

# A CRYOGENIC TESTING ENVIRONMENT FOR SPT-3G, THE NEXT GENERATION SOUTH POLE TELESCOPE RECEIVER

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## ABSTRACT

The next generation optical system for the South Pole Telescope, SPT-3G, is set to be installed in early 2016. This report outlines the fundamental science goals and operation behind SPT-3G, and covers the development of a cryogenic testing environment at the University of Toronto for characterizing the next generation of detectors.

### 1. INTRODUCTION

The South Pole Telescope (SPT) is a 10 metre microwave telescope, located at the geographic South Pole in Antarctica. Designed to observe temperature and polarization anisotropies in the Cosmic Microwave Background (CMB) (Ruhl et al. 2004), the telescope has been optimized to operate in the millimetre (mm) band spanning from 75 GHz to 240 GHz. The next generation optical system to be installed at the beginning of 2016, SPT-3G, is to contain over 16,000 polarization sensitive detectors in the focal plane array. This order of magnitude increase in the number of detectors over the current receiver will allow for high signal-to-noise mapping of both the *E*-mode and *B*-mode CMB polarization anisotropies (Benson et al. 2014). With the increased sensitivity achieved by SPT-3G, significant advances can be made in the fields of large scale structure formation, particle physics, and cosmic inflation.

The SPT-3G detector wafers are currently being fabricated by Argonne National Laboratory, using a range of designs in order to tweak device parameters. Each wafer is tested within the SPT collaboration, providing characteristic feedback for the nanofabrication process. The detectors operate in the superconducting transition region for titanium, requiring a sub-kelvin cryogenic environment for detector testing. This report outlines the development of such a system at the University of Toronto (UofT), to assist in the testing and characterization of SPT-3G wafers. In conjunction, this system also features the SPT-3G Digital Frequency Multiplexing (DfMUX) readout system. This enables testing of the entire SPT-3G detector readout chain at UofT. In Section 2, the science goals of SPT-3G are outlined, with the instrumentation required to achieve these goals covered in Section 3. Section 4 details the development of the cryogenic testing at UofT, with current testing results in Section 5. Finally, Section 6 takes a brief look at the processing of SPTpol detector timestreams into usable scientific data.

### 2. SPT-3G SCIENCE GOALS

The telescopes location at the Amundsen-Scott South Pole Station provides one of best sites on Earth for ob-

serving mm-wavelength anisotropies. This is in part due to the South Pole's elevation of 2.8 kilometres above sea level, resulting in desirably low levels of atmospheric fluctuation power. The near zero air humidity also weakens the strong absorption and emission features of atmospheric water vapour at mm-wavelengths. The current optical design produces a beamwidth of  $\sim 1$  arcmin at 150 GHz, allowing for high resolution mapping of small-scale CMB features. Coupled with the high raw sensitivity achievable through the new multi-chroic polarization-sensitive pixel design, SPT-3G will be able to extract a wealth of previously unobtainable cosmological information from the CMB.

Lensing measurements of the CMB are capable of probing matter fluctuations out to the last scattering surface, providing a detailed lensing power spectrum. SPT-3G's precise measurement of the growth of structure on small angular scales places tight constraints on the number of relativistic species at recombination. Combined with measurements from the *Planck* experiment, it is expected that the sum of neutrino masses will be constrained to within  $\sigma(\Sigma m_\nu) \sim 0.06$  eV (Benson et al. 2014).

Currently pursued by a number of other experiments is the measurement of the energy scale of inflation, described by the tensor-to-scalar ratio  $r$  of primordial perturbations (Samtleben et al. 2007). While instruments such as BICEP2/KECK are optimized for measuring low angular modes, they have little or no sensitivity to small-scale temperature and polarization anisotropies. In order to fully characterize the inflationary and lensing *B*-mode signals, it is vital to take a high-resolution, multi-frequency approach. SPT-3G will be capable of producing a high signal-to-noise map of the lensed *B*-modes, achieving a noise level of  $\sim 3.5 \mu\text{K-arcmin}$ . When used in conjunction with its exquisite *E*-mode measurements, the lensing potential can be reconstructed, allowing for the separation of the lensing *B*-mode signal from the inflationary signal. This process is known as "delensing", improving the shape of the tensor power spectrum and constraining  $r$  to within  $\sigma(r) \ll 0.01$  (Benson et al. 2014).

