MECHANICS OF MOBILE ROBOTS

miércoles, 2 de octubre de 2019 8:04 a.m.

- Outline:
 - Wheels
 - Kinematics structures
 - Mobility and constraints
 - Nonholonomic Constraints
 - Rolling coin example
- Mobile robots (ground):
 - Wheeled: (WMR wheelede mobile robots)
 - o One main body (base or chassis) that is in contact with the ground via wheels
 - They can have trailers in addition to the main body, otherwise WMR are single-body robots.
 - Legged:
 - Several bodies:
 - Trunk
 - Limbs
 - Head
 - Contact with the ground happens via feet
 - Ground robots may also include other forms of locomotion
 - Snake robots.

WHEELS

Kind	Description
Fixed	One axis of rotationThe wheel cannot change orientation with respect to the chassis
Orientable (steerable)	 Two axis of rotation that meet at the center of the wheel Both axis are actuated and the orientation of the wheel wrt the chassis is controlled
Caster	 Two axis of rotation that do not meet at the center of the wheel Orientation of the wheel wrt is variable but not controlled.

Differential: It is a device that distributes the speed among the two wheels of an axl using the same torque on both. If you don't add a differential to a car the car will slip

BALANCE OF MOBILE ROBOTS

- **Statical balance**: the projection of the robot CoM on the ground must fall **inside** the **polygon of support**.
 - Wheeled robots need at least 3 wheels for balances. Casters are usually used as a 3rd wheel that are only used for support.

KINEMATIC STRUCTURES

Structure	Components	
Differential-drive mobile robot	• Wheels:	

	 2 fixed wheels connected with a differential drive 1 caster wheel Motors: 2 motors, one on each of the fixed wheels
Synchro-drive mobile robot	 Wheels: 3 orientable wheels Motors: One motor that rotates all wheels simultaneously One motor that rolls all wheels simultaneously
Tricycle	 Wheels: 2 fixed wheels connected via a mechanical axel 1 orientable wheel that steers the robot Motors: One motor to power the rear axel One motor tho steer the front wheel
Car-like	 Wheels: 2 fixed wheels connected via a mechanical axel 2 orientable wheels connected via a mechanichal axel Motors: One to power the motion (rear or front) One to steer the front wheels
Omnidirectional	 Wheels: 3 (actuated) caster wheels Motors: One on every wheel

MOBILITY AND CONSTRAINTS

- Global mobility is guaranteed: they can go anywhere
- Local mobility is restricted: there are some instantaneous motions are not possible.

Constraints in mechanical systems:

- Kinds of constraints:
 - o **Equality**: bilateral constraints
 - Geometric constraint: is an equality which includes only the configuration q
 - $h_i(q) = 0$
 - \Box $i=0,\ldots,k$
 - \Box *k* is the number of constraints
 - \Box *C* is *n*-dimensional
 - \Box The set of admissible configurations is (n-k)-dimensional
 - $\ \square$ They represents a **global mobility** limitation. This means that some coordinates can be eliminated and only (n-k) parameters are required to describe the motion.
 - This is done using the **implicit function theorem** for eliminating k variables by solving h(q) = 0. This woks only locally.
 - For a global solution, a better choice of generalized coordinates for the constrained system is necessary.
 - **Kinematic** constraint: is an equality that includes the configuration q and its time derivative \dot{q}

$$\Box a_i(q,\dot{q}) = 0$$

- \Box i = 0, ..., k
- \Box k is the number of constraints
- \Box *C* is *n*-dimensional
- \Box These constraints are usually found in the form $a_i^T(q)\dot{q}=0$. Pfeffien constraints
 - ◆ Nonlinear in *q*
 - ◆ Linear in *q*
- □ In matrix form:

$$\bullet \begin{pmatrix} a_1^T(q) \\ a_2^T(q) \\ \dots \\ a_k^T(q) \end{pmatrix} \dot{q} = 0$$

- $A^T(q)\dot{q} = 0$
 - \diamond Admissible generalized velocities must belong to $M^{(r)}(q)$
- k-rows and n-columns
- ☐ This constraints represent a **local mobility** limitation. However we don't know anything about the global mobility limitations.
- Relationship between geometric and kinematic constraints:
 - □ Every geometric constraint implies a kinematic constraint.

