A dynamical system is given as

$$\begin{cases} \dot{x} = Ax + Bu \\ x(0) = x_0 \end{cases} \tag{1}$$

where  $A \in \mathbb{R}^{nxn}$ ,  $B \in \mathbb{R}^{nxm}$ ,  $x \in \mathbb{R}^{nx1}$  and  $u \in \mathbb{R}^{mx1}$ . The control signal is constrained with

$$g_i \le u \le h_i \quad i = 1, 2, \cdots, m \tag{2}$$

Let's assume the system matrices as follows

$$A = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix}, \quad B = \begin{bmatrix} b_{11} \\ b_{21} \end{bmatrix}, \tag{3}$$

and hence, n=2 and m=1. Then,

$$g \le u \le h \tag{4}$$

and

$$L = \begin{bmatrix} l_{11} \\ l_{21} \end{bmatrix} \tag{5}$$

can be stated. The closed-loop matrix is obtained as,

$$A + BL^{T} = \begin{bmatrix} a_{11} + b_{11}l_{11} & a_{12} + b_{11}l_{21} \\ a_{21} + b_{21}l_{11} & a_{22} + b_{21}l_{21} \end{bmatrix}$$
 (6)

E(L) is defined as follows

$$E(L) = \{ z | z \in \mathbb{R}^2 \text{ and } g \le l_i^T z \le h \}$$
  
=  $g \le l_{11} z_{11} + l_{21} z_{21} \le h$  (7)

F(L) is defined as follows

$$F(L) = \bigcap_{t \in [0,\infty]} \{ (e^{A_c t})^{-1} E(L) \}$$
 (8)

where F(L) is a subset of E(L). Let  $K = k_1$ , then

$$u = sat[(L^T - KB^T P)x] \tag{9}$$

is defined. Consider

$$u = L^{T}x + v$$
  
=  $l_{11}x_{1} + l_{21}x_{2} + v$  (10)

then the closed-loop system is

$$\dot{x} = (A + BL^T)x + Bv \tag{11}$$

which is openly,

$$\dot{x}_1 = (a_{11} + b_{11}l_{11})x_1 + (a_{12} + b_{11}l_{21})x_2 
\dot{x}_2 = (a_{21} + b_{21}l_{11})x_1 + (a_{22} + b_{21}l_{21})x_2$$
(12)

The derivative of the Lyapunov function  $V = x^T P x$  is obtained as,

$$\dot{V} = \dot{x}^{T} P x + x^{T} P \dot{x} 
= ((A + BL^{T})x + Bv)^{T} P x + x^{T} P ((A + BL^{T})x + Bv) 
= (v^{T} B^{T} + x^{T} L B^{T} + x^{T} A^{T}) P x + x^{T} P ((A + BL^{T})x + Bv) 
= v^{T} B^{T} P x + x^{T} L B^{T} P x + x^{T} A^{T} P x + x^{T} P A x + x^{T} P B L^{T} x + x^{T} P B v 
= x^{T} (A^{T} P + P A + P B L^{T} + L B^{T} P) x + 2x^{T} P B v$$
(13)

For stability,

$$2x^T P B v \le 0 \tag{14}$$

is needed. Choosing  $v = -RB^TPx$  gives,

$$2x^{T}PBv = 2x^{T}PB(-RB^{T}Px)$$

$$2x^{T}PBv = -2x^{T}(PBRB^{T}P)x$$

$$2x^{T}PBv \le 0$$
(15)

where  $R = diag([r_1, r_2, \cdots, r_m])$ . Therefore,

$$\dot{V} = x^{T} (A^{T}P + PA + PBL^{T} + LB^{T}P)x + 2x^{T}PBv 
\dot{V} = x^{T} (A^{T}P + PA + PBL^{T} + LB^{T}P)x - 2x^{T} (PBRB^{T}P)x 
\dot{V} = x^{T} (A^{T}P + PA + PBL^{T} + LB^{T}P - 2PBRB^{T}P)x 
\dot{V} = x^{T} (A^{T}P + PA + PB(L^{T} - RB^{T}P) + (L - PBR)B^{T}P)x$$
(16)

Solving,

$$L^T x - RB^T P x = sat[L^T x - KB^T P x] \tag{17}$$

for any diagonal K.