The high angular resolution of the telescope also pro-

vides a unique way of probing the largest gravitationally bound objects in the universe, clusters of galaxies. CMB photons collide with high energy electrons contained within galaxy clusters, where they inverse Compton scatter to higher energies. This produces a distortion in the CMB signal, known as the Sunyaev-Zel'dovich (SZ) effect. This effect is largely redshift independent, allowing for the identification of almost every massive cluster above a given mass threshold, depending on instrument sensitivity. SPT-3G will be surveying a nearly identical  $2500 \text{ deg}^2$  area to SPT-SZ, albeit with noise levels  $\sim 12$ ,  $7$ , and  $20$  times lower at  $95$ ,  $150$ , and  $220 \text{ GHz}$ , respectively. The lowering of the cluster mass threshold and extension of redshift reach will allow SPT-3G to find  $\sim 5000$  clusters at a signal-to-noise  $> 4.5$ , an order of magnitude more clusters than SPT-SZ. Complimenting and calibrating the Dark Energy Survey (DES) cluster survey, the SZ data is predicted to result in a dark energy figure-of-merit of  $\sim 100$ .

### 3. SPT-3G INSTRUMENTATION

While the SPT third-generation receiver design also features a new optical system and cryostat, this report is to focus on the detectors contained in the focal plane array and its novel readout system.

#### 3.1. Focal Plane Array

A significant contribution to SPT-3G's leap forward in sensitivity can be attributed to the newly designed focal plane array, featuring 2710 independent pixels compared to SPT-POL's 768. Each pixel is polarization sensitive across three observing bands at  $95$ ,  $150$ , and  $220 \text{ GHz}$ . Using a sinuous log-periodic antenna, each pixel can absorb a wide band of mm-wave photons at orthogonal polarizations. Once absorbed, microstrip transition line filters route the power from each band to one of six independent transition edge sensor (TES) bolometers (one for each band and polarization). This design results in over 16,000 detectors across the entire focal plane array. The focal plane array itself consist of 10 nanofabricated 6" wafers, each containing 217 of these polarization sensitive tri-chroic pixels in both left and right-handed configurations (to account for polarization wobble induced by the antenna shape).

Each detector is essentially a microstrip termination resistor located on a thermally isolated TES bolometer island. The TES bolometer itself is held in its superconducting phase transition, where a small increase in temperature results in a dramatic increase in resistance. By passing current through the TES, a change in resistance can be measured when an absorbed photon dumps energy onto the island through the microstrip. This configuration allows for a negative feedback loop, where the increase in resistance restricts the bias current. This lowers the power passing through the TES, dropping the detector back into its superconducting phase transition. The bolometer time constant for this process is  $\sim 3 \text{ ms}$ .

#### 3.2. Readout System

If each bolometer within the focal plane array were read out using independent wire pairs, the resulting thermal load would make it near impossible to maintain the array below the TES superconducting transition temper-

ature. As such, a Digital Frequency Multiplexing (DfMUX) readout system is utilised, allowing 64 bolometers to be read out using a single pair of wires. Developed by McGill University, the DfMUX system relies on each resistive bolometer being placed in series with a unique inductance  $L$  and capacitance  $C$ . This configuration forms an  $LCR_{bolo}$  resonator, allowing the bolometer to be interrogated using a unique resonant frequency. Recent improvements in the DfMUX bandwidth now allows 64 of these  $LCR_{bolo}$  resonators to be placed in parallel, up from 16, with resonances spaced from  $1.6$  to  $4.6 \text{ GHz}$ . A sinusoidal voltage bias can then be fed in on a single pair of wires, consisting of every bolometer's resonant frequency summed together into a single waveform (referred to as a *comb of carriers*) (Bender et al. 2014). Changes in bolometer resistance from absorbed photons modulates each carrier, appearing as sidebands in the current. This resulting signal is then amplified using Superconducting Quantum Interference Device (SQUID) amplifiers.

