

# **REACTION CONTROL SYSTEM FOR HIGH ALTITUDE BALLOONS**

Characterizing the Cold Gas Thruster for Reaction Control

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A thesis presented in partial fulfillment for  
Honors in the Bachelor's of Science Degree



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## **Abstract**

Several methods exist which allow scientists to collect various types of data from Earth's atmosphere. High altitude balloons are one of these methods, which provide scientists a cost effective, simple system for data collection. At the cost of simplicity, however they lack control. Sporadic winds in the atmosphere affect data collection for sensors on board these balloon's payloads. A reaction control system would allow stabilization through regions of the atmosphere to allow better data collection. Here, the development of a reaction control system utilizing cold gas thrusters has been outlined. From the decision of fuel to the methods of characterization. An analysis has been done to characterize the behaviour of the thrusters and a high-level outline on future work has been laid out.

## **0.1 Some Context**

This was a two semester project, performed in last year of a Bachelor's of Science Degree. The first semester was spent working to develop the background knowledge and experiment. The second was spent actually setting up the experimental apparatus and data acquisition system; as well as collecting data. However, the University of Central Arkansas began online instruction March 13, 2020 and access to the research labs was limited due to COVID-19. Because of this, some necessary data collection was not completed and progress on the project was halted. The analysis and results that could be completed are discussed here.

In hopes of future work being completed, an outline will be presented for later work to be done.

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# Nomenclature

$\gamma$	Ratio of specific heats
$\omega_z$	Angular velocity about z axis
$a_w$	Acceleration caused by wind
$C$	A constant relevant to the enthalpy at stagnation
$F$	Force or thrust
$F_w$	Force caused by wind
$H$	Enthalpy
$I_w$	Impulse caused by wind
$I_{sp}$	The specific impulse
$J$	The mechanical equivalent of heat
$KE$	Kinetic energy
$M$	Mach number
$m_p$	Mass of propellant
$m_{pd}$	Mass of the payload
$n$	Number of moles
$N1$	No expansion, trial 1
$N2$	No expansion, trial 2
$O1$	Optimum area ratio, trial 1
$O11$	Overexpanded area ratio 1, trial 1
$O12$	Overexpanded area ratio 1, trial 2

$O2$	Optimum area ratio, trial 2
$O21$	Overexpanded area ratio 2, trial 1
$O22$	Overexpanded area ratio 2, trial 2
$O31$	Overexpanded area ratio 3, trial 1
$O32$	Overexpanded area ratio 3, trial 2
$O41$	Overexpanded area ratio 4, trial 1
$O42$	Overexpanded area ratio 4, trial 2
$P$	Pressure
$Q$	Heat put into a system
$R$	Universal gas constant
$r$	Radius
$S$	Entropy
$T$	Temperature
$t$	Time
$U$	Internal energy
$U11$	Underexpanded area ratio 1, trial 1
$U12$	Underexpanded area ratio 1, trial 2
$U21$	Underexpanded area ratio 2, trial 1
$U22$	Underexpanded area ratio 2, trial 2
$U31$	Underexpanded area ratio 3, trial 1
$U32$	Underexpanded area ratio 3, trial 2
$U41$	Underexpanded area ratio 4, trial 1
$U42$	Underexpanded area ratio 4, trial 2
$V$	Volume
$v$	Gas velocity

$W$	Molecular weight of the gas
$W$	Work
$w$	Mass flow rate
$X_c$	Represents some variable, X, in the nozzle chamber
$X_e$	Represents some variable, X, in exit plane of the nozzle
$X_f$	Represents some variable, X, at some final state
$X_i$	Represents some variable, X, at some initial state
$X_s$	Represents some variable, X, at stagnation
$X_t$	Represents some variable, X, in the nozzle throat
$X_x$	Any variable, X at some point, x
$X_x$	Represents some variable, X, at some point x

# **Chapter 1**

## **Introduction**

### **1.1 Background**

High altitude balloons (HABs) are large balloons to which one or several payloads are attached that can reach high altitudes. These payloads are insulated packages typically holding scientific equipment for data collection. Here, high altitude balloon payloads will be referred to as HABPs. Some examples of sensors that may be on board the HABPs are: temperature, altitude, pressure, wind, radiation, and so on. These can provide information for meteorologists and researchers about conditions in high levels of the atmosphere with prolonged data collection. This is unlike other methods of atmospheric data collection like rockets which can also reach these altitudes but do it over a much shorter time-span. HABs can also provide safer, more cost effective options for data collection. However, there are some downfalls of using balloons as a means of data collection. They can be subject to high winds and any on board sensors will be affected by this. For example, during the 2017 total solar eclipse any payloads sent up to observe this would have been subject to winds throughout their flight. This means that camera footage observing the sun's corona would never be stable and set on the subject it is observing. The cameras would be passive observers controlled by the wind rather than the scientist. Another example is Geiger counters observing radiation in the atmosphere. These may have inconsistent data depending on what part of the payload is in its path from the sun. Wind speed sensors will also be subject to the forces of the winds. Keeping up with the inconsistent direction of the payload is a difficult task and the sensor is provided wind speed that is not in any particular direction. This is not ideal to determine the direction of the winds and would require much post-processing to match up the direction the payload was facing at a given wind speed data point. These are only three specific examples, but winds will affect many other data collection systems. The goal of this project is to develop a system that stabilizes the payload against wind speeds.

## 1.2 Outline

The ultimate objective here is to fly a reaction control system on board a HABP. Getting to this point requires several steps. A high-level overview is listed:

1. Determining viability of different RCSs
2. Choosing a RCS
3. Characterizing the chosen RCS
4. Implementing the RCS
5. Ultimate objective

### 1.2.1 Options

The relevant options that were considered for the RCS can be divided into two categories. The first is of the gyroscopic type. These can offer both passive and active stabilization. Reaction wheels (RWs) are commonly used in satellites and telescopes in order to change the attitude of a craft with extreme accuracy. There are also control moment gyroscopes (CMGs) which are essentially reaction wheels mounted on a gimbal controlled by a motor. These produce much higher torques than RWs and more typically provide active stabilization. Both CMGs and RWs rely on electricity as their energy source; while crafts like the International Space Station along with others can utilize solar panels for the longevity of missions, HABs cannot. They would rely on a battery to store all of the energy used to move the craft. Another drawback to these gyroscopic systems is their slow reaction time. These are typically not used for stabilizing a craft throughout a flight. Rather they provide reactions to torques from solar radiation pressure, gravity gradient, magnetic fields, micrometeorite impact, and internal effects like gas leakage and moving parts [3]. In the case of these scenarios it is not a matter of time and unpredictability. Additionally, they rely on motors spinning up to change the direction of the craft which takes considerable time. The other type of option considered here is the thruster type. This takes the form of both combustion and cold gas thrusters. These cannot offer the same amount of accuracy as the former, but can provide extremely fast changes in momentum. They are more commonly used for stabilizing crafts utilizing rockets and rely on compressed air energy storage (CAES) or chemical energy storage rather than electricity.

Of the two, the thruster types have more desirable properties. Primarily in their ability to provide faster changes in the attitude of the craft. Now, the consideration to be made is between the combustion or cold gas thruster. Obviously, sticking combustible fuel on board a HAB is not considered safe so the CGT is more desirable. Also, the design of a CGT system (CGTS) has a lower level of complexity. The choice of system for this project is the CGT.

