

# MODÉLISATION ET RÉSOLUTION DE LA RÉPONSE À LA COLLISION

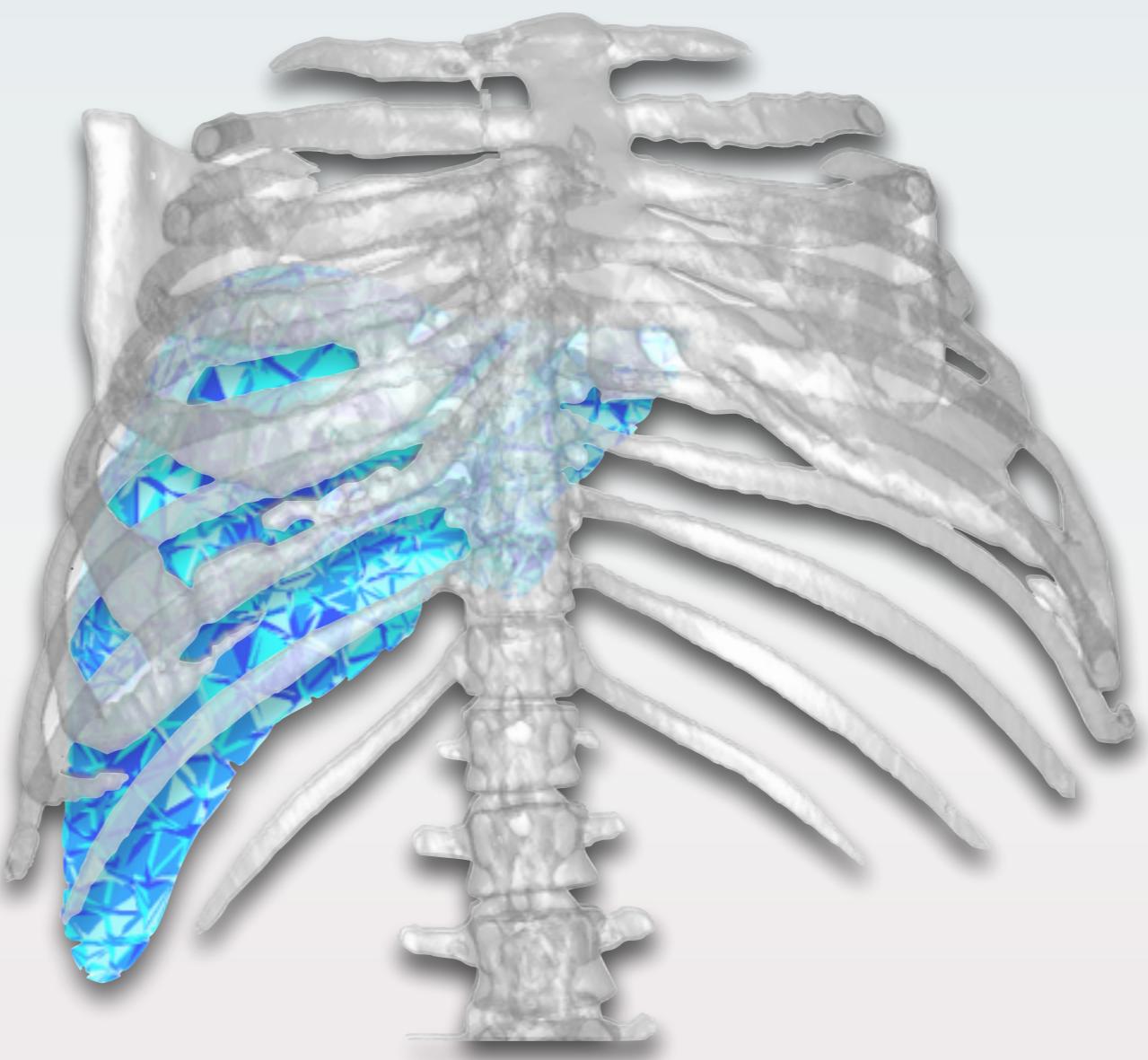
Christian Duriez  
INRIA Defrost-Team Lille

# WHY IMPORTANT ?

- Tool-tissue interaction realism
  - Post interaction deformation
  - Behavior of the instruments
  - Haptic rendering
- Boundary conditions
  - For both tools and soft tissues
  - Interactions between anatomical structures
- Surgical simulator  $\neq$  scripted game
  - Limited possible precomputation
  - Should allow for mistakes...
- NEED OF PHYSICS !

# OUTCOME

- Mechanical models for real-time computation (rappel)
- Constraint-based modeling of biomechanical interactions



(RAPPELS)  
MECHANICAL MODELS FOR  
REAL-TIME COMPUTATION

# MECHANICAL MODELS

- Newton's second law

$$\mathbb{M}(\mathbf{q})\dot{\mathbf{v}} = \mathbb{P}(t) - \mathbb{F}(\mathbf{q}, \mathbf{v}) + \mathbf{H}^T \lambda$$

$\mathbf{q} \in \mathbb{R}^n$  Vector of generalized degrees of freedom (nodes of a deformable model)

$\mathbf{v} \in \mathbb{R}^n$  Vector of velocities

$\mathbb{M}(\mathbf{q}) : \mathbb{R}^n \mapsto \mathcal{M}^{n \times n}$  Inertia Matrix

$\mathbb{F}(\mathbf{q}, \mathbf{v})$  Internal forces (non-linear model)

$\mathbb{P}(t)$  External forces

$\mathbf{H}^T \lambda \in \mathbb{R}^n$  Constraint force contribution

# TIME INTEGRATION SCHEMES

- Explicit Methods:

$$\mathbb{M} \dot{\mathbf{v}} = \mathbb{P}(t) - \mathbb{F}(\mathbf{q}, \mathbf{v})$$



- Conditionnally stable
- High constraint on the time step used in the simulation
- $h \leq Le/c$  ( $h$ : time step,  $Le$ : Caracterstic length of smallest element,  $c$ : velocity of the deformation wave)

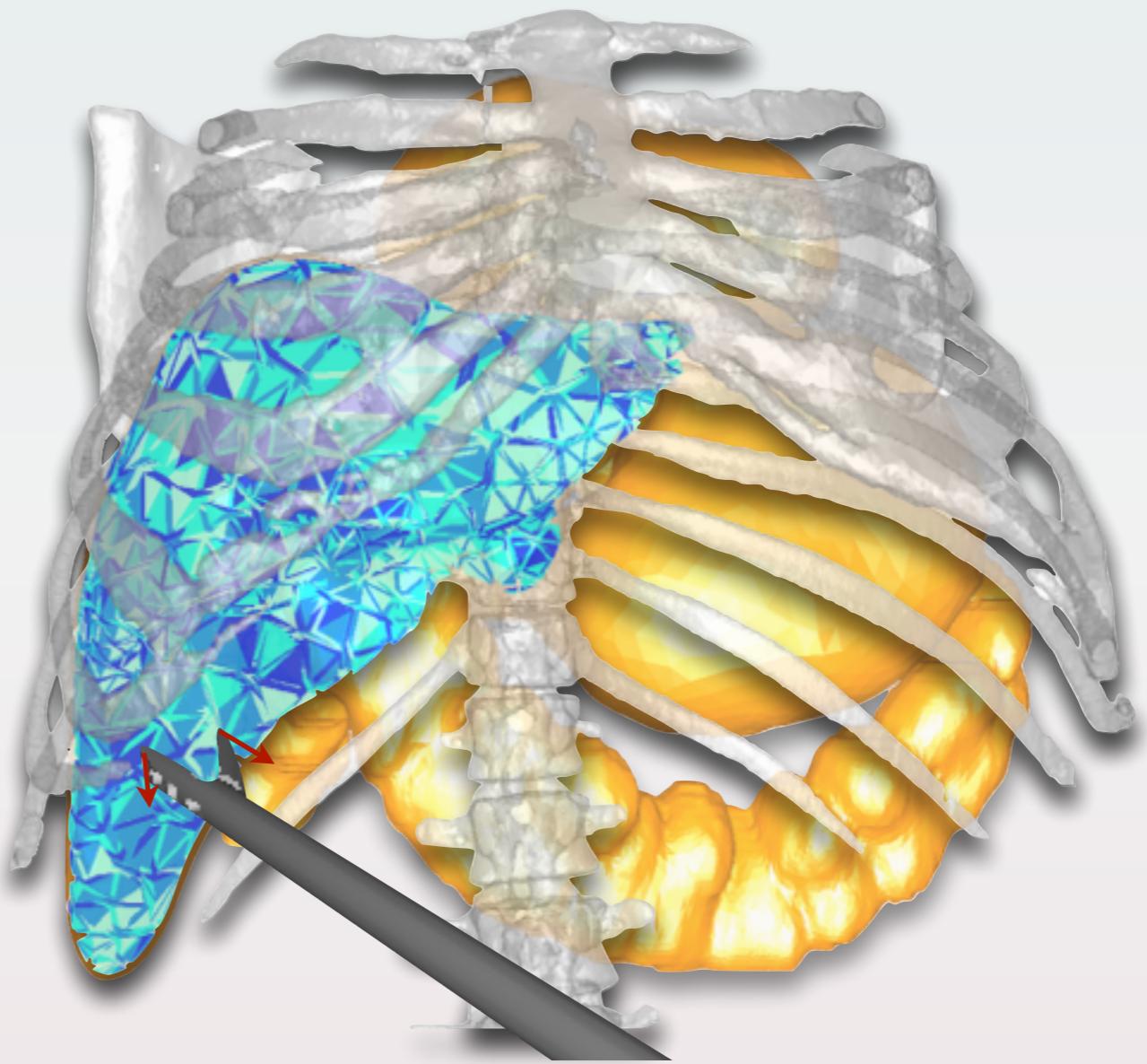
# TIME INTEGRATION SCHEMES

- Implicit Methods:

$$\mathbb{M} \dot{\mathbf{v}} = \mathbb{P}(t) - \mathbb{F}(\mathbf{q}, \mathbf{v})$$



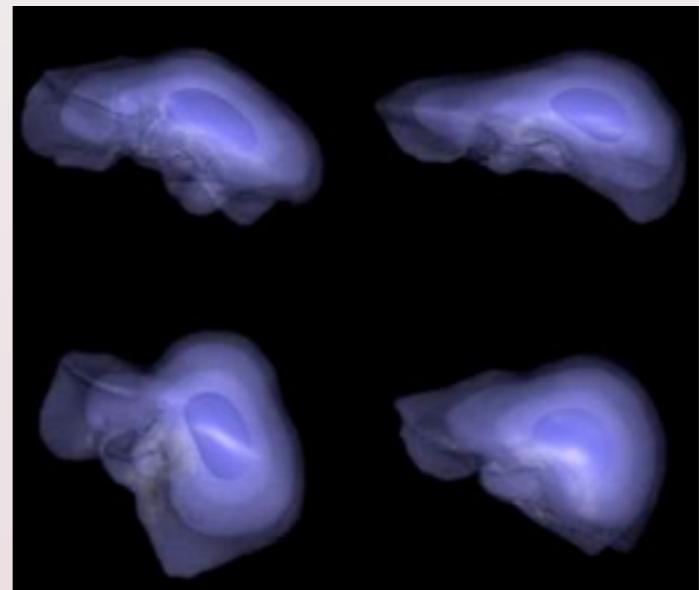
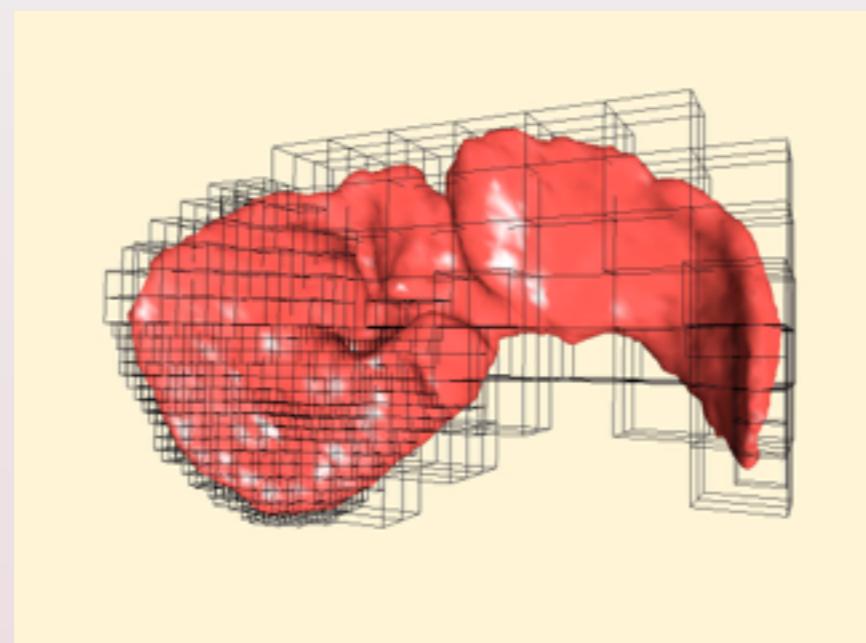
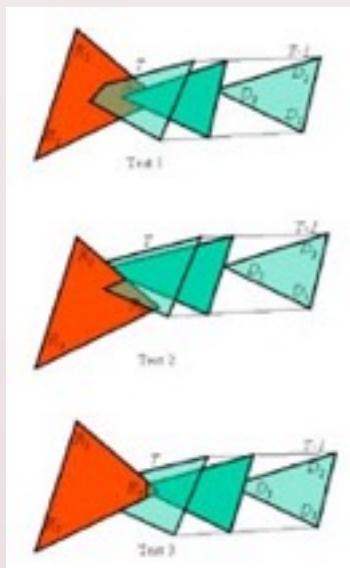
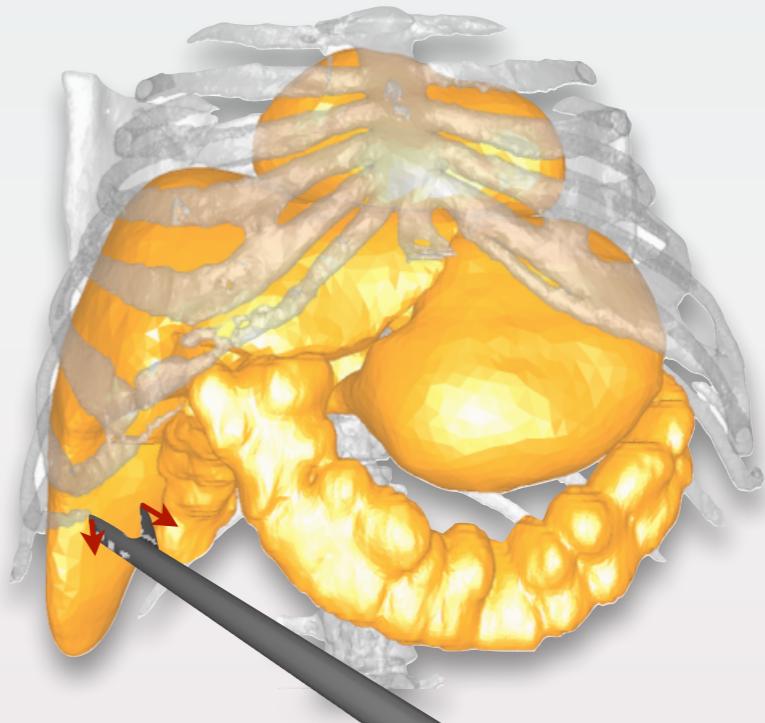
- Unconditionally stable
- Possible use of «large» time step  $\mathbf{h}$  in the simulation
- Needs the resolution of a large non-linear problem



