Fourier Basic Functions

Here we suppose the solution to steady state equation is a linear combination of Fourier basic functions

$$\psi_{1c} = u_0 + u_1 cos(y_1 - s_1) + u_2 cos2(y_1 - s_1) + u_3 sin2(y_1 - s_1)$$

And ψ square:

$$\psi_{1c}^2 = (u_0^2 + rac{u_1^2}{2} + rac{u_2^2}{2} + rac{u_3^2}{2}) + (2u_0u_1 + u_1u_2)cos(y_1 - s_1) + u_1u_3sin(y_1 - s_1) + (2u_0u_2 + rac{u_1^2}{2})cos2(y_1 - s_1) + 2u_0u_3sin2(y_1 - s_1) + u_1u_2cos3(y_1 - s_1) + u_1u_3sin3(y_1 - s_1) + (rac{u_2^2}{2} - rac{u_3^2}{2})cos4(y_1 - s_1) + u_2u_3sin4(y_1 - s_1)$$

Congruent Group's Equation

$$\psi(y_1) = rac{
ho J_{rc}}{D_1} \int dy_2 V(y_1-y_2,a_0) \psi^2(y_2) + rac{
ho J_{rp}}{D_2} \int dy_2 V(y_1-y_2,a_0) ar{\psi}^2(y_2) + I_1 V(y_1-x_1,a_0/2) + I_b \ \ \ (1)$$

Global Inhibition

$$D_n = 1 + \omega \int
ho \left[u_n^2(x,k) + J_{int} u_{ar{n}}^2(x,k)
ight] dx = 1 + \pi \omega
ho \left[2 u_0^2 + u_1^2 + u_2^2 + u_3^2 + J_{int} (2 ar{u}_0^2 + ar{u}_1^2 + ar{u}_2^2 + ar{u}_3^2)
ight]$$

Let's define:

$$B(n,k) = \frac{I_n(k)}{I_0(k)}$$

The square term:

$$egin{split} rac{
ho J_{rc}}{D_1} \int dy_2 V(y_1-y_2,a_0) \psi^2(y_2) &= rac{
ho J_{rc}}{D_1} \left[(u_0^2 + rac{u_1^2}{2} + rac{u_2^2}{2} + rac{u_2^2}{2}) + (2u_0u_1 + u_1u_2) B(1,a_0) cos(y_1-s_1)
ight. \ &+ u_1u_3 B(1,a_0) sin(y_1-s_1) + (2u_0u_2 + rac{u_1^2}{2}) B(2,a_0) cos2(y_1-s_1) + 2u_0u_3 B(2,a_0) sin2(y_1-s_1) + u_1u_2 B(3,a_0) cos3(y_1-s_1) \ &+ u_1u_3 B(3,a_0) sin3(y_1-s_1) + (rac{u_2^2}{2} - rac{u_3^2}{2}) B(4,a_0) cos4(y_1-s_1) + u_2u_3 B(4,a_0) sin4(y_1-s_1)
ight] \end{split}$$

Projection

Multiply both sides by $1 \cos(y_1-s_2) \sin(y_1-s_2) \cos 2(y_1-s_2) \sin 2(y_1-s_2)$ and integrate over y_1

$$\begin{split} u_{10} &= \frac{\rho J_{rc}}{D_1} \left[u_{10}^2 + \frac{u_{11}^2}{2} + \frac{u_{12}^2}{2} + \frac{u_{13}^2}{2} \right] + \frac{\rho J_{rp}}{D_2} \left[u_{20}^2 + \frac{u_{21}^2}{2} + \frac{u_{22}^2}{2} + \frac{u_{23}^2}{2} \right] + \frac{I_1}{2\pi} + I_b \\ u_{11} &= \frac{\rho J_{rc}}{D_1} (2u_{10}u_{11} + u_{11}u_{12}) B(1, a_0) + \frac{I_1 B(1, a_0/2)}{\pi} cos(x_1 - s_1) + \\ \frac{\rho J_{rp}}{D_2} [(2u_{20}u_{21} + u_{21}u_{22}) B(1, a_0) cos(s_2 - s_1) - u_{21}u_{23} B(1, a_0) sin(s_2 - s_1)] \\ 0 &= \frac{\rho J_{rc}}{D_1} u_{11} u_{13} B(1, a_0) + \frac{I_1 B(1, a_0/2)}{\pi} sin(x_1 - s_1) + \\ \frac{\rho J_{rp}}{D_2} [(2u_{20}u_{21} + u_{21}u_{22}) B(1, a_0) sin(s_2 - s_1) + u_{21}u_{23} B(1, a_0) cos(s_2 - s_1)] \end{split}$$

