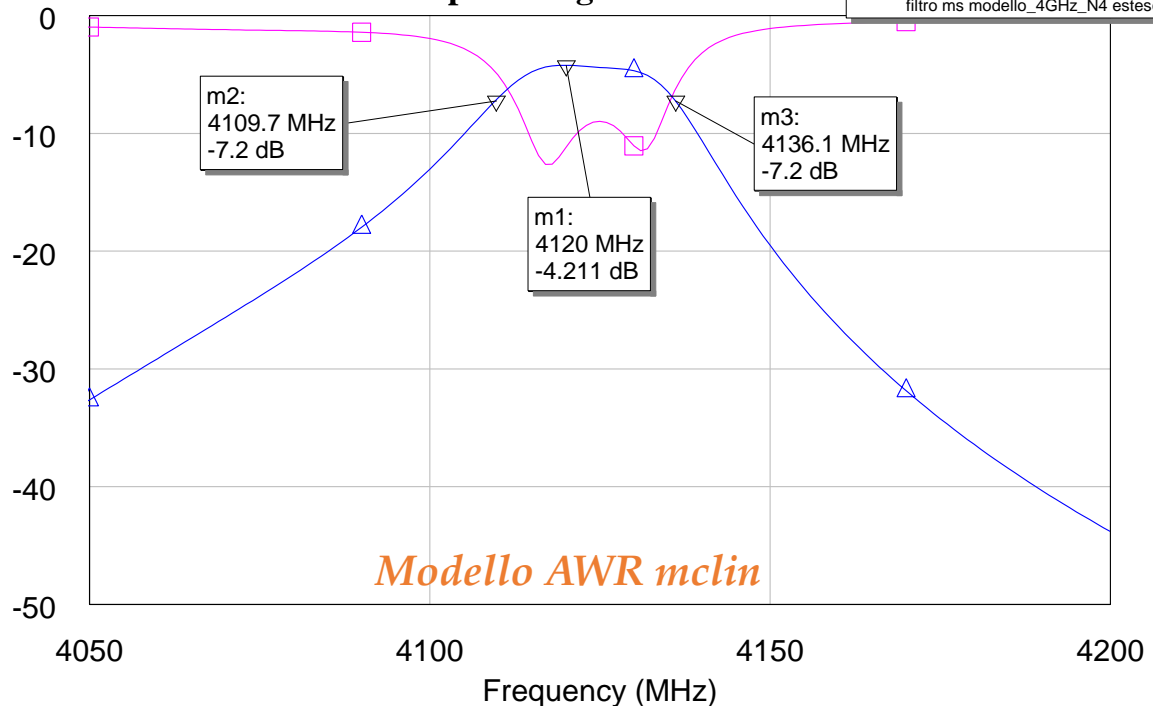
PROBLEMA: distanza minima di fresatura non rispettata
(MIN dist: 0.2 mm)

Si estendono alcuni punti cercando di modificare la lunghezza delle linee il meno possibile