SQUIDS are used as the first amplification stage due to their high gain, low input-impedance, and low noise performance. The amplifiers consist of a superconducting loop containing two Josephson junctions that allow the current to be measured. Any applied magnetic flux to the SQUID will produce a screening current, requiring that the flux within the loop remains at an integer number of magnetic flux quanta. This results in a periodic voltage output as a function of the magnetic flux in the input coil. The DfMUX SQUID operation requires them to first be tuned to the region of maximum gain and linearity, by applying known current flux biases to the input coil (Bender et al. 2014). The dynamic range of the SQUIDS is capable of limiting the multiplexing factor, and so an inverted copy of the carrier comb is injected prior to the SQUID input coil (referred to as the *nuller*). The improved DfMUX multiplexing factor of 64 is realised through the use of Digital Active Nulling (DAN), an active feedback loop that nulls both the carriers and sidebands for each bolometer. Following the DAN stage, the signal is demodulated back to baseband allowing the current from each bolometer to be measured.

### 4. TESTING ENVIRONMENT

The operation of SPT-3G wafers and readout demands sub-Kelvin temperatures, requiring a cryogenic testbed. The Long Wavelength Lab (LWlab) at UoF currently houses an Olympus 104 cryostat, designed and fabricated by *High Precision Devices* (HPD) in Colorado. The cryostat consists of several stages, with successively colder and smaller stages located within one another. The largest of these, a  $50 \text{ K}$  stage and  $3 \text{ K}$  stage, are driven by a PT415 helium pulse tube refrigerator developed by *Cryomech*. This refrigerator relies on the acoustic resonance of sharply pulsed highly-pressurised helium gas. Pulses travelling through the tube, tuned to a particular resonance, produce heating on one end and cooling temperatures as low as  $2 \text{ K}$  at the other. The sub-Kelvin temperatures required for testing SPT-3G wafers are then realised using an Adiabatic Demagnetization Refrigerator (ADR) based on the  $3 \text{ K}$  stage.

The ADR itself consists of two paramagnetic salt pills, situated within a powerful superconducting electromagnet ( $L \sim 10 \text{ H}$ ). When a large current is applied to the electromagnet, the produced magnetic field aligns

the magnetic domains within the paramagnetic salt pills. This freezes out a thermal degree of freedom within the salt pills. Once soaked, removing the current from the coil allows the magnetic domains to realign, reintroducing the thermal degree of freedom. In accordance with the conservation of energy, this adiabatic realignment process lowers the temperature of the paramagnetic salt pills. The ADR system installed in the Olympus 104 cryostat features two salt pills, one of Ammonium Iron(III) Sulfate (FAA) and one of Gadolinium Gallium Garnet (GGG), with base temperatures 35 mK and 500 mK respectively. The FAA pill drives what is referred to as the *ultra-cold stage*, while the GGG pill drives the *intermediate stage*. The inclusion of an intermediate stage allows the ultra-cold stage to be buffered by the GGG pill's greater cooling power. This configuration ensures most of the thermal loading from the cold wiring is absorbed at the GGG pill, rather than the FAA.

The ADR's superconducting electromagnet contains  $\sim 5$  km of Niobium-Titanium (NbTi) wire looped around the magnet bore. This NbTi wire is superconducting below  $T_c = 9.2$  K, resulting in a series resistance of  $\sim 0.1 \Omega$  below the critical temperature. While superconducting, the NbTi wire has a critical current density of  $J_c = 10^3 \text{ A}\cdot\text{mm}^{-2}$  beyond which the superconducting state will break down. This sets an magnet current upper limit of 19.0 A for this given implementation. By exceeding this current or the critical temperature  $T_c$ , the superconductivity of the wire will cease, resulting in the dumping of magnet's field energy to the 3 K stage. This scenario is called a magnet "quench", and can cause significant damage to the system. As such, multiple safeguards have been implemented in both hardware and software to avoid such a scenario.

Following demagnetization, the ADR's ultra-cold temperature is regulated at a chosen setpoint using a Proportional-Integral-Derivative (PID) loop control system. Thermometry feeds in the stage temperature to the PID controller, which if below the chosen setpoint, will apply current to the coil heating up the stage. If above the chosen setpoint, the current is decreased, cooling the stage through the aforementioned adiabatic process. While regulating at 250 mK, this control loop can maintain the FAA temperature to within 0.05 mK. Once the regulation current supplying the cooling power has been depleted, a full magnetization cycle must be repeated.