# CONSTRAINT-BASED MODELING OF BIOMECHANICAL INTERACTIONS

# COLLISION DETECTION

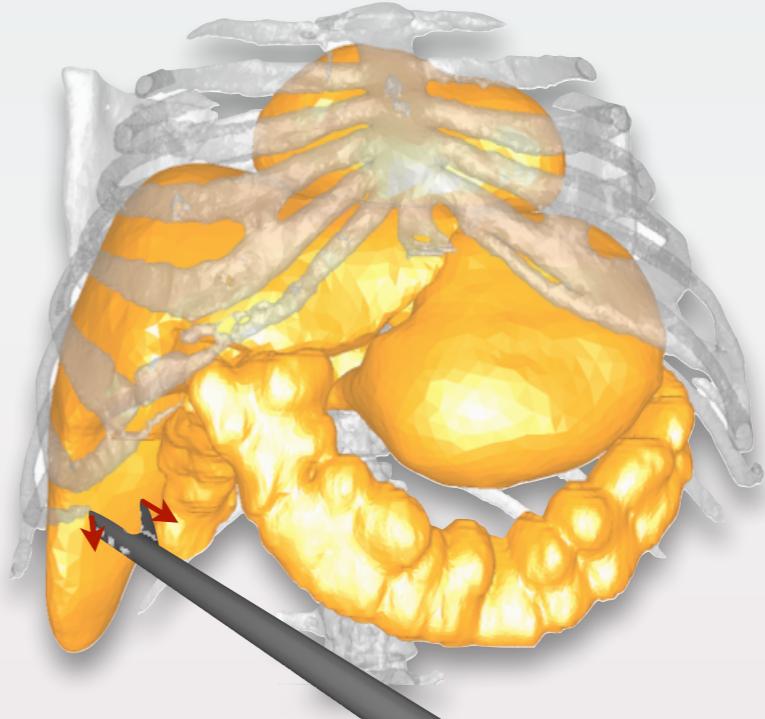
- A simple problem: find the colliding primitives of two meshes...
  - ...that requires many computation !!!
  - Various optimization:
    - Bounding Volume hierarchy
    - Spatial coherency
    - Distance maps, implicit representation...



# NON-SMOOTH (BIO)-MECHANICS IN REAL-TIME

- Why important ?
  - Boundary conditions between anatomical structures
  - Device-tissues interactions
- Why difficult ?
  - Non-smooth events
  - Multi-Contact response
    - Contact: Signorini's law (linear inequalities)
    - Friction: Coulomb's law (non-linear inequalities)
  - Many other interactions...
    - Complex anatomical and mechanical links between organs
    - Specific interactions for some devices

$$\begin{aligned}\mathbf{M}(\mathbf{v}_f - \mathbf{v}_i) &= h (\mathbb{P}(t_f) - \mathbb{F}(\mathbf{q}_f, \mathbf{v}_f)) + h\mathbf{H}^T \boldsymbol{\lambda}_f \\ \mathbf{q}_f &= \mathbf{q}_i + h\mathbf{v}_f\end{aligned}$$



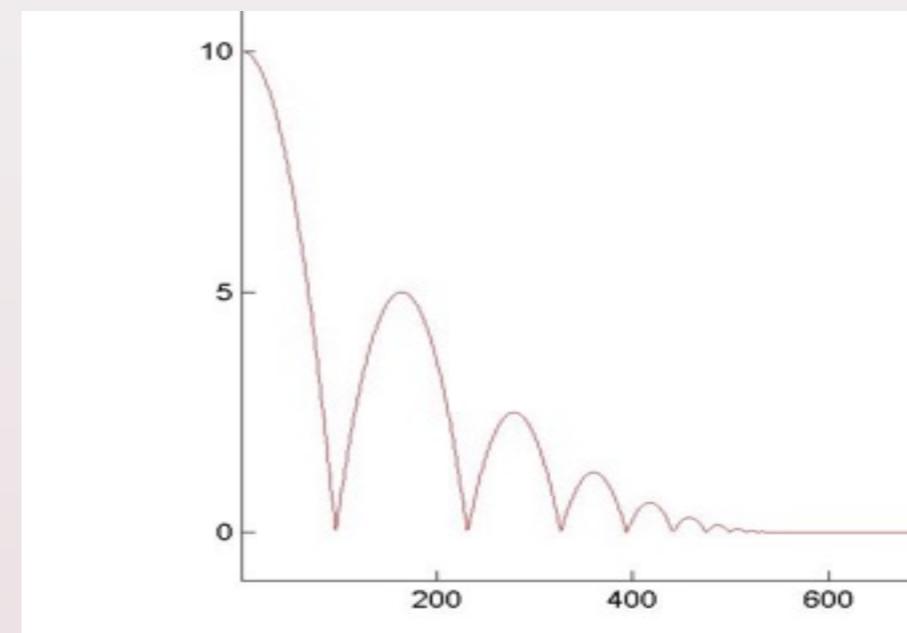
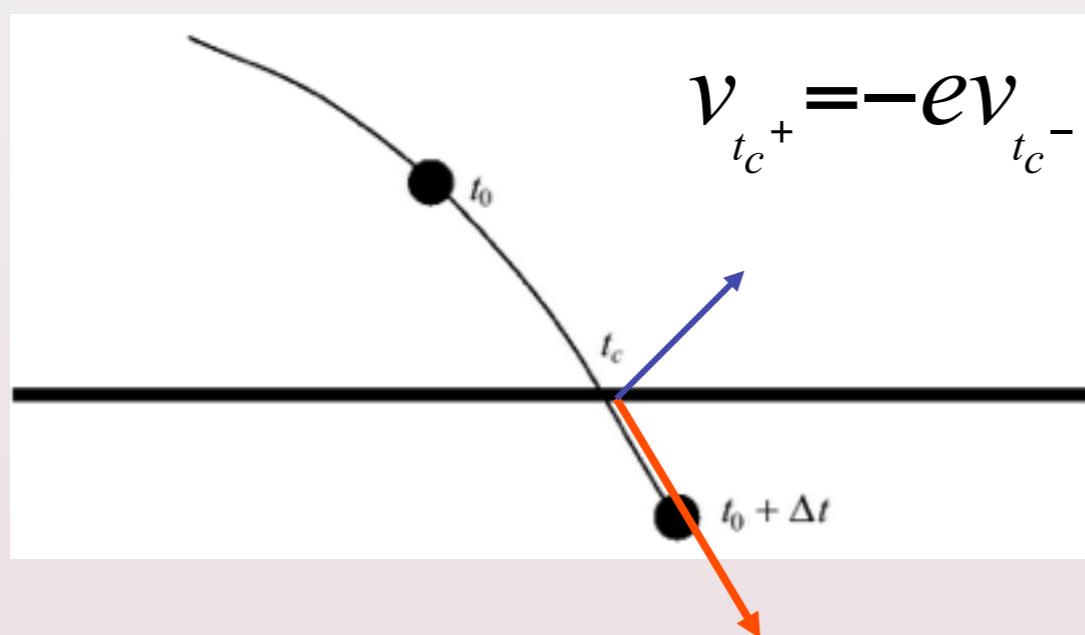
Example :  $V^- < 0$  before impact  
and  $V^+ > 0$  after impact.. between them, an very small time step

# EVENT-DRIVEN

- A chaque nouvelle collision:
  - On détermine l'instant du premier impact,
  - On arrête l'intégration en temps,
  - On résout l'impact,
  - On redémarre l'intégration en temps
- Intérêt:
  - Entre deux évènements, on respecte la continuité nécessaire aux schémas d'intégration « élevés », donc précis.
- Défaut:
  - Coûteux en résolution si on a beaucoup de contacts,
  - Rebond « infini »... on est obligé de donner un critère d'arrêt

# EVENT-DRIVEN

- Collision contre un mur
  - Temps de collision  $t_c$
  - Facteur de restitution  $e$  de Newton
  - Problème du rebond à l'infini

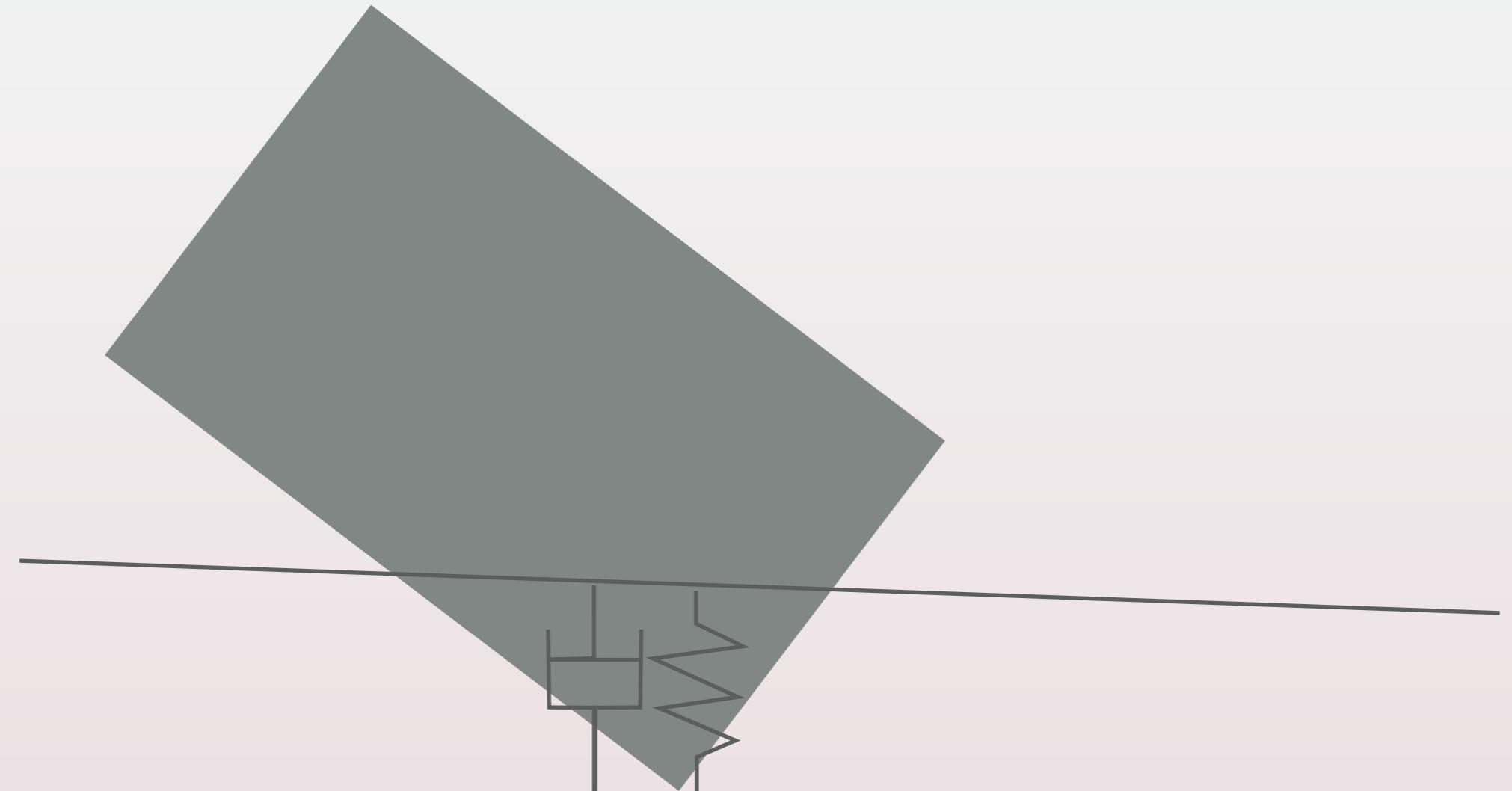


# TIME-STEPPING

- Pas de temps FIXE
  - On détecte toutes les collisions apparues durant le pas de temps,
  - On résout toutes ces collisions « en même temps »,
  - Mouvement « constraint » avec toutes les forces
- Intérêt:
  - Plus rapide si il y a beaucoup de contacts,
- Défaut :
  - Utilisation de schéma d'intégration d'ordre faible  
(Forces de contact / impact deviennent des impulsions)
  - Pas de temps d'intégration petits