### 1.2.2 Fuel Options

An in-depth analysis was not necessarily done regarding the choice of the CGT for stabalization in the previous section. So it is important to determine the viability of several types of common fuels. To determine the viability of a CGT, a variable called the specific impulse ( $I_{sp}$ ) must be defined. Equation 1.1 provides the definition of the specific impulse.

$$I_{sp} = \frac{F}{dm_p/dt} \quad (1.1)$$

Where  $F$  is the force and  $dm_p/dt$  is the change in mass of propellant with respect to time. This value provides a *standard* so to speak for characterizing fuels as it describes the force production per some amount of mass of a fuel. Different fuels have different  $I_{sp}$ 's and generally speaking the higher the value the better the fuel.

<sup>1</sup> Additionally, given an impulse, the amount of fuel required to counteract an impulse can be determined. This describes stabalization well. Looking at some sample data from [2], the amount of fuel required to stabilize a flight can be estimated. The raw flight data was not given in form of a .txt or .csv, but plots of the raw data are shown. From this, a digitizer tool was used to extract numbers from the gyroscopic plots. Specifically, the angular velocity about the axial direction ( $\omega_z$ ). Multiplying this by the radius of rotation ( $r$ ) and then taking the derivative with respect to time gives the acceleration ( $a_w$ ) due to the forces ( $F_w$ ) of the wind. Multiplying this by the mass of the payload ( $m_{pd}$ ) then determines the force in the relevant direction due to the wind. Using the theoretical values for the specific impulse of different gases, the mass of fuel needed for a flight could be determined. In other words,

$$a_w = \frac{d(\omega_z r)}{dt} \quad (1.2)$$

$$F_w = m_{pd}a_w \quad (1.3)$$

The integration of all these values would provide the total impulse caused by the wind ( $I_w$ ).

$$I_w = \int |F_w|dt \quad (1.4)$$

$$m_p = \frac{I_w}{I_{sp}} \quad (1.5)$$

In reality equations 1.2, 1.3, and 1.4 are performed for each data point throughout the data set. The derivative is the difference in two points next to each other and the integral is a trapezoidal sum throughout the flight. Also, since the force would take both positive and negative values, the absolute value of each force term was taken.

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<sup>1</sup>It is worth noting the units for  $I_{sp}$  are  $Ns/kg$ , but most sources will record the value in units of  $s$ . While this is not necessarily true to the definition, all that they are doing is multiplying  $m_p$  by the acceleration due to gravity and this makes no difference for the purpose the  $I_{sp}$  is serving here.

### Fuels

The most commonly used gas in a CGT is by far nitrogen; the reason for this is reasonable propellant storage density, performance and lack of contamination concerns [5]. Some other options are  $CO_2$ ,  $H_2$ , and  $He$ ;  $H_2$  having the highest specific impulse. Obviously, the specific impulse is not the only important variable when considered what makes the best fuel for a system. Factors such as safety, availability, cost, energy storage density, and so on all contribute to the choice of gas. The theoretical specific impulse values of the gases listed above are shown in table ???. Along with the specific impulse, the mass required for each gas to stabilize the payload for the total trip is recorded. In the third column, the mass of fuel needed for the time

Gas	$I_{sp}$ (s)	Mass (g)	Mass Ozone (g)
$H_2$	296	172	5
$He$	179	284	8
$N_2$	80	636	18
$CO_2$	67	760	21

the payload spends in the ozone layer is also recorded. It is not always necessary to stabilize the payload throughout the entirety of the flight. In fact, the target may be a specific altitude region so in this case stabilization in other regions is irrelevant. To put these numbers into perspective, the  $CO_2$  cannisters that mountain bikers use to refill their tires are typically 16g cartridges. The  $CO_2$  and the cartridge together weigh approximately 60g. The maximum mass allowed by the FDA for the type of HABP dealt with here is 2721.554g; meaning one of these 16g cartridges is only approximately 2% the total mass of the payload. A 25g cartridge is still only approximately 3.8% the total mass and well within the volume constraints as well. So, at a high-level view, the CGTS is a seemingly viable option.

Since several trials will be recorded availability of the gas is largely important to this project. Out of these gases the availability of  $CO_2$  is by far the highest. Even with the lowest  $I_{sp}$ , it is still an attractive option. Additionally, the actual implementation of the CGT is a distance away from this point in the project. As each gas should behave similarly in the system, it would not be a difficult task to switch the type of gas at any given point during the project. If further analysis finds the specific impulse to be of more importance then  $N_2$  would be the most likely option for the aforementioned reasons.

## 1.3 Characterizing

The characterization of the RCS is referring to fitting the actual results of the system to the pre-existing theory's results. This is referring to the theory discussed in chapter 2. From a high-level, it is likely the assumptions made to generate the mathematical equations do not fit the actual behaviour of the system. In fact, the book, reference [4], from which the actual nozzle theory is taken states the theory produces an error of approximately 12% for actual rocket engines. [\*\*\*\*\*CHECKTHIS] The goal in characterizing the system

is to create a proportionality between the predicted and actual results in order to specify the predicted results for the system developed here. To accomplish this, an on-ground testing rig is built consisting of the same parts to be integrated into the actual payload. The on-ground rig measures variables of interest in the system that will allow the comparison between the predicted and actual results. This will be discussed in more detail in chapter ??, section ?? . In the high-level outline provided, this is the section where progress was halted due to the COVID-19 crisis. From this point further in the project is considered an outline for future work.

## 1.4 Integration

After characterization of the system, the actual integration into a HABP must be made. This is a straightforward task and involves adding another thruster and solenoid to the on-ground testing rig and removing some sensors that are no longer necessary. Then fitting the plumbing into the HABP. Additionally, the scripting for stabilization must be developed further and specified for the characteristics determined. A CAD rendering of the plumbing system is shown in figure ?? . This integration would include simulating windy conditions and determining impulse data from accelerometer sensors to see how the system would work for actual flights. As well as determining the type of feedback system to be used for the RCS script. Examples of these are all negative feedback systems using some type of sensor such as a magnetometer, photoresistor, accelerometer, etc to provide the controller a reference for the pointing direction. This is the point where the amount of fuel needed for a flight objective could be well defined and the necessary changes could be implemented.

## 1.5 Flight

After confidence in the system has been established from the on-ground testing and simulations, the goal and best test is a flight of the RCS. Here, it is important that the system is integrated with a data acquisition system and acts as an aid in the data acquisition. The flight objective has not been well-defined yet. Some vague examples are listed:

- "Look" at a ground target for a duration of the flight
- Take footage of only the sun for a duration of flight
- Record radioactivity with the sensor unobstructed towards the sun through the ozone layer

The system should be robust enough such that completion of these tasks is not a matter of altering the CGTS in any way, but rather altering the scripting and feedback system.

# Chapter 2

## Theory

The objective of this section is to derive the relationships used for the analysis of the data collection. First, the general thermodynamic relationships will be established, then they will be applied to converging-diverging nozzle. At this point, the relevant relationships for the data will be established and the experimental design can be discussed in detail.

### 2.1 General Thermodynamic Relationships

The theory used here is mostly taken from pre-existing nozzle theory. The source for this project is reference [4]. Much of the derivation for the equations to be used are based on the following assumptions and rely on Classical Thermodynamics:

1. The propellant is homogeneous throughout the nozzle.
2. The propellant behaves like a perfect gas.
3. There is no friction between the propellant and the nozzle walls
4. The system is adiabatic
5. The propellant flow is one-dimensional
6. The propellant flow is stagnate in the nozzle chamber
7. The propellant velocity is uniform across any cross-section normal to the nozzle axis

Reference [4] refers to three other assumptions, but they either do not apply or are redundant for the CGTS. Additionally, all of the variables are clearly defined in the nomenclature section but will not be defined along the discussion here.

