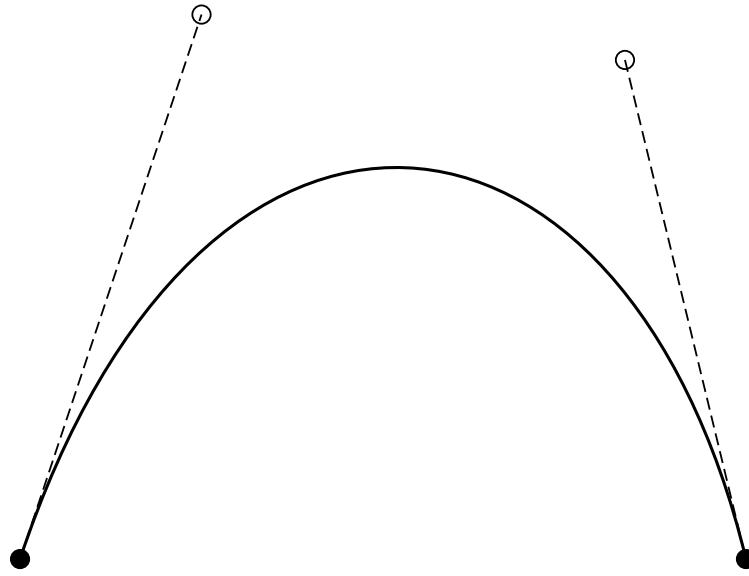


# A Monte Carlo Method for Image Decomposition into Collections of B-Splines

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## B-Splines

### Cubic Bezier Curves



A

### $C_2$ Continuous B-Splines of Cubic Bezier Curves

Thus a spline of  $n$  segments can be described in terms points  $\vec{p}_k$  and vectors  $\vec{v}_k$  with  $0 \leq k \leq n$ .

In the  $k$ -th segment the position  $\vec{r}$  and its derivative with respect to  $s$  with  $s \in [0, 1]$  are:

$$\begin{aligned}\vec{r} &= (1-s)^3 \vec{p}_k + 3(1-s)^2 s (\vec{p}_k + \vec{v}_k) + 3(1-s)s^2 (\vec{p}_{k+1} - \vec{v}_{k+1}) + s^3 \vec{p}_{k+1} \\ \frac{\partial}{\partial s} \vec{r} &= 3(1-s)^2 \vec{v}_k + 6(1-s)s (\vec{p}_{k+1} - \vec{p}_k - \vec{v}_{k+1} - \vec{v}_k) + 3s^2 \vec{v}_{k+1} \\ \frac{\partial^2}{\partial s^2} \vec{r} &= 6(1-s) (\vec{p}_{k+1} - \vec{p}_k - \vec{v}_{k+1} - 2\vec{v}_k) - 6s (\vec{p}_k - \vec{p}_{k+1} + \vec{v}_k + 2\vec{v}_{k+1})\end{aligned}$$

By setting  $k = \lfloor s \rfloor$  and  $\hat{s} = \{s\}$  the fractional part of  $s$  this definition can be extended to whole range of  $s$   $[0, n]$

$$k = \frac{\dot{\vec{r}}_x \ddot{\vec{r}}_y - \ddot{\vec{r}}_x \dot{\vec{r}}_y}{\|\dot{\vec{r}}\|^3}$$

$$dl = \|\dot{\vec{r}}\| ds$$

## Energies

Each energy term exist to promote a certain goal for the fitting of the splines. In this section all energy terms are derived and the reasoning behind them is explained.

### Strain Energy

The strain energy promotes the splines to keep their length. As the name suggests it is inspired by the strain energy in elastic materials.

$$E_s = S \frac{(L - L_0)^2}{L_0^2} L$$

### Bending Energy

The bending energy promotes splines which are straight.

$$\begin{aligned} E_b &= B \int_0^L k^2 dl \\ &= B \int_0^n \frac{(\dot{\vec{r}}_x \ddot{\vec{r}}_y - \ddot{\vec{r}}_x \dot{\vec{r}}_y)^2}{\|\dot{\vec{r}}\|^5} ds \end{aligned}$$

### Potential Energy

The potential energy promotes the correct density of the splines.

$$\begin{aligned} E_\Phi &= Q \int_0^L \Phi(\vec{r}) dl \\ &= Q \int_0^n \Phi(\vec{r}(t)) \|\dot{\vec{r}}\| ds \end{aligned}$$

### Field Energy

The field energy promotes the alignment of the splines to a vector field.

$$\begin{aligned} E_{\vec{v}} &= P \int_0^L -\frac{|\dot{\vec{r}} \cdot \vec{v}(\vec{r})|}{\|\dot{\vec{r}}\|} dl \\ &= -P \int_0^n |\dot{\vec{r}} \cdot \vec{v}(\vec{r})| ds \end{aligned}$$