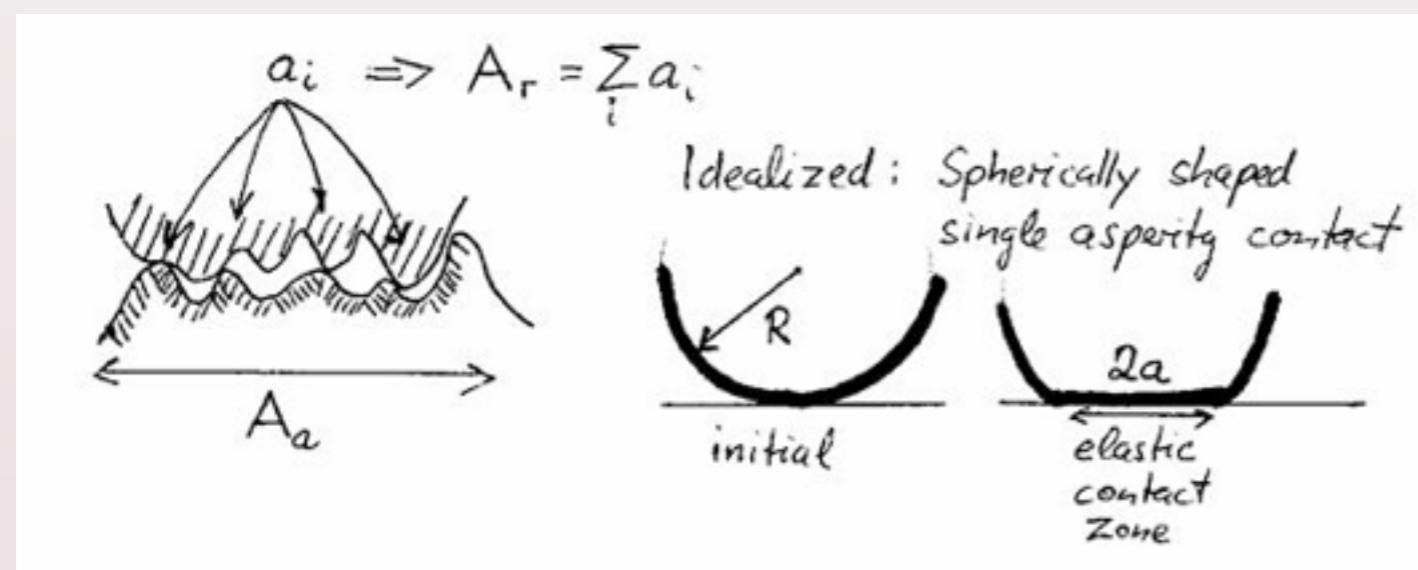
# CONTACT'S LAW

- Penalty approach
  - Collision is modeled using (damped) spring



# CONTACT'S LAW

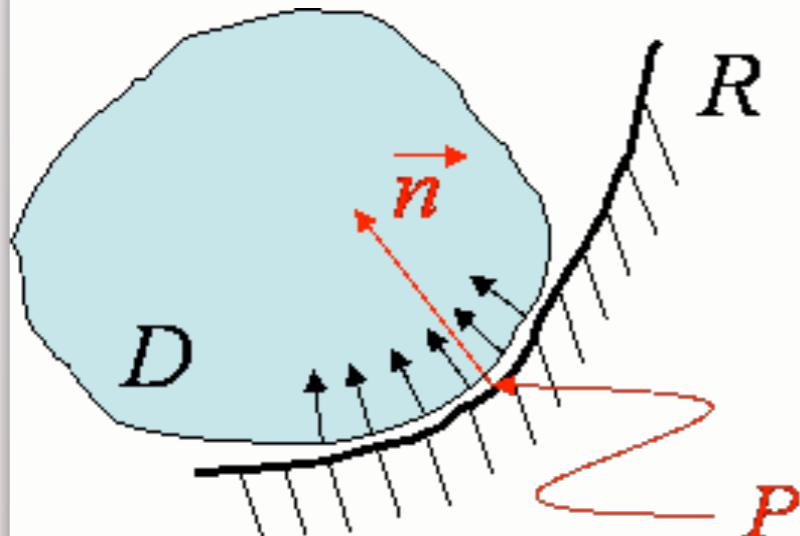
- Hertz model:
  - the strains are small and within the elastic limit,
  - each body can be considered an elastic half-space, i.e., the area of contact is much smaller than the characteristic radius of the body,
  - the surfaces are continuous and non-conforming
  - the surfaces are frictionless.
  - **analytical solutions**



$$a^3 = \frac{3PR}{4E^*}; \quad E^* = \left( \frac{1-v_1^2}{E_1} + \frac{1-v_2^2}{E_2} \right); \quad a \ll R$$

# CONTACT'S LAW

- Signorini's law
  - Complementarity
  - Contact between soft object and its environment



Non pénétration :

$$\delta_n(P) \geq 0$$

Pression à la surface :

$$\sigma_{nn}(P) \geq 0$$

Complémentarité :

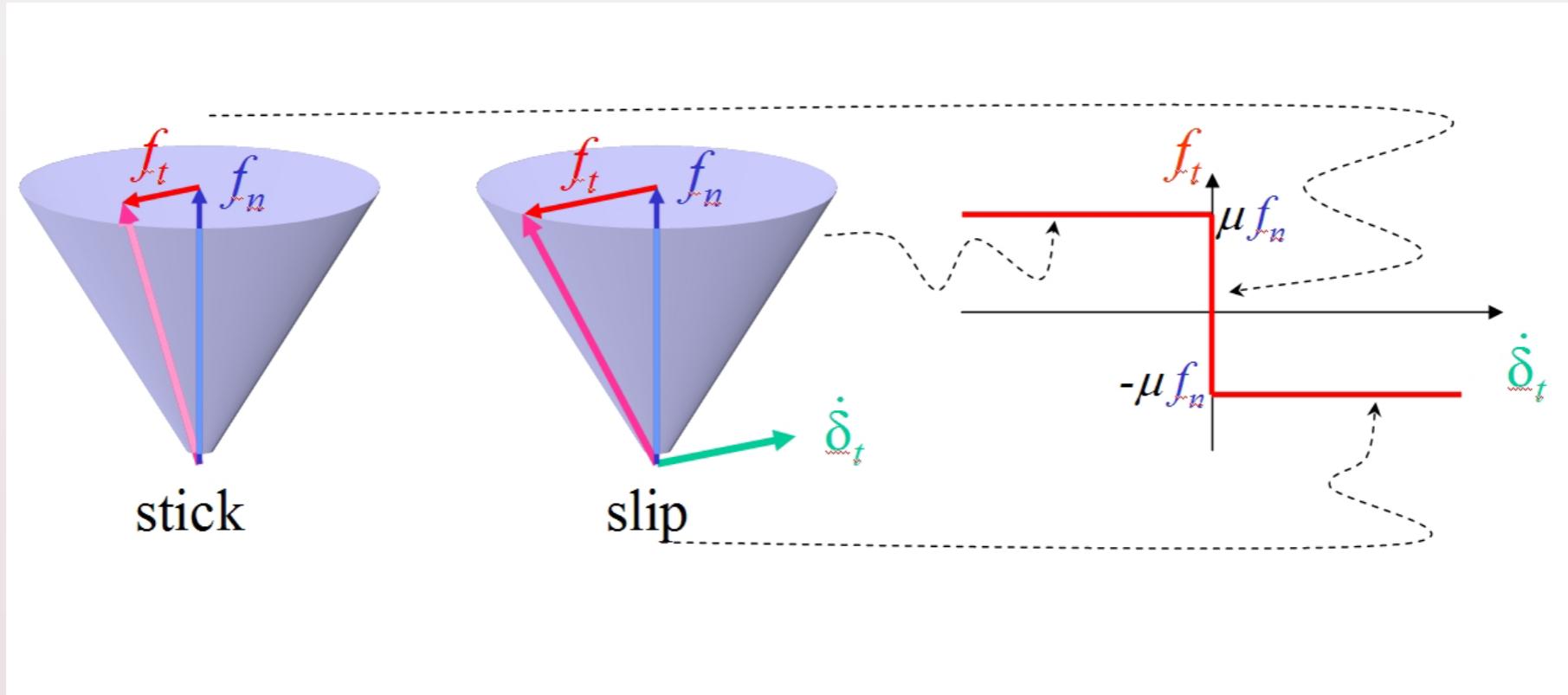
$$\delta_n(P) \perp \sigma_{nn}(P)$$

# FRICTION'S LAW

- Coulomb's law
  - Complementarity too...

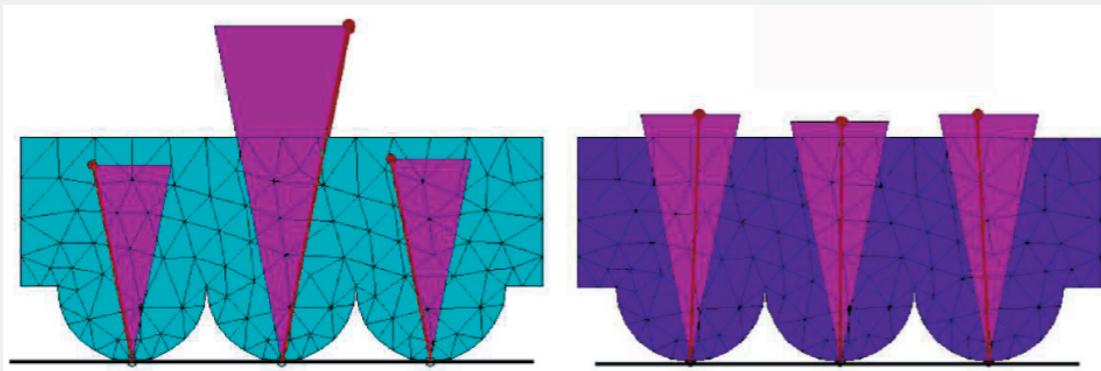
$$\dot{\delta}_{\vec{T}} = \vec{0} \Rightarrow \|f_{\vec{T}}\| < \mu \|f_{\vec{n}}\| \text{ (stick)}$$

$$\dot{\delta}_{\vec{T}} \neq \vec{0} \Rightarrow f_{\vec{T}} = -\mu \|f_{\vec{n}}\| \frac{\dot{\delta}_{\vec{T}}}{\|\dot{\delta}_{\vec{T}}\|} = -\mu \|f_{\vec{n}}\| \vec{T} \text{ (slip)}$$



# CHALLENGES...

- Non-unique solution (mainly with rigid objects)



- Non-linearity

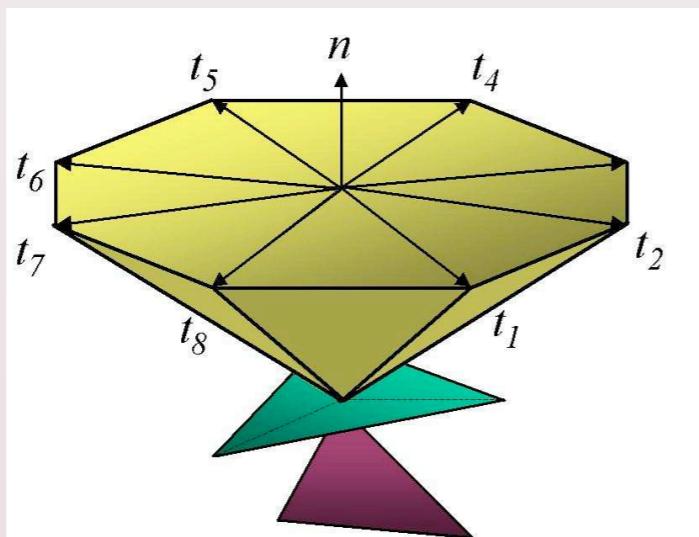
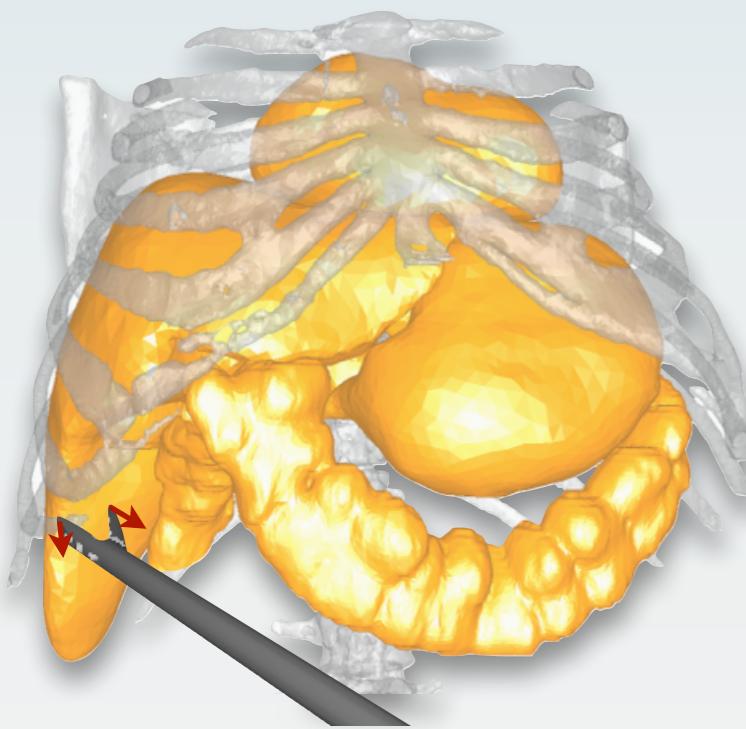


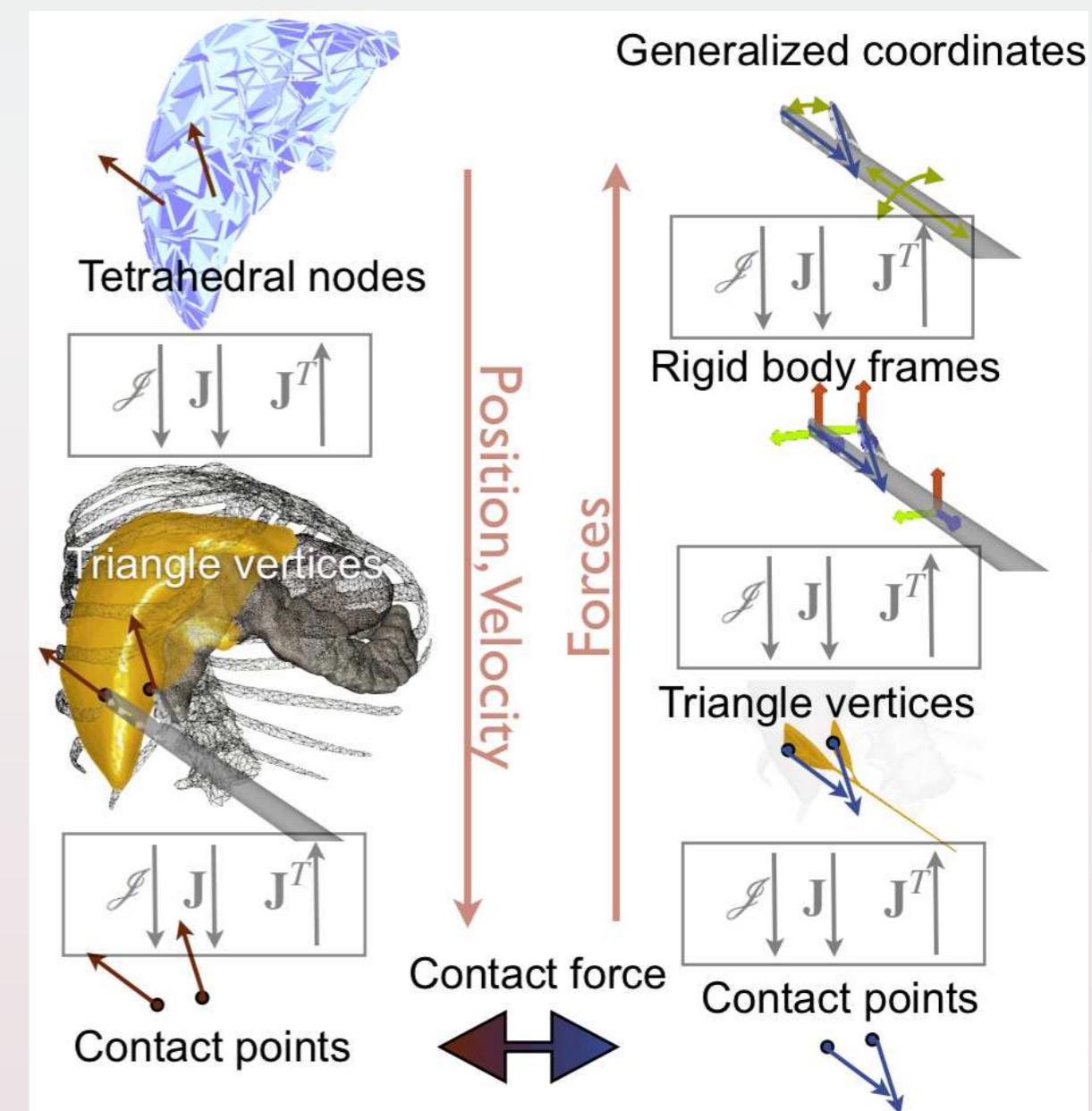
FIG. 2.27 – Cône à  $k = 8$  faces



# «CONTACT MAPPING»

- How to build matrix  $\mathbf{H}^T$  ?
  - Direction of the contact  $\mathfrak{F}_\alpha = [\mathbf{n}_\alpha, \mathbf{t}_\alpha, \mathbf{s}_\alpha]$ .
  - Link between constraint motion and DOFs
$$\boldsymbol{\delta}_\alpha = \mathbb{A}_\alpha(\mathbf{q}_1, t) - \mathbb{A}_\alpha(\mathbf{q}_2, t)$$
- Derivation
$$\mathbb{H}_\alpha(\mathbf{q}) = \frac{\partial \mathbb{A}_\alpha}{\partial \mathbf{q}}$$