Starting with the first law of thermodynamics (FLT),

$$dQ = dU + PdV \quad (2.1)$$

and according to the second law,

$$dQ = TdS \quad (2.2)$$

defining the specific heats at constant volume and pressure respectively,

$$c_V = \left( \frac{\partial Q}{\partial T} \right)_V \quad (2.3)$$

$$c_P = \left( \frac{\partial Q}{\partial T} \right)_P \quad (2.4)$$

and using Joule's equation to define a perfect gas

$$\left( \frac{\partial U}{\partial V} \right)_T = 0 \quad (2.5)$$

substituting 2.1 into  $\partial Q$  in 2.3

$$c_V = \left( \frac{\partial U}{\partial T} \right)_V \quad (2.6)$$

Also, substituting ?? into  $\partial Q$  in 2.3

$$c_V = T \left( \frac{\partial S}{\partial T} \right)_V \quad (2.7)$$

so

$$c_V = \left( \frac{\partial U}{\partial T} \right)_V = T \left( \frac{\partial S}{\partial T} \right)_V \quad (2.8)$$

similarly with  $c_P$

$$c_P = \left( \frac{\partial U}{\partial T} \right)_P = P \left( \frac{\partial V}{\partial T} \right)_P \quad (2.9)$$

this means ?? can be written as

$$dQ = c_V dT + PdV \quad (2.10)$$

Considering a perfect gas, the equation of state is

$$PV = nRT \quad (2.11)$$

substituting  $n = m/W$  provides

$$PV = \frac{mRT}{W} \quad (2.12)$$

so the equation for 1 unit of mass is

$$PV = \frac{RT}{W} \quad (2.13)$$

differentiating  $PV$  gives

$$d(PV) = VdP + PdV \quad (2.14)$$

$$= \frac{R}{W}dT \quad (2.15)$$

so

$$PdV = \frac{R}{W}dT - VdP \quad (2.16)$$

Defining a new constant,  $\gamma$

$$\gamma = \frac{c_P}{c_V} \quad (2.17)$$

from this ??, 2.10, and 2.4

$$c_V = \frac{R}{W(\gamma - 1)} \quad (2.18)$$

similarly,

$$c_P = \frac{\gamma R}{W(\gamma - 1)} \quad (2.19)$$

It can also be determined for an adiabat,  $dQ = 0$ , that

$$P_i V_i^\gamma = P_f V_f^\gamma \quad (2.20)$$

From the previous relations and the definition of enthalpy,

$$H = U + pV \quad (2.21)$$

the enthalpy per unit mass can now be expressed as

$$H = \frac{\gamma RT}{W(\gamma - 1)} \quad (2.22)$$

## 2.2 The Nozzle

Until this point, all of these relations are quite general. Figure 2.1 displays a typical converging diverging nozzle. It consists of three important regions. The furthest left is the chamber, it is here that we assume the variables to be stagnate. Stagnate meaning the velocity of the gas is zero. The next section going in the  $+x$  direction is the nozzle throat. This is the smallest cross-sectional area of the system. Next is not a particularly important point, but represents the variables at any point,  $x$ , in the nozzle. Lastly is the exit plane of the nozzle. To apply the previous definitions to a nozzle, the kinetic energy of 1 unit of mass will be considered along with the enthalpy. If the flow of the gas is considered, the enthalpy will increase by the amount equal to the kinetic energy of the gas per 1 unit of mass, given the gas exchanges no heat with the environment

$$KE = \frac{v^2}{2} \quad (2.23)$$

$$H_x = \frac{\gamma RT_x}{W(\gamma - 1)} \quad (2.24)$$

$$H_f = H_x + KE \quad (2.25)$$

A region where the gas is stagnant ( $v = 0$ ) can be considered, here the enthalpy is a constant. Substitutting ?? and the specific volume ( $V = 1/\rho$ ) as well,

$$H_s = C = \frac{\gamma P_s}{W \rho_s (\gamma - 1)} \quad (2.26)$$

$$= \frac{\gamma}{(\gamma - 1)} \frac{P_x}{W \rho_x} + \frac{v_x^2}{2} \quad (2.27)$$

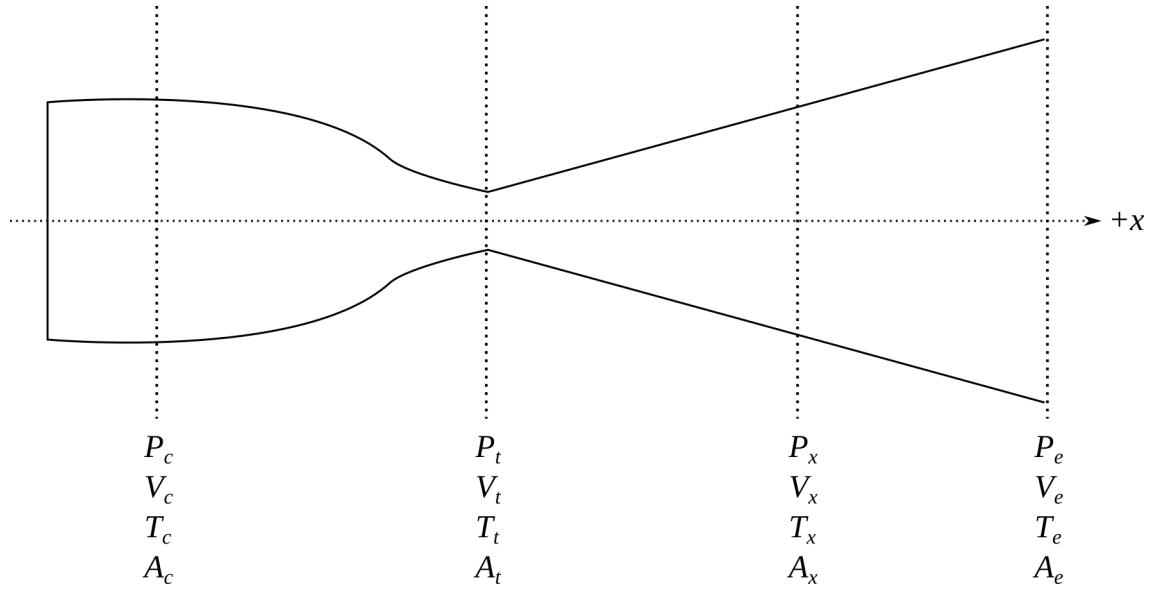


Figure 2.1: Simplified nozzle, with axis and some variables defined.

Now, considering an adiabatic system

$$\frac{V_s}{V_x} = \left( \frac{P_x}{P_s} \right)^{\frac{1}{\gamma}} \quad (2.28)$$

From 2.26 and 2.28 it can be found that

$$\frac{P_x}{P_s} = \left( 1 - \frac{v^2}{2C} \right)^{\frac{\gamma}{\gamma-1}} \quad (2.29)$$

### 2.2.1 Mach Number

An important parameter is the mach number, which is defined as the ratio of the gas velocity at some point to the velocity of sound in the gas. Here, this will be manipulated to determine the parameter in terms of temperature variables.

$$M_x = \frac{v_x}{v_{sound}} \quad (2.30)$$

$$= \frac{v_x}{\sqrt{\gamma R T_x}} \quad (2.31)$$

$$(2.32)$$

This can be substituted into the previously defined relationships to find

$$\frac{T_s}{T_x} = 1 + M_x^2 \frac{\gamma - 1}{2} \quad (2.33)$$

From 2.4 and the fact that the net heat change is equal to the change in kinetic energy per unit mass, the

$$dQ = c_P dT \quad (2.34)$$

$$= c_P(T_x - T_{x+dx}) \quad (2.35)$$

$$= \frac{(v_{x+dx}^2 - v_x^2)}{2J} \quad (2.36)$$

Where  $J$  is defined as

$$J = \frac{W}{Q} \quad (2.37)$$

Substitutting 2.19, using the stagnation conditions for the initial values, and solving for  $v_x$ ,

$$v_x = \sqrt{\frac{2\gamma RT_s}{(\gamma - 1)W} \left( 1 - \left( \frac{P_x}{P_s} \right)^{\frac{\gamma-1}{\gamma}} \right)} \quad (2.38)$$

