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IECTURE 15
 - REVIEW
  - \wedge -
 SO FAR WE DERIVED ALL OF THE BALANCE LAWS
 THAT GOVERN THE MOTTON OF WATINUA
  BALANCE OF MASS
     4P + 1 (PV) = 0
                                   \forall x \in \Sigma
    0P3 = 0 , P3 = PJ
                                  \forall X \in \Sigma
  BALANCE OF MOMENTUM
                                    \forall x \in \mathbb{Z}
    PV = V· T + 5
                                   \forall x \in S_{2}
    P. V = 7 P + B
  (V_{\underline{}}V_{\underline{}}V_{\underline{}}Q_{\underline{}}) P_{\underline{}}V_{\underline{}}V_{\underline{}}V_{\underline{}}
 BALANCE OF ANGULAR MOMENTUM
    <u>_</u> _ <u>_</u> _ _
BALANCE OF ENERGY (1s+ LAW)
                                           \forall x \in SZ
     pii = \( \frac{1}{2} \) + + - \( \frac{1}{2} \) 9
                                            \forall X \in \Sigma_{\infty}
     Poil = P F + R - V Q
 ENTROPY ENERVALITY (2nd LAW) CLAUSIUS-DUHEM
      PY = PY - - - (Pi - - - - - ) - - - - 9 > 0 + x < 5 z
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A STRONGER FORM OF THE ABOVE FOURIER INEQUALTY  $-\frac{1}{8} \times \frac{1}{2} \times \frac{1$ PN-1(Pii-PE)>0 CLAUSIUS PLANK UNKNOWNS P, P, Y, 9, D, N, M - IN PRACTICE P & O ARE PRIM THE ABOVE BALANCE EQUATIONS ARE AUGMENTED
BY EQUATIONS OF STATE (AKA CONSTITUTIVE
EQUATIONS) THAT RELATE THERMODYNAMIC STATE WARIABLES THE BASIC ASSUMPTION OF THER MODYNAMICS IS THAT TO FULLY CHARACTERIZE OUR THERMODY NAMIC STATE (IE HE INTERNAL ENERGY) WE NEED IN SUBSTATE VARIABLES AND A THERMAL LIKE VARIABLE NOTE PN-E(PU-PE)>0 =>PON-PN-PT>0

AND SINCE IN F CAN BE THOUGHT OF ARBITRARY
TRAJECTORIES WE HAVE

$$\Theta = \left(\frac{4N}{4N}\right)^{\left[\frac{1}{2},\frac{1}{2}\right]}, \quad \frac{4}{1} = \left(\frac{4}{4N}\right)^{\left[\frac{1}{2},\frac{1}{2}\right]}$$

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I FGENDRE TRANSFORM
 A LEGENDRE TRANSFOR CONVERTS A CONVEX FUNCTION OF ONE SET OF VARIABLES TO ANDTHER FUNCTION
 OF CONJUGATE VARIABLES
   Df = (Df^*) \quad OR = f'(f^*(x^*)) = x^* \notin f^*(f'(x)) = x
THE LEGENDRE TRANSFORM F* OF F IS DEFINED BY THE
RELATION
LET X & X* BE CONJUGATE VARIABLES THEN FOR f(X) IT'S LEGENDRE TRANSFORM F*(X) IS GIVEN BY
                              +(x)
   f^*(x^*) = INF f(x) - x^*
   INF f(x) - x^*x \Rightarrow f'(x) - x^* = 0
              => f'(x) = X*
   +(x) = ex, LET x BE WNJUGATE TO x x = 4f = ex
    (x*) = INF (x) - x+x
      INF ex-xx => ex=xx => x= lu xx
   f*(x*) = f(lux*) - x* lux* = x* (1 - lux*)
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THE INTERNAL ENERGY IS ONE OF FOUR THERMODYNAMIC POTENTIALS

Ψ(O, E, --) = M(Y, E, --) - OY ← HELMHOLIZ TREE EN THE PORTION OF THE INTERNAL ENERGY ABLE TO DO WORK AT A CONSTANT TEMPERATURE

h(n,P,-)=u(n,F,-)-P:F

PORTION OF THE INTERNAL ENERGY THAT CAN BE RELEASED AS HEAT WHEN STRESS ARE HELD CONSTANT

9(0,P, \_\_) = U(4, F, \_\_) - D1-P: F GIBBS FREE ENERGY

THE PORTION OF THE FREE ENERGY AVAILABLE TO DO NORK AT A CONSTAN STRESS & TEMP.