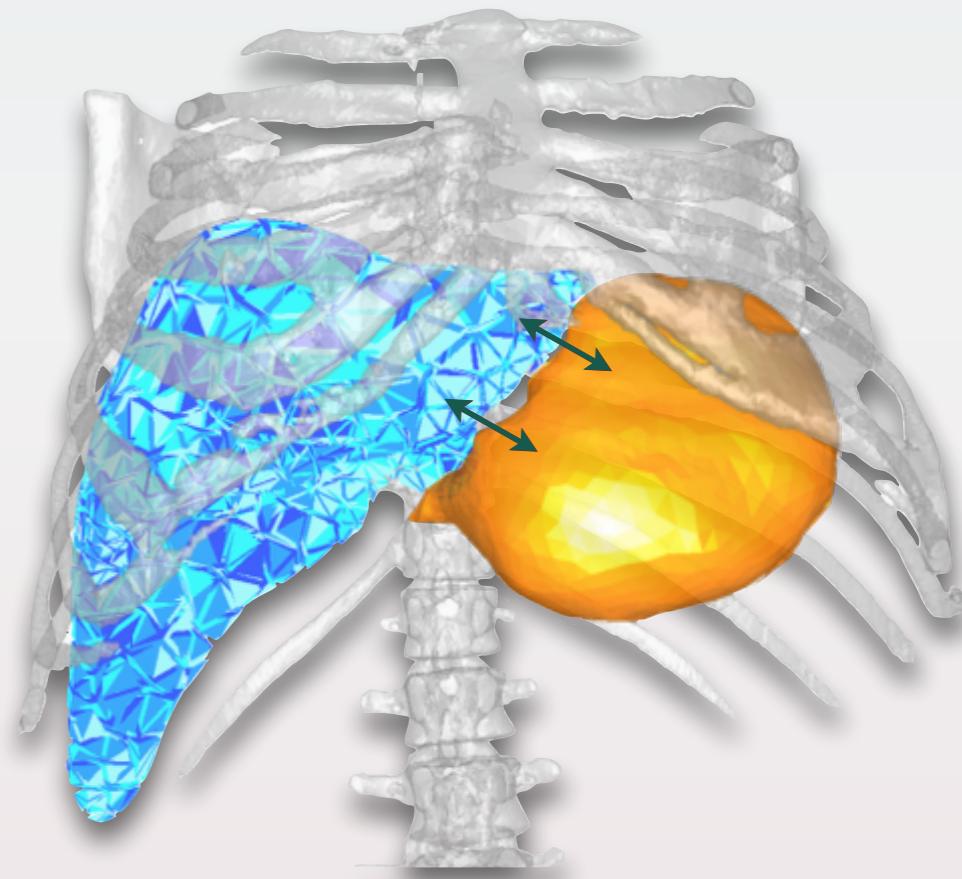
$$\dot{\boldsymbol{\delta}}_\alpha(t) = \mathbb{H}_\alpha(\mathbf{q}_1)\mathbf{v}_1(t) - \mathbb{H}_\alpha(\mathbf{q}_2)\mathbf{v}_2(t)$$
- Virtual work principle
  - Force =  $\mathbb{H}(\mathbf{q}_i)^T \boldsymbol{\lambda}_f$



# INTERACTION BETWEEN TWO DEFORMABLE MODELS

- 2 system of equations  $A x = b$  for each object
- «Direct approach»
  - Penalty forces: additional stiffness in the system
  - Lagrange Multipliers: very large system of (in)-equations

$$\begin{bmatrix} A & H \\ -H^T & \lambda \geq -\delta \end{bmatrix} \begin{bmatrix} x \\ \lambda \end{bmatrix} = \begin{bmatrix} b \\ b \end{bmatrix}$$



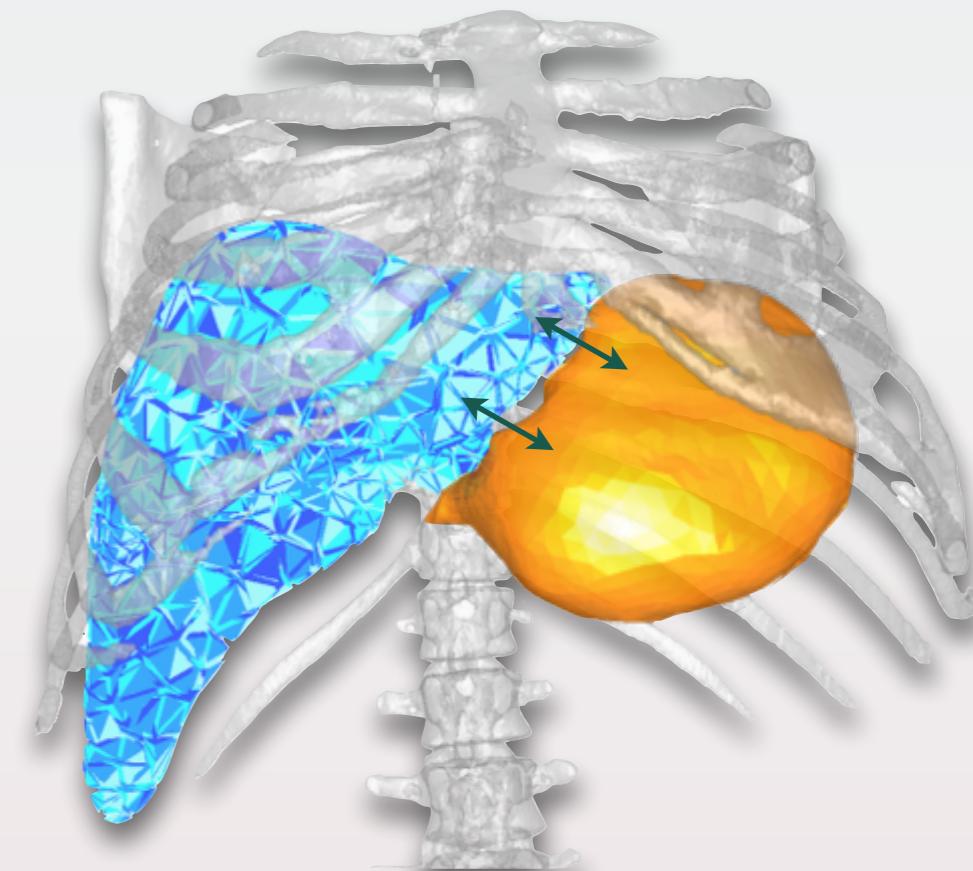
QP approach

# INTERACTION BETWEEN TWO DEFORMABLE MODELS

- Indirect approach
  - Free Motion
  - Constraint setting
  - Constraint solving
  - Constraint correction:  
 $x = x^{\text{free}} + Dx$

$$\begin{bmatrix} A \\ H^T \end{bmatrix} \begin{bmatrix} \delta^{\text{free}} \\ b \end{bmatrix} = \begin{bmatrix} \lambda \\ H^T \end{bmatrix}$$

$$\begin{bmatrix} A \\ H^T \end{bmatrix} \begin{bmatrix} \delta^{\text{free}} \\ b \end{bmatrix} = \begin{bmatrix} \lambda \\ H^T \end{bmatrix}$$



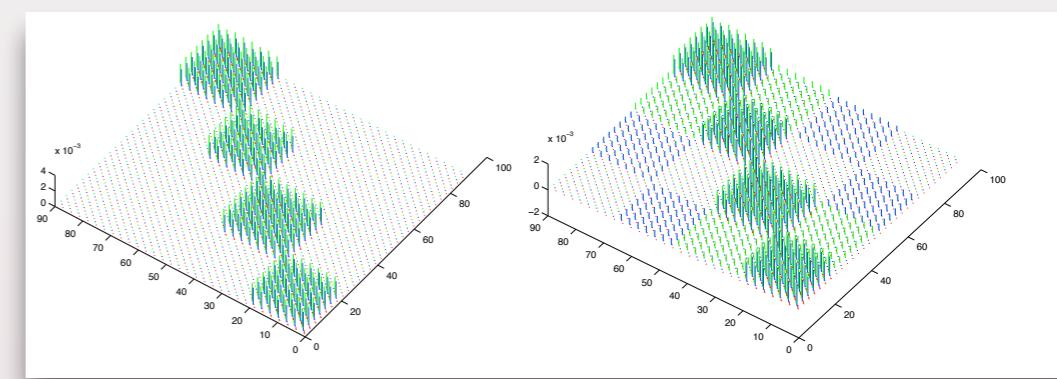
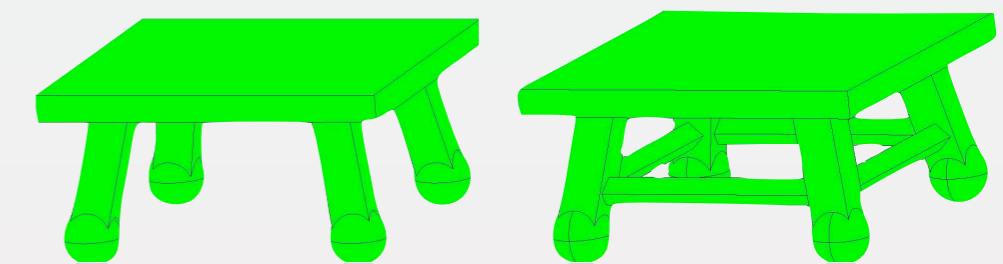
$$0 \leq \delta^{\text{free}} + \begin{bmatrix} -I \\ W \end{bmatrix} + \begin{bmatrix} -I \\ W \end{bmatrix} \geq 0$$

[ Compliance in constraint space ]

(N)LCP approach

# (N)LCP APPROACH

- Build and solve (N)LCP
  - Direct solvers (Lemke) vs. iterative (Gauss-Seidel)
  - Inputs:  $W$ ,  $\delta^{\text{free}}$  (and constraints law), Output:  $\lambda$
- What represents  $W$ ?
  - Mechanical coupling between constraints
  - Footstool example
- How to compute  $W = H A^{-1} H^T$  for non-linear models?
  - Linear model:  $A^{-1}$  can be precomputed
  - $A$  is changing so computing  $A^{-1}$  in real-time is challenging!



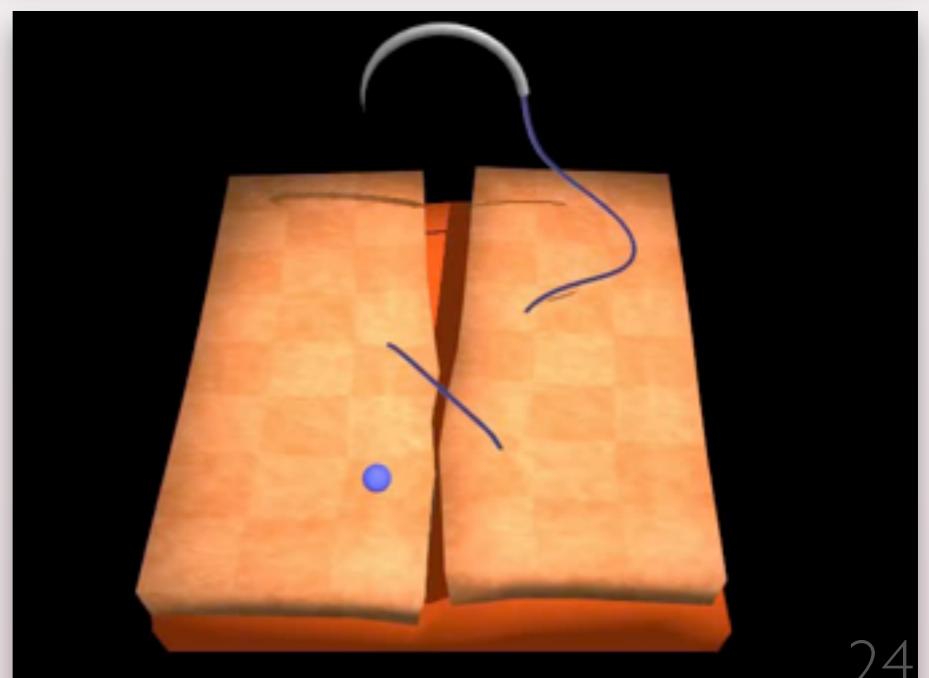
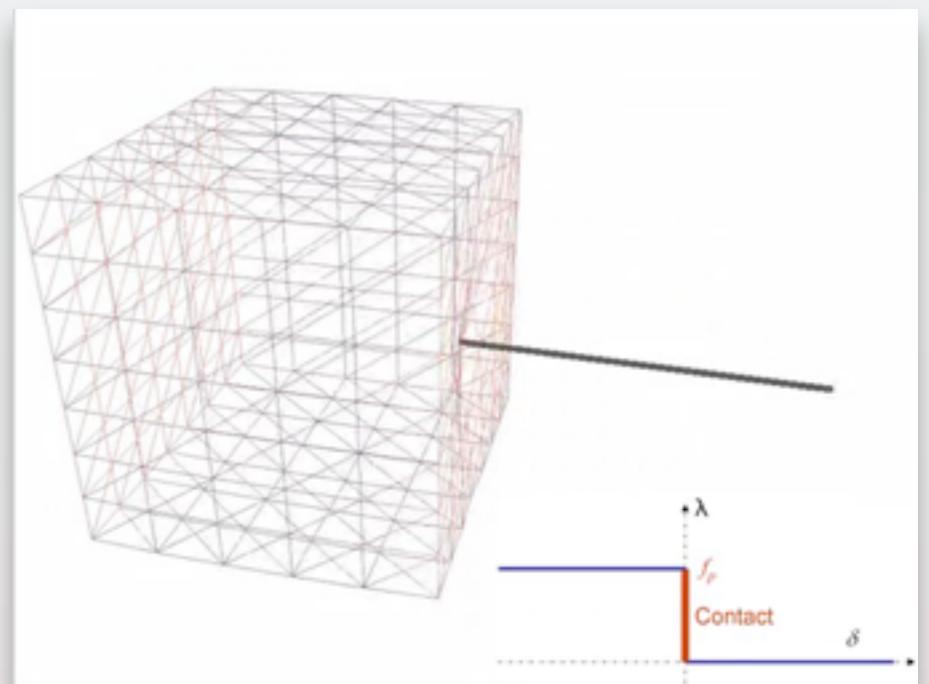
# (N)LCP APPROACH