$$egin{aligned} u_{12} &= rac{
ho J_{rc}}{D_1} (2u_{10}u_{12} + rac{u_{11}^2}{2}) B(2,a_0) + rac{I_1 B(2,a_0/2)}{\pi} cos2(x_1-s_1) + \ rac{
ho J_{rp}}{D_2} \Bigg[(2u_{20}u_{22} + rac{u_{21}^2}{2}) B(2,a_0) cos2(s_2-s_1) - 2u_{20}u_{23} B(2,a_0) sin2(s_2-s_1) \Bigg] \ u_{13} &= rac{
ho J_{rc}}{D_1} 2u_{10}u_{13} B(2,a_0) + rac{I_1 B(2,a_0/2)}{\pi} sin2(x_1-s_1) + \ rac{
ho J_{rp}}{D_2} \Bigg[(2u_{20}u_{22} + rac{u_{21}^2}{2}) B(2,a_0) sin2(s_2-s_1) + 2u_{20}u_{23} B(2,a_0) cos2(s_2-s_1) \Bigg] \end{aligned}$$

Mean

So

Firing rate $R_i(s_1,u_0,u_1,u_2,u_3)=rac{\psi_i^2}{D_i}$, then \hat{s} will be

$$\hat{s}_i = arg(\sum_{-\pi}^{\pi} R_i e^{j heta})$$

 $egin{aligned} Real\ Part &= \pi(2u_0u_1+u_1u_2)cos(s) - \pi u_1u_3sin(s) \ Imaginary\ Part &= \pi(2u_0u_1+u_1u_2)sin(s) + \pi u_1u_3cos(s) \end{aligned}$

 $\hat{s} = a$

$$\hat{s} = atan2[(2u_0u_1 + u_1u_2)sin(s) + u_1u_3cos(s), (2u_0u_1 + u_1u_2)cos(s) - u_1u_3sin(s)]$$

Concentration

Next we need to take noise into consideration.

$$au rac{\partial}{\partial t} \psi(y_1) = -\psi(y_1) + rac{
ho J_{rc}}{D_1} \int dy_2 V(y_1 - y_2, a_0) \psi^2(y_2) + rac{
ho J_{rp}}{D_2} \int dy_2 V(y_1 - y_2, a_0) ar{\psi}^2(y_2) + I_1 V(y_1 - x_1, a_0/2) + I_b + \sqrt{FI_1 V(y_1 - x_1, a_0/2)} \xi_1 + \sqrt{FI_b} \epsilon_1$$

Consider the dynamics of the displacement mode and multiply both sides by $sin(y_1-s_1)$, integrate over y_1

$$egin{aligned} aurac{\partial}{\partial t}\delta s_1 &= -\delta s_1 + rac{
ho J_{rc}}{D_1 u_{11}}(2u_{10}u_{11} + u_{11}u_{12})B(1,a_0)\delta s_1 \ &+ rac{
ho J_{rp}}{D_2 u_{11}}[(2u_{20}u_{21} + u_{21}u_{22})B(1,a_0)cos(s_2 - s_1) - u_{21}u_{23}B(1,a_0)sin(s_2 - s_1)]\,\delta s_2 \ &+ rac{\sqrt{FI_1}}{\pi u_{11}}\int \sqrt{V(y_1 - x_1,a_0/2)}sin(y_1 - s_1)\xi_1 dy_1 + rac{\sqrt{FI_b}}{\pi u_{11}}\int sin(y_1 - s_1)\epsilon_1 dy_1 \end{aligned}$$

Noise Temperature

$$egin{split} T_1 &= rac{F}{2\pi^2
ho u_{11}^2} \left[I_1 \int V(y_1-x_1,a_0/2) sin^2(y_1-s_1) dy_1 + I_b \int sin^2(y_1-s_1) dy_1
ight] \ &= rac{F}{2\pi^2
ho u_{11}^2} \left[(rac{I_1}{2} + \pi I_b) - rac{I_1}{2} B(2,a_0/2) cos2(x_1-s_1)
ight] \end{split}$$

Results