Distanza OK

S param 4ghz N4 esteso

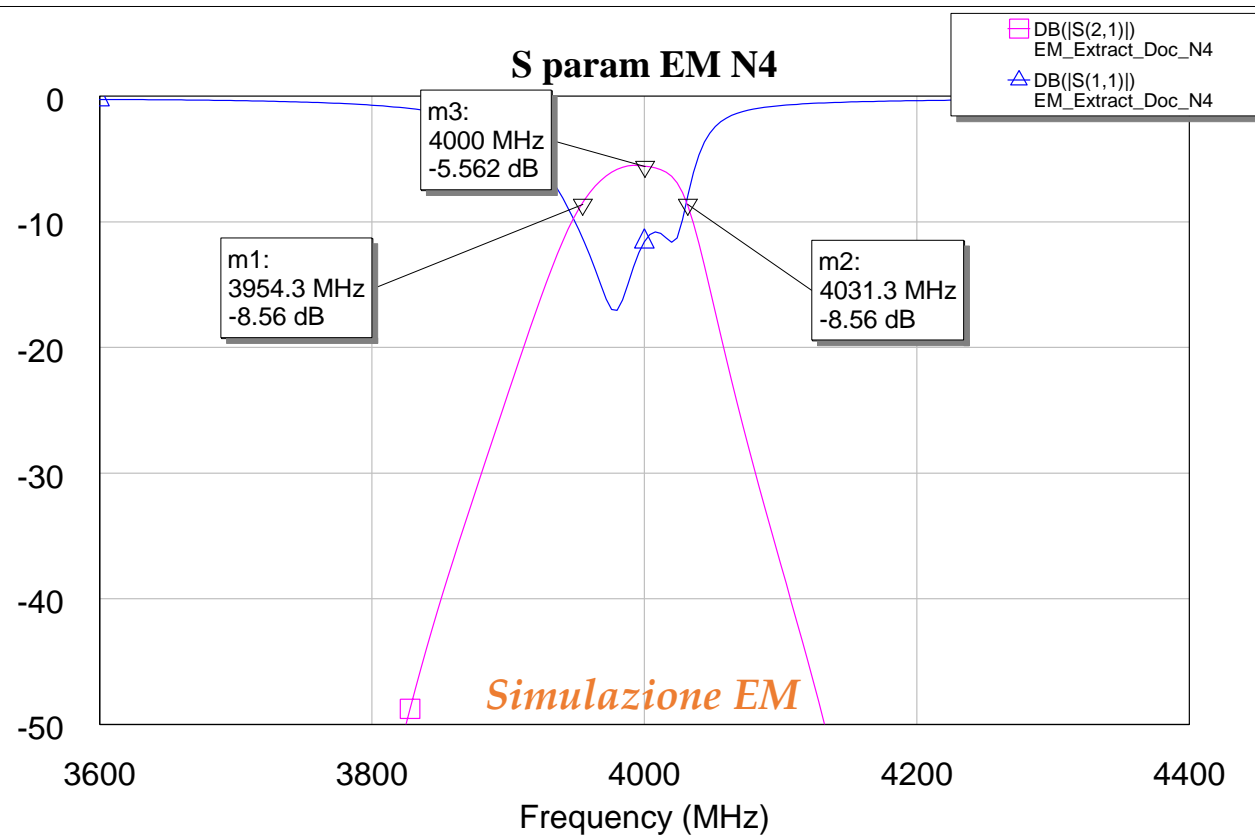


La simulazione EM produce risposta con centrobanda a 4 GHz dimensionando