- Solve (N)LCP
  - Inputs:  $\mathbf{W}$ ,  $\boldsymbol{\delta}^{\text{free}}$  (and constraints law), Output:  $\boldsymbol{\lambda}$
  - Direct solvers
    - pivoting method: Lemke (see Siconos Library)
    - LCP  $\Leftrightarrow$  QP and use of QP solver algorithms
  - Iterative (block-Gauss-Seidel)
    - Block contact+friction
    - Iterative solver (slow convergence but it works well !)

$$\underbrace{\delta_\alpha - \mathbf{W}_{\alpha\alpha} \lambda_\alpha}_{\text{unknown}} = \underbrace{\sum_{\beta=1}^{\alpha-1} \mathbf{W}_{\alpha\beta} \lambda_\beta + \sum_{\beta=\alpha+1}^m \mathbf{W}_{\alpha\beta} \lambda_\beta}_{\text{frozen}} + \delta_\alpha^{\text{free}}$$

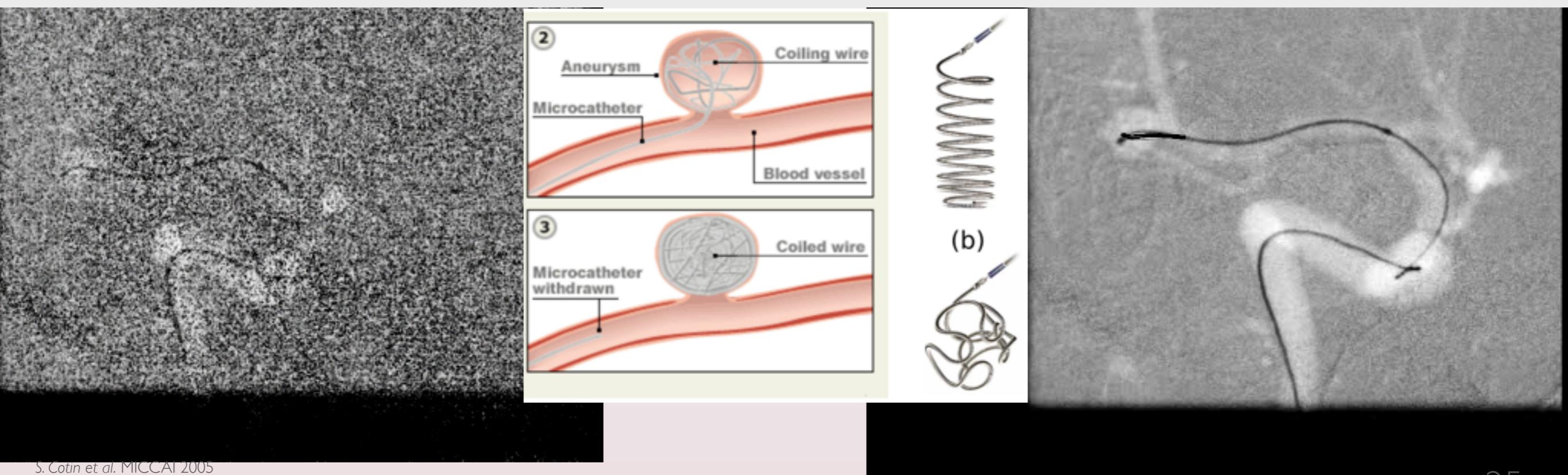
# CONSTRAINT-BASED NEEDLE-INSERTION MODEL

- Many surgical techniques involve needle insertion (biopsy, brachytherapy, ...)
  - These needles are rigid or flexible
  - Different constraint laws for puncture, cutting, friction... etc...
  - Results validated by comparing with experiments of the literature
- Suturing simulation
  - The beam model can be used for the whole suture (including the needle)
  - Constraint based approach to simulate the suturing
  - Work in progress with DigitalTrainers
- NLCP Generic solver for all type of mechanical interactions



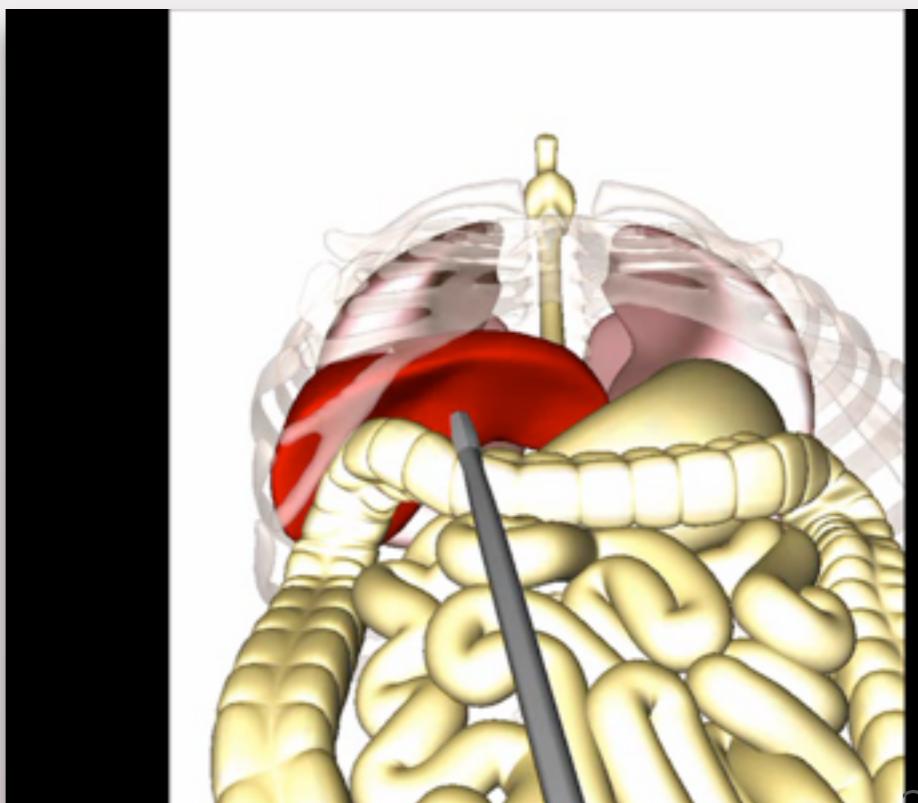
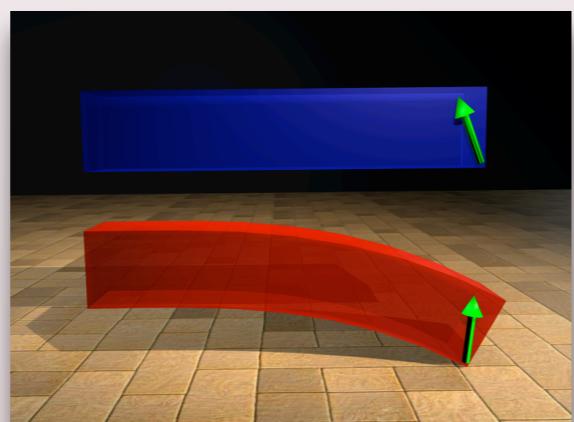
# COMPLIANCE FOR WIRE-LIKE STRUCTURES

- $\mathbf{A}$  is a block tri-diagonal matrix...
  - Order the contact along the curvilinear abscissa
  - Gauss-Seidel NLCP solver using unbuilt matrix  $\mathbf{H} \mathbf{A}^{-1} \mathbf{H}^T$ :
  - Interactive simulation of more than 200 beams with hundreds of contacts
  - Frictional contact between coil and vessel wall



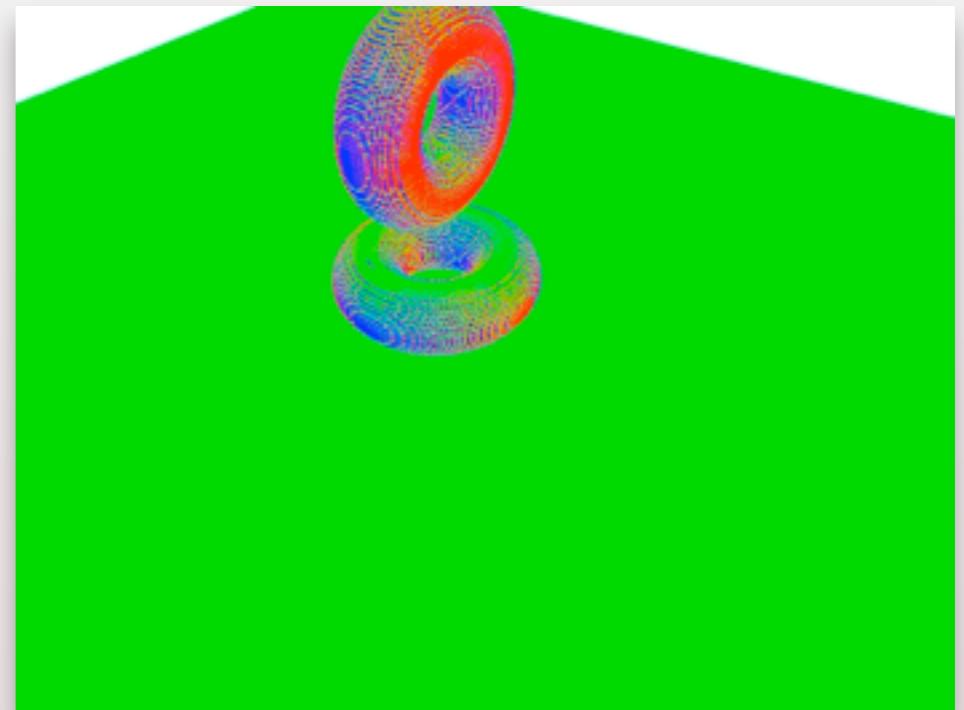
# COMPLIANCE WARPING

- Computation of  $W=H A^{-1} H^T$  on a volume deformable object ?
  - In general, too long for real-time
  - The main role of  $W$  is to get the mechanical coupling between contacts.
- Could we «precompute»  $A^{-1}$ ?
  - No... as we are using non-linear model,  $A$  is changing
  - Yes... but it is the approximation that the compliance is only «rotated» by deformation:  $A^{-1} \sim R A_0^{-1} R^T$



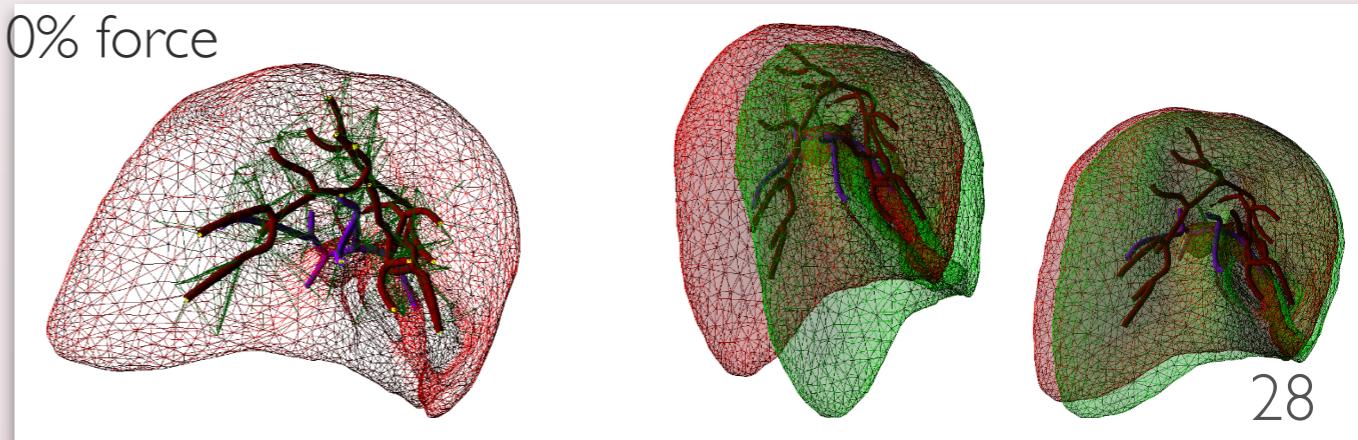
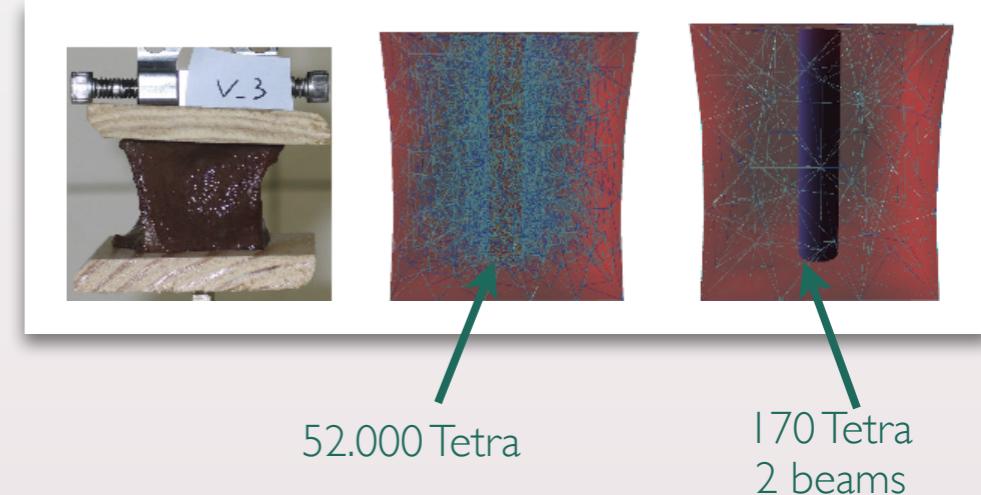
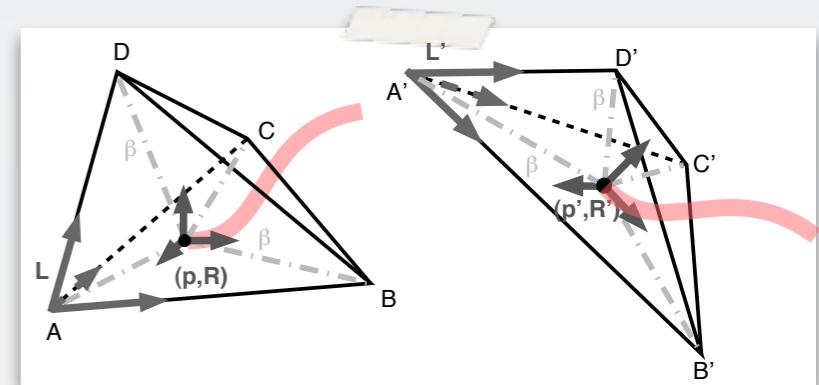
# VOLUME CONTACT MODEL AT ARBITRARY RESOLUTION