#### 4.1. Control System Development

The LWlab cryostat system is operated using the *cryo-server*, a python-based control program featuring a tornado web-interface (written in coffeescript). The *cryo-server* is responsible for a multitude of tasks, from monitoring and logging system parameters (temperature, pressure, *etc.*), running commands from the web-interface, to performing ADR magnetization cycles with a suite of error checking. In preparation for integrating the SPT-3G testbed, some major improvements were made to the functionality of the *cryo-server*. These include, but are not limited to;

- The monitoring of electromagnet back-EMF, preventing ADR magnetization cycles from quenching due to excessive current ramping.
- Editing of cycle parameters through the web-

interface, controlling ramp-up time, hold current, hold time, and ramp-down time.

- A scheduling interface for automatically starting magnetization cycles, allowing wafer testing to proceed at a specified time.
- An email alert system in the result of a Uninterruptible Power Supply (UPS) failure.
- Stability fixes preventing the *cryo-server* from crashing due to multiple connection requests.

The *cryo-server* now serves as a stable and reliable piece of control system software, allowing the cryostat system to be run remotely for the majority of a cooldown cycle. Given the six-hour duration of a "full" magnetization cycle, the addition of the scheduling interface enables detector testing to take place during work hours without lost time to cycling the ADR, maximising testing throughput.

#### 4.2. Hardware Development

To accommodate the integration of an SPT-3G wafer holder and LC towers (containing the inductors and capacitors for the DfMUX readout), a new 'cold-stage' was purchased and installed. The cold-stage consists of three Oxygen-free High thermal Conductivity (OHFC) Copper rings, each separated by six insulating carbon fibre struts. The upper-most ring attaches to the bottom of the 3 K stage, with the middle and lower rings connected to the intermediate and ultra-cold stages respectively via OHFC copper braids. The SPT-3G wafer holder is then mounted to the ultra-cold stage, allowing its temperature to be finely controlled and monitored through the control system.

A suite of additional *Lakeshore* thermometry (five *Cernox* and two diodes) was calibrated and distributed across the SPT-3G wafer installation. Using a 'Cryoboard' (developed at McGill University) for readout, this setup allows for quick identification of high thermal loading points within the wafer setup by monitoring several points of interest in real time. The Cryoboard installation also accommodates the use of heater blocks (essentially resistors in an OHFC copper seat), allowing varying amounts of thermal power to be dumped onto the ultra-cold stage.

#### 4.3. DfMUX Integration

The DfMUX readout system is run from an ICE motherboard FPGA platform (referred to as an *Iceboard*) developed by McGill. Along with Cryoboard, a custom-built enclosure is needed to house the two motherboards for both protection and compactness. A  $17 \times 12 \times 5$  inch steel box provided sufficient volume for containing the boards, their power supplies, and a dual fan-driven ventilation system. The front and back panels were modelled using *Solidworks* and exported to *SprutCAM*, where tool paths were generated for cutting out front panel slots, fan ports, and holes for power and Ethernet jacks. These tool paths can then be loaded onto a Computer Numeric Control (CNC) machine as G-code. The *Dunlap Institute's* Tormach PCNC 770 was used to mill the front and back panels, which along with suitable mounting points and stand-offs, provided a suitable enclosure for the Iceboard and Cryoboard.

The second major design challenge with integrating the DfMUX system lies with passing hundreds of wires

through each stage of the cryostat to the inside the 3 K can. Conveniently, the HPD 104 cryostat comes with additional ports, for which the SPT collaboration has supplied a custom fitting wire harness. The wire harness provides seven slots to the interior of the cryostat, for which one ‘cryo-card’ and two ‘SQUID-cards’ have been installed. The cryo-card collects all the thermometry and heater cables for connection to the Cryoboard, while the SQUID-cards each contain four SQUID amplifiers (with each card connected to an LC tower via a stripline). The wire harness exterior features two DB-37 connectors per card slot. The DfMUX readout chain design requires a SQUID controller board to be plugged in directly to the wire harness exterior, for which two are used in our configuration. Unfortunately these devices are extremely sensitive to radio-frequency (RF) interference. As such, an RF-tight box was ordered and installed externally to the cryostat to house the SQUID controller boards. Finally, 37-pin custom cables needed to be fabricated for linking the SQUID controller boards to the Iceboard. To meet noise requirements, the cables must be of a Category 7 standard, meaning each wire pair is individually shielded including the cable as a whole. Two DfMUX cables bundles were fabricated, each consisting of five individual Category 7 Ethernet cables (often used for 10 Gigabit Ethernet connections) with breakouts to DB-37 connectors at each end.

