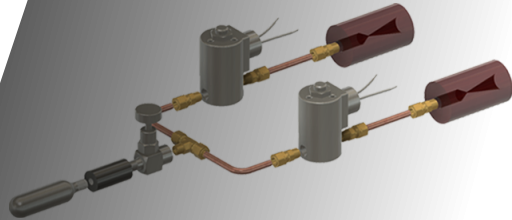


# Reaction Control System for High Altitude Balloons

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# Nozzles

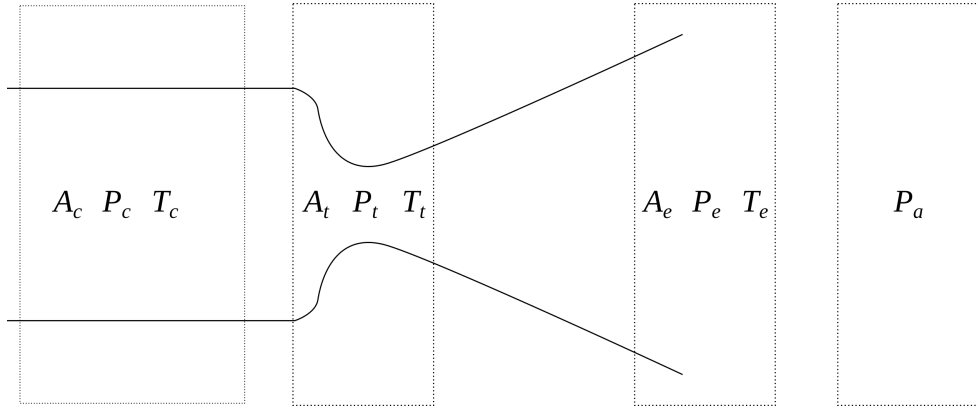


Figure: Basic nozzle design and some parameters.

# Existing Nozzle Theory

$$\frac{A_e}{A_t} = \left( \frac{\gamma + 1}{2} \right)^{\frac{1}{1-\gamma}} \left( \frac{P_a}{P_c} \right)^{\frac{1}{\gamma}} \left( \left( \frac{\gamma + 1}{\gamma - 1} \right) \left[ 1 - \left( \frac{P_c}{P_a} \right)^{\frac{\gamma-1}{\gamma}} \right] \right)^{-\frac{1}{2}} \quad (1)$$

Optimum expansion ratio for nozzle

# Nozzle Design

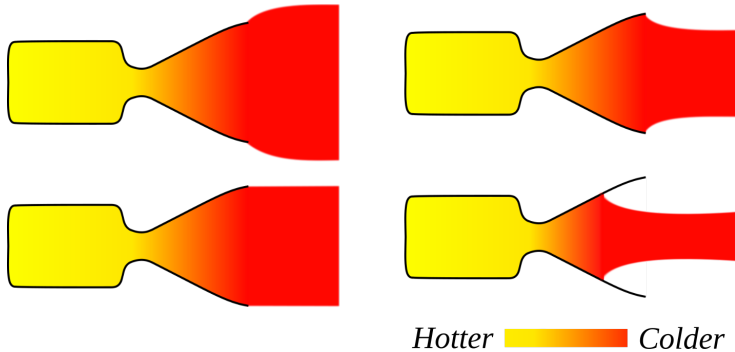


Figure: Nozzle expansion and temperature gradient visualized.

# Specific Impulse

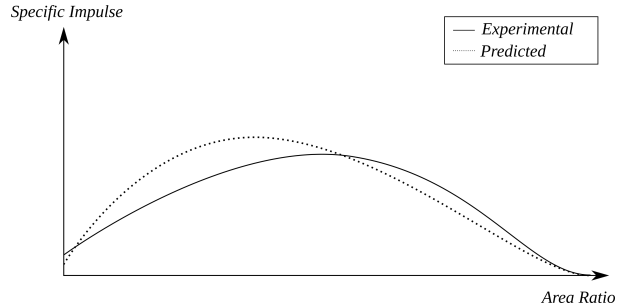
Definition of specific impulse:

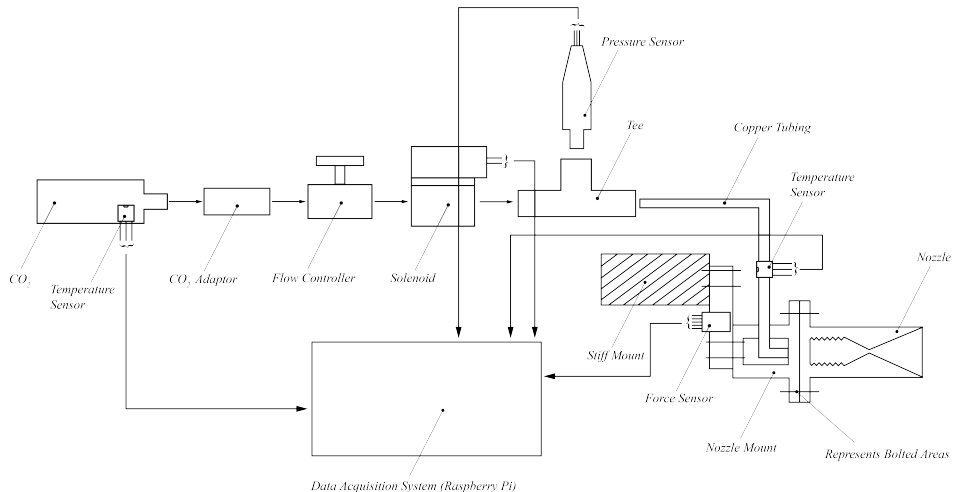
$$I_{sp} = \frac{\text{Thrust}}{\text{rate of mass ejection}} \quad (2)$$

$$I_{sp} = \left( \frac{2\gamma GT_c}{(\gamma - 1)W} \left( 1 - \left( \frac{T_e}{T_c} \right) \right)^{\frac{1}{2}} \right) + \frac{A_e}{A_t} \left( \left( \frac{T_e}{T_c} \right)^{\frac{\gamma}{\gamma-1}} \right) \sqrt{\frac{P_c}{\gamma \rho_c}} \left( \frac{\gamma + 1}{2} \right)^{\frac{\gamma+1}{2(\gamma-1)}} \quad (3)$$

Derived specific impulse

# Develop an Experiment





# Manufacturing

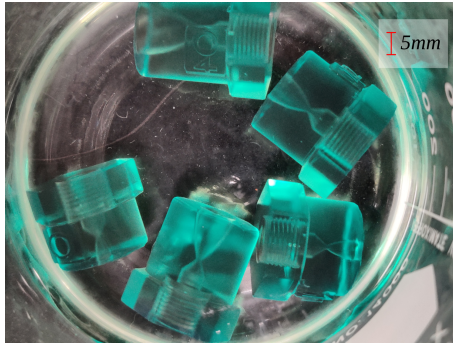
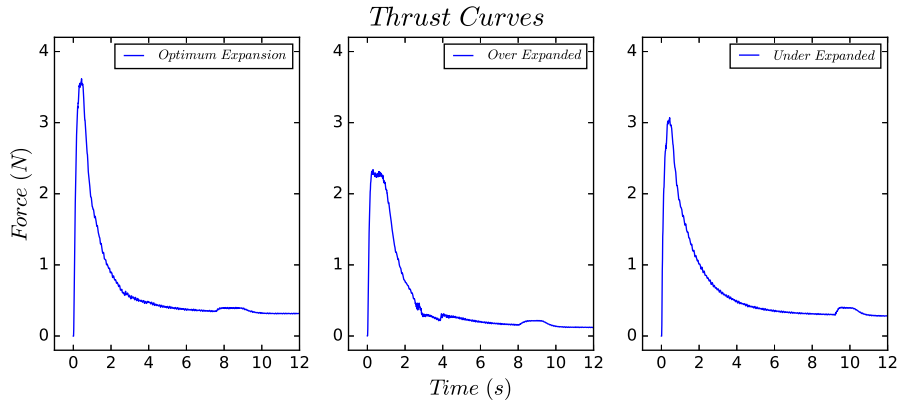


Figure: Nozzles bathing in isopropyl alcohol.