- **Goal: reduce the size of  $W$  using less contact constraints**
- Volume of Interpenetration instead of distance
- Algorithm
  - Use GPU to render the simulation scene along 3 directions
  - This generates a volumetric image
  - From this image we identify the intersection volumes
  - These volumes are used to compute the collision response (forces)
- Independent from the mesh resolution
- No additional cost to detect self-collisions



# VASCULARIZED ORGAN MODEL

- Mechanical coupling between vessel and parenchyma
  - Corotational frame inside tetra elements
    - Coupled with the beam nodes (displacements & internal forces)
  - *In vivo* measurement of vascularized sample response
    - Significant difference of stiffness with and without the vessel
    - Try to reproduce this difference numerically
  - Numerical Simulation of Vascularized Tissue
    - Numerical validation of the coupling (err <10% force response)



# PRÉCONDITIONNEUR ASYNCHRONE

Calcul temps-réel de modèles FEM hétérogènes et de la compliance des contraintes

Problématique:

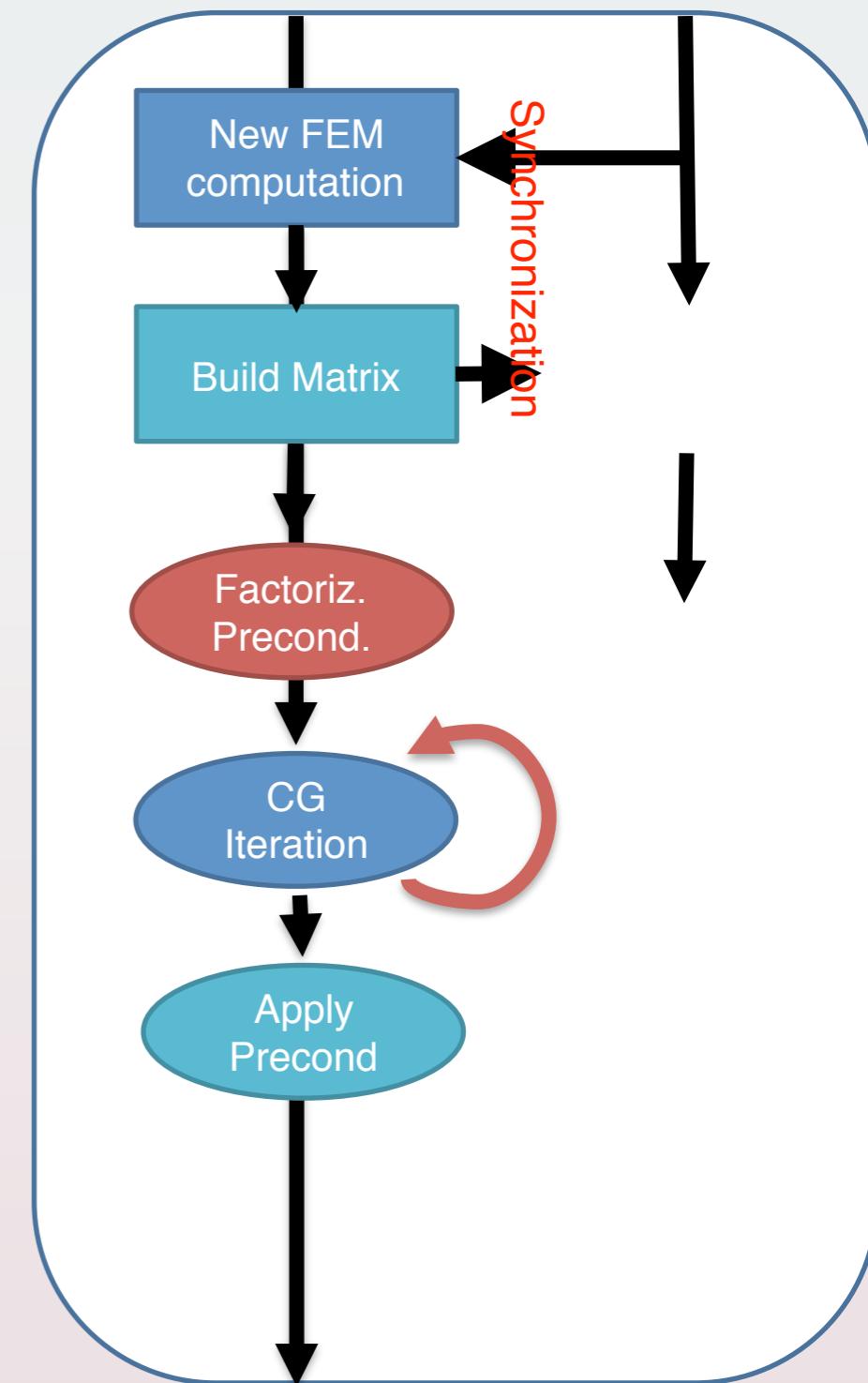
- Grandes déformations = Modèles FEM non-linéaires
  - Linéarisation à chaque pas de la simulation
  - Un système  $\mathbf{Ax} = \mathbf{b}$  à résoudre
  - Matrice  $\mathbf{A}$  de grande taille mais creuse
- Hétérogénéités = Systèmes matriciels mal conditionnés
  - Mauvaise convergence algorithmes itératifs
  - Non compatible avec temps-réel

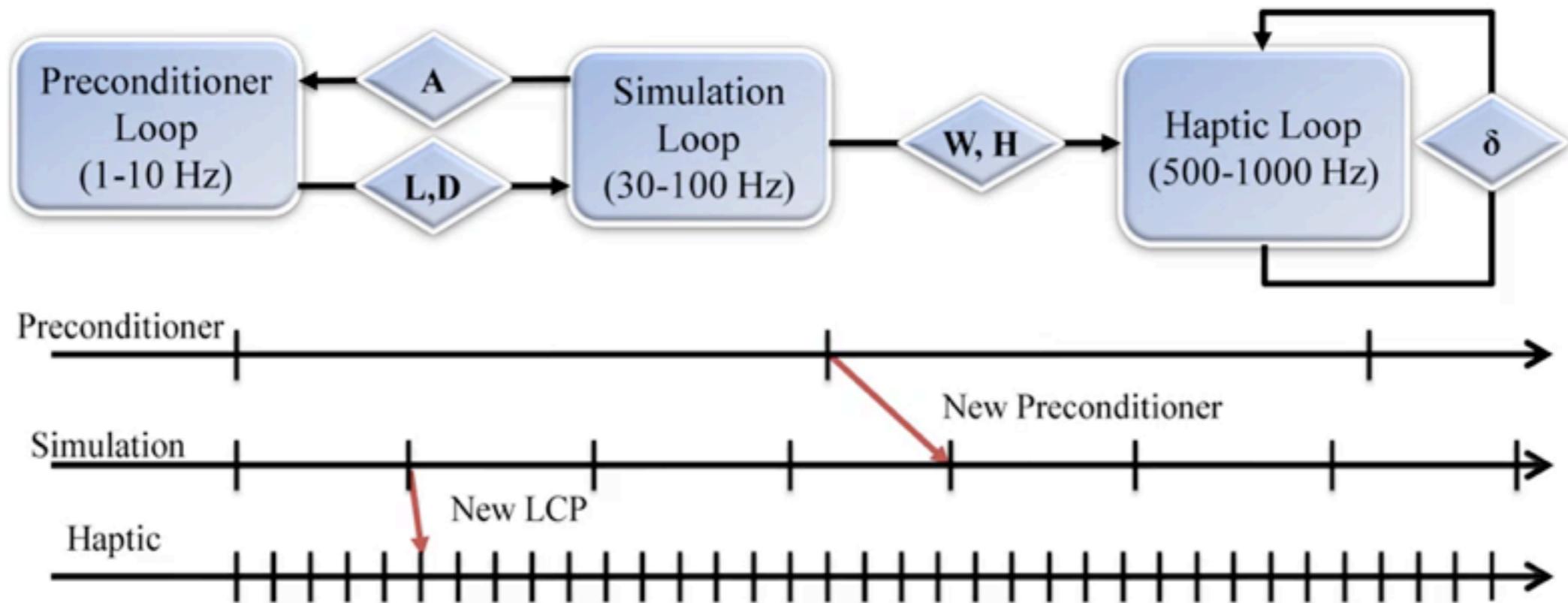
préconditionneur:

$$\underbrace{\mathbf{P}^{-1}\mathbf{A}}_{\approx \mathbf{I}} \mathbf{x} = \mathbf{B}^{-1}$$

Motivations pour le préconditionneur asynchrone:

- Cohérence temporelle de la valeur de  $\mathbf{A}$
- Factorisation d'une valeur «ancienne» de  $\mathbf{A}$  pour  $\mathbf{P}$
- Le coût de la factorisation de  $\mathbf{P}$  est déporté





- The MJED method is used to simulate hyperelastic material in real time (30Hz) with an implicit time integration.
- An asynchronous preconditioner is updated at low rates (10 Hz) to provide an evaluation of the compliance matrix necessary to solve contacts.
- A local contact problem is updated and solved at high rates (1KHz) to provide realistic Haptic Feedback.

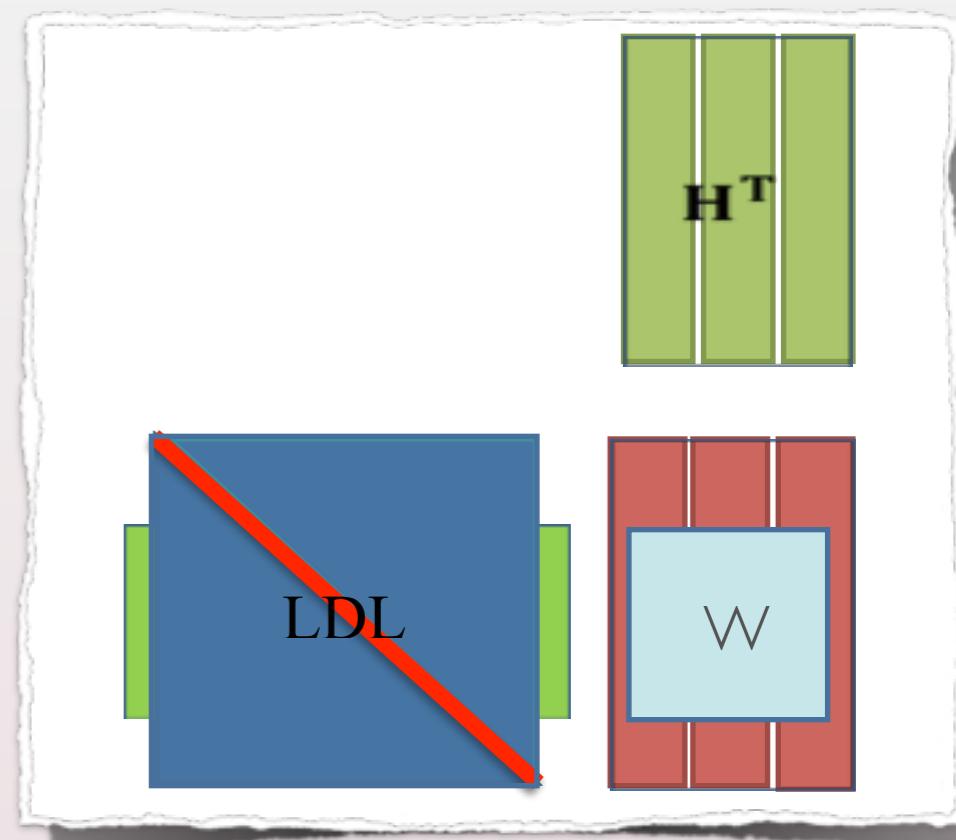
# PRÉCONDITIONNEUR ASYNCHRONE

Calcul temps-réel de modèles FEM hétérogènes et de la compliance des contraintes

On utilise le préconditionneur asynchrone pour approximer la matrice inverse:

$$W \approx H A L D L^T H^T$$

1. Comme on a un très bon préconditionneur, on a une très bonne approximation de la matrice du LCP
2. Préconditionneur appliqué sur chaque colonne de  $H^T$   
On obtient:  $S = (LDL)^{-1}H^T$
3. Matrice de compliance par multiplication  $H S$   
On obtient:  $W = H (LDL)^{-1}H^T$



# PRÉCONDITIONNEUR ASYNCHRONE

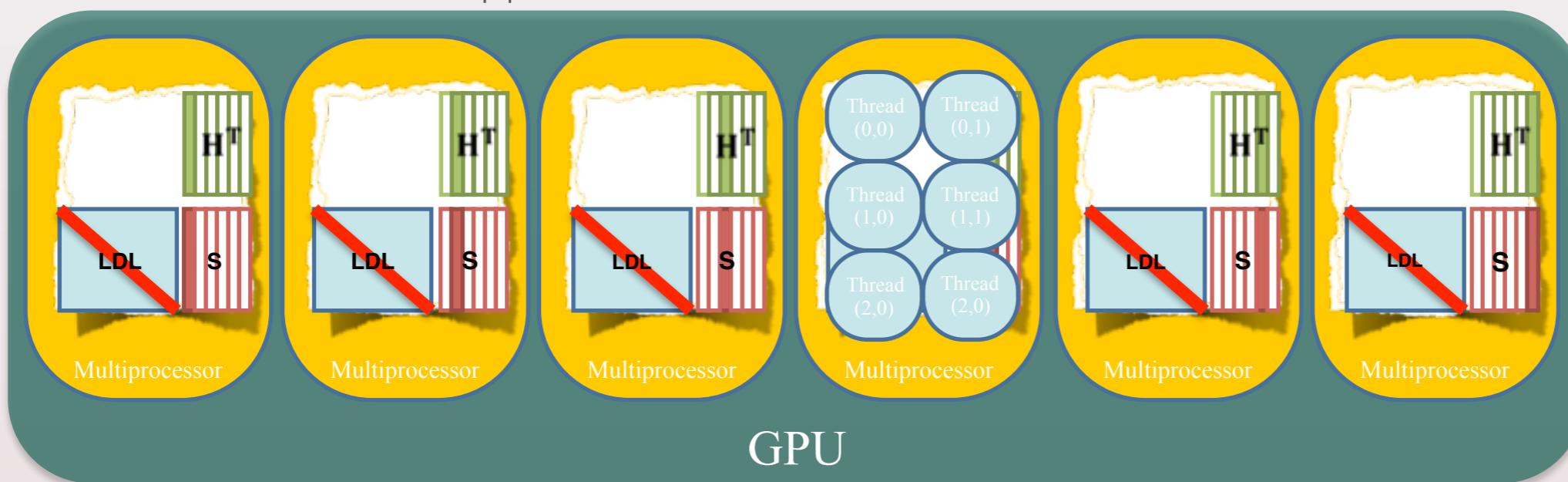
Calcul temps-réel de modèles FEM hétérogènes et de la compliance des contraintes

