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A new single lane car following model of traffic flow is presented. The model is inertial and free of collisions. It demonstrates experimentally observed features of traffic flow such as the existence of three regimes: free, fluctuative (synchronized) and congested (jammed) flow; bistability of free and fluctuative states in a certain range of densities, which causes the hysteresis in transitions between these states; jumps in the density-flux plane in the fluctuative regime and gradual spatial transition from synchronized to free flow. Our model suggests that in the fluctuative regime there exist many stable states with different wavelengths, and that the velocity fluctuations in the congested flow regime decay approximately according to a power law in time.

In the last years, growing effort has been made in understanding traffic flow dynamics. Recent experiments [1,2] show that traffic flow demonstrates complex physical phenomena, among which are:

- (i) The existence of three states: free flow, "synchronized" (or "fluctuative") flow and traffic jams (for low, intermediate and high densities correspondingly). The second state has two essential features: synchronization of flow in different lanes (for the multilane traffic) and fluctuation performed by the system in density-flux plane. Since our model is single-lane we will refer to this state as "fluctuative".
- (ii) Hysteresis which is observed in transitions between the free and the fluctuative flow.
- (iii) Long survival time of traffic jams.

Modeling of traffic flow is traditionally performed using two approaches. The microscopic, or car-following models approach, which describes the nearest-neighbor interaction between two consecutive cars and investigates its influence on the flow (see e.g. [3-5]), and the macroscopic, or continuous models approach, which represents the flowing traffic as a continuous media and describes it using the hydrodynamical partial differential equations (see e.g. [7-9]). Wide surveys of these models are given in [10-12].

In this Letter we inroduce an inertial single lane carfollowing model, which is free of collisions. We study the model both numerically and analytically and find the existence of three regimes in traffic flow: free flow regime at low densities (where each car moves with almost a constant velocity), fluctuative flow regime at inetrmediate densities (where stable periodic oscillations of velocities of all cars are observed) and congested or jammed flow regime at high densities (where due to high density all the cars tend to move with the same, relatively small velocity). Our model predicts the existence of many inhomogeneous stable states in the fluctuative regime and demonstrates hysteresis in transitions between free and fluctuative regimes. The experimentally observed long survival time of jams may be explained by our finding that the fluctuations in the congested flow regime decay slowly according to a power law.

To formulate the model we assume that car acceleration is affected by three factors:

- (a) aspiration to keep safety time gap from the car ahead.
- (b) pre-braking if the car ahead is much slower,
- (c) aspiration not to exceed significantly the permitted velocity.

In mathematical description, the acceleration of the *n*th car a_n is given by a sum of three terms depending on its coordinate x_n , velocity v_n , distance to the car ahead $\Delta x_n = x_{n+1} - x_n$ and the velocities difference $\Delta v_n = v_{n+1} - v_n$:

$$a_n = A(1 - \frac{\Delta x_n^0}{\Delta x_n}) - \frac{Z^2(-\Delta v_n)}{2(\Delta x_n - D)} - kZ(v_n - v_{per}),$$
 (1)

where A is a sensitivity parameter, D is the minimal distance between consecutive cars, v_{per} is the permitted velocity and k is a constant. The safety distance $\Delta x_n^0 = v_n T + D$ depends on T, which is the safety time gap constant. The function Z is defined as Z(x) = (x+|x|)/2. Note that Eq.(1) can be generalized by adding a noise term.

In the following we discuss in more details the terms in the right side of (1):

(a) The first term plays an important role when velocity difference between consequtive cars is relatively small. In this case the *n*th car accelerates if $\Delta x_n > \Delta x_n^0$ and brakes if $\Delta x_n < \Delta x_n^0$.

The choice of function in this term is not unique. Replacing it by other functions of Δx_n which are increasing, equal to zero if $\Delta x_n = \Delta x_n^0$ and tend to $-\infty$ if $\Delta x_n \to 0$, such as $A \log(\Delta x_n/\Delta x_n^0)$, gives similar results.