### Pair Interaction Energy

The pair interaction energy creates a repulsive force between the splines. In contrast to all other energies this energy depends on two splines.

$$\begin{aligned}
E_g &= C \int_0^{L_0} \int_0^{L_1} \frac{1}{\|\vec{r}_0 - \vec{r}_1\|} dl_1 dl_0 \\
&= C \int_0^{n_0} \int_0^{n_1} \frac{\|\dot{\vec{r}}_0\| \|\dot{\vec{r}}_1\|}{\|\vec{r}_0 - \vec{r}_1\|} ds_1 ds_0
\end{aligned}$$

## Boundary Energy

The boundary energy exist so the splines stay within the boundaries during the simulation. Let  $d(\vec{r})$  be the signed distance function to the boundary, defined such that  $d(\vec{r}) < 0$  if  $\vec{r}$  is with in the simulation boundaries.

Let  $f(x) = \begin{cases} \infty & \text{if } x > 0 \\ \frac{1}{x^2} & \text{else} \end{cases}$

$$\begin{aligned}
E_r &= R \int_0^L f(d(\vec{r})) dl \\
&= R \int_0^n f(d(\vec{r})) \|\dot{\vec{r}}\| ds
\end{aligned}$$

## Total Energy

In Table 1 the formulas for the energies are summerized some constants are renamed and the parameters are given.

Energy	Formula
strain energy	$E_{s,i} = S \frac{(L_i - L_{i,0})^2}{L_{i,0}^2} L_i$
bending energy	$E_{b,i} = B \int_0^{n_i} \frac{(\dot{\vec{r}}_{i,x} \ddot{\vec{r}}_{i,y} - \ddot{\vec{r}}_{i,x} \dot{\vec{r}}_{i,y})^2}{\ \dot{\vec{r}}_i\ ^5} dt$
potential energy	$E_{\Phi,i} = Q \int_0^{n_i} \Phi(\vec{r}_i(t)) \ \dot{\vec{r}}_i\  dt$
field energy	$E_{\vec{v},i} = P \int_0^{n_i} \dot{\vec{r}}_i \cdot \vec{v}(\vec{r}_i) dt$
pair interaction energy	$E_{g,ij} = C \int_0^{n_i} \int_0^{n_j} \frac{\ \dot{\vec{r}}_i\  \ \dot{\vec{r}}_j\ }{\ \vec{r}_i - \vec{r}_j\ } dt_j dt_i$
boundary energy	$E_{r,i} = R \int_0^{n_i} f(s(\vec{r}_i)) \ \dot{\vec{r}}_i\  dt$

Table 1: All energy terms

The total energy  $E_{\text{tot}}$  is simply the sum of all energies.

$$E_{\text{tot}} = \sum_i (E_{s,i} + E_{b,i} + E_{\Phi,i} + E_{\vec{v},i} + E_{r,i}) + \sum_i \sum_{j,j>i} E_{g,ij}$$

or

$$E_{\text{tot}} = \sum_i (E_{s,i} + E_{b,i} + E_{\Phi,i} + E_{\vec{v},i} + E_{r,i}) + \frac{1}{2} \sum_i \sum_{j,j \neq i} E_{g,ij}$$

## Lagrangian View

The generalized coordinates are  $\vec{p}_{ij}$  and  $\vec{v}_{ij}$  with  $1 \leq i \leq N$  and  $0 \leq j \leq n_i$  where  $N$  is the total number of particles and  $n_i$  is the number of segments of particle  $i$ .

$$E_{\text{kin}} = \int_0^L \frac{1}{2} \vec{v}^2 \rho dl = \frac{1}{2} \rho \int_0^n (\dot{\vec{r}})^2 \left\| \frac{\partial \vec{r}}{\partial s} \right\| ds$$

Setting  $V$  to  $E_{\text{tot}}$  and  $T$  to the sum of kinetic energies  $\sum_i E_{\text{kin},i}$

Plugging  $L = T + V$  into Lagrange's equation and assuming no external forces we get:

For any  $q$  in our coordinates:

$$\frac{d}{dt} \left( \frac{\partial}{\partial \dot{q}} T \right) - \frac{\partial}{\partial q} T + \frac{\partial}{\partial q} V = 0$$

With fixed  $i$  and  $q \in \{\vec{p}_{ij}\} \cup \{\vec{v}_{ij}\}$   $T$  can be rewritten as  $E_{\text{kin},i}$  since this is the only term in  $T$  which depends on any coordinate with index  $i$ .