Now, the velocity of the gas at any point  $x$  is in terms of variables in regions where flow is stagnated. The temperature can be found similarly,

$$T_x = T_s - \frac{v_x^2}{2Jc_P} \quad (2.39)$$

substitutting 2.38 and 2.39 into the mach number

$$M^2 = \frac{2}{(\gamma - 1)} \left( \frac{T_s}{T_x} - 1 \right) \quad (2.40)$$

Lastly,

$$\frac{M_{x+dx}}{M_x} = \frac{v_{x+dx}}{v_x} \sqrt{\frac{T_x}{T_{x+dx}}} \quad (2.41)$$

## 2.2.2 Area Ratio

The expansion ratio is the single most important parameter when designing an efficient nozzle. This is the ratio of the exit plane area to the throat plane area. To introduce the variable, the mass flow rate will be defined.

$$w = \frac{dm}{dt} \quad (2.42)$$

In terms of the geometry of the nozzle, the velocity of the gas, and the density

$$w = A_x v_x \rho_x \quad (2.43)$$

The mass flow rate must be constant throughout any given time in the system. This is the equation of continuity for the flow. The ratio of any two points for a unit mass can now be analyzed,

$$\frac{A_{x+dx}}{A_x} = \frac{V_{x+dx} v_x}{V_x v_{x+dx}} \quad (2.44)$$

Using 2.28 for the general case, 2.40, and 2.41

$$\frac{A_{x+dx}}{A_x} = \frac{M_x}{M_{x+dx}} \left( \frac{T_x}{T_{x+dx}} \right)^{\frac{1}{2}} \left( \frac{1 + \frac{(\gamma-1)}{2} M_{x+dx}^2}{1 + \frac{(\gamma-1)}{2} M_x^2} \right)^{\frac{1}{\gamma-1}} \quad (2.45)$$

The expansion ratio then can be expressed as

$$\epsilon = \frac{A_e}{A_t} = \frac{M_t}{M_e} \left( \frac{T_t}{T_e} \right)^{\frac{1}{2}} \left( \frac{1 + \frac{(\gamma-1)}{2} M_e^2}{1 + \frac{(\gamma-1)}{2} M_t^2} \right)^{\frac{1}{\gamma-1}} \quad (2.46)$$

To determine the best value for the expansion ratio, the mass flow rate will be maximized and using previously found relationships the value for the expansion ratio will be found. Starting with substitutting 2.38 into 2.44.

$$w = \frac{A_x}{V_x} \sqrt{\frac{2\gamma R T_s}{(\gamma-1)W} \left( 1 - \left( \frac{P_x}{P_s} \right)^{\frac{1}{\gamma}} \right)} \quad (2.47)$$

and

$$\left( \frac{T_x}{T_s} \right)^{\frac{1}{\gamma-1}} = \left( \frac{P_x}{P_s} \right)^{\frac{1}{\gamma}} \quad (2.48)$$

Also,

$$\frac{1}{V_x} = \frac{1}{V_s} \left( \frac{T_x}{T_s} \right)^{\frac{1}{\gamma-1}} \quad (2.49)$$

substitutting 2.49 and 2.48 into 2.47 and rearranging

$$w = \frac{A_x}{V_s} \sqrt{\frac{2\gamma K T_s}{(\gamma-1)} \left( \left( \frac{P_x}{P_s} \right)^{\frac{2}{\gamma}} - \left( \frac{P_x}{P_s} \right)^{\frac{\gamma+1}{\gamma}} \right)} \quad (2.50)$$

This can now be maximized by differentiating with respect to  $P_x$  and set equal to zero. This gives

$$\frac{dw}{dP_x} = \frac{A_x}{2V_s} \left[ \frac{2\gamma K T_s}{(\gamma-1)} \left( \left( \frac{P_x}{P_s} \right)^{\frac{2}{\gamma}} - \left( \frac{P_x}{P_s} \right)^{\frac{\gamma+1}{\gamma}} \right) \right]^{-\frac{1}{2}} * \frac{d}{dP_x} \left( \left( \frac{P_x}{P_s} \right)^{\frac{2}{\gamma}} - \left( \frac{P_x}{P_s} \right)^{\frac{\gamma+1}{\gamma}} \right) = 0 \quad (2.51)$$

Obviously,

$$\left( \left( \frac{P_x}{P_s} \right)^{\frac{2}{\gamma}} - \left( \frac{P_x}{P_s} \right)^{\frac{\gamma+1}{\gamma}} \right) \neq 0 \quad (2.52)$$

so

$$\frac{d}{dP_x} \left( \left( \frac{P_x}{P_s} \right)^{\frac{2}{\gamma}} - \left( \frac{P_x}{P_s} \right)^{\frac{\gamma+1}{\gamma}} \right) = 0 \quad (2.53)$$

differentiating and solving for  $P_x/P_s$

$$\frac{P_x}{P_s} = \left( \frac{2}{\gamma+1} \right)^{\frac{\gamma}{\gamma-1}} \quad (2.54)$$

Now, substitutting ?? it can be seen that

$$\frac{T_x}{T_s} = \frac{2}{\gamma+1} \quad (2.55)$$

which when compared to 2.33 it is seen that they are equal when if  $M = 1$ , and if  $x = t$ , then the optimum value for  $P_t$  can be determined. When  $M = 1$  at the throat is not necessarily the only condition which maximizes  $w$  but it is also a condition which satisfies maximum force production of the nozzle.

This will be finished at a later date. IT IS BED TIME!!!! Determine maximum value for  $w$  and find best expansion ratio use that to find values for expansion ratio (in methods section) determine force equation determine the Isp equation

## 2.3 Relationships

\*explain about the redefining of equations for use of better variables the nozzles used for the system

RELEVANT EQUATIONS:

$$F = A_t P_c \left( \sqrt{\frac{2\gamma^2}{\gamma-1} \left( \frac{2}{\gamma+1} \right)^{\frac{\gamma+1}{\gamma-1}} \left( 1 - \frac{T_e}{T_c} \right)} + \left( \left( \frac{T_e}{T_c} \right)^{\frac{\gamma}{\gamma-1}} - \frac{P_a}{P_c} \right) \epsilon \right) \quad (2.56)$$

$$I_{sp} = \left[ \frac{2\gamma R T_c}{W(\gamma-1)} \left( 1 - \frac{T_e}{T_c} \right) \right]^{\frac{1}{2}} + \left[ \left( \frac{T_e}{T_c} \right)^{\frac{\gamma}{\gamma-1}} - \frac{P_a}{P_c} \right] \frac{A_e}{A_t} \sqrt{\frac{P_c}{\gamma \rho_c}} \left( \frac{\gamma+1}{2} \right)^{\frac{\gamma+1}{2(\gamma-1)}} \quad (2.57)$$

# Chapter 3

## Methods

The objective is to determine the difference between the measured specific impulse and the theoretical values. To determine the experimental value for the specific impulse is a matter of measuring the force production of the nozzle and the change in mass of the system. This is done with the use of two force sensors. One measuring the change in mass of the  $CO_2$  cylinder and the other measuring the force production of the nozzle. To determine the theoretical values for the same system requires measuring  $T_c$ ,  $T_e$ ,  $P_c$ , and  $P_a$  where the ambient pressure is a constant and can be determined from the forecast that day. The same variables are needed for the predicted force equation. This information is coming from equations 2.56 and 2.57. It is important that these variables are represented well by the data collected, however the experimental setup used in the data collection presented here does a poor job of this. The setup and methods will be presented here along with solutions to the problems faced.