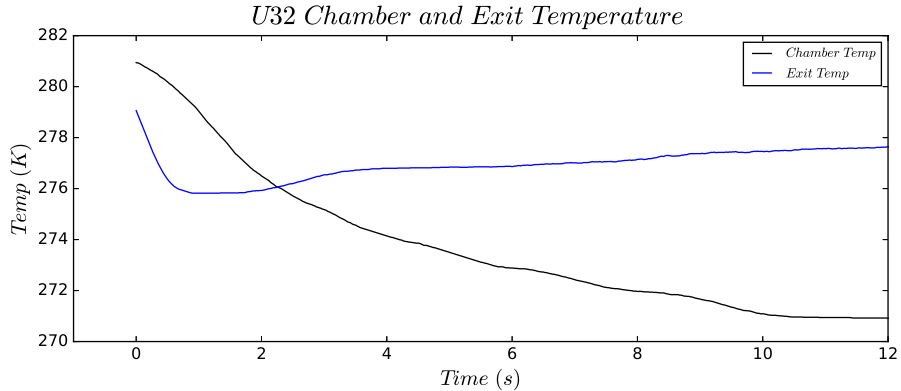
# Data Collection



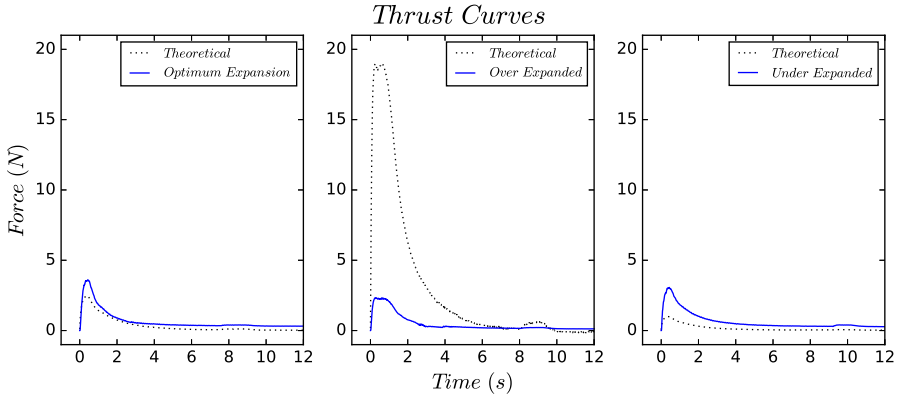
# Analysis

$$F = A_t P_c \left( \sqrt{\frac{2\gamma^2}{\gamma-1} \left( \frac{2}{\gamma+1} \right)^{\frac{\gamma+1}{\gamma-1}} \left( 1 - \frac{T_e}{T_c} \right)} + \left( \left( \frac{T_e}{T_c} \right)^{\frac{\gamma}{\gamma-1}} - \frac{P_a}{P_c} \right) \frac{A_e}{A_t} \right) \quad (4)$$

# Analysis



# Analysis



# Solutions

- Placing thermocouples in better locations
- Measure change in mass over time

# Payload Integration

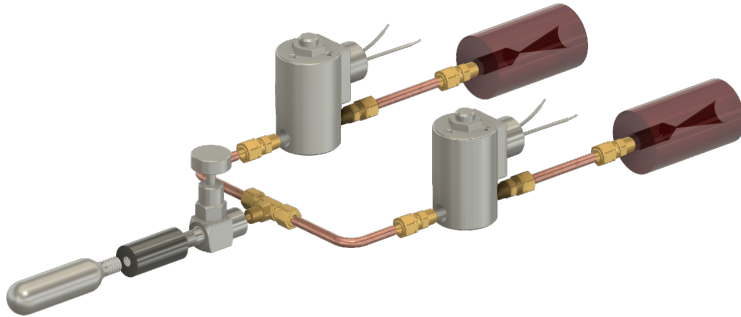


Figure: CAD Render of the plumbing system for my RCS.

# Conclusion

1. Missing some information to complete characterization of the CGT
2. Solid foundation for future work
3. Integration into HABP
4. Flight on board a HAB

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