

Discrete-Time LTI Systems

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Difference Equations

Analog system behavior is specified by differential equations. Analog LTI systems are specified by linear differential equations.



Q : charge on capacitor

$$V_o - IR - \frac{Q}{C} = 0$$

$$V_o - \frac{dQ}{dt} R - \frac{Q}{C} = 0$$

$$V_o - \frac{Q}{C} = \frac{dQ}{dt} R$$

$$\frac{V_o}{R} - \frac{Q}{RC} = \frac{dQ}{dt}$$

$$\frac{CV_o - Q}{RC} = \frac{dQ}{dt}$$

$$\frac{dQ}{CV_o - Q} = \frac{dt}{RC}$$

$$\int \frac{dQ}{CV_o - Q} = \int \frac{dt}{RC}$$

$$\int_0^{\cdot} \frac{dQ}{CV_0 - Q} = \int_0^{\cdot} \frac{dt}{RC}$$

$$\left[\ln(CV_0 - Q) \right]_0^{q(t)} = -\frac{t}{RC} + \underbrace{C'}_{\text{integration constant}}$$

$$\ln(CV_0 - q(t)) - \ln(CV_0) =$$

$$\ln \left(\frac{CV_0 - q(t)}{CV_0} \right) = -\frac{t}{RC} + C'$$

$$1 - \frac{q(t)}{CV_0} = e^{C'} e^{-t/RC}$$

$$\frac{q(t)}{CV_0} = 1 - e^{C'} e^{-t/RC}$$

$$q(t=0) = 0 \Rightarrow e^{C'} = 1.$$

$$q(t) = CV_0 (1 - e^{-t/RC})$$

$$I(t) = \frac{dq(t)}{dt} = \frac{CV_0}{RC} e^{-t/RC} = \frac{V_0}{R} e^{-t/RC}$$

We can see that, for example, a linear ODE completely specifies the behavior of an analog RC circuit. In discrete-time circuits, we use difference equations to specify LTI DT systems.

$$y[n] = a_1 y[n-1] + a_2 y[n-2] + \dots + a_p y[n-p] \\ + b_0 x[n] + b_1 x[n-1] + \dots + b_q x[n-q]$$

We specify the initial conditions of an LTI DT System as 0.
why? To guarantee linearity.

Proof:

If the initial conditions of the output are not chosen as 0, then a system w/ non-zero difference equation coefficients may map a 0-input to an non-zero output, violating the linearity condition that

$$S\{\alpha x[n]\} = \alpha S\{x[n]\} \text{ for } \alpha=0. \quad \blacksquare$$

Example $y[n] = ay[n-1] + bx[n]$

n	$x[n]$	$y[n]$
-1	0	0
0	1	b
1	0	ab
2	0	a^2b
3	0	a^3b
4	0	a^4b
:	:	:

Find $S\{s[n]\}$. \uparrow

Systems w/ an infinitely non-zero response to an impulse input (like the example) are called IIR filters (Infinite Impulse Response).

Systems w/ a finite non-zero response to an impulse input ($a_1, \dots, a_p = 0$) are called FIR filters (finite impulse response).

impulse input ($\alpha_1, \dots, \alpha_p = 0$) are called FIR filters (finite impulse response).

DT Filters in Frequency Domain

$$x[n] = X e^{j2\pi f_n}$$

$$y[n] = Y e^{j2\pi f_n}$$

$$Y e^{j2\pi f_n} = \sum_{m=1}^p a_m X e^{j2\pi f(n-m)} + \sum_{m=0}^q b_m X e^{j2\pi f(n-m)}$$

$$Y \left(1 - \sum_{m=1}^q a_m e^{-j2\pi f_m} \right) = \left(\sum_{m=0}^q b_m e^{-j2\pi f_m} \right) X$$

$$H(e^{j2\pi f}) = \frac{Y}{X} = \frac{\sum_{m=0}^q b_m e^{-j2\pi f_m}}{1 - \sum_{m=1}^q a_m e^{-j2\pi f_m}}$$

This relation can also be derived from Fourier Transforms.

$$Y[n] = \mathcal{S}\{x[n]\} \quad \leftarrow (\text{Take DTFT of both sides})$$

The unit sample response $h[n]$ is the output of LTI system S for input $S[1]$.

