

# Convection In A Box

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## What is this?

A document where I can write down my working for modelling convection in a box as paper isn't the best at conveying ideas remotely. This is in no way polished document.

## The Problem

We seek to model 2D convection for a slow moving fluid. We will format this problem using streamfunctions with the aim of solving it numerically. First, the solution in a box using cartesian coordinates is discussed. The problem is then formatted in polar coordinates and solved on a disk.

## The bousinesque Approximation

In the bousinque approximation we assume density fluctuations are small. This leads us to considering only density fluctuations when they are multiplied by a gravity term.

We begin with the NSE, equation 6. We approximate the density by

$$\rho = \rho_0 + \rho', \quad (1)$$

where  $\rho_0$  is a constant reference density and  $\rho' \ll \rho_0$  is a perturbation that depends on space. We similarly split pressure up by equation 2.

$$p = p_0 + p' \quad (2)$$

Applying equation 1 and 2, the Navier-Stokes equation reads:

$$(\rho_0 + \rho') \frac{\partial \vec{u}}{\partial t} + (\rho_0 + \rho')(\vec{u} \cdot \nabla) \vec{u} = (\rho_0 + \rho') \vec{g} - \nabla(p_0 + p') + \mu \nabla^2 \vec{u} \quad (3)$$

By assuming  $\vec{u}$  is also first order, equation 3 to zeroth order produces:

$$\rho_0 \vec{g} = \nabla p_0, \quad (4)$$

and so to first order:

$$\rho \frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} = \frac{\rho'}{\rho_0} \vec{g} - \frac{\nabla p'}{\rho_0} + \nu \nabla^2 \vec{u}, \quad (5)$$

where  $\mu = \rho\nu$ .

And that's the bousinesque equation.

## Equations

The navier stokes equation (equation 6) describes the conservation of momentum for an incompressible fluid.

$$\rho \frac{\partial \vec{u}}{\partial t} + \rho(\vec{u} \cdot \nabla) \vec{u} = \rho \vec{g} - \nabla p + \mu \nabla^2 \vec{u} \quad (6)$$

The density  $\rho$  is assumed to be a function of temperature  $T$  and governed by equation 7

$$\rho = \rho_0(1 - \alpha(T - T_0)), \quad (7)$$

where  $\alpha$  is a coefficient of thermal expansion and  $\rho_0$  and  $T_0$  are reference densities and temperatures. The temperature is non constant, and modelled using equation ??

$$\frac{\partial T}{\partial t} + (\vec{u} \cdot \nabla) T = \kappa \nabla^2 T + \frac{Q}{C_p}, \quad (8)$$

where  $\kappa$  is the diffusion constant,  $C_p$  the specific heat capacity per volume and  $Q$  a heat source. We apply the creeping flow approximation first, giving:

$$\rho \frac{\partial \vec{u}}{\partial t} = \rho \vec{g} - \nabla p + \mu \nabla^2 \vec{u} \quad (9)$$

Next we apply the bousinesque approximation giving:

$$\frac{\partial \vec{u}}{\partial t} = \frac{\rho'}{\rho} \vec{g} - \frac{\nabla p'}{\rho_0} + \nu \nabla^2 \vec{u} \quad (10)$$

We now aim to numerically solve equations 10, 8 and 7 using a finite difference scheme.

## Streamfunction-vorticity formulation in cartesian coorindates

We consider the problem in 2D cartesian co-ordinates (x,y) with  $\vec{u} = (u, v)$ , where  $u$  and  $v$  are the  $x$  and  $y$  velocities of the fluid respectively. We define a streamfunction  $\psi$  by equation ??

$$u = -\frac{\partial \psi}{\partial y}, v = \frac{\partial \psi}{\partial x}. \quad (11)$$

We also define the vorticity in the  $x - y$  plane  $\omega$  by:

$$\omega = \nabla \times \vec{u} = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y}. \quad (12)$$

By these definitions of the streamfunction and vorticity we get the incompressibility condition (equation 13) and the vorticity-streamfunction relation, equation 14:

$$0 = \frac{\partial^2 \psi}{\partial x \partial y} - \frac{\partial^2 \psi}{\partial x \partial y} = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = \nabla \cdot \vec{u} \quad (13)$$

$$\omega = \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2}. \quad (14)$$

Using the streamfunction we can immediately rewrite equation 8 as equation 15.

$$\frac{\partial T}{\partial t} - \frac{\partial \psi}{\partial y} \frac{\partial T}{\partial x} + \frac{\partial \psi}{\partial x} \frac{\partial T}{\partial y} = \kappa \nabla^2 T + \frac{Q}{C_p} \quad (15)$$

The streamfunction-vorticity equation for the Navier Stokes equation is a little more involved. We first split equation 10 into its components:

$$\frac{\partial u}{\partial t} = \frac{\rho'}{\rho_0} g_x - \frac{1}{\rho_0} \frac{\partial p'}{\partial x} + \nu \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right) \quad (16)$$

and,

$$\frac{\partial v}{\partial t} = \frac{\rho'}{\rho_0} g_y - \frac{1}{\rho_0} \frac{\partial p'}{\partial y} + \nu \left( \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right). \quad (17)$$

Taking  $\frac{\partial}{\partial x}$  of equation 17 and subtracting  $\frac{\partial}{\partial y}$  of equation 16 we rearrange to get equation 18:

$$\frac{\partial \omega}{\partial t} = \frac{g_y}{\rho_0} \frac{\partial \rho'}{\partial x} - \frac{g_x}{\rho_0} \frac{\partial \rho'}{\partial y} + \nu \nabla^2 \omega \quad (18)$$

Equations 18 and 15 complete our streamfunction-vorticity description.