DEPENDING WHICH THERMODYNAMIC STATE VARIABLE YOU CAN CONTROL IN AN EXPERIMENT IT MAY BE CONVENIENT TO WORK WITH ONE POTENTIAL OVER ANOTHER

AS DEFORMATION & TEMPERATURE ARE OFTEN THE EASIEST AND MORE MEASURABLE MACROSCOPIC QUANTITIES WE OFTEN DEAL WITH  $\psi(e, f, --)$ 

WITH THE ABOVE

JoM = P + R - V·Q →

 $P_0OY-P_0U+P==>0$   $P_0F-P_0(U-OY)>0$ 

 $= \sum_{n=1}^{\infty} \frac{1}{n} \left( \frac{1}{n} - \frac{1}{n} \right) \left( \frac{1}{n} - \frac{1}{n} - \frac{1}{n} - \frac{1}{n} - \frac{1}{n} \right) \left( \frac{1}{n} - \frac{1$ 

ASSUME (PRINCIPLE OF LOCALITY)  $\psi = \psi(0, \pm, \nabla \theta)$  $(\frac{P}{A} - \frac{A}{A} + \frac{$ 

SINCE THE ABOVE MUSTHOLD TRUE FOR ANY ARBITRARY I, O, TO (COLEMAN EXPLOITATION)

 $\Rightarrow \int_{-\infty}^{\infty} \frac{1}{b^2} \frac$ 

NOTE IN GENERAL IN PROBLEMS INVOLVING INELASTICITY U = Y(O, F, Z)

> INTERNAL STATE VARIABUES

WHERE AN ADDITIONAL INITIAL VAUT PROBLEM GOVERNS
THE EVOUTION OF Z.

GOING BACK TO CLAUSIUS - PLANK

-b. 47 5 30

OR, IF 9:=- +2 4, 9.2>0

INTERNAL STATE VARIABLES ARE WIDELY USED IN THE CONSTITUTIVE FORMULATION OF DISSIPATIVE MATERIALS

INTERNAL STATE VARIABLES MAY BE OBSERVED BUT IN GENERAL NOT CONTROLLED

THE THERMODYNAMICAL FORCES OF CONJUGATE TO Z ARE GENERALLY NOT EXTERNALLY DEFINED HENCE THEY DO NOT EXPLICITLY APPEAR IN BALANCE OF ENERGY

## FRAME INDITTERENCE

EFFECTIVELY BALANCE LAWS GOVERN ALL WATTERALS

THE STATEMENT OF MATERIAL FRAME INDEFFERENCE STATES
THAT THE MATERIAL THERMOMECHANICAL POTENTIAL SHOULD BE
INDEPENDENT OF OBSERVER IE INVARIANT UNDER
TRANSLATION & ROTATION TO FORMALIZE THE ABOVE
WE NEED TO BUILD OF TO IT

CONSIDER  $X = \mathcal{Q}(X, t)$ 

ST  $X_0 = P(X, t_0)$ ,  $X_1 = P(X, t_1)$ 

NOW LET (x, t;) +> (xt, tt) SUCH THAT DISTANCE 1x-x,1

ETME ELAPSED ARE PRESERVED

ONE SUCH MAP IS

 $x^{+} = c(t) + c(t)x$   $t^{+} = t + c$ 

WHERE  $Q \in SO(3)$ 

MAPPING OF THE ABOVE FORM ARE KNOWN AS EUCLED AN TRANSFORMATIONS