$$\mathcal{S}\{S[1]\} = \sum_{n=-\infty}^{n=\infty} S[n] e^{-j2\pi f n} = 1$$

$$h[n] = \mathcal{F}^{-1} \left\{ H(e^{j2\pi f}) \cdot \mathcal{F} \{ \delta[n] \} \right\}$$

$$= \mathcal{F}^{-1} \left\{ H(e^{j2\pi f}) \right\}.$$

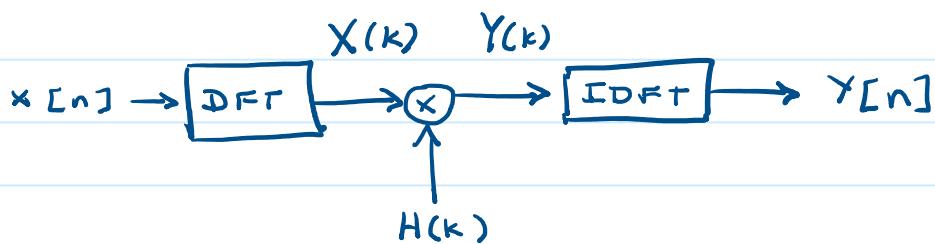
We have shown $h[n] \xleftrightarrow{\mathcal{F}} H(e^{j2\pi f})$

We can use the DFT to perform filtering in the discrete-time frequency domain.

$$H(k) = H(e^{j\frac{2\pi f k}{N}}) \text{ for } k \in [0, 1, \dots, N-1]$$

The IDFT will always be periodic with period N , so if $h[n]$ is longer than N , filtering in the frequency will not work as aliasing in the time domain will occur.

So for FIR filters, we require $N \geq g$.
 IIR filters cannot be implemented in the frequency domain.

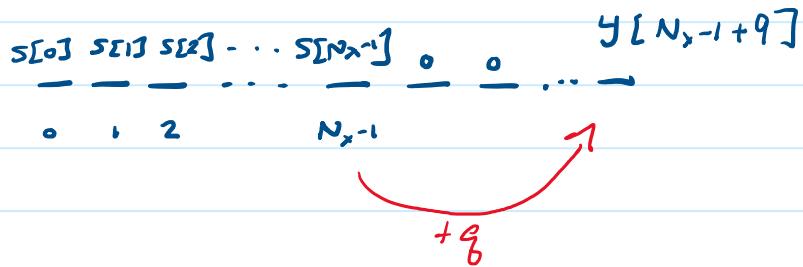


Above shows how to implement an FIR filter in the frequency domain. There is an additional subtlety, however.

Suppose we input a signal of length N_x into an FIR filter with length $q+1$.

$$y[n] = b_0 \times [n] + b_1 \times [n-1] + \dots + b_q \times [n-q]$$

$$s[n] \rightarrow \boxed{s} \rightarrow S\{s[n]\}$$



The last non-zero (potentially) output occurs when $n = N_x - 1 + q$. $S\{s[n]\}$ has length $N_x + q$.

To prevent time-domain aliasing, we require $N_x + q$ samples of $h[k]$ and $x[k]$.

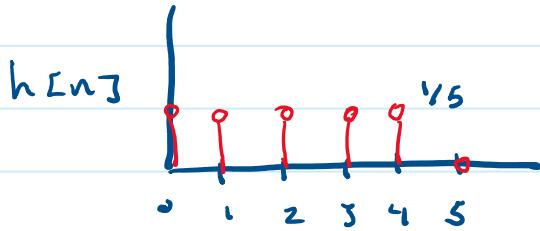
$$X(k) = \sum_{n=0}^{N_x-1} s[n] e^{-j \frac{2\pi k n}{N_x}}$$

$$X(k) = X(k+N_x).$$

To sample at $N_x + q$ frequencies, we need an $N_x + q$ -length input signal w/ the same behavior as the original one. So we zero-pad both $h[n]$ and $x[n]$.

DJIA Averaging

Let's look at an example use-case. Suppose we want to compute a running average of DJIA values. For a year, we have 253 stock prices. We will use a length-5 averager.



The output will be length 253, so we must use a 512-length FFT.