### 3.1 On-Ground Testing Rig

A simplified schematic of the experimental apparatus is shown in figure 3.1.

#### 3.1.1 Hardware

All of the parts, except the  $CO_2$  adaptor and pressure transducer were ordered from McMaster-Carr. The adaptor was custom machined and the transducer was purchased from a third party seller with no datasheet provided. However, the voltage output from it varied linearly with pressure and could be calibrated with a simple linear regression function. The solenoid is a 24V DC 1000PSI solenoid valve, it was controlled by a simple digital signal run through a push pull (NPN-PNP pair) amplifier. Each temperature sensor was a type k thermocouple, interfacing with a XXXXXXX\* breakout board made by Adafruit. The force sensor used was a 1kg load cell interfacing with an HX711 (24-bit analog to digital converter) breakout board. The plumbing system used is 1/4" OD copper tubing with compression fittings that allowed adaptations between

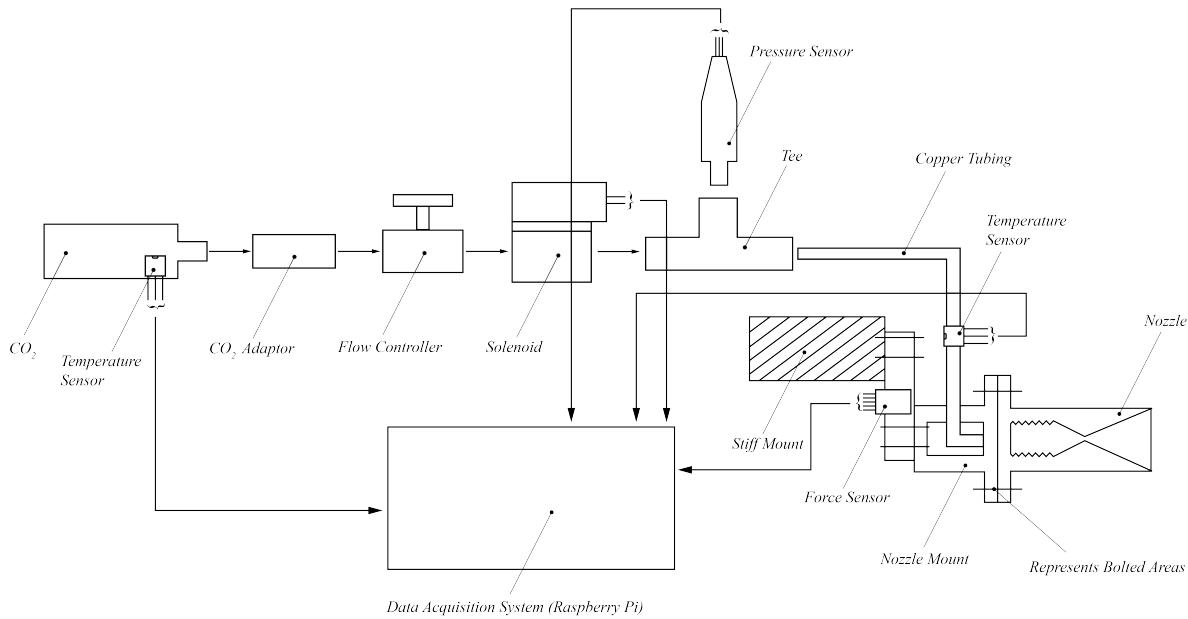


Figure 3.1: Simplified on-ground testing rig

the copper pipe and the 1/8" National Pipe Threading (NPT) that was used for the non-pipe fittings. The choice of this plumbing system is the high pressure rating and relatively low weight. The most massive part of the system was the solenoid valve budgeting approximately 10% \*\*\*\*CHECK THIS the maximum allowed weight of the HABP. On final thought, a choice was made to omit the flow controller because the mass flow rate should be limited by the nozzle throat.<sup>1</sup>

### 3.1.2 Nozzle Manufacturing

Several options were considered for the manufacturing of nozzles. These included the processes listed below:

- Fused deposition modeling (FDM) 3D printing
- Resin 3D printing
- Machining by hand
- Modeling and casting by hand

However, in dealing with such small parts modeling and casting by hand was immediately discarded. Modeling differences of expansion ratios on the scale of parts of a millimeter was out of the question. Machining by hand is both costly in terms of money and time. Also, such small nozzles would present difficulties in the machining process. FDM 3D printing was by far the most accessible out of these, but there are problems related to both accuracy and actual function of the nozzles. FDM 3D printers typically use a .4mm nozzle.

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<sup>1</sup>This, however, was not necessarily the best decision. This will be discussed further in 5

This limitation on accuracy is relatively large considering the nozzle throat is designed to be no larger than .625mm in diameter. Also, the .4mm nozzle refers to the actual size of the hole in the nozzle, *not* the size of the filament extruded from the nozzle. FDM printers typically produce layer heights no smaller than .1mm. In addition to the problem of accuracy, the parts are relatively porous. The method of FDM printing calls for the extrusion of a hot filament onto a cooled layer of filament to produce a 3D model. This does well creating structural parts not dependent on high tolerances and do not need to be air-tight, but for a CGT nozzle it will not work well. Much of the fuel would be lost in the layers of the nozzle and the friction between the layers and exhaust gases would be more so than any of the other methods. This leaves resin printing, often referred to as stereolithography (SLA) printing. This method has been out of reach for many in years past, but recent manufacturers have developed robust, inexpensive resin printers. These printers can provide layer heights of .01mm and do not rely on laying lines of hot filament on top of other layers. Rather, they use two main methods of creating the part. The cheaper versions use a 5.5x3.5in UV LCD screen with resolutions of approximately 2560x1400 pixels. These resolutions are much finer than the FDM printer's capabilities. Additionally, these layers are formed by a chemical curing of one layer of resin to the previous. Given no impurities in the resin, this will provide an air-tight seal in the part. Figure 3.2 shows a pressure test that was performed on a printed part, similar to the designed nozzles. The part was essentially an end cap, filled

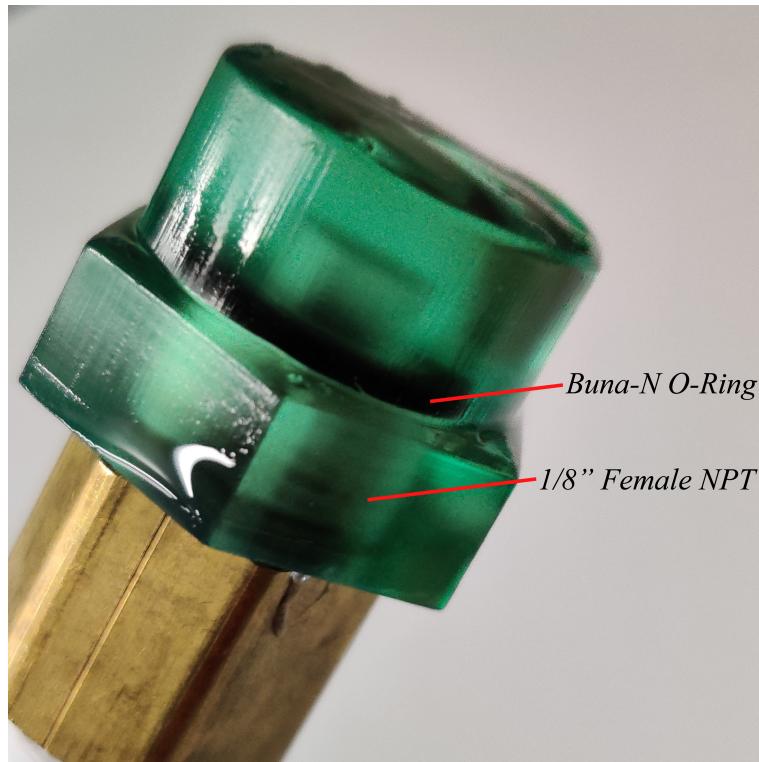


Figure 3.2: Pressure test of resin print from the ELEGOO MARS 3D printer

in increments of 20psi up to 400psi. It was held at 400psi for 6 hours and it held that pressure with no noticeable change in the needle on the gauge throughout that time. Similar tests with FDM printed parts

held no pressure, even after being treated with an epoxy coating. For comparing the accuracy of the parts, several prints were done. Figure 3.3 displays an example of the difference in detail and figure 3.4 shows a closeup of the two at the same scale.

