

Analysis of Piezoelectric Microcantilever

Key Variables

- **Geometric Parameters:**

- w_t : Beam width.
- l_t : Beam length.
- t : Beam thickness.
- electrode_length, electrode_width: Electrode dimensions.
- w_c, l_c : Spectral dimensions of the mass block at the end of the beam.
- d : Gap between electrodes.

- **Material Parameters:**

- E : Young's modulus.
- ρ : Material density.
- ϵ_0 : Vacuum permittivity.

- **Electrical and Vibrational Parameters:**

- Q : Quality factor.
- V : Driving voltage.
- Vac: AC voltage amplitude (harmonic driving).
- ϕ : Harmonic driving phase range.
- β, α_n : Parameters related to the modal shape.

Key Calculations

Modal Shape Calculation

Modal shape describes the deformation distribution of the beam under resonance, based on Euler-Bernoulli beam theory:

$$\text{modeshape_unnormalized} = - \left(-\sin(\beta x/l_t) + \sinh(\beta x/l_t) + \alpha_n(-\cos(\beta x/l_t) + \cosh(\beta x/l_t)) \right)$$

Normalized modal shape:

$$\text{modeshape1} = \frac{\text{modeshape_unnormalized}}{\max(\text{modeshape_unnormalized})}$$

Mechanical Properties

The stiffness and mass of the beam are calculated as follows:

- Normalized stiffness coefficients:

$$k_{\text{coef_b}} = \int \frac{\text{second_derivative}^2}{l_t} dx,$$
$$k_{\text{coef_b3}} = \int \frac{\text{first_derivative}^2}{l_t} dx.$$

- Actual stiffness:

$$k_{tt} = \frac{k_{\text{coef_b}}}{12} Et \left(\frac{w_t}{l_t} \right)^3,$$
$$k_{t3} = k_{\text{coef_b3}} Et \frac{w_t}{l_t^3}.$$

- Total stiffness:

$$k_t = k_{tt}.$$

- Total mass:

$$M = \rho (tw_t l_t m_{\text{coef_b}} + \text{electrode_length} \cdot \text{electrode_width} \cdot t + 2w_c \cdot l_c \cdot t).$$

- Natural angular frequency:

$$\omega_0 = \sqrt{\frac{k_t}{M}}, \quad f_0 = \frac{\omega_0}{2\pi}.$$

Electromechanical Coupling

Electromechanical effects introduce additional stiffness and non-linear terms:

- Coupling factor:

$$\text{trans_factor} = \frac{\epsilon_0 V \cdot \text{electrode_length} \cdot t}{d^2}.$$

- Electromechanical stiffness:

$$k_e = 2 \cdot \text{trans_factor} \cdot \frac{V}{d},$$
$$k_{e3} = 4 \cdot \text{trans_factor} \cdot \frac{V}{d^3}.$$

Dynamic Response Under Harmonic Driving

The dynamic response is computed by solving a nonlinear system of equations for frequency and motional current:

$$-M\omega^2 y + (k_t - k_e)y + (k_{t3} - k_{e3})\frac{3}{4}y^3 - F_{ac} \cos(\phi) = 0,$$
$$c\omega y - F_{ac} \sin(\phi) = 0.$$

Where:

$$F_{ac} = V_{ac} \cdot \text{trans_factor},$$
$$c = \frac{\sqrt{Mk_t}}{Q}.$$

The solutions are filtered according to the following condition:

$$\frac{\omega_0}{2} < \omega < \frac{3\omega_0}{2}, \quad \omega > 0.$$

主要变量

- 几何参数:

- w_t : 梁的宽度。
- l_t : 梁的长度。
- t : 梁的厚度。
- electrode_length , electrode_width : 电极的长度和宽度。
- w_c , l_c : 梁末端集中质量块的宽度和长度。
- d : 电极间隙距离。

- 材料参数：
 - E : 弹性模量。
 - ρ : 材料密度。
 - ϵ_0 : 真空介电常数。
- 电学和振动条件：
 - Q : 品质因数。
 - V : 驱动电压。
 - V_{ac} : 交流电压幅值（谐波驱动）。
 - ϕ : 谐波驱动的相位范围。
 - β, α_n : 与模态形状相关的参数。

主要计算过程

模态形状计算

模态形状描述梁在共振条件下的变形分布，基于欧拉-伯努利梁理论：

$$\text{modeshape_unnormalized} = - \left(-\sin(\beta x/l_t) + \sinh(\beta x/l_t) + \alpha_n \left(-\cos(\beta x/l_t) + \cosh(\beta x/l_t) \right) \right)$$

归一化模态形状：

$$\text{modeshape1} = \frac{\text{modeshape_unnormalized}}{\max(\text{modeshape_unnormalized})}$$

力学特性

梁的弯曲刚度和质量计算如下：

- 刚度系数（归一化）：

$$k_{\text{coef_b}} = \int \frac{\text{second_derivative}^2}{l_t} dx,$$

$$k_{\text{coef_b3}} = \int \frac{\text{first_derivative}^2}{l_t} dx.$$

- 实际刚度：

$$k_{tt} = \frac{k_{\text{coef_b}}}{12} Et \left(\frac{w_t}{l_t} \right)^3,$$

$$k_{t3} = k_{\text{coef_b3}} Et \frac{w_t}{l_t^3}.$$

- 总刚度：

$$k_t = k_{tt}.$$

- 总质量：

$$M = \rho (tw_t l_t m_{\text{coef_b}} + \text{electrode_length} \cdot \text{electrode_width} \cdot t + 2w_c \cdot l_c \cdot t).$$

- 自然角频率：

$$\omega_0 = \sqrt{\frac{k_t}{M}}, \quad f_0 = \frac{\omega_0}{2\pi}.$$

电耦合效应

电场引入附加刚度和非线性效应：

- 转换因子：

$$\text{trans_factor} = \frac{\epsilon_0 V \cdot \text{electrode_length} \cdot t}{d^2}.$$

- 电耦合刚度：

$$k_e = 2 \cdot \text{trans_factor} \cdot \frac{V}{d},$$

$$k_{e3} = 4 \cdot \text{trans_factor} \cdot \frac{V}{d^3}.$$

谐波驱动下的动态响应

通过求解非线性方程组，计算频率和运动电流：

$$-M\omega^2 y + (k_t - k_e)y + (k_{t3} - k_{e3})\frac{3}{4}y^3 - F_{\text{ac}} \cos(\phi) = 0,$$

$$c\omega y - F_{\text{ac}} \sin(\phi) = 0.$$

其中：

$$F_{\text{ac}} = V_{\text{ac}} \cdot \text{trans_factor},$$

$$c = \frac{\sqrt{Mk_t}}{Q}.$$

解的筛选条件：

$$\frac{\omega_0}{2} < \omega < \frac{3\omega_0}{2}, \quad \omega > 0.$$