$$L^{T}x - RB^{T}Px = sat[L^{T}x - KB^{T}Px]$$
(18)

which is expanded as

$$l_{11}x_1 + l_{21}x_2 - (b_{11}p_{11}r + b_{21}p_{12}r)x_1 + (-b_{11}p_{12}r - b_{21}p_{22}r)x_2$$

$$= sat(l_{11}x_1 + l_{21}x_2 - (b_{11}p_{11}k + b_{21}p_{12}k)x_1 + (-b_{11}p_{12}k - b_{21}p_{22}k)x_2)$$
(19)

if  $x \in E(L)$  then

$$g \le l_{11}x_1 + l_{21}x_2 \le h \tag{20}$$

but if also

$$g \le l_{11}x_1 + l_{21}x_2 - (b_{11}p_{11}k + b_{21}p_{12}k)x_1 - (b_{11}p_{12}k + b_{21}p_{22}k)x_2 \le h \quad (21)$$

then r = k. On the other hand, if

$$l_{11}x_1 + l_{21}x_2 - k(b_{11}p_{11} + b_{21}p_{12})x_1 - k(b_{11}p_{12} + b_{21}p_{22})x_2 > h$$
 (22)

if a smaller r then the term

$$l_{11}x_1 + l_{21}x_2 - r(b_{11}p_{11} + b_{21}p_{12})x_1 - r(b_{11}p_{12} + b_{21}p_{22})x_2$$
 (23)

would increase. Therefore,

$$l_{11}x_1 + l_{21}x_2 - r(b_{11}p_{11} + b_{21}p_{12})x_1 - r(b_{11}p_{12} + b_{21}p_{22})x_2 = h$$
 (24)

The algorithm is given as follows:

- 1. Determine  $\mathbb{D}$ . (set of initial states)
- 2. Find L. Control penalty R in LQR is increased until  $L^Tx$  satisfies

$$g \le L^T x \le h \tag{25}$$

for x in  $\mathbb{D}$ . This can be done via

$$g \le \max_{x \in \mathbb{D}} l_i^T x \le h \tag{26}$$

If this cannot be satisfied then there is no design.

3. Find P and c. P can be used from LQR. c is obtained from

$$\sup_{x \in \mathbb{D}} x^T P x \le c \le \min_{\delta E(L)} x^T P x$$

$$\min_{\delta E(L)} x^T P x = \min_{i} \frac{g_i^2}{l_i^T P^{-1} l_i}, \frac{h_i^2}{l_i^T P^{-1} l_i}$$

$$(27)$$

If this fails choose another P, if it still fails cut down the size of  $\mathbb{D}$ .

4. Set up the control u according to

$$u = sat[L^T x - KB^T P x] (28)$$

Tune k with simulations.

An example system is given,

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$-1 < u < 1$$
(29)

The initial condition solution is given as follows,

$$x(t) = e^{At}x(0) (30)$$

hence,

$$x(t) = e^{At}x(0)$$

$$x(t) = \left(I + At + \frac{A^2t^2}{2!} + \cdots\right)x(0)$$

$$x(t) = (I + At)x(0)$$

$$x(t) = \begin{bmatrix} 1 & t \\ 0 & 1 \end{bmatrix}x(0)$$
(31)

The solution of the given system is obtained as

$$\begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} = \begin{bmatrix} x_1(0) + tx_2(0) \\ x_2(0) \end{bmatrix}$$
 (32)

The LQR weights are chosen as

$$Q = \begin{bmatrix} 10 & 0 \\ 0 & 1 \end{bmatrix} \quad R = 500000 \tag{33}$$

hence the LQR matrix is calculated as

$$L = \begin{bmatrix} -0.0045 & -0.0946 \end{bmatrix} \tag{34}$$

The closed-loop system is calculated as

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -0.0045 & -0.0946 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} v \tag{35}$$

and solving it gives

$$\Phi(1,1) = e^{-0.0473t} (\cos(0.0473t) + 1.0002\sin(0.0473t)) 
\Phi(1,2) = 21.1498e^{-0.0473t} \sin(0.0473t) 
\Phi(2,1) = -0.0946e^{-0.0473t} \sin(0.0473t) 
\Phi(2,2) = e^{-0.0473t} (\cos(0.0473t) - 1.0002\sin(0.0473t))$$
(36)

The control law is obtained as

$$u(t) = e^{-0.0473t} (-0.0045\cos(0.0473t) + 0.0045\sin(0.0473t))x_1(0) + e^{-0.0473t} (-0.0946\cos(0.0473t) + 0.00002115\sin(0.0473t))x_2(0)$$
(37)

The set  $\mathbb{D}$  is defined as

$$\mathbb{D} = \{ x \in \mathbb{R}^2 \mid -10 \le x_1, x_2 \le 10 \}$$
 (38)

Control signals of corner points in  $\mathbb{D}$  are shown in Figure 1.

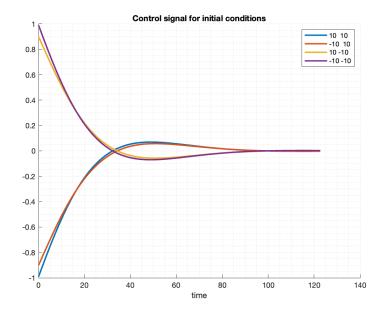


Figure 1: Control signals for different initial conditions