On utilise le préconditionneur asynchrone pour approximer la matrice inverse:

$$\mathbf{W} \approx \mathbf{H} \mathbf{A} \mathbf{L} \mathbf{D} \mathbf{L}^T \mathbf{H}^T$$

Parallélisation:

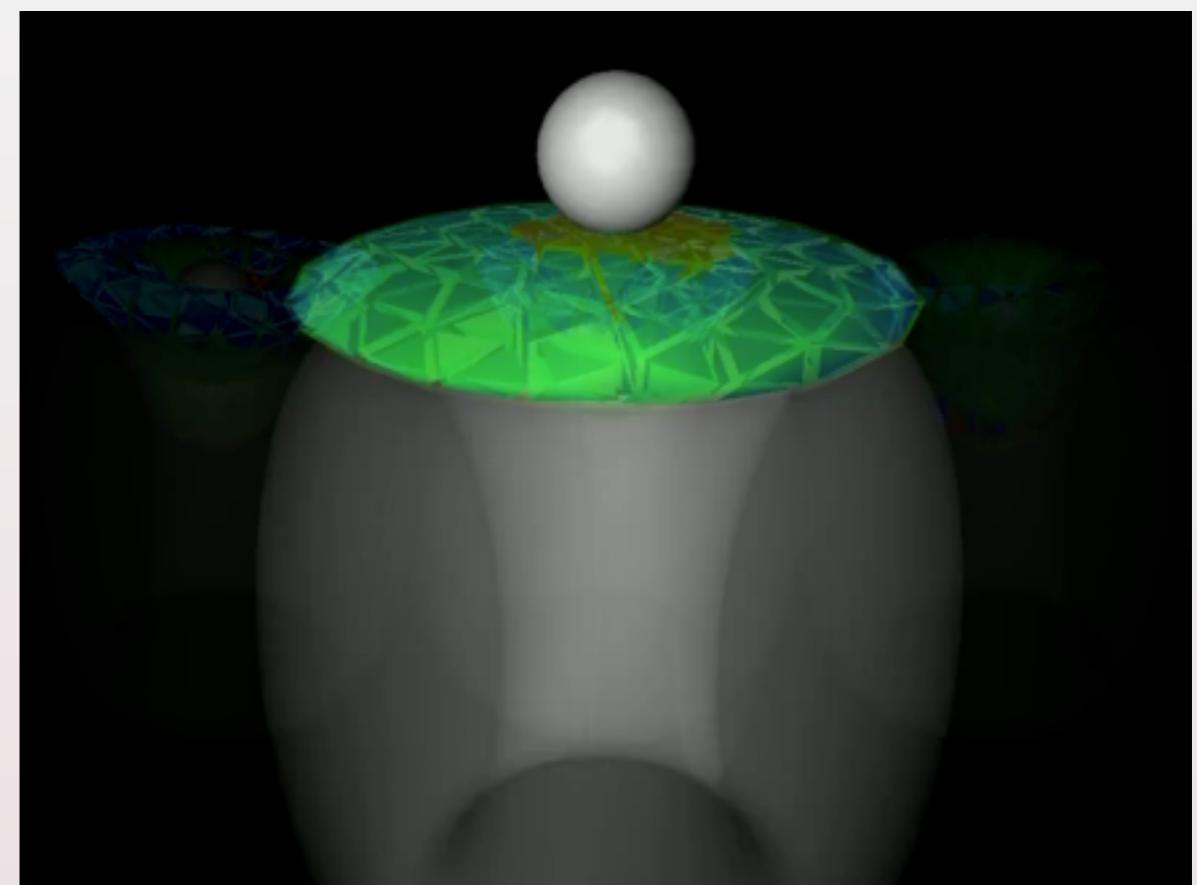
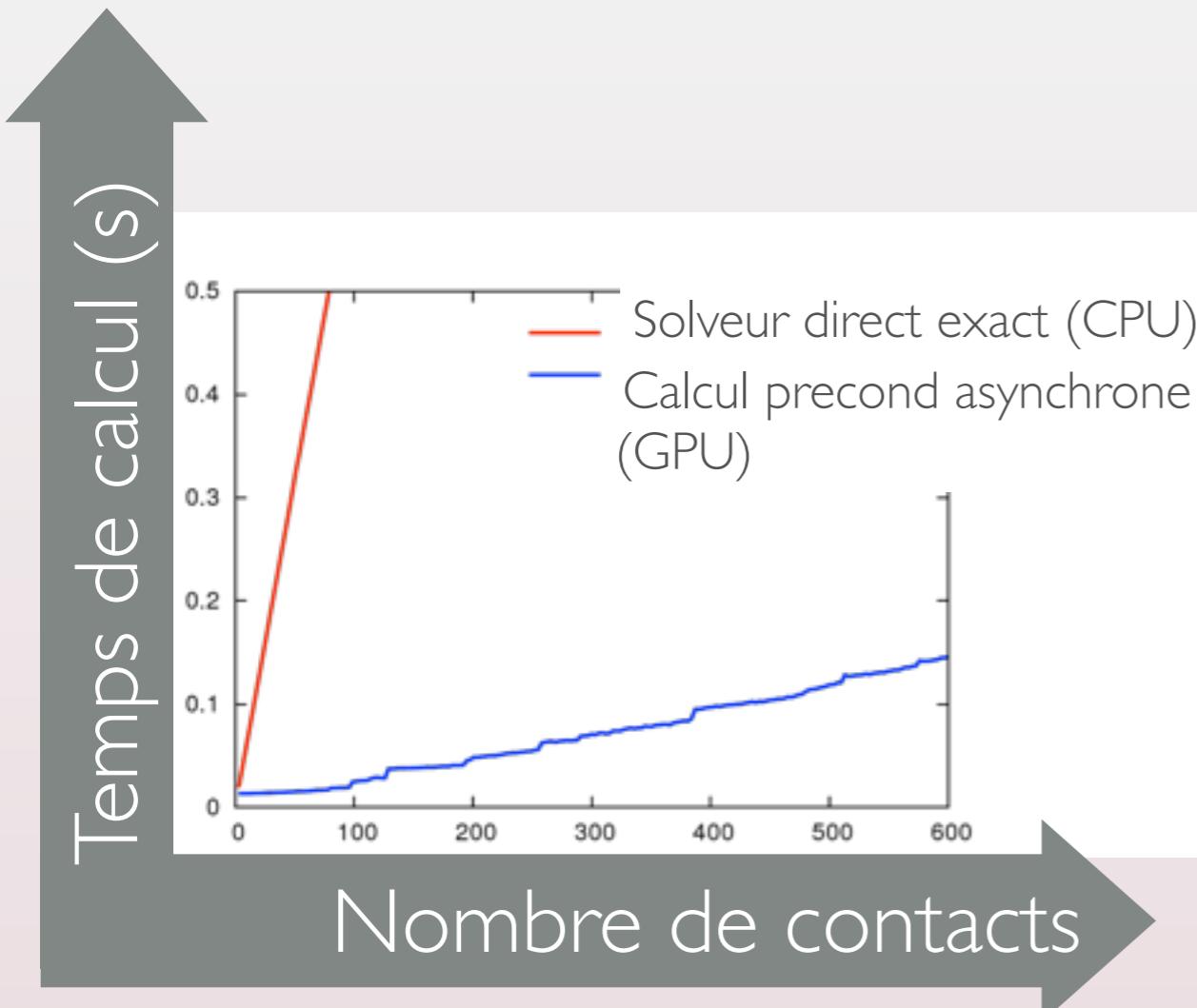
- Premier niveau: Résolution séparée pour chaque contrainte
- Deuxième niveau: Application de la factorisation LDL



# PRÉCONDITIONNEUR ASYNCHRONE

Calcul temps-réel de modèles FEM hétérogènes et de la compliance des contraintes

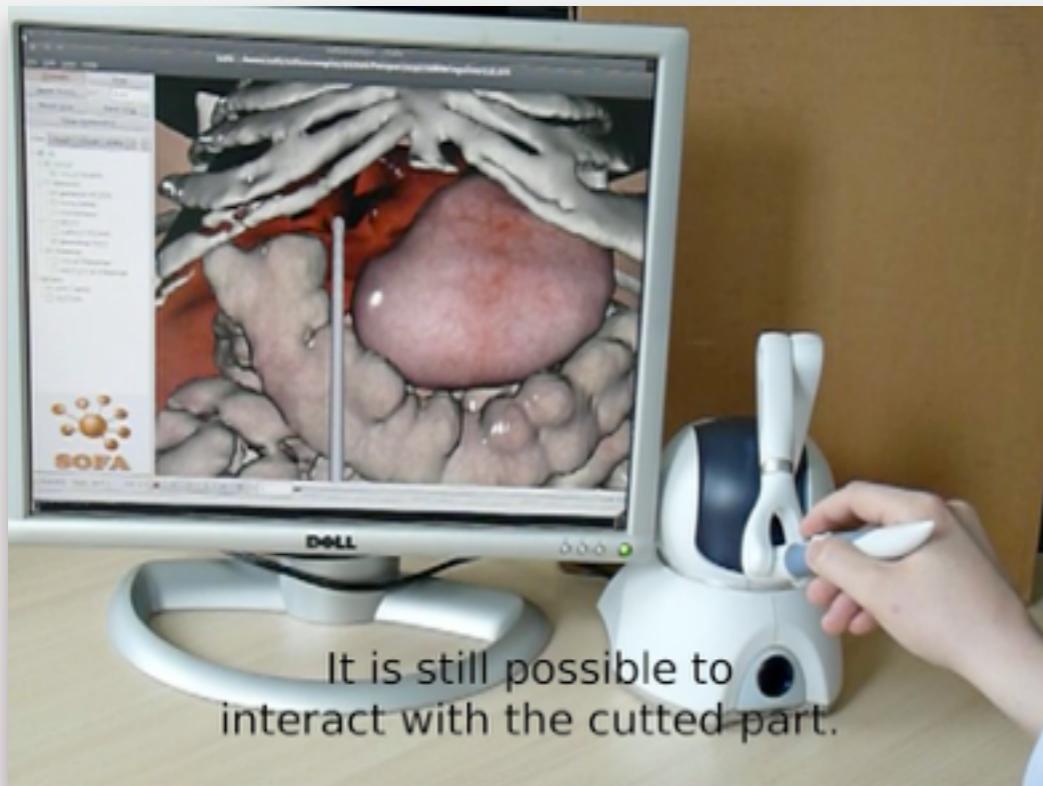
- Contacts sur des objets avec propriétés mécaniques hétérogènes
- Validation par comparaison avec la solution exacte
- Temps de calcul très réduit par rapport au calcul exact sur CPU



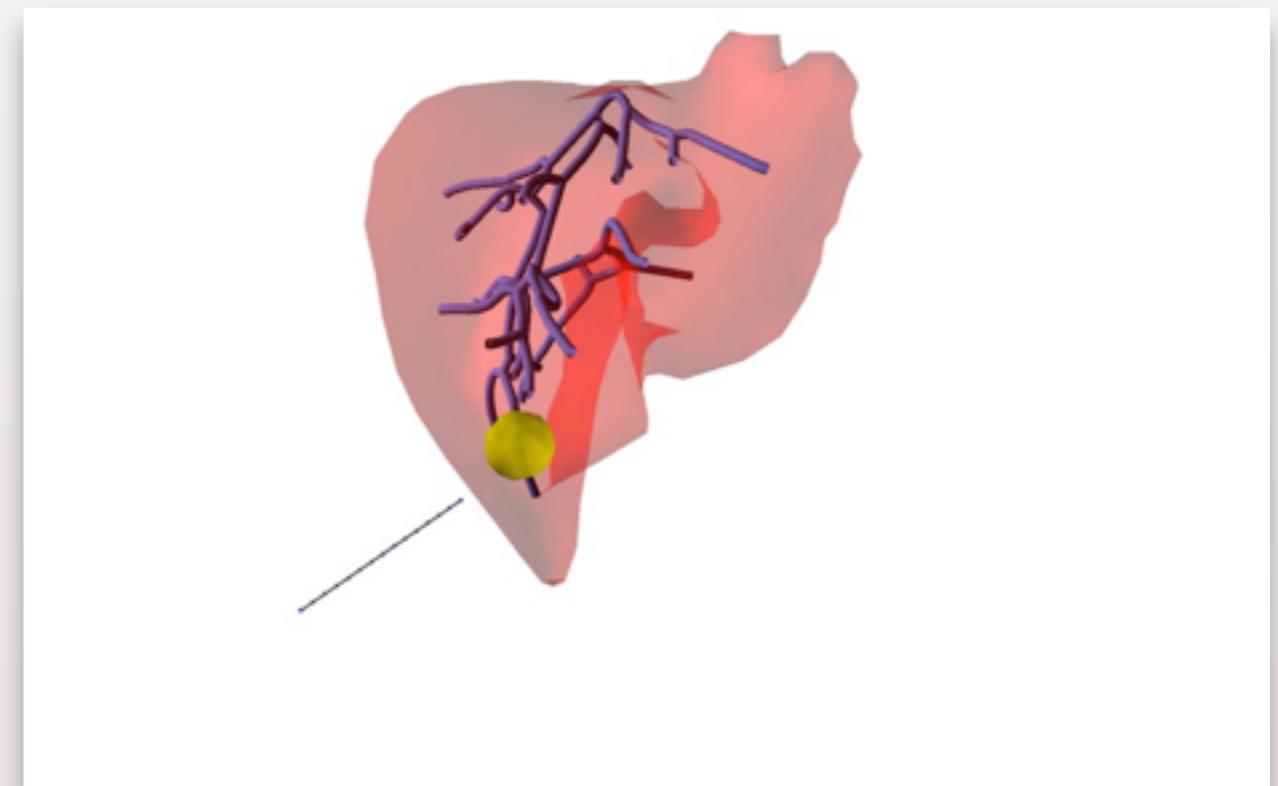
Vert: solution exacte  
Bleu/rouge: notre méthode