•
$$h(q) = 0 \rightarrow \frac{dh(q)}{dt} = 0 \rightarrow \frac{\partial h}{\partial q} \dot{q} = 0 \rightarrow a^{T}(q) \dot{q} = 0$$

- $\frac{\partial h}{\partial t}$ is the transpose of the gradient.
- Geometrically this means that the admissible velocities must be orthogonal to the gradient vector.
- □ In other words, if the mobility is globally limited then it is also locally limited.
- □ Does a kinematic constraint imply a geometric constraint?
 - ◆ A kinematic constraint may or may not imply a geometric constraint
 - ◆ Example:

$$\diamond$$
 $C = R^2$

 \diamond Consider $q_1q_2=c$, where c is a constant. After differentiation wrt time we get:

♦ Geometrically this represent a hyperbola and *c*, which becomes the integration constant, is determined by the initial conditions of the robot.

$$q_1(t_0)q_2(t_0) = c$$

- ♦ In this case the kinematic constraint implies a geometric constraint
- Example:

$$\diamond$$
 $C = R^2$

♦ Consider $q_1^2 + q_2^2 = c$. After differentiation we get:

$$q_1 \dot{q_1} + q_2 \dot{q_2} = 0$$

- ♦ Geometrically the function represents a circle and, again, *c* is determined by the initial conditions of the robot.
- ♦ In this case the kinematic constraint implies a geometric constraint.
- ◆ Example:

$$\diamondsuit$$
 $C = R^3$

$$\Leftrightarrow \left(\begin{array}{c} \sin(q_3) \\ -\cos(q_3) \\ 0 \end{array} \right)^T \dot{q} = 0$$

- ♦ This is **not integrable**, so there are not global mobility restrictions associated with this constraint.
- In general, all linear kinematic constraints are integrable and represent a global mobility constraints.
 - $\Rightarrow a^T(q)\dot{q} = 0$ may be integrable if:

♦ Generalizing:

- ▶ The condition is that the integrating factor $\gamma(q)$ should not be zero.
- ◆ **HOLONOMIC**: kinematic constraints that can be integrated to geometric constraints.
 - ♦ Restrict both local and global mobility.
- NON-HOLONOMIC: kinematic constraints that cannot be integrated to geometric constraints. Non-holonomic robots are subject to at least one non-holonomic constraint.
 - ♦ Restrict only local mobility.
- Rolling coin (disk) example Non-holonomic constraint: There is a coin rolling upright on a flat surface. To define the configuration we need the position of the contact point on the surface and the orientation.

- \diamond C = SE(2)
- ♦ Constraints:
 - ▶ Pure rolling:

$$- \dot{x}\sin(\theta) - \dot{y}\cos(\theta) = \begin{bmatrix} \sin(\theta) \\ -\cos(\theta) \\ 0 \end{bmatrix} \dot{q} = 0$$

- It is a Pfeffien constraint
- Geometrically it means that $\begin{bmatrix} \sin(\theta) \\ -\cos(\theta) \\ 0 \end{bmatrix}$ is orthogonal to

the velocity vector \dot{q} .

- ♦ Is it holonomic? If we can prove that the system can go anywhere then the constraint is NH (i.e. the system is controllable)
- \diamond Admissible velocities: N k = 2 Dimensional space.

$$\dot{q} \in Na(T(q))$$

$$\blacktriangleright Nd^{T}(q) \neq \begin{bmatrix} \cos\theta \\ \sin(\theta) \\ 0 \end{bmatrix}, \begin{pmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

- ► The first vector represents rolling and the second represents rotation.
- ▶ The null space will then span any linear combination of these two vectors, which means that it can reach any point in the plane. So the constraint is **Non-holonomic**.

Autonomous and Mobile Robotics

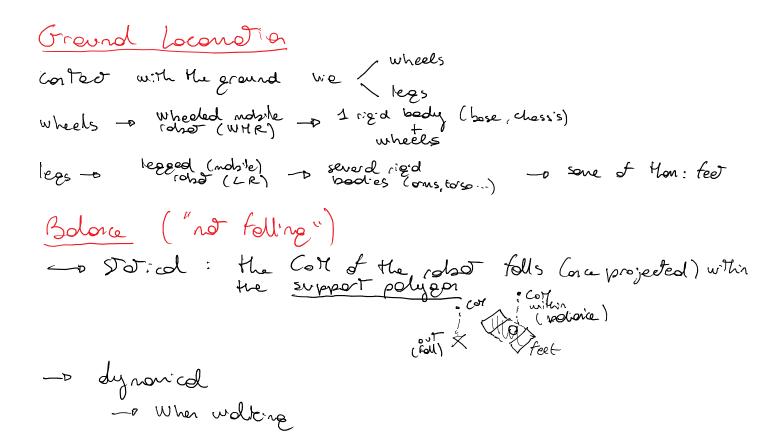
Prof. Giuseppe Oriolo

Wheeled Mobile Robots I Mechanics of Mobile Robots

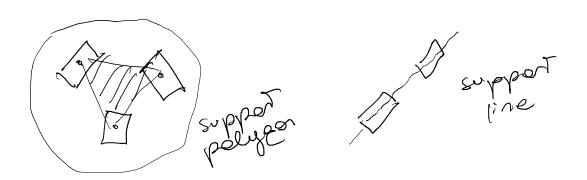
companion slides for the blackboard lecture