Complexity in Time and Frequency Domains

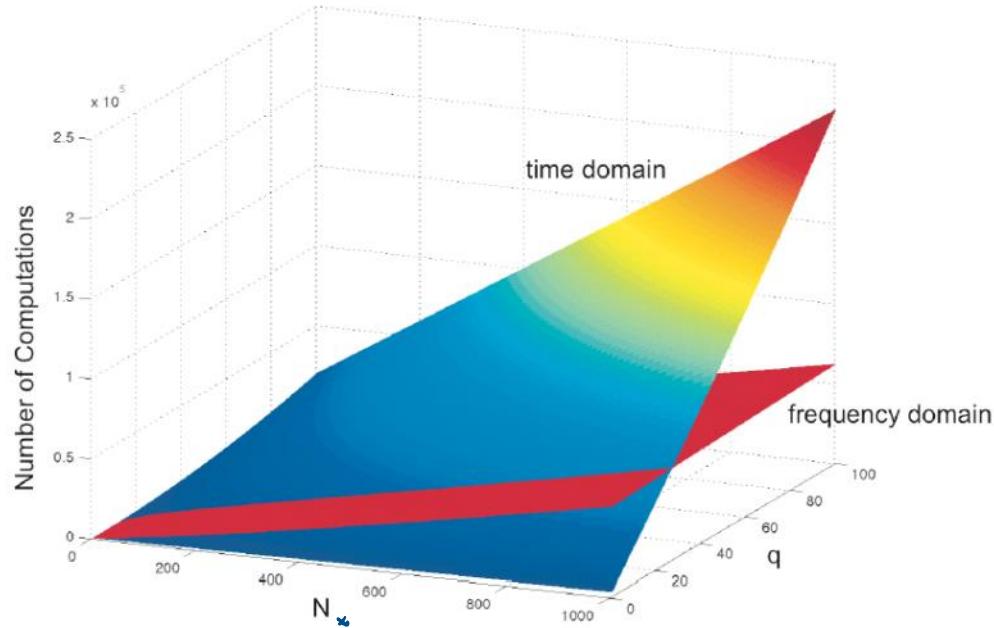
For a g -order FIR filter, time-domain filtering requires $(N_x + g)(2g + 1)$ operations. We must compute $N_x + g$ potentially non-zero outputs, and each requires g multiplications and $g+1$ additions or $2g+1$ total arithmetic operations.

For a g -order FIR filter, frequency-domain filtering requires $\left(\frac{512}{2} \log_2(K)\right) \cdot 2 + 6K$ where $K = N_x + g$.

$\underbrace{\quad}_{\text{FFTs}}$ $\underbrace{\quad}_{H(k)X(k)}$

$5(N_x + g) \log_2(N_x + g) + 6(N_x + g)$ is the total number of frequency-domain operations required.

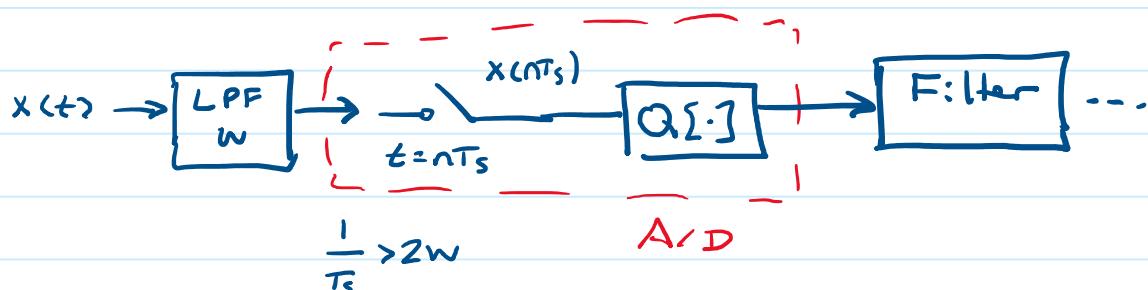
Plotting # of computations vs. q and N_x yields the following figure from the textbook:



Filtering Infinite-Length Inputs

To filter an infinite-length signal, we section it into N_x -length non-overlapping sections and filter each section, combining the results at the end thanks to linearity.

Computationally Filtering Analog Signals



$$\frac{1}{T_s} > 2w$$

A/D