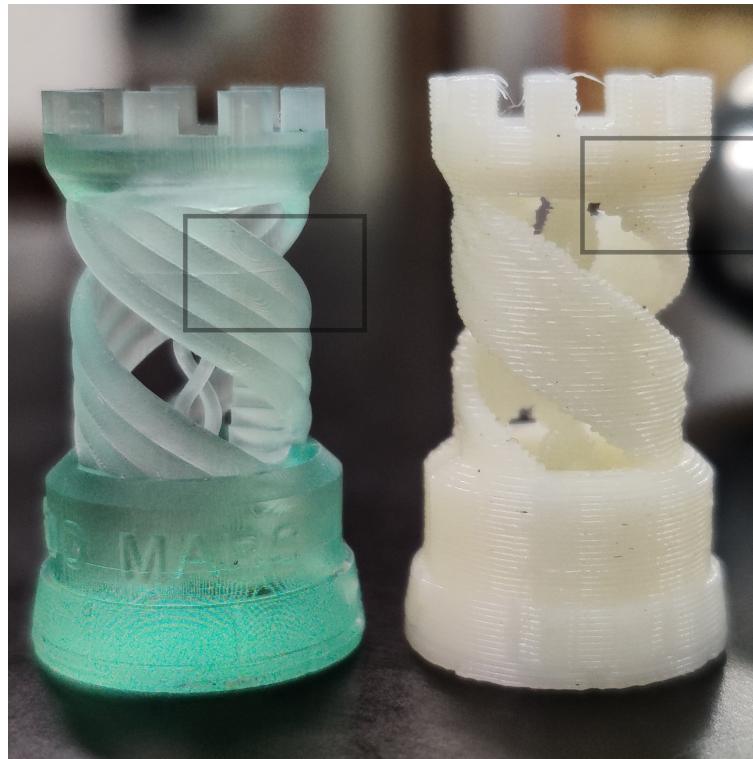


Figure 3.3: Two 3D printed rooks for detail comparison. On left, resin and on right, FDM

The layer height for the resin printed part was set to .05mm and the FDM is .25mm. The difference is easily noticed.

Nozzle design was done in two programs. First, the nozzle geometry was made in OpenSCAD. An open source program was used to set the parameters for the nozzle geometry. A .stl file was generated from OpenSCAD and imported into Blender. From here, the actual functional parts were added to the model like the hex flatends, NPT fitting, exterior walls, and labelling. Figure ?? shows several nozzles begin cleaned in isopropyl alcohol (IPA). The actual nozzle geometry can be seen while the part is covered in IPA.

### 3.1.3 Data Acquisition System

RASPBERRY PI STUFF

### 3.1.4 Anything else??

## 3.2 What tf is wrong here?

Most of it...



(a) Resin printed rook closeup



(b) FDM printed rook closeup

Figure 3.4: Rook closeups

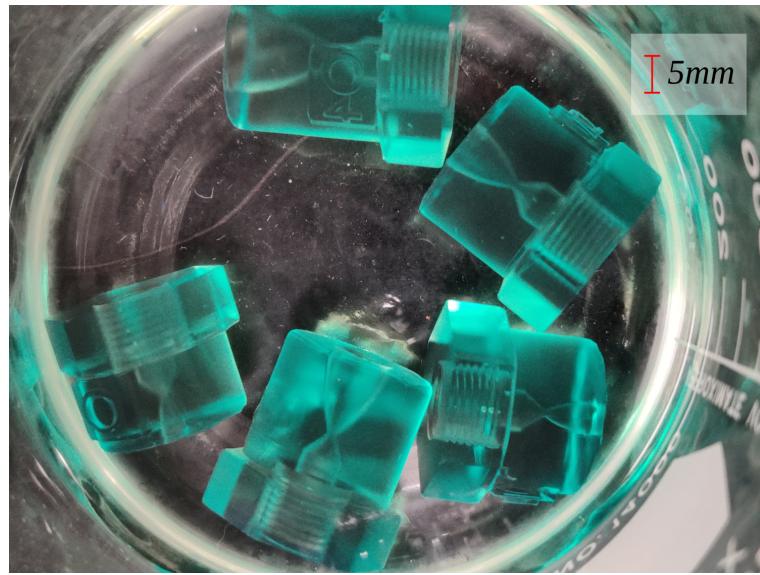


Figure 3.5: Several 3D printed nozzles bathing in IPA

# Chapter 4

## Analysis

### 4.0.1 Data Collection

The data taken was for the variables in equation ???. There were a total of 10 nozzle expansion ratios used with 2 trials each. The expansion ratio kept  $A_t$  constant and varied  $A_e$ . There were 4 over expanded, 4 underexpanded, 1 optimum, and 1 with no expansion. The naming scheme goes something like ERT, where E stands for either U (Underexpanded), N (None), or O. O stands for either optimum or overexpanded. R is the ratio number (1-4) except in the case that there is no third character. In this case the O stands for optimum, which there is only one of. T stands for trial number which can be either 1 or 2. So for example, U22 is underexpanded, ratio number 2, trial number 2. O1 is optimum ratio, trial number 1. These are explicitly defined in the nomenclature section. This naming scheme will be updated in future experiments because it was slightly problematic in the analysis of the data.

#### Data Sensors

There should be some light discussion on the sensors used for data collection. There was a single pressure transducer located near the inlet of the nozzle, a thermocouple located on the nozzle, a thermocouple located inside of the adaptor that the  $CO_2$  connected to the rest of the plumbing, and a load cell setup to measure the thrust produced from the CGT. For sake of simplicity I will refer to these as "sensors" preceded by the variable they measured. So, respectively,  $P_c$  sensor,  $T_e$  sensor,  $T_c$  sensor, and  $F$  sensor. Additionally,  $\gamma$  is dependent on temperature, but only changes slightly in the temperature differences noticed here. In later models,  $\gamma$  will be set to be a function of temperature for greater accuracy. For now it is not necessary because the force has a small dependence on  $\gamma$  compared to the temperature. So, for the sake of this project  $\gamma$  is a constant. The data acquisition system was running python on a RaspberryPi 3 and since all of these sensors are analog devices 2 different analog-to-digital converters (ADCs) was used to interface with the Pi. The  $P_c$ ,  $T_e$ , and  $T_c$  sensors interfaced with a 10-bit ADC and the  $F$  sensor interfaced with a 24-bit ADC. In future experiments, a

24-bit ADC will be used for all data acquisition because of the limited resolution with the 10-bit ADC. This is especially evident with the thermocouple data. All of the python scripts for data collection are available at my [GitHub repository](#).

