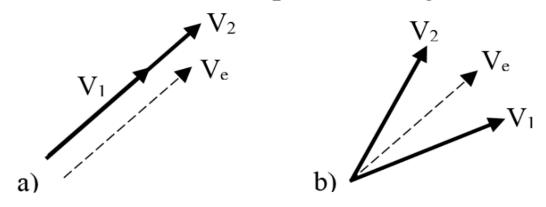
Models for synchrophasor with step discontinuities in magnitude and phase: estimation and performance

- Motivation
- Proposed mathematical models
 - Magnitude Step
 - Phase Step
- Estimation of model parameters from discrete-time signals
 - Hilbert transform
 - Non-linear least-squares estimator
- Numerical simulations: computation errors
- Lab prototype system assessment

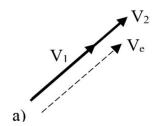
PMU calibrators do need to perform magnitude or phase tests.



- a) We should be able to measure frequency and phase
- b) We should be able to measure frequency and magnitude

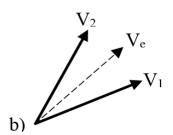
Moreover, V_e can be used as a reference value as an intermediate phasor.

$$y(t) = x_1[1 + x_2u(t - \tau)]\cos(\omega t + \varphi) + \eta(t)$$



Phase Step

$$y(t) = x_1 \cos(\omega t + \varphi + x_3 u(t - \tau)) + \eta(t)$$

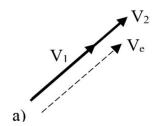


Additive white gaussian noise

Noise variance

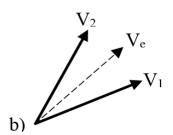
$$\eta_0 = \left(\frac{\sigma_y}{10^{\frac{SNR}{20}}}\right)^2,$$

$$y(t) = x_1[1 + x_2u(t - \tau)]\cos(\omega t + \varphi) + \eta(t)$$



Phase Step

$$y(t) = x_1 \cos(\omega t + \varphi + x_3 u(t - \tau)) + \eta(t)$$



Additive white gaussian noise

Noise variance

$$\eta_0 = \left(\frac{\sigma_y}{10^{\frac{SNR}{20}}}\right)^2,$$

$$y(t) = x_1[1 + x_2u(t - \tau)]\cos(\omega t + \varphi) + \eta(t)$$

Phase Step

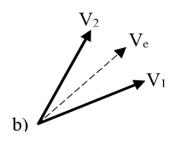
$$y(t) = x_1 \cos(\omega t + \varphi + x_3 u(t - \tau)) + \eta(t)$$



$$\widehat{V}_e = \widehat{X}_e \angle \widehat{\varphi} = \frac{\widehat{x}_1 \widehat{\tau} + \widehat{x}_1 (1 + \widehat{x}_2) (T - \widehat{\tau})}{T} \angle \widehat{\varphi}$$

$$V_1$$
 V_2 V_e

$$\widehat{V}_e = \widehat{X} \angle \widehat{\varphi}_e = \widehat{X} \angle \frac{\widehat{\varphi} \widehat{\tau} + (\widehat{\varphi} + \widehat{x}_3)(T - \widehat{\tau})}{T}$$
_{b)}



$$y(t) = x_1[1 + x_2u(t - \tau)]\cos(\omega t + \varphi) + \eta(t)$$

Phase Step

$$y(t) = x_1 \cos(\omega t + \varphi + x_3 u(t - \tau)) + \eta(t)$$

Given a real narrowband monocomponent signal x(t), $-\infty < t < \infty$, let z(t) be called the analytic signal associated to x(t), defined as

$$z(t) = x(t) + j\tilde{x}(t), \tag{7}$$

where

$$\tilde{x}(t) = H(x(t)) = \int_{-\infty}^{\infty} \frac{x(u)}{\pi(t-u)} du, \tag{8}$$

is the Hilbert transform of x(t). If z(t) is expressed in the polar form

$$z(t) = A(t)e^{j\theta(t)}, (9)$$

$$A(t) = \sqrt{x^2(t) + \tilde{x}^2(t)},$$
 (10)