le linee con freq. 4.12 GHz

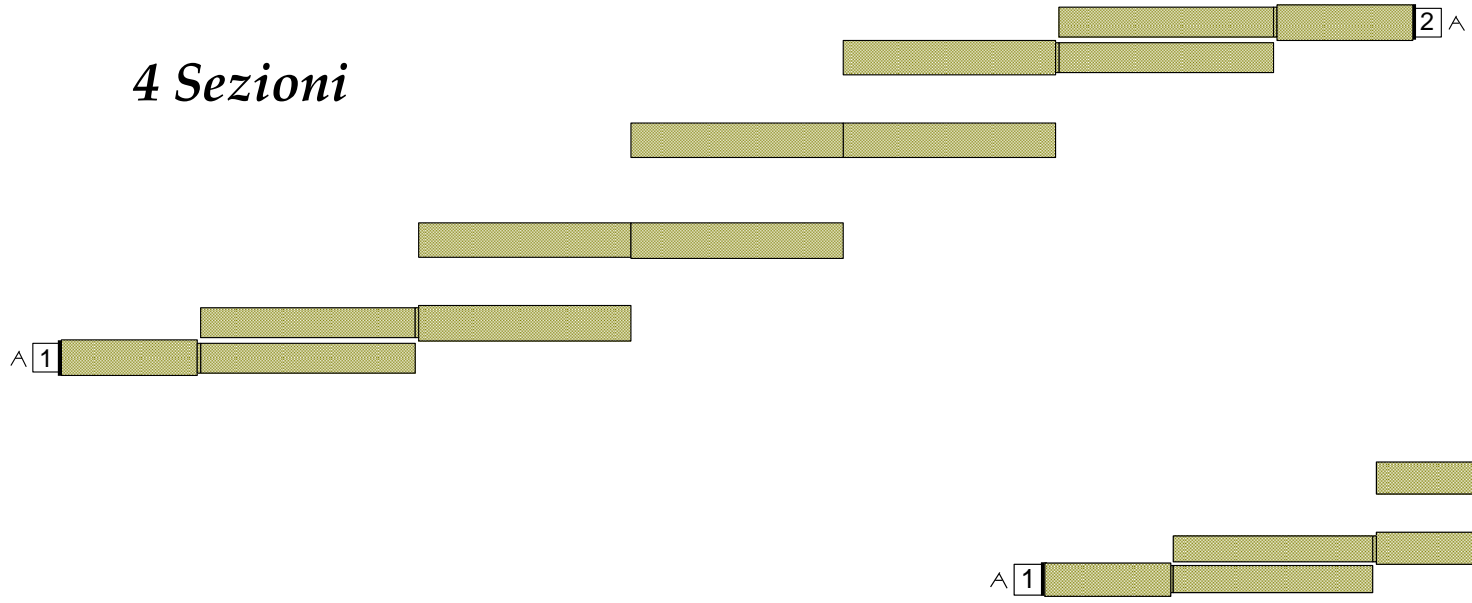
*Quale delle due è più affidabile?
E' stata data «fiducia» al modello EM*