The code began the experiment after all sensors were calibrated and functioning properly. Data collection ran until the force production was below a certain threshold for a predefined number of points. This would also need to be updated because often times the force sensor would lose its zero position so defining the threshold value was not so easy. A better method would be using the change in force to determine when the experiment was over. This would work well because the force is transient until the  $CO_2$  was all spent. After it was over the mass of the  $CO_2$  canister was measured. All of this data was written to two separate .txt files. One included the calibration values for the sensors and changes in mass, the other included  $P_c$ ,  $T_c$ ,  $T_e$ , and  $F$ . The previous was not recorded in a useful format and later work had to be done to resolve this. In the future this should be updated. The latter was simply comma delimited and worked fine for reading into python for analysis. The data files can be found at this [GitHub repository](#) as well.

#### 4.0.2 Initial Analysis

To begin the analysis, simple plots were made to look at the sensor data over time. Immediately, it was found that the temperature data is quite poor! The resolution of the ADC is evident in the discrete steps that the temperature takes. Figure 4.1 shows an example of the temperature data. The limited resolution

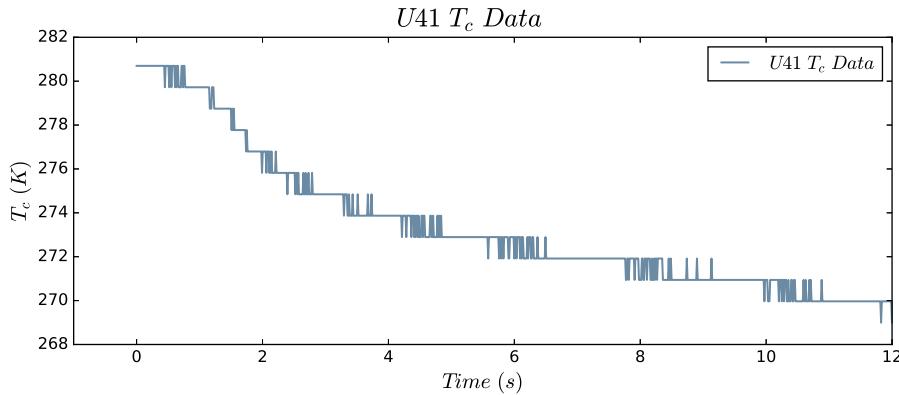


Figure 4.1: Example plot of the temperature over time for a trial

of the ADC can be seen quite clearly. However, this is not terribly problematic and several things can be done to smooth the curve. Since smoothing this data is not the objective here, I have simply taken a function from the pandas python library that handles smoothing quite well. It uses a moving averages method. The smoothed plot is shown in figure 4.2. There are additional problems that come with smoothing data, though. The total number of points is typically reduced and therefore all of the data that is going to

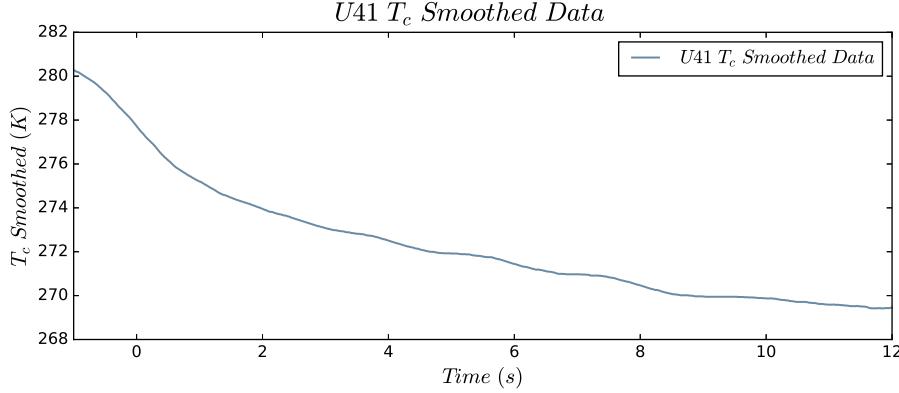
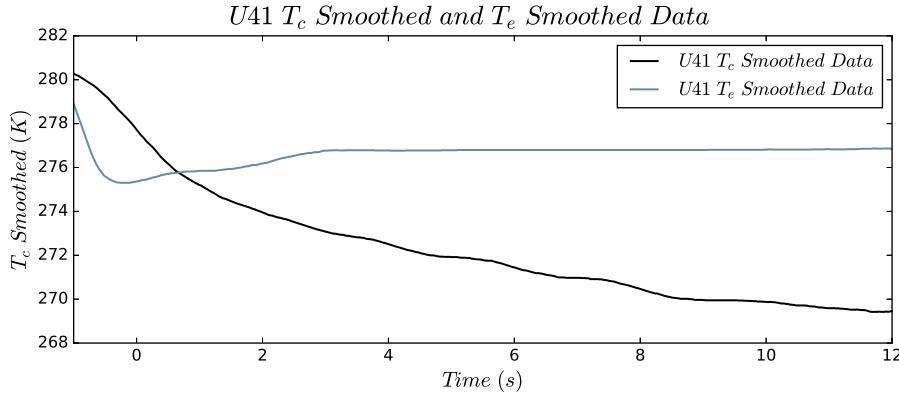


Figure 4.2: Example plot now smoothed

be used must then be smoothed by the same factor. Also, the data is shifted to the left as can be seen from figures 4.1 and 4.2. Alternatively, a function could be fit to the data and this would allow the possibility of a continuous data set. For now though, there are bigger problems with the data recorded. Figure 4.3 shows the two different temperature data sets plotted against time for one of the trials. It can be seen immediately

Figure 4.3: Smoothed  $T_c$  and  $T_e$  plotted with time for one of the trials

that at some point the  $T_c$  line drops below the  $T_e$  line. Looking back at equation ?? this is troublesome. This means that  $\left(1 - \frac{T_e}{T_c}\right) < 0$  giving an overall negative sign under the square root. Obviously the force produced is not imaginary, so either the data collected for these temperatures is not representative of the actual variables or the theory is wrong. It is obvious that the former is the problem for several reasons. The first is that the  $T_c$  variable represents the temperature directly before the converging section of the nozzle.  $T_e$  is the temperature of the exit plane of the nozzle. The two thermocouples are not placed in these regions. Admittedly, there was not enough attention when inspecting the theory to develop the experiment. Under normal circumstances some simple changes would be made and new data would be taken, however due to the closure of the university nothing can be done about collecting new data. Because of this we will proceed with what analysis can be completed and use a more general approach to characterizing the CGT. First, I've

plotted the predicted force with the experimental force in figure 4.4. As expected, we see segments where the

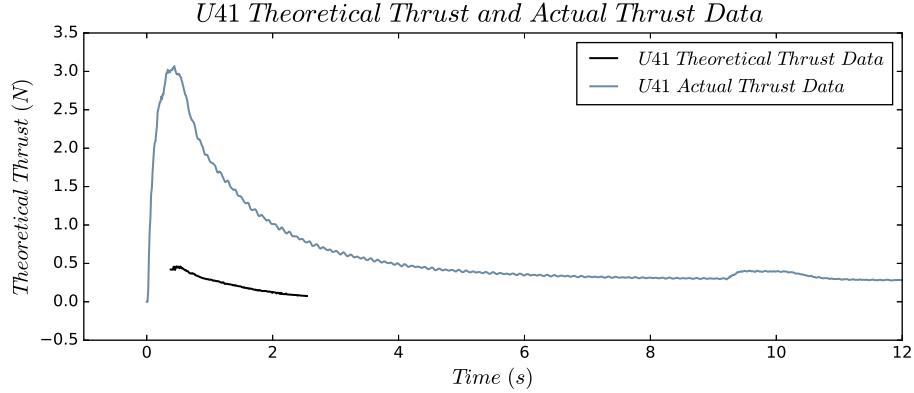


Figure 4.4: First attempt at plotting the thrust and predicted thrust against time

force is undefined due to a runtime error in the numpy package. What can be done here? Well, some more consideration should be taken into the theory. Starting with a gas obeying the ideal gas law in an adiabatic system.

after some substitution we can obtain 4.1.

$$\left(\frac{P_x}{P_{x+dx}}\right)^{\frac{\gamma-1}{\gamma}} = \frac{T_x}{T_{x+dx}} \quad (4.1)$$

now, if  $P_x = P_c$  and  $P_{x+dx} = P_e$ , we can look at this negative sign more intuitively. We know that a nozzle will never function properly in a state where the exit plane pressure is less than the chamber pressure. Also, since the  $\gamma$  value is always greater than 1, the overall term will be greater than 1 which means the exit plane temperature must always be less than the chamber temperature. In other words, we know  $P_c > P_e$  and  $\gamma > 1$  therefore,  $\left(\frac{P_c}{P_e}\right)^{\frac{\gamma-1}{\gamma}} > 1$  which also means  $T_c > T_e$  always. Additionally, since gases cool as they expand, it is sensible that the chamber will be warmer than the exit plane of the nozzle.