- (b) The second term plays an important role when $v_n \gg v_{n+1}$. A car getting close to a much slower car starts braking even if $\Delta x_n > \Delta x_n^0$. This term corresponds to the negative acceleration needed to reduce $|\Delta v_n|$ to 0 as $\Delta x_n \to D$.
- (c) The dissipative third term is a repulsive force acting when the velocity exceeds the permitted velocity.

Unlike optimal velocity models [5] the acceleration in our model depends explicitly on Δx which enables us to make the flow free of collisions.

The motion of cars is therefore described by the following system of ordinary differential equations

$$\begin{cases} \dot{x}_n = v_n, \\ \dot{v}_n = A(1 - \frac{v_n T + D}{x_{n+1} - x_n}) \\ -\frac{Z^2(v_n - v_{n+1})}{2(x_{n+1} - x_n - D)} - kZ(v_n - v_{per}), \end{cases}$$
(2)

 $n = 1, 2, \dots N$ with periodic boundary conditions

$$x_{N+1} = x_1 + \frac{N}{\rho}, \quad v_{N+1} = v_1.$$

A solution of Eqs. (2) which corresponds to homogeneous flow is

$$v_n^0 = v^0 = \begin{cases} \frac{A(1 - D\rho) + kv_{per}}{A\rho T + k}, & \rho \le \frac{1}{D + Tv_{per}}, \\ \frac{1 - D\rho}{\rho T}, & \rho \ge \frac{1}{D + Tv_{per}}, \end{cases}$$
(3)

$$x_n^0 = \frac{n-1}{\rho} + v^0 t.$$

In the following numerical results we use parameters values $v_{per}=25(m/s), T=2(s), D=5(m), 1 \leq A \leq 5(m/s^2)$ and $k=2(s^{-1})$.

The flux-density relation (often called the fundamental diagram) for the homogeneous flow is shown in Fig.1(a) as a dashed line. Comparison of this curve with the fundamental diagrams (solid lines) obtained by the numerical solution of equations (2) for different values of A starting from nonhomogeneous initial conditions indicates that for values of ρ smaller than some critical value ρ_1 or greater than another critical value ρ_2 the flux is the same, while for the intermediate values of density $(\rho_1 < \rho < \rho_2)$ the measured flux is considerably lower than the homogeneous solution flux. Plotting the variance of velocities $\sigma_v = \left[\frac{1}{N} \sum_{n=1}^{N} (v_n - \langle v \rangle)^2\right]^{1/2}$ (where $\langle v \rangle$ is the average velocity) against ρ (Fig.1(b)) shows the

existence of velocity fluctuations for $\rho_1 < \rho < \rho_2$. We can therefore define three regimes in traffic flow: the free flow regime $(\rho < \rho_1)$, the fluctuative flow regime $(\rho_1 < \rho < \rho_2)$ and the congested flow regime $(\rho > \rho_2)$. Note that the flow in the first and the last regimes is homogeneous. Note also that for small values of $A \rho_2$ is greater than the maximal possible density $\rho_{max} = 1/D$ and the congested flow regime does not exist. See Fig. 1(b) for A = 2. This finding is supported by the analytical results shown below.

30 80 600 560 270

FIG. 1. (a) Fundamental diagram for $A=5,3,2(m/s^2)$ (top to bottom). Dashed line corresponds to the homogeneous solution. (b) Ratio of variance of velocities to the average velocity for $A=2,3,5(m/s^2)$ (top to bottom). (c) Qualitative plot of function $S(\rho)$. (d),(e) Hysteresis loops in transitions between free and fluctuative flow states for A=3, arrows show the direction of changing the global density. (f) Results of local measurements of density and flux in free (almost straight line) and fluctuative regimes.

In order to estimate the values of ρ_1 and ρ_2 we analyse the stability of the homogeneous flow solution. The linearization of Eqs. (2) near the homogeneous flow solution (3) in variables $\xi_n = x_n - x_n^0$ has the form

$$\ddot{\xi}_n = -p\dot{\xi}_n + q(\xi_{n+1} - \xi_n), \quad n = 1, \dots, N,$$
(4)

$$\xi_{N+1} = \xi_1,$$

where $p = AT\rho + k$, $q = \frac{AT + kTv_{per} + kD}{AT\rho + k} \cdot A\rho^2$ for $\rho \le \frac{1}{D + Tv_{per}}$ and $p = AT\rho$, $q = A\rho$ otherwise.