PROBLEMA: la simulazione EM e la simulazione modello AWR producono risultati con offset in frequenza di circa 100 MHz

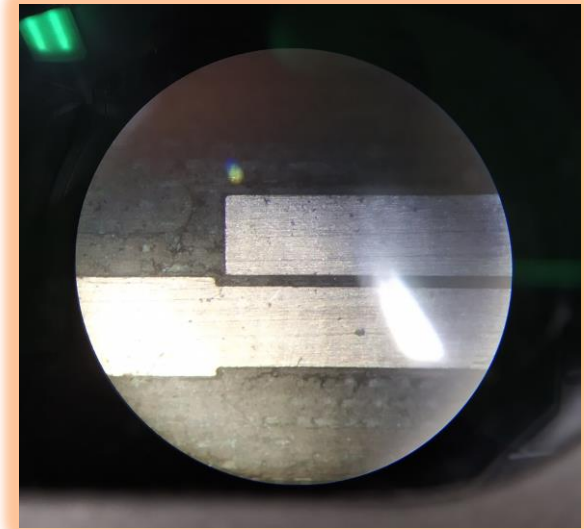
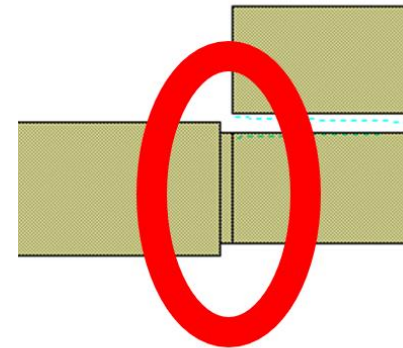
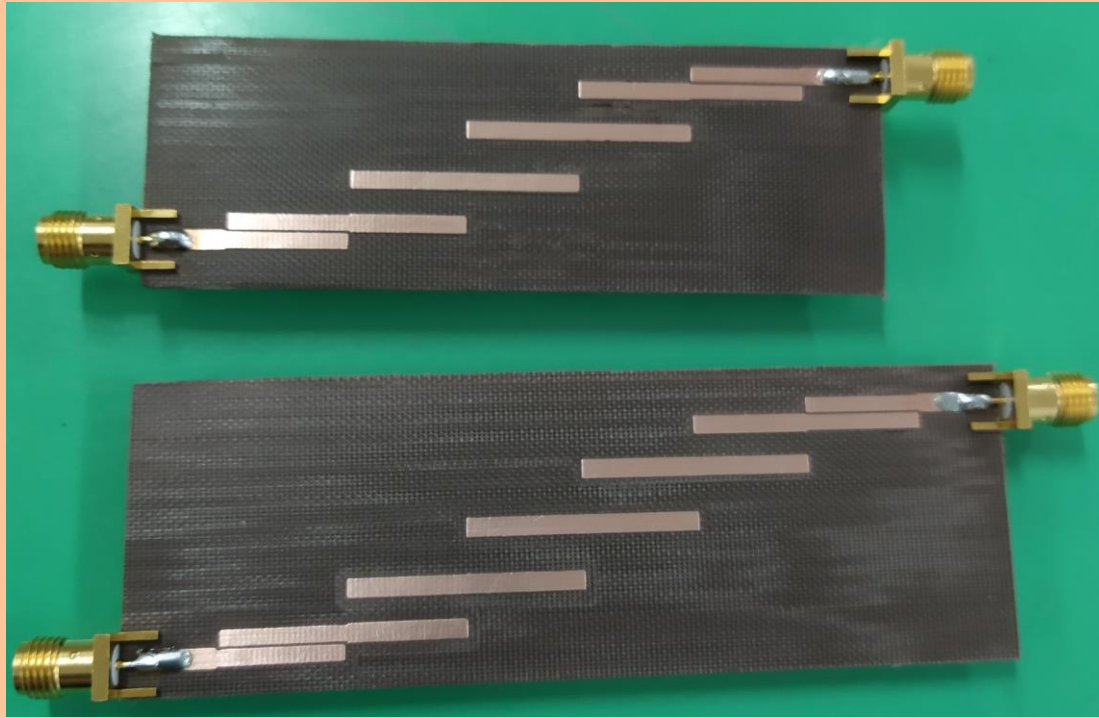
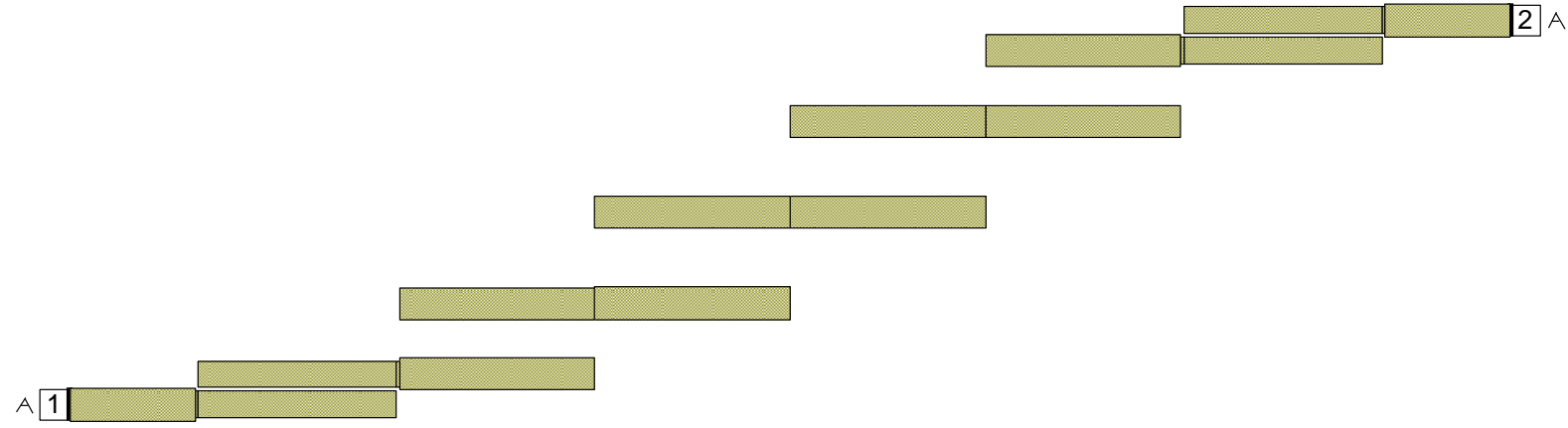
S param EM N4