# LIVER SIMULATION

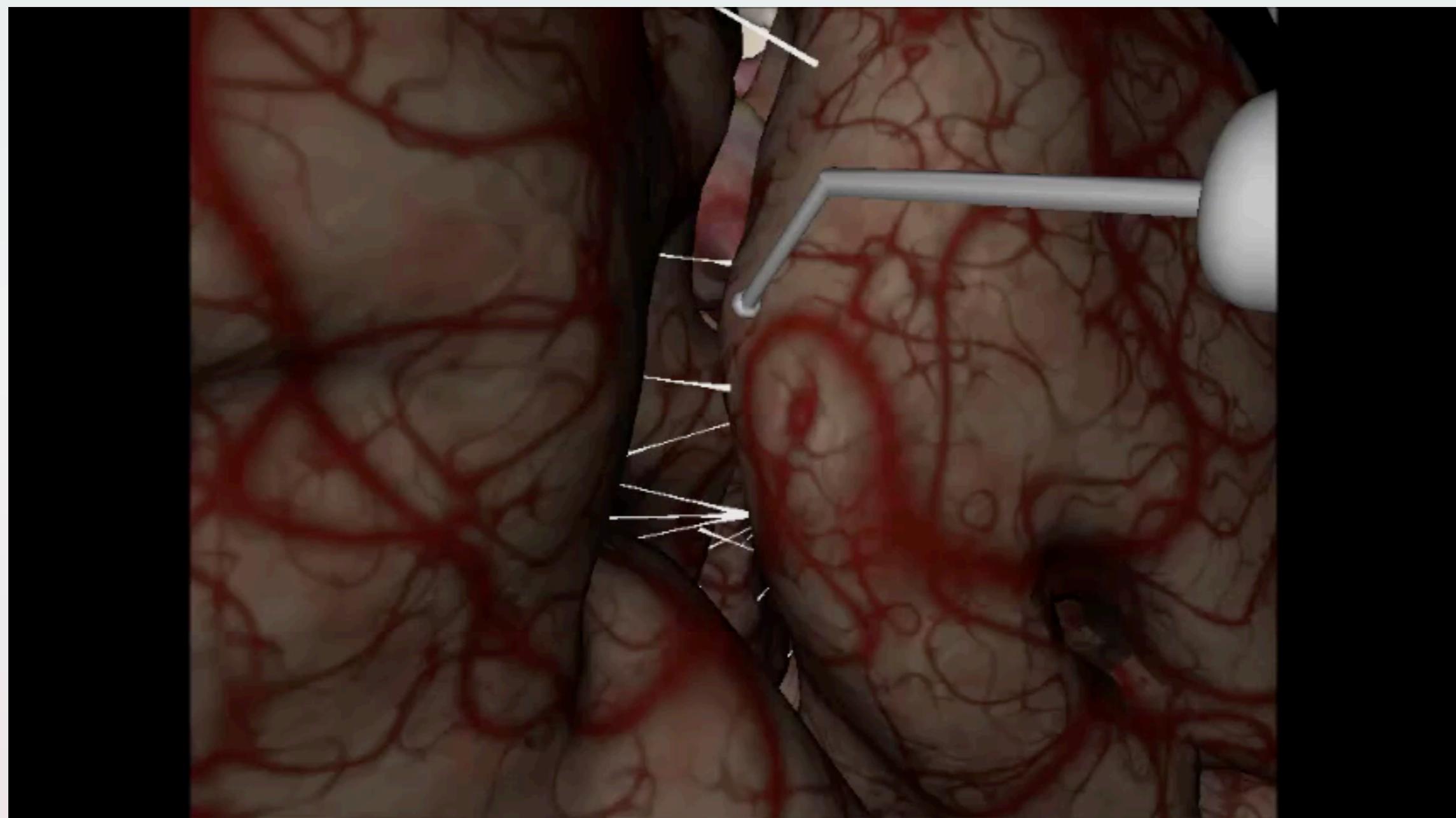
All these method can be combined...

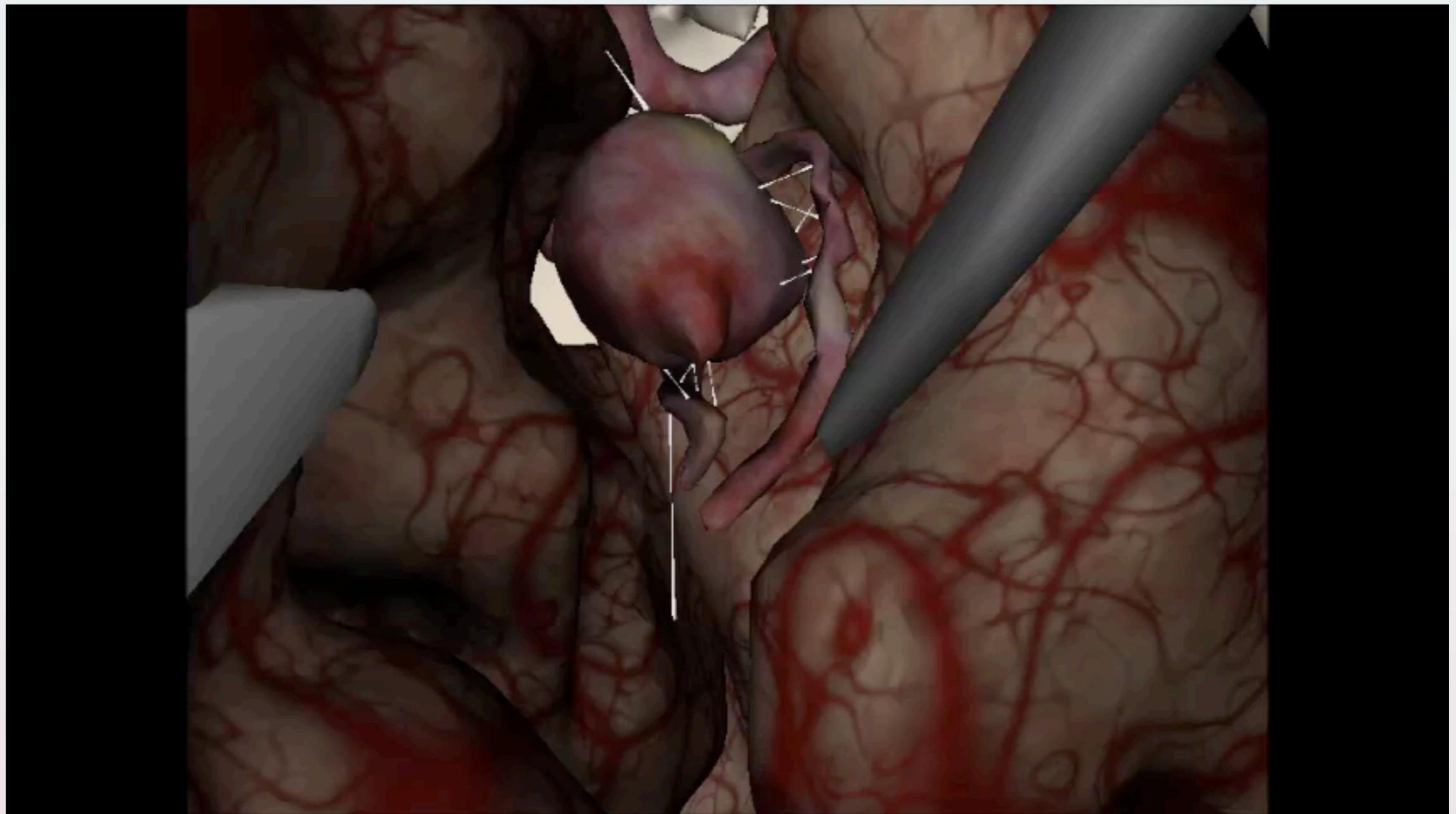


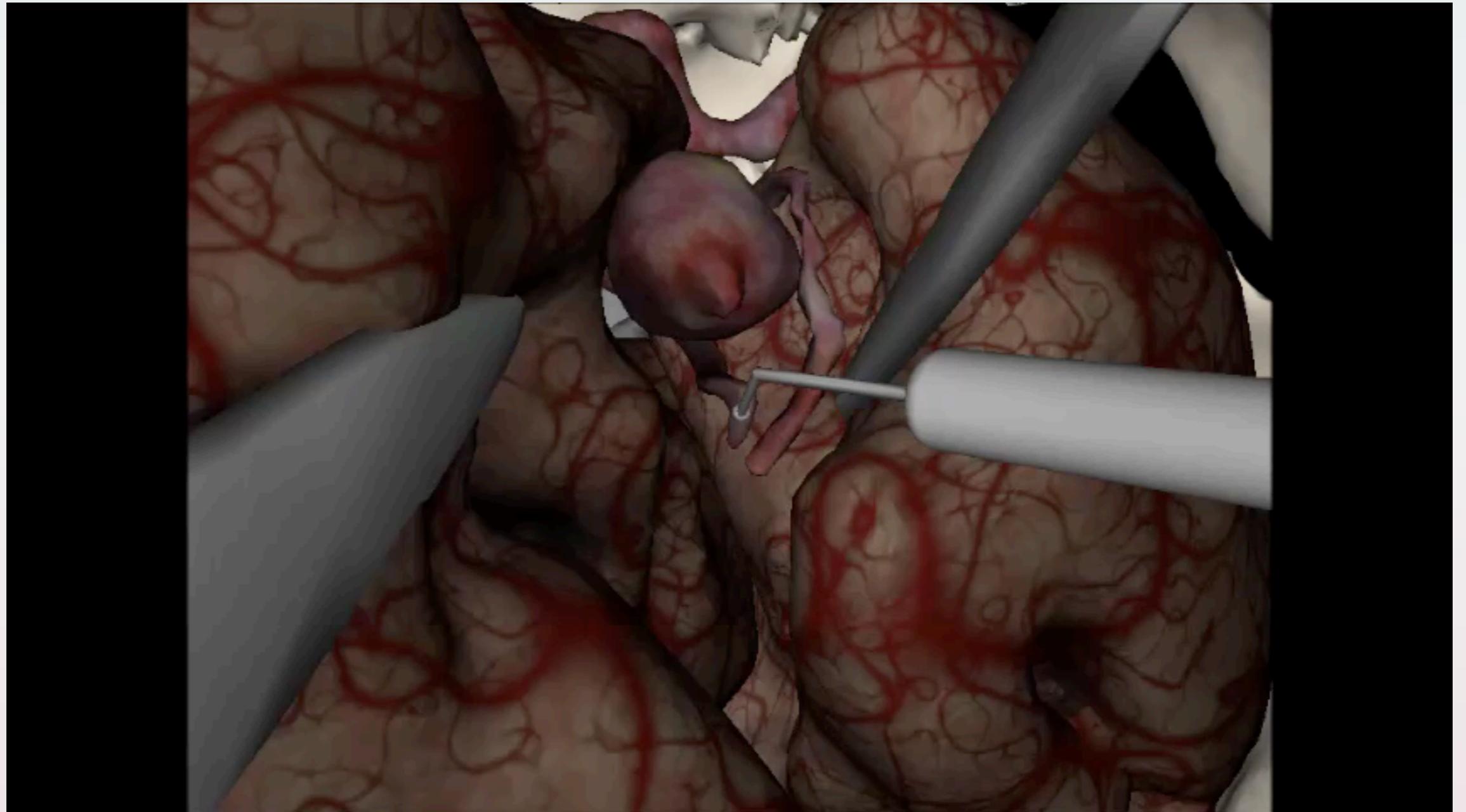
Asynchronous Preconditionner  
+ Volume contact model

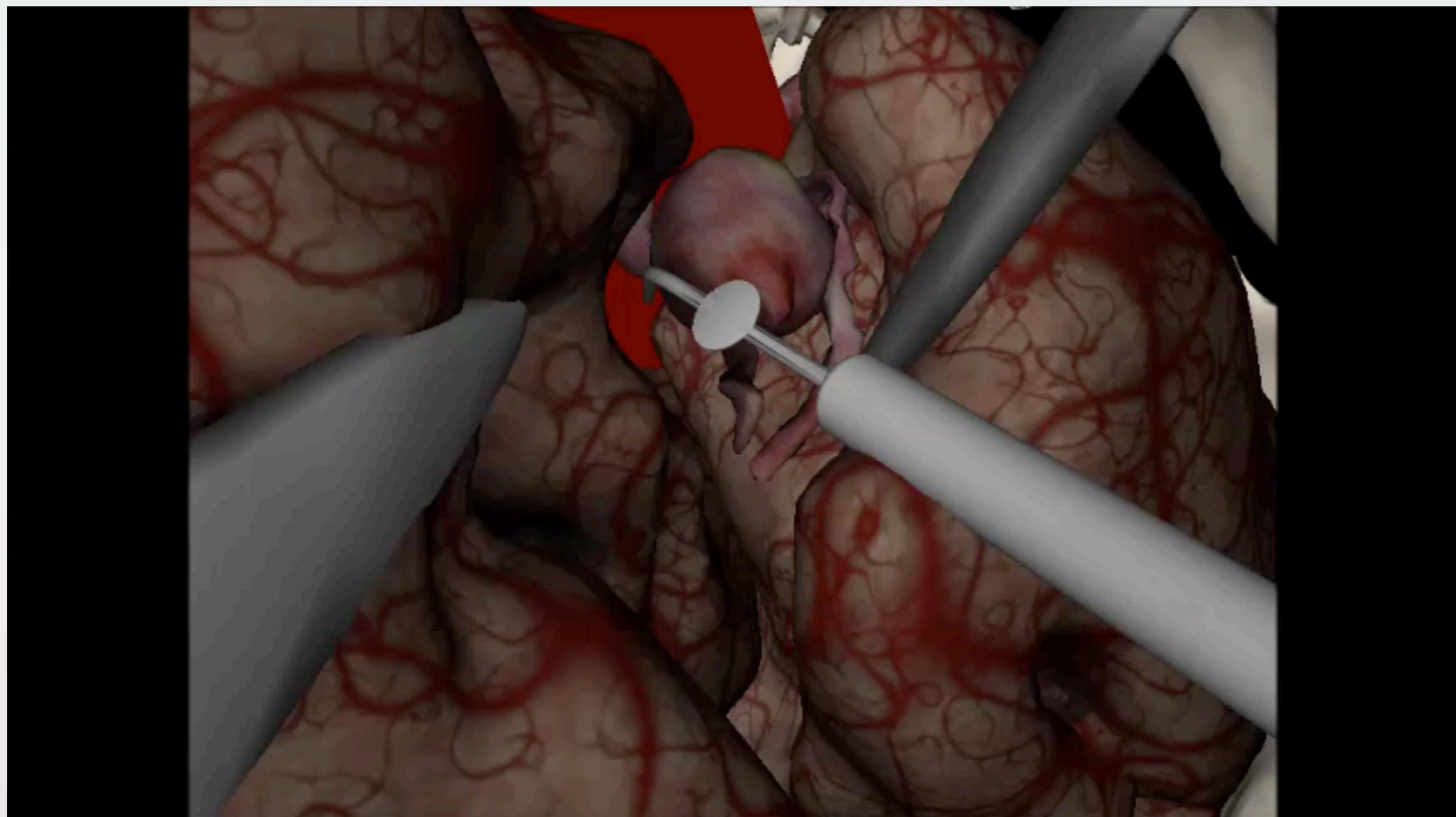


Asynchronous Preconditionner  
+ Vascularized Liver  
+ Constraint-based needle insertion











PERSPECTIVE  
AND CONCLUSION

# A RETENIR...

- Importance de bien modéliser les interactions
  - Grande influence sur le comportement mécanique
  - Peut générer des instabilités numériques
- Différentes classes d'approches
  - Event driven / Time stepping
  - Lois de contact utilisé
  - Approche par Pénalisation / Contrainte Lagrangienne
  - Optimisation numérique pour obtenir une solution en temps-réel