## Boundry conditions

There are two classes of boundry conditions we must adress, fluid related boundry conditions and temperature related boundry conditions. We first consider the fluid related boundry conditions. We take the four boundries as stationary impermeable walls. (I cant draw latex graphics yet so I dont have a figure for this). We have four walls at  $x = 0, x = L, y = 0, y = L$ . At each wall, the normal fluid velocity is zero. For example, at the  $y = 0$  and  $y = L$  walls, we have:

$$u = \frac{\partial \psi}{\partial y} = 0 \quad (19)$$

and thus,

$$\psi = \text{constant}. \quad (20)$$

This is true for all four walls, which are connected. So on the walls,  $\psi = \text{constant}$ . From equation 12 on the left and right walls:

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} = \frac{\partial^2 \psi}{\partial y^2} = \omega_{\text{wall}} \quad (21)$$

and similiary on the top and bottom wall:

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} = \frac{\partial^2 \psi}{\partial x^2} = \omega_{\text{wall}}. \quad (22)$$

Equations 20, 21 and 22 compose the boundry conditions used here.

## Streamfunction-vorticity formulation in polar coorindates

We consider polar coorindates  $r$  and  $\theta$  with  $r \in \{0, \dots, R\}$  and  $\theta \in \{0, \dots, 2\pi\}$ . We discritize our domain  $\mathcal{D}$  with grids points  $(r_i, \theta_j)$  with  $r_i = i\Delta r, \theta_j = j\Delta\theta$ . We define a velocity vector  $\vec{u} = (u, v)$  with  $u$  pointing radially and  $v$  pointing azimuthally. A streamfunction  $\psi$  is used to define  $u$  and  $v$  as shown:

$$u = \frac{1}{r} \frac{\partial \psi}{\partial \theta}, v = -\frac{\partial \psi}{\partial r}. \quad (23)$$

In defining  $u$  and  $v$  this way, the incompressability condition (equation 24) is satisfied:

$$\nabla \cdot \vec{u} = 0, \quad (24)$$

where  $\nabla$  is the del operator in cylindrical coordinates with any terms terms out of the  $r - \theta$  plane supressed. The voriticty,  $\omega$  is defined as:

$$\omega = (\nabla \times \vec{u}) \cdot \hat{z} = -\nabla^2 \psi, \quad (25)$$

where  $\hat{z}$  points out of the  $r - \theta$  plane.

The simplified navier stokes equation (equation ??) can be written in polar co-ordinates as:

$$\frac{\partial u}{\partial t} = -\frac{1}{\rho_0} \frac{\partial p'}{\partial r} + \frac{\rho'}{\rho_0} g_r + \nu(\nabla^2 u - \frac{u}{r^2} - \frac{2}{r^2} \frac{\partial v}{\partial \theta}) \quad (26)$$

$$\frac{\partial v}{\partial t} = -\frac{1}{r\rho_0} \frac{\partial p'}{\partial \theta} + \frac{\rho'}{\rho_0} g_\theta + \nu(\nabla^2 v - \frac{v}{r^2} + \frac{2}{r^2} \frac{\partial u}{\partial \theta}) \quad (27)$$

Multiplying equation 27 by  $r$  and cross-differentationing  $\frac{\partial}{\partial r}$  r (27) -  $\frac{\partial}{\partial \theta}$  (26) we get:

$$\frac{\partial}{\partial t} (r \frac{\partial v}{\partial r} - \frac{\partial u}{\partial \theta}) = -\frac{g_r}{\rho_0} \frac{\partial \rho'}{\partial \theta} + \nu((\frac{\partial}{\partial r} r (\nabla^2 u - \frac{u}{r^2} - \frac{2}{r^2} \frac{\partial v}{\partial \theta})) - (\frac{\partial}{\partial \theta} (\nabla^2 v - \frac{v}{r^2} + \frac{2}{r^2} \frac{\partial u}{\partial \theta}))), \quad (28)$$

where we have assumed that  $\theta$  and  $r$  derivatives commute and  $g_\theta = 0$ . Using the definition of  $\omega$  in equation 25 we write equation 28 as:

$$\frac{\partial \omega}{\partial t} = -\frac{g_r}{\rho_0 r} \frac{\partial \rho'}{\partial \theta} + \nu \nabla^2 \omega \quad (29)$$