The first term becomes:

$$\begin{aligned} \frac{d}{dt} \left( \frac{\partial}{\partial \dot{q}} T \right) &= \frac{d}{dt} \left( \frac{\partial}{\partial \dot{q}} \frac{1}{2} \rho \int_0^{n_i} (\dot{\vec{r}}_i)^2 \left\| \frac{\partial \vec{r}_i}{\partial s} \right\| ds \right) \\ &= \rho \frac{d}{dt} \int_0^{n_i} \left( \dot{\vec{r}}_i \cdot \frac{\partial \dot{\vec{r}}_i}{\partial \dot{q}} \right) \left\| \frac{\partial \vec{r}_i}{\partial s} \right\| ds \\ &= \rho \int_0^{n_i} \left( \left( \ddot{\vec{r}}_i \cdot \frac{\partial \dot{\vec{r}}_i}{\partial \dot{q}} \right) + \left( \dot{\vec{r}}_i \cdot \frac{d}{dt} \frac{\partial \dot{\vec{r}}_i}{\partial \dot{q}} \right) \right) \left\| \frac{\partial \vec{r}_i}{\partial s} \right\| ds \end{aligned}$$

Note that in our case  $\frac{\partial \dot{\vec{r}}_i}{\partial \dot{q}}$  is independent of  $t$  since  $\dot{\vec{r}}$  depends linearly on  $q$ . Thus, its derivative with respect to  $t$  is 0.

$$\frac{d}{dt} \left( \frac{\partial}{\partial \dot{q}} T \right) = \rho \int_0^{n_i} \ddot{\vec{r}}_i \cdot \frac{\partial \dot{\vec{r}}_i}{\partial \dot{q}} \left\| \frac{\partial \vec{r}_i}{\partial s} \right\| ds$$

Furthermore note that  $\vec{r}_i$  only depends on the coordinates with subscript  $j$  for  $s \in (j-1, j)$  and  $s \in (j, j+1)$ . For  $j=0$  and  $j=n$  the first or the second interval respectively is not included. For  $\vec{p}_{ij}$  we get

$$\begin{aligned} \rho \int_{j-1}^j \ddot{\vec{r}}_i \frac{\partial \dot{\vec{r}}_i}{\partial \dot{p}_{ij}} \left\| \frac{\partial \vec{r}_i}{\partial s} \right\| ds &= \rho \int_0^1 \ddot{\vec{r}}_{ij} (3s^2(1-s) + s^3) \left\| \frac{\partial \vec{r}_{ij}}{\partial s} \right\| ds \\ \rho \int_j^{j+1} \ddot{\vec{r}}_i \frac{\partial \dot{\vec{r}}_i}{\partial \dot{p}_{ij}} \left\| \frac{\partial \vec{r}_i}{\partial s} \right\| ds &= \rho \int_0^1 \ddot{\vec{r}}_{ij+1} ((1-s)^3 + 3s(1-s)^2) \left\| \frac{\partial \vec{r}_{ij+1}}{\partial s} \right\| ds \end{aligned}$$

Similarly for  $\vec{v}_{ij}$

$$\rho \int_{j-1}^j \ddot{\vec{r}}_i \frac{\partial \dot{\vec{r}}_i}{\partial \dot{v}_{ij}} \left\| \frac{\partial \vec{r}_i}{\partial s} \right\| ds = \rho \int_0^1 \ddot{\vec{r}}_{ij} (-3s^2(1-s)) \left\| \frac{\partial \vec{r}_{ij}}{\partial s} \right\| ds$$

$$\rho \int_j^{j+1} \ddot{\vec{r}}_i \frac{\partial \dot{\vec{r}}_i}{\partial \dot{v}_{ij}} \left\| \frac{\partial \vec{r}_i}{\partial s} \right\| ds = \rho \int_0^1 \ddot{\vec{r}}_{ij+1} (3s(1-s)^2) \left\| \frac{\partial \vec{r}_{ij+1}}{\partial s} \right\| ds$$

The second term becomes:

$$\begin{aligned} \frac{\partial}{\partial q} T &= \frac{\partial}{\partial q} \frac{1}{2} \rho \int_0^{n_i} (\dot{\vec{r}}_i)^2 \left\| \frac{\partial \vec{r}_i}{\partial s} \right\| ds \\ &= \frac{1}{2} \rho \int_0^{n_i} (\dot{\vec{r}}_i)^2 \frac{1}{\left\| \frac{\partial \vec{r}_i}{\partial s} \right\|} \left( 2 \frac{\partial \vec{r}_i}{\partial s} \cdot \frac{\partial}{\partial q} \frac{\partial \vec{r}_i}{\partial s} \right) ds \\ &= \frac{1}{2} \rho \int_0^{n_i} (\dot{\vec{r}}_i)^2 \frac{\frac{\partial \vec{r}_i}{\partial s} \cdot \frac{\partial}{\partial q} \frac{\partial \vec{r}_i}{\partial s}}{\left\| \frac{\partial \vec{r}_i}{\partial s} \right\|} ds \end{aligned}$$