Dipartimento di Ingegneria Informatica Automatica e Gestionale Antonio Ruberti



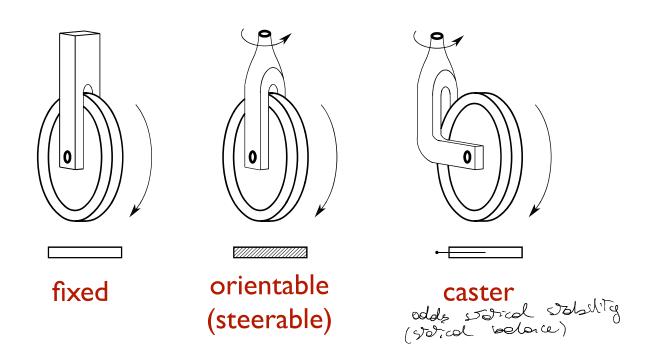


Bolone in WMR each wheel to I point contact with ground to get on ideal support polygon, need 3 wheels

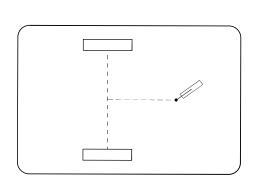


wheels

three basic types



kinematic structures

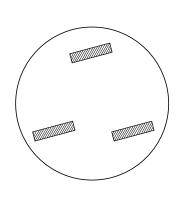




differential-drive mobile robot

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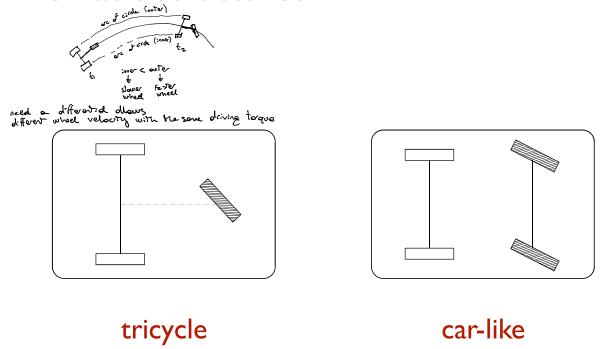
kinematic structures





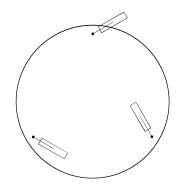
synchro-drive mobile robot

kinematic structures



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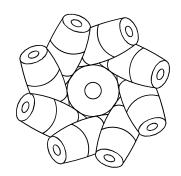
kinematic structures





omnidirectional mobile robot with 3 (actuated) caster wheels

kinematic structures



Mecanum (Swedish)
wheels can be also used
to build omnidirectional
mobile robots





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Implicit function theorem

h(q)=0 it is locally possible to note it explicit as 9, = ((q2, ..., qn)

provided that some singularity conditions

exomple 96 R2 9,2+922=1 (GC)

92= + VI-9,2 express 92 as \$\psi(9,)\$

locally I can solve saying "only + in the upper half orde"

· Oldsolly: better close veridales

In this case - orc length s (curvilines) or phose length of

· es we did for the noripulators

<u>kc</u> a; (9,9)=0 i=1,...,k therefore also relacity is involved typically linear in à -> at (q) à = 0 => (a,(q) ... a,(q)) à=0 orange than like this

$$\begin{pmatrix} \alpha_{1}^{T}(q) \\ \alpha_{2}^{T}(q) \\ \vdots \\ \alpha_{k}^{T}(q) \end{pmatrix} \stackrel{\circ}{q} = 0$$

k { A (a) q = 0 Pfeffin form of KC (linear in q)