$$\theta(t) = \tan^{-1}(x(t)/\tilde{x}(t)), \tag{11}$$

the instantaneous frequency (IF) can be defined as

$$f_i(t) = \frac{1}{2\pi} \left(\frac{d\theta(t)}{dt} \right). \tag{12}$$

$$z[n] = x[n] + jH(x[n])$$

$$d[n] = |f_i[n]| - m(f_i[n])$$

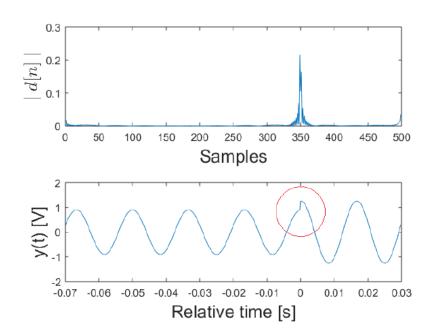


Fig. 2 Detection signal d[n] (top plot) associated with a phasor waveform with magnitude step (bottom plot). ($\tau = 70\%$ of window duration).

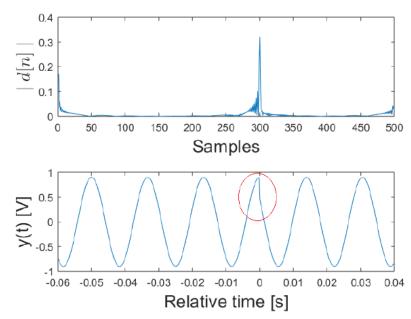


Fig. 3 Detection signal d[n] (top plot) associated with a phasor waveform with phase step (bottom plot). ($\tau = 60\%$ of window duration).

$$y(t) = x_1[1 + x_2u(t - \tau)]\cos(\omega t + \varphi) + \eta(t)$$

Phase Step

$$y(t) = x_1 \cos(\omega t + \varphi + x_3 u(t - \tau)) + \eta(t)$$

$$\varepsilon(\mathcal{P}) = \frac{1}{2} \sum_{k=1}^{N} (y(k) - \hat{y}(k\Delta t))^{2}$$
$$\min_{\mathcal{P}} \varepsilon(\mathcal{P})$$

Non-linear least-squares estimator: Levenberg-Marquardt

- Non-linear functions w.r.t parameters
- Iterative
- Gauss-Newton + steepest descent
- Numerical approximation of Jacobian
- Local minima, needs convex function

Parameter	<i>x</i> ₁	<i>x</i> ₂	<i>x</i> ₃	$\omega/2\pi$	φ
Nominal	1 V _p	± 0.1	± 10°	60 Hz	360°, ±120°
U[%]	1	1	1	0.05	1

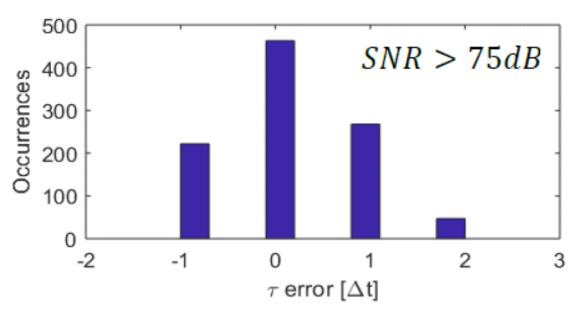


Fig. 4 Histogram of errors in step instant estimation.

GOVERNO FEDERAL

TABLE I NOMINAL VALUES AND UNCERTAINTIES USED IN THE SIMULATIONS

Parameter	<i>x</i> ₁	<i>x</i> ₂	<i>x</i> ₃	$\omega/2\pi$	φ
Nominal	1 V _p	± 0.1	± 10°	60 Hz	360°, ±120°
U[%]	1	1	1	0.05	1

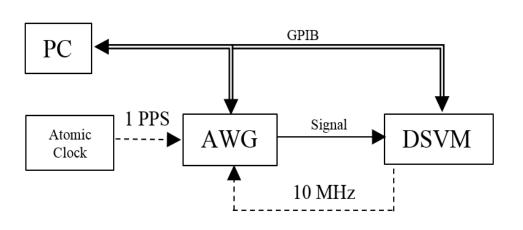
TABLE II STANDARD DEVIATION OF NUMERICAL ERRORS FOR MAGNITUDE STEPS

SNR [dB]	90	93	97
Frequency $[\mu Hz/Hz]$	0.14	0.1	0.06
Magnitude [$\mu V/V$]	1.5	1.0	0.6
Phase [m °]	0.4	0.1	0.06