## 5. TESTING RESULTS

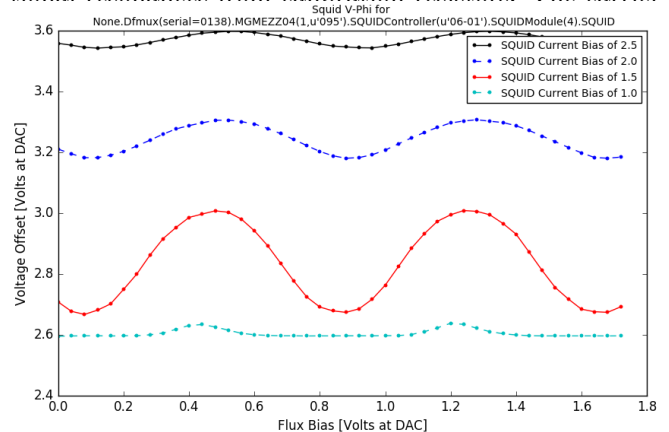
The end goal of characterising detectors conveniently allows multiple facets of the SPT-3G readout chain to be tested in parallel. Prior to operating the bolometers in their superconducting transition, the SQUIDs are tuned to the optimal bias point, testing SQUID performance. Following this is a network analysis to locate each  $LCR_{bolo}$  resonance, verifying wafer connectivity whilst also testing LC tower performance. Finally the bolometers can be biased, providing a wealth of information on the wafer characteristics. To date, approximately 30 wafers have been fabricated by the SPT collaboration. The previously tested ‘Wafer 44’ is used to validate the functionality of the cryogenic SPT-3G testing environment developed at UofT.

### 5.1. SQUID Tuning

The algorithm for tuning the SQUIDs to the region of maximum gain and linearity first starts by producing voltage-flux (V-Phi) curves for assorted SQUID current biases. The flux bias Digital-to-Analog Converter (DAC) is swept through a range of values, mimicking the effect of a changing external magnetic field (Bender et al. 2014). The voltage required to zero the demodulated output is measured, forming a periodic function with peaks corresponding to  $1/2$  of the SQUID flux quanta. The produced V-Phi curves for one of the SQUIDs is shown in Figure 1. The tuning algorithm correctly identifies the SQUID current and flux bias for maximum gain, verifying SQUID performance.

### 5.2. Network Analysis

Once the SQUIDs have been successfully tuned, a network analysis algorithm works to identify each of the 64  $LCR_{bolo}$  resonant frequencies along with four additional resonances from calibration resistors. The carrier



**Figure 1.** A voltage-flux curve produced by sweeping through flux biases for a range of SQUID bias currents, measuring the voltage required to zero the demodulated output. The tuning algorithm correctly identifies the region of maximum gain and linearity in this case for a SQUID current bias of  $\sim 1.6$  A and flux bias of  $\sim 0.7$  V

and nuller DACs scan through a range of frequencies in the area of 200 kHz to 7 MHz, operating all 64 readout channels simultaneously until the full bandwidth of the system is probed. The output demodulated amplitude is measured and averaged, producing the readout module response as a function of frequency. A curve-fitting algorithm identifies each peak in the response, ideally producing 68 frequencies corresponding to each  $LCR$  resonance.

Early network analyses of the system produced poor results, with large noise levels causing the curve-fitting algorithm to fail. Revisions to the cryostat grounding scheme (where ground loops can produce stray currents through electromagnetic induction) and RF environment were successful in reducing the noise level in the readout module response. All 68 resonances were correctly identified, verifying this stage of the DfMUX readout system and permitting each bolometer to now be targeted and biased through its unique frequency.

### 5.3. Bolometer Biasing

## 6. DATA PROCESSING

## 7. CONCLUSION

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