o Modsility kinitation

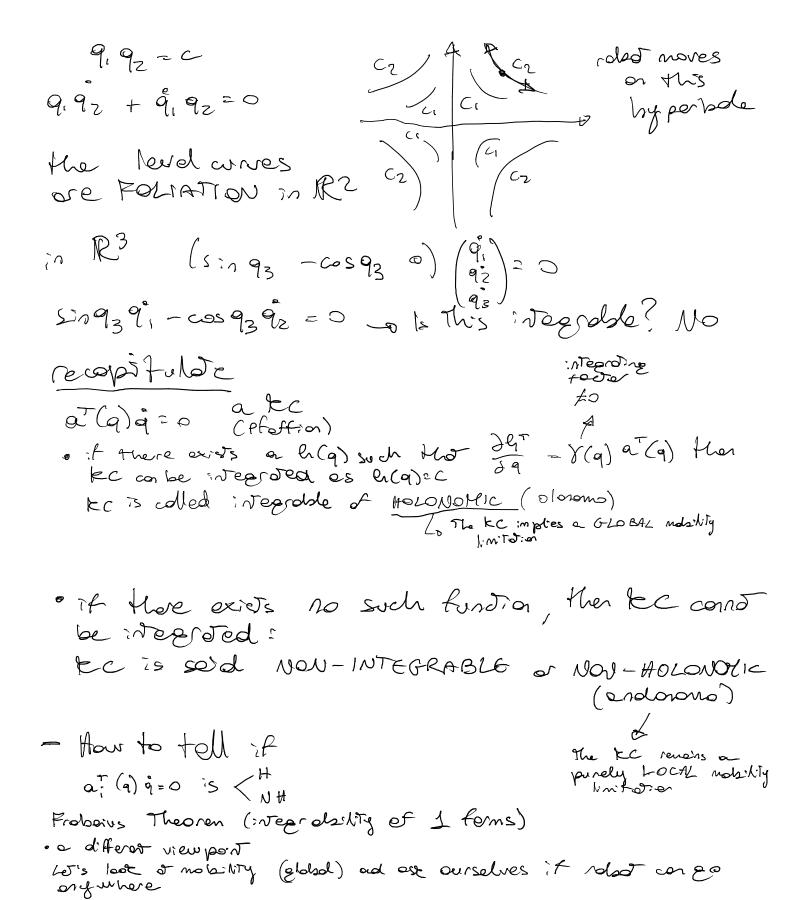
It each q the admissible g must belong to N(AT(9))

a linear space of dimension N-K

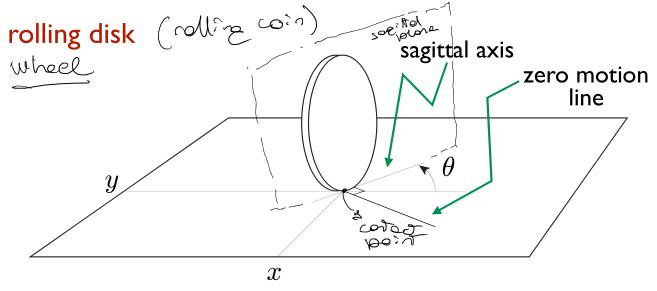
To hyper plane

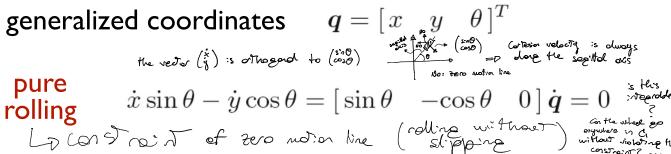
it is limitine the possible motion, not the configuration itself - I local mobility knitotion

Roldinship GC/EC a GC duays implies on EC en (9)=0 continuous soistection de (9) =0 $\frac{\partial h}{\partial t} = \frac{\partial h}{\partial q} \stackrel{\circ}{q} = 0 = 0 \quad (\frac{\partial h}{\partial q_1} \quad \frac{\partial h}{\partial q_2}) = \nabla \stackrel{\circ}{q} \stackrel{\circ}{h}$ (Vgh) g = 0 Pfotien tronspose of the greatest (a (9)) geonetrical interprotation: it we have 60 h(q)=0 then recessorily of new be orthogonal to Toph Rygh obie. It must be target by the round to the surface $\frac{1}{2}$ ble sufale of q · a KC does not duays : mysties a GC 9,9, + 92 92 =0 :n RZ (9, 92) (9, 92) = 0At (a) . 9 Pfetra constroit of GC Con this be written es li(q)=0 for some h, i.e., is it integrable? Yes: it is dearly integrable 92+92=C derivolve 29,9,+29z9z=0 the original EC 9,9,+9292=0 | con be integrated as 19,2+92=c A lacol modsitify Blobal industry the robot is constrained to more slone too level circle



example of nonholonomic constraint



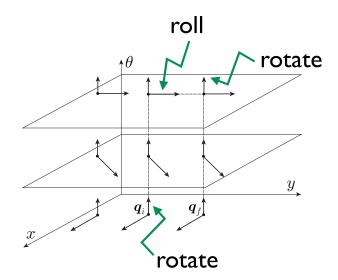


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the disk can go from any initial to any final configuration

e.g.

- 1. rotate so as to align with the final position
- 2. roll up to the final position
- 3. rotate up to the final orientation



hence, the rolling constraint is nonholonomic

we proved that the rolling without slipping constraint is Non-holonomic by exhibiting on monouver that steers the cor between my two configurations (" constructive controllablation).

(" constructive controllablation).

because the case is simple because the case is simple.

In general I use on algebraic test.