Diode Applications: Rectifiers and Power Supplies

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Diode Applications Overview

Why Study Rectifiers?:

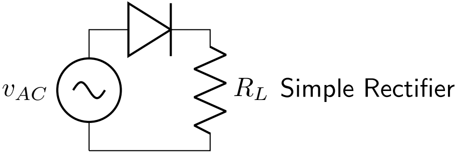
- Most electronics need DC power
- Wall outlets provide AC power
- Rectifiers convert AC to DC
- Foundation of power supplies

Key Applications:

- Battery chargers
- Computer power supplies
- LED drivers
- Motor controllers

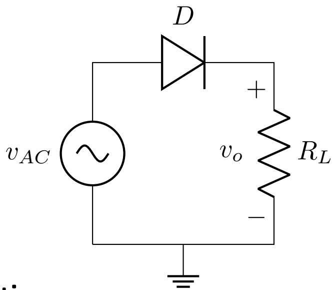
Topics We'll Cover:

- Half-wave rectifiers
- Full-wave rectifiers
- Bridge rectifiers
- Filtering capacitors
- Ripple voltage
- Voltage regulation with Zeners



Half-Wave Rectifier Circuit

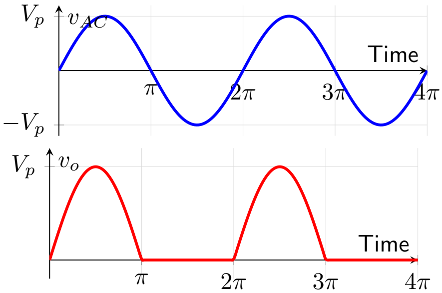
Basic Circuit:



Operation:

- Input: $v_{AC} = V_p \sin(\omega t)$
- Positive half-cycle: diode ON
- Negative half-cycle: diode OFF
- Output: positive half-waves only

Waveforms:



Half-Wave Rectifier Analysis

Average (DC) Output Voltage:
For ideal diode ($V_D = 0$):

$$V_{DC} = \frac{V_p}{\pi} \approx 0.318 V_p$$

For real silicon diode ($V_D \approx 0.7$ V):

$$V_{DC} = \frac{V_p - V_D}{\pi}$$

Peak Inverse Voltage (PIV):

- Maximum reverse voltage on diode
- PIV $= V_p$
- Must select diode with PIV $> V_p$

Example Calculation:
Given: $V_{AC,RMS} = 12$ V

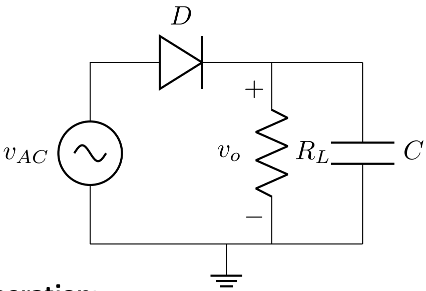
1. Peak voltage:
   $V_p = \sqrt{2} \times V_{RMS} = 16.97$ V
2. Calculate DC output:
   $V_{DC} = \frac{16.97 - 0.7}{\pi} = \frac{16.27}{\pi} = 5.18$ V
3. PIV requirement:
   PIV ≥ 16.97 V

Limitations:

- ☹ Low DC output (only 31.8%)
- ☹ Poor power utilization
- ☹ Large ripple voltage

Half-Wave Rectifier with Filter Capacitor

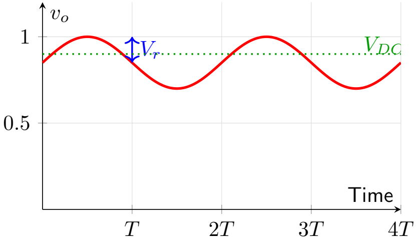
Filtered Rectifier:



Operation:

- Capacitor charges to $\approx V_p$
- Capacitor discharges through R_L
- Creates "ripple" voltage
- DC voltage higher than unfiltered

Output Waveform:



Ripple Voltage:

$$V_r \approx \frac{V_p}{f R_L C}$$

Ripple Voltage Analysis

Key Equations:
Ripple voltage (peak-to-peak):

$$V_r \approx \frac{V_p}{f R_L C}$$

DC output voltage:

$$V_{DC} \approx V_p - \frac{V_r}{2}$$

Ripple factor:

$$r = \frac{V_{r,RMS}}{V_{DC}}$$

Design Guidelines:

- ☺ Larger C reduces ripple
- ☺ Larger R_L reduces ripple
- ☺ Higher frequency reduces ripple

Example:
Given:

- $V_p = 17$ V
- $f = 60$ Hz
- $R_L = 2.2$ kΩ
- $C = 470\ \mu$F

Calculate ripple:

$$V_r = \frac{17}{60 \times 2200 \times 470 \times 10^{-6}} = 0.274 \text{ V}$$

$$V_{DC} = 17 - \frac{0.274}{2} = 16.86 \text{ V}$$

Trade-offs:

- Large C: less ripple, larger size
- Peak diode current increases with C

Bridge Rectifier Circuit

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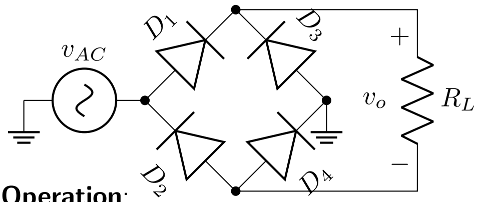
Bridge Configuration:



Operation:

- Positive half-cycle: D_1, D_4 conduct
- Negative half-cycle: D_2, D_3 conduct
- Both half-cycles produce output
- Two diodes always in series

Output Characteristics:

- v_o is always positive
- Output is full-wave rectified
- Continuous current through load

Advantages:

- ☺ No center-tap transformer needed
- ☺ Full-wave rectification
- ☺ Higher DC output
- ☺ Lower ripple frequency ($2f$)

Disadvantages:

- ☹ Two diode drops (≈ 1.4 V)
- ☹ Requires four diodes

Bridge Rectifier Analysis

DC Output Voltage:
For ideal diodes ($V_D = 0$):

$$V_{DC} = \frac{2V_p}{\pi} \approx 0.637V_p$$

For real silicon diodes ($V_D \approx 0.7$ V each):

$$V_{DC} = \frac{2(V_p - 2V_D)}{\pi}$$

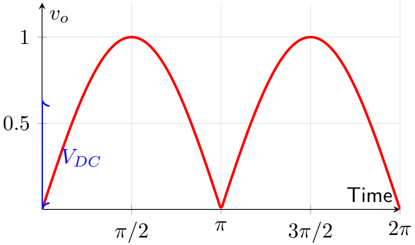
Peak Inverse Voltage:

- Each diode: PIV $= V_p$
- Lower than center-tap configuration

Comparison to Half-Wave:

- DC output is 2x higher

Output Waveform:



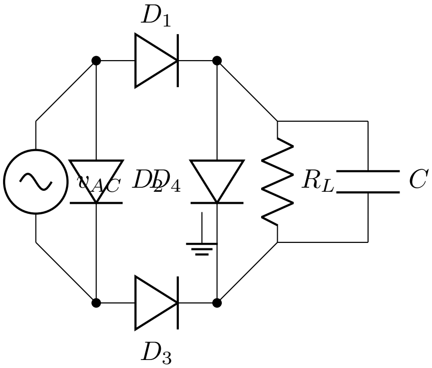
Example:
$V_{AC,RMS} = 12$ V, $V_p = 16.97$ V

$$V_{DC} = \frac{2(16.97 - 1.4)}{\pi} = \frac{31.14}{\pi} = 9.91 \text{ V}$$

Compare to half-wave: 5.18 V (nearly 2x

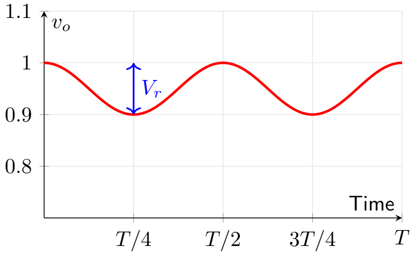
Bridge Rectifier with Filter

Filtered Bridge Rectifier:



Key Difference:
Ripple frequency is **2**f (120 Hz for 60 Hz

Output Waveform:



Design Example:
Same parameters as before, but $f \to 2f$:

$$V_r = \frac{17}{2 \times 60 \times 2200 \times 470 \times 10^{-6}}$$

$$= \frac{17}{\;} = 0.137\ \text{V}$$

Need for Voltage Regulation

The Problem:

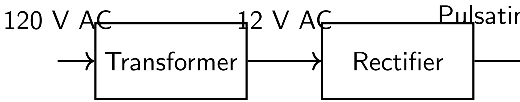
- Rectifier output varies with:
  - Input (line) voltage changes
  - Load current changes
  - Ripple voltage
- Most circuits need stable DC
- Example: Logic circuits need $\pm 5\%$ tolerance

The Solution:

Voltage regulator:

- Maintains constant output voltage
- Compensates for input variations
- Compensates for load variations
- Types: Linear, switching, Zener

Block Diagram:

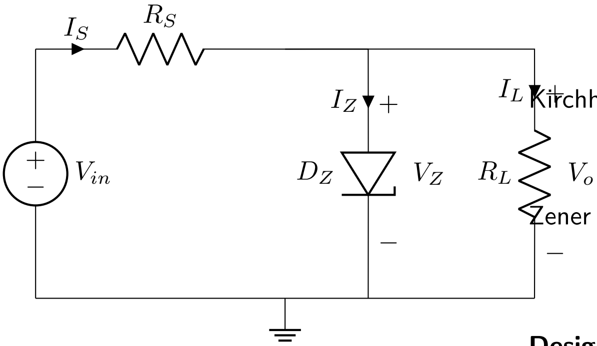


Performance Metrics:

- **Load regulation**: how much V_o changes with load
- **Line regulation**: how much V_o changes with input
- **Efficiency**: P_{out}/P_{in}

Zener Diode Shunt Regulator

Basic Shunt Regulator:



Operation Principle:

- Zener maintains constant V_Z

Key Equations:

Series resistor current:

$$I_S = \frac{V_{in} - V_Z}{R_S}$$

Kirchhoff's current law:

$$I_Z = I_S - I_L$$

Zener power dissipation:

$$P_Z = V_Z \cdot I_Z$$

Design Constraints:

- $I_Z \geq I_{Z,min}$ (stay in breakdown)
- $P_Z \leq P_{Z,max}$ (power rating)

Shunt Regulator Design Example

Design Specifications:

- Output: $V_o = 5.1$ V (use 5.1 V Zener)
- Input: $V_{in} = 12$ V (from filtered rectifier)
- Load: $I_L = 0$ to 50 mA
- Zener: $I_{Z,min} = 5$ mA, $P_{Z,max} = 500$ mW

Design Process:

Step 1: Choose I_S at no-load
Let $I_S = 2 \times I_{L,max} = 100$ mA
This ensures enough current for regulation

Step 2: Calculate R_S

$$R_S = \frac{V_{in} - V_Z}{\ldots} = \frac{12 - 5.1}{\ldots} = 69\ \Omega$$

Step 3: Verify worst-case conditions
At no load ($I_L = 0$):

$$I_Z = I_S - I_L = 100 - 0 = 100 \text{ mA}$$
$$P_Z = 5.1 \times 0.1 = 510 \text{ mW}$$

Problem! Exceeds 500 mW rating

Step 4: Redesign with lower I_S
Maximum safe I_Z:

$$I_{Z,max} = \frac{P_{Z,max}}{V_Z} = \frac{0.5}{5.1} = 98 \text{ mA}$$

Choose $I_S = I_{Z,max} = 98$ mA, then:

$$R_S = \frac{12 - 5.1}{0.098} = 70.4\ \Omega$$

Regulation Performance

Load Regulation:
Measures output voltage change with load current:

$$\text{Load Reg} = \frac{V_{o,no-load} - V_{o,full-load}}{V_{o,full-load}} \times 100\%$$

Affected by:

- Zener dynamic resistance r_z
- Series resistance R_S
- Load current range

Line Regulation:
Measures output voltage change with input voltage:

Efficiency:

$$\eta = \frac{P_o}{P_{in}} = \frac{V_o I_L}{V_{in} I_S} \times 100\%$$

Example (from previous design):
At full load ($I_L = 50$ mA):

$$P_o = 5.1 \times 0.050 = 0.255 \text{ W}$$
$$P_{in} = 12 \times 0.098 = 1.176 \text{ W}$$
$$\eta = \frac{0.255}{1.176} = 21.7\%$$

Key Points:

- ☹ Shunt regulators have poor efficiency
- ☹ Power wasted in R_S and Zener
- ☺ Simple and inexpensive

Component Selection

Diode Selection:

Key ratings:

- **PIV rating**: Must exceed peak voltage with safety margin (2x)
- **Average current**: Must handle DC load current
- **Peak current**: Can be 10x average for capacitive loads
- **Forward voltage**: Lower is better for efficiency

Common types:

- 1N4001-1N4007 series (1A, 50V-1000V)
- Fast recovery for high frequency
- Schottky for low voltage drop

Safety Considerations:

- Capacitors store charge—discharge before handling
- Use fuses for overcurrent protection
- Heat sinks for high-power diodes
- Proper grounding essential

Common Mistakes:

- ☹ Reversed diode polarity
- ☹ Reversed capacitor polarity
- ☹ Undersized PIV rating
- ☹ Insufficient heat sinking
- ☹ Forgetting safety margin

Testing Tips:

Summary: Diode Applications

Rectifier Circuits:

Half-Wave:

- $V_{DC} = V_p/\pi \approx 0.318V_p$
- PIV $= V_p$
- Ripple frequency $= f$
- Low efficiency

Bridge (Full-Wave):

- $V_{DC} = 2V_p/\pi \approx 0.637V_p$
- PIV $= V_p$ (per diode)
- Ripple frequency $= 2f$
- Better efficiency

Filtering:

- Capacitor smooths output
- $V_r = V_p/(fR_LC)$

Voltage Regulation:

Zener Shunt Regulator:

- Maintains constant output
- $I_S = I_Z + I_L$
- $R_S = (V_{in} - V_Z)/I_S$
- Check power dissipation

Performance:

- Load regulation: ΔV_o with ΔI_L
- Line regulation: ΔV_o with ΔV_{in}
- Efficiency: typically poor (20-50%)

Next Topics:

- Transistor fundamentals
- MOS transistors
- BJT transistors