A solution of equation (4) can be written as

$$\xi_n = \exp\{i\alpha n + zt\},\tag{5}$$

where $\alpha = \frac{2\pi}{N}\kappa$ ($\kappa = 0, ..., N-1$) and z - a complex number. Substituting (5) into (4) we obtain the algebraic equation for z

$$z^{2} + pz - q(e^{i\alpha} - 1) = 0. (6)$$

Each of the N equations (6) has two solutions. These 2N different complex numbers are the eigenvalues of system (4). One of them (which corresponds to $\kappa=0$) is equal to zero regardless of values of parameters. In this case all ξ_n in (5) are equal to a constant and belong to the one-dimensional subspace of equilibria of system (4) (defined by equations $\xi_1 = \ldots = \xi_N, \ \dot{\xi}_1 = \ldots = \dot{\xi}_N = 0$). This indicates that the disturbed state x_n for z=0 is also homogeneous. For $z \neq 0$ ξ_n in (5) is a wave with increasing or decreasing amplitude. Therefore, if we find conditions under which other 2N-1 eigenvalues have negative real parts (the magnitude of wave (5) decreases

with time) we can say that under these conditions the homogeneous flow solution (3) is stable.

Following the approach of [5] we can derive this condition as $\frac{p^2}{q} > 2$ or $S(\rho) > 2$, where

$$S(\rho) = \begin{cases} \frac{(AT\rho + k)^3}{\rho^2 A(AT + kv_{per}T + kD)}, & \rho \le \frac{1}{D + Tv_{per}}, \\ A\rho T^2, & \rho \ge \frac{1}{D + Tv_{per}}. \end{cases}$$
(7)

A qualitative plot of $S(\rho)$ is sketched in Fig.1(c). From this figure it follows that depending on ρ we have three regimes of stability/instability of the homogeneous flow solution. If $\rho < \rho'$ (free flow) or $\rho > \rho''$ (congested flow) the homogeneous flow solution is stable and if $\rho' < \rho < \rho''$ it is unstable, where $\rho' = \frac{1}{D+Tv_{per}}$ and $\rho'' = \frac{2}{AT^2}$. Note that there are possible sets of parameters under which the minimum of the left part of $S(\rho)$ can be less than 2 and the flow can have five different regimes of stability/instability. Nevertheless, under the set of parameters specified above we have up to three regimes, where the third regime does not exist for $\rho'' \geq \rho_{max}$ $(A \leq 2D/T^2)$.

Our numerical simulations show that $\rho_2 \approx \rho''$, but ρ' is considerably greater than ρ_1 , thus we expect that for $\rho_1 < \rho < \rho'$ both homogeneous and fluctuative states are stable.

In the fluctuative regime $(\rho_1 < \rho < \rho_2)$ the flow is characterized by presence of humps (dense regions) moving backwards or forwards. When the flow has stabilized the humps are equidistant and the evolution of traffic in time and space resembles the spreading of a wave. The existence of a fluctuative regime was predicted by other car-following (e.g. [5] where it was called "jammed flow") and continuous (e.g. [9], where it was called "recurring humps state") models and measured experimentally [1].

Simulations of our model show that the fluctuative flow state is not unique. Figs. 2(a-c) present the cars velocities after the fluctuative flow regime has stabilized for three different initial conditions. It can be seen that the "wavelengths" of these states are different. Fig. 2(d) presents the convergence of flux in these experiments to distinct values. Our simulations also show the existence of solutions with other "wavelengths" and flux values. Fig. 2(e) shows the fundamental diargams for three different wavelengths. Consequently, depending on initial conditions different stable fluctuative states emerge with different values of flux and distances between neighboring humps. This indicates that for $\rho_1 < \rho < \rho_2$ system (2) has many stable periodic (in Δx_n , v_n variables) solutions, and hence in the 2N-dimensional space of variables Δx_n , v_n there exist many attractive limit cycles.