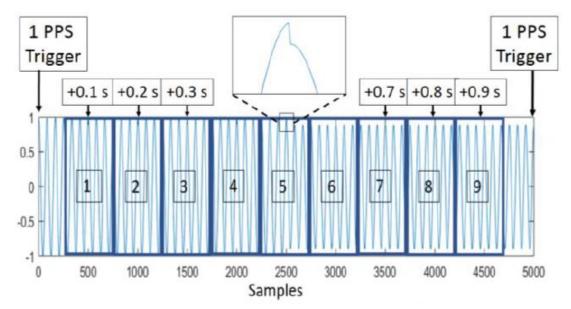
TABLE III
STANDARD DEVIATION OF NUMERICAL ERRORS FOR PHASE STEPS

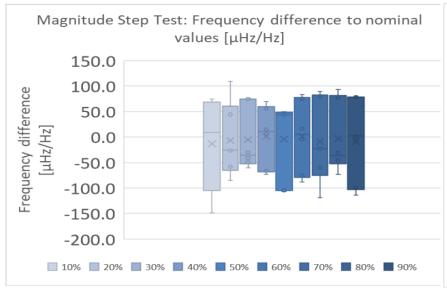
SNR [dB]	90	93	97
Frequency $[\mu Hz/Hz]$	0.26	0.19	0.1
Magnitude $[\mu V/V]$	1.5	1.0	0.7
Phase [m °]	0.17	0.11	0.07

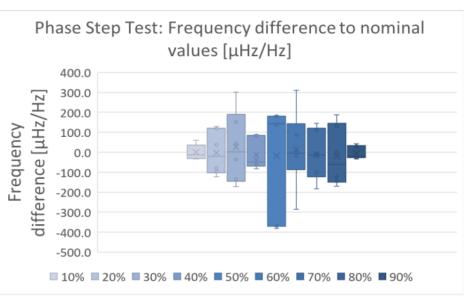
GOVERNO FEDERAL











Standard deviation from $F_{nom} = 60 \ Hz$

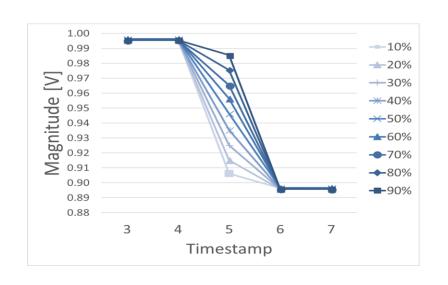
Steady State: $9 \mu Hz/Hz$ (0.5 mHz)

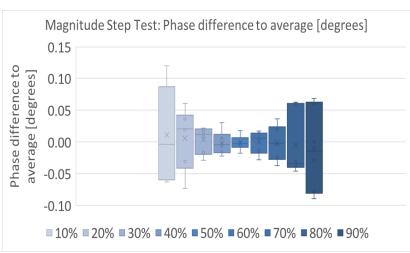
Magnitude Step: 70 μ Hz/Hz (4 mHz)

Phase Step: 40 $\mu Hz/Hz$ (2 mHz) to 280 $\mu Hz/Hz$ (17 mHz)

Magnitude Step Phasor

GOVERNO FEDERAL



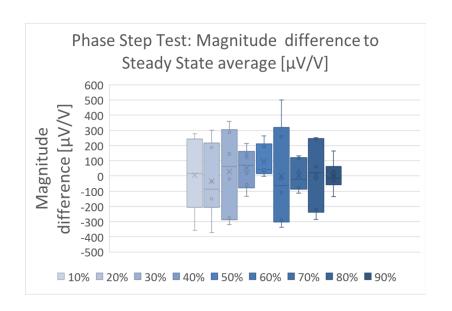


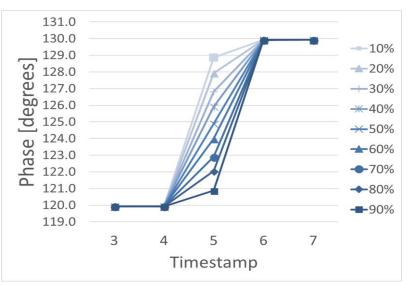
Phase (difference from the average values)

Standard deviations

Steady State: $1.7 m^{\circ}$

Magnitude Step: $10 m^o$ to $70 m^o$





Magnitude (difference from the Steady State average values)

Standard deviations

Steady State: $160 \mu V/V$

Magnitude Step: $200 \mu V/V$

Questions?

Thank you!



- **Ouvidoria:** 0800 285 1818
- inmetro.gov.br
- f facebook.com/Inmetro
- witter.com/Inmetro
- youtube.com/tvinmetro