At this point, confidence has been established in the theory and changes should be made to the experimental setup. Again, unfortunately, these changes cannot be made but we will continue with the analysis regardless.

#### 4.0.3 Attempt at Reconciliation

The most obvious way to resolve the negative sign is to include an absolute value around the problematic term. This solves the runtime error, but is unfounded. We know the optimum nozzle expansion ratio should have the largest thrust production, but we have essentially removed  $T_e$ 's dependence on the expansion ratio in doing this. This means the thrust will be highest for the value which has the greatest expansion ratio which is geometry O4. This can be seen in figure 4.5. I have plotted several trials there and included the predicted force according to equation ???. O4 is indeed the largest thrust curve. Also, in viewing these thrust curves it is important to recognize the predicted force is the predicted force per unit mass, but the actual curve is per some different mass value. However, the unit for the mass can be set to some convenient unit

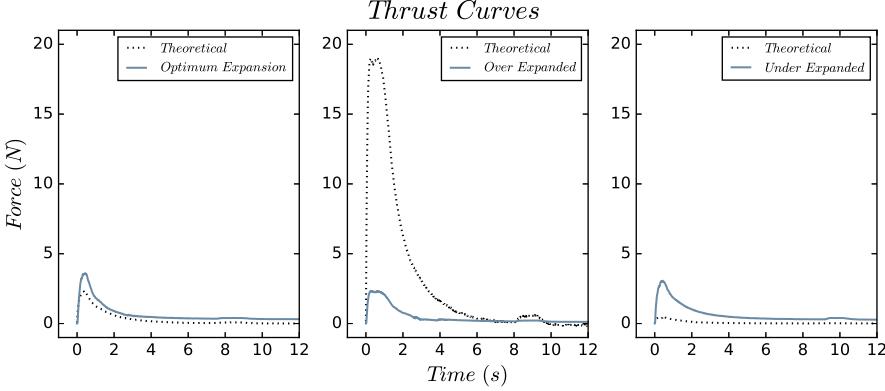


Figure 4.5: Several trials thrust curves plotted with the predicted thrust

and be compared through all the data. This won't change the actual analysis and design conditions.

Tacking on an absolute value will not only fail to resolve the issue here but it is also unfounded. The next thought is to solve for  $T_e$  in terms of the other available variables. It turns out that  $T_e$  can be put in terms of  $T_c$ ,  $P_c$ ,  $A_e$ ,  $\rho_c$ , and  $w$ . Unfortunately, there are several problems with this. The first is that the change in mass, the mass flow rate, was only measured as an initial and final value. Meaning the total mass used throughout the experiment is known, but the mass flow rate throughout is not. For now, the assumption will be made that the mass flow rate is constant. Next, as can be seen from equation 4.2  $T_e$  cannot be solved algebraically. It is not difficult to solve for it computationally though.

$$T_e = T_c \left[ \frac{\gamma - 1}{2\gamma P_c \rho_c} \left( \frac{w}{A_e} \right)^2 \left( \frac{T_c}{T_e} \right)^{\frac{\gamma+1}{\gamma-1}} + 1 \right]^{-1} \quad (4.2)$$

The simplest method is to use the relaxation method as described in [?]. The process is to iterate the equation by plugging in  $T_e = 1$  on the right side, finding a new value for  $T_e$  on the left side, substituting this value back into the right side, and so on.  $T_e$  should converge to a value and that is the solution for  $T_e$ . Using this method, I've made the same plots in figure 4.6 as in figure 4.5. The similarity between the two figures is

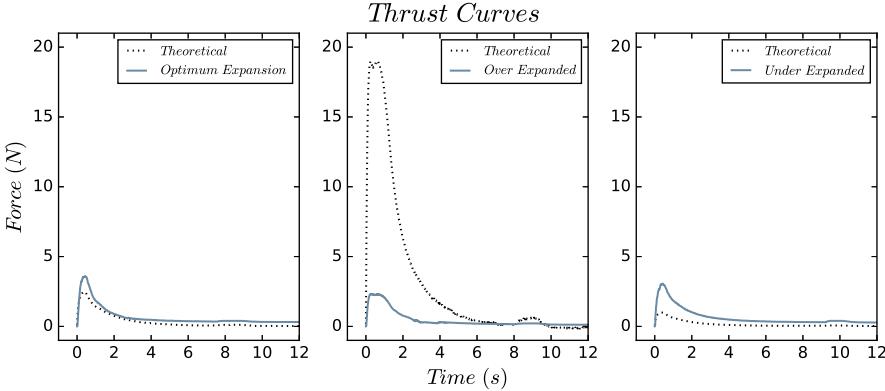


Figure 4.6: Several trials thrust curves plotted with the predicted thrust

quite apparent. At first glance, they nearly look the same, but looking at the far right plot the theoretical curve can be seen to be different from the other. The reason for this is because the assumption made about the mass flow rate being constant through time was naive. The mass flow rate, at any point  $x$  can be defined by equation 4.3.

$$w_x = A_x v_x \rho_x \quad (4.3)$$

Both the velocity and density of the gas have dependence on pressure and temperature so  $w$  is *not* constant with respect to time. That is not to say it is not constant at any given time throughout the entire system, however. If  $T_e$  is not represented correctly it is clear that the result is that the nozzle with the largest expansion ratio is predicted to function best because of equation ??'s dependence on  $A_e$ .

In the end, there is not much reconciliation that can be done for the poor data collection. What we can look at effectively is the experimental value for the specific impulse. Unfortunately, this won't tell much because the theoretical values cannot be calculated for the same reasons as the force. Additionally, it is not ideal to look at the specific impulse over the entire experiment because the temperature and pressure are so transient. However, since the change in mass is only known for two data points it is the best that can be done. Determining these values is a simple trapezoidal sum over all time. I've tabulated all of these in table 4.1. There isn't much to see here, except that the values found are close to the known values from

Geometry	<i>Trial 1</i> $I_{sp}$	<i>Trial 2</i> $I_{sp}$
N	61.1	54.0
U4	58.0	44.1
U3	33.5	52.8
U2	62.5	60.3
U1	33.9	62.6
O	57.5	37.3
O1	58.6	59.5
O2	50.5	48.3
O3	29.0	60.3
O4	44.6	56.0

Table 4.1: Experimental specific impulses

reference [1]. The  $I'_{sp}$ 's dependence on temperature and pressure means that these values are meaningless without the theoretical values at the same pressure and temperature. Reference [1] is using values for the maximum possible  $I_{sp}$  values.

## **Chapter 5**

## **Discussion**

## **Chapter 6**

## **Conclusion**

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## **Appendix A**

### **Appendix Title**

Some appendix stuff here