 $170\ 35\ 590\ 655$ 270

FIG. 2. Three different stable states in the fluctuative regime, obtained from different initial conditions. Global density $\rho=0.06(veh/m),\,A=3(m/s^2).$ (a-c) Cars velocities. (d) Convergence of flux to different values in these three experiments. (e) Fundamental diagrams for three different stable fluctuative states with wavelengths 20, 5 and 6.67 cars (top to bottom). A dashed line corresponds to the homogeneous solution.

As follows from above for $\rho_1 < \rho < \rho'$ not only fluctuative flow solutions are stable, but also the homogeneous flow solution. This bistability is the origin of hysteresis in transitions between free and fluctuative flow regimes. Such bistability was observed experimentally [1] and was found in other models [5,6,9]. Fig. 1(d) shows a hysteresis loop in the density-flux plane. The upper curve is obtained by increasing the density of cars adiabatically preserving the road length L [14]. It can be seen that up to the value of density ρ' the homogeneous flow is preserved. The lower curve was obtained by adiabatically decreasing the density in the same manner. While decreasing the density the flow remains fluctuative even for $\rho < \rho'$. Fig.1(e) presents the hysteresis loop in the global density - velocities fluctuations plane.

Our results also illustrate the well-known phenomenon [1,2,5,9,10] of jumps which the system performs in the density-flux plane in the fluctuative flow regime when the density and the flux are measured locally. In our numerical simulation (Fig. 1(f)) we started from a value of density below ρ' , increased it gradually in the described above manner up to a value greater than ρ' and decreased it back. These jumps may be explained by our finding of many stable states in the fluctuative regime.

Our model also demonstrates the gradual spatial transition from the fluctuative to free flow in the downstream direction which was measured by [1]. The results of local measurements of density and flux at different distances from an on-rump [15] are shown in Fig.3. which is in good agreement with Fig.3 of [1].

410 30 585 650 270

FIG. 3. Results of local measurements of flux and density at different distances from the on-ramp. (a) 500~m upstream the on-rump, (b) and (c) 250~and~1000~m downstream respectively

In the congested flow regime the only stable solution is the homogeneous flow solution. We have not found evidence of existence of bistability or hysteresis in transitions between the fluctuative and congested flow regimes. Starting from random initial conditions, we observe that initial fluctuations of the velocity seem to decay according to a power law

$$\sigma_v \sim \begin{cases} t^{-\beta}, & t \ll t^* \\ e^{-t/\tau}, & t \gg t^*. \end{cases}$$
 (8)

where t^* is the crossover time between the power law and exponential decay. We find $t^* \sim L^z$ and $\tau \sim L^z$ with $z=2.0\pm0.1$. These results are qualitivly similar to that obtained by [11] for a cellular automata model [4], but with different values of exponents. The result $z\approx 2$ seems to be in agreement with random walk arguments of [6]. For the parameters values A=4, $\rho=0.15$ we get $\beta\approx0.21\pm0.04$ (Fig.4).

270 FIG. 4. Decay of the velocities variance in time in the congested flow regime. Road length is 1, 4 and 16 km (bottom to top). The dashed line has a slope -0.21

In summary, we present a single lane car-following model which explains important features of traffic observed experimentally. The model predicts the existence of many stable periodic states in the fluctuative (synchronized) flow regime.

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- [14] Every new car is placed in the middle between two consecutive cars chosen randomly and gets the velocity of the car ahead. The safety time gap of the new car and the car behind is halved and then gradually increased linearly up to the initial value T.

[15] Starting from a low value of density (free flow) the density is increased by the influx $f_{in}=0.133(veh/sec)$ at the on-ramp situated at $x_{in}=L/4$, where L=10000(m). The off-rump is at $x_{out}=3L/4$ and the outflux changes instantly from 0 to $f_{out}=f_{in}$ when the global density ρ reaches the maximal value 0.03 (veh/m).