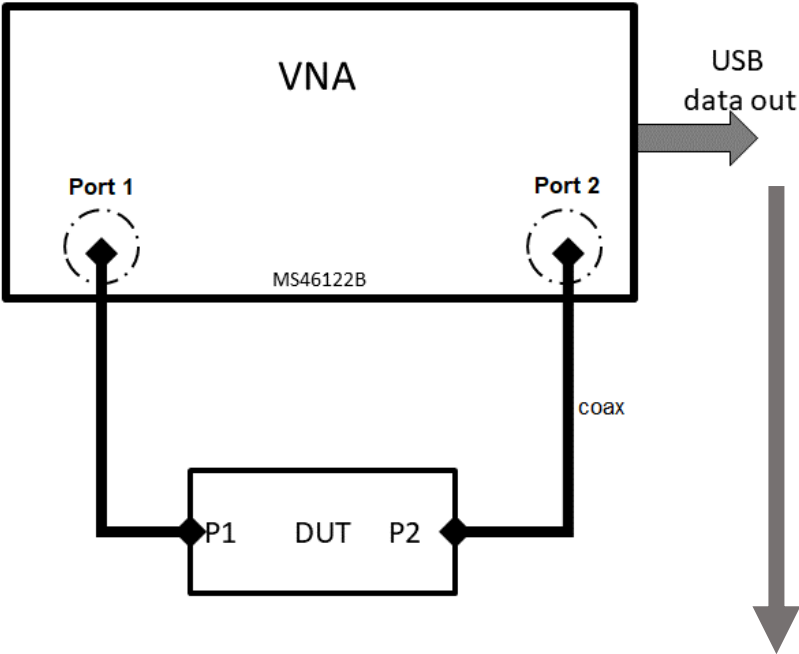
4 Sezioni



5 Sezioni



Misure



Output: .s2p file

```
! 3/25/2021 4:59:21 PM
! C:\USERS\MATTI\DOCUMENTS\UNIVERSITA\METODI DI PROGETTAZIONE ELETTROMAGNETICA\TESINA FILTRO\4GHZN4\SPARAMN4_25_03_FILLED.S2P
! CHANNEL.1
! TR.MEASUREMENT
! CORRECTED.DATA
# GHZ S RI R 50.0
! FREQ.GHZ
!; PortSelection: Port_12
2.000000000 -0.8961431 0.4219566 0.0012121 0.0015205 0.0011156 0.0017113 -0.8947470 0.4160532
2.000400000 -0.8958023 0.4226803 0.0012170 0.0015208 0.0011290 0.0017072 -0.8942813 0.4167988
2.000800000 -0.8948580 0.4245912 0.0012213 0.0015307 0.0011261 0.0017031 -0.8939692 0.4175499
2.001200000 -0.8957133 0.4229515 0.0012316 0.0015303 0.0011374 0.0017126 -0.8936117 0.4182037
2.001600000 -0.8947821 0.4248238 0.0012367 0.0015327 0.0011387 0.0017162 -0.8934842 0.4188855
2.002000000 -0.8944988 0.4254482 0.0012412 0.0015285 0.0011428 0.0017180 -0.8927935 0.4199751
2.002400000 -0.8942976 0.4260643 0.0012507 0.0015307 0.0011503 0.0017158 -0.8930171 0.4199895
2.002800000 -0.8938575 0.4268279 0.0012489 0.0015285 0.0011523 0.0017218 -0.8923733 0.4210781
2.003200000 -0.8941478 0.4264507 0.0012610 0.0015324 0.0011574 0.0017223 -0.8916491 0.4221396
2.003600000 -0.8932333 0.4282369 0.0012603 0.0015293 0.0011708 0.0017220 -0.8920567 0.4220450
2.004000000 -0.8929275 0.4288519 0.0012646 0.0015301 0.0011672 0.0017275 -0.8916045 0.4229805
2.004400000 -0.8923500 0.4295441 0.0012693 0.0015277 0.0011784 0.0017245 -0.8913860 0.4233768
2.004800000 -0.8914553 0.4313065 0.0012676 0.0015265 0.0011825 0.0017285 -0.8909621 0.4243078
2.005200000 -0.8923281 0.4297595 0.0012706 0.0015260 0.0011867 0.0017260 -0.8905634 0.4250216
2.005600000 -0.8913345 0.4316021 0.0012711 0.0015272 0.0011959 0.0017293 -0.8904660 0.4253288
2.006000000 -0.8910637 0.4322005 0.0012673 0.0015309 0.0011953 0.0017361 -0.8897797 0.4265786
2.006400000 -0.8913137 0.4317921 0.0012727 0.0015287 0.0012037 0.0017365 -0.8895956 0.4269475
2.006800000 -0.8896632 0.4346969 0.0012698 0.0015334 0.0011966 0.0017411 -0.8893471 0.4276288
2.007200000 -0.8906217 0.4330955 0.0012761 0.0015385 0.0012059 0.0017393 -0.8890819 0.4283139
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