



# ELEC 341: Systems and Control

## Lecture 14

### Root locus: Lead-lag compensator design

# Course roadmap

## Modeling

- ✓ Laplace transform
- ✓ Transfer function
- Models for systems
  - ✓ • Electrical
  - ✓ • Electromechanical
  - ✓ • Mechanical
- ✓ Linearization, delay

## Analysis

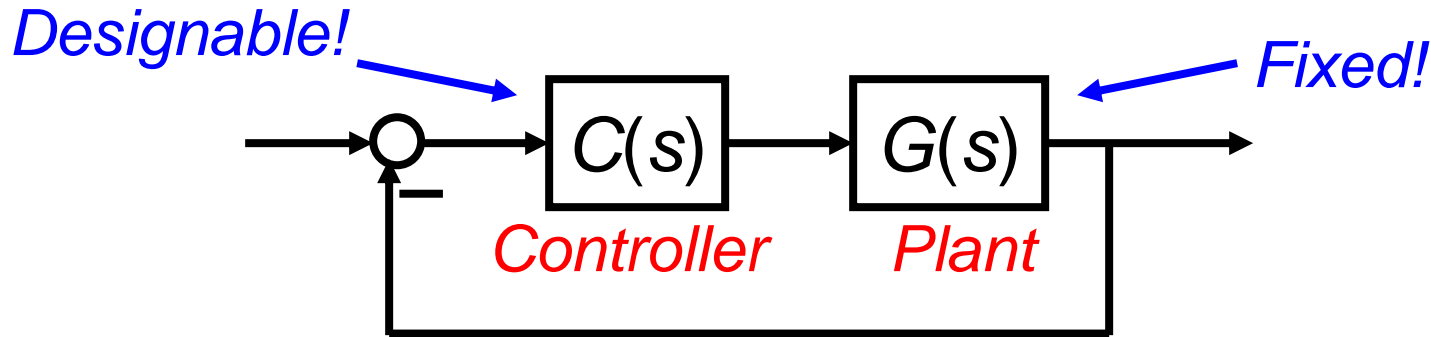
- ✓ Stability
  - Routh-Hurwitz
  - Nyquist
- Time response
  - ✓ • Transient
  - ✓ • Steady state
- Frequency response
  - Bode plot

## Design

- Design specs
- Root locus
- Frequency domain
- PID & Lead-lag
- Design examples

*Matlab simulations*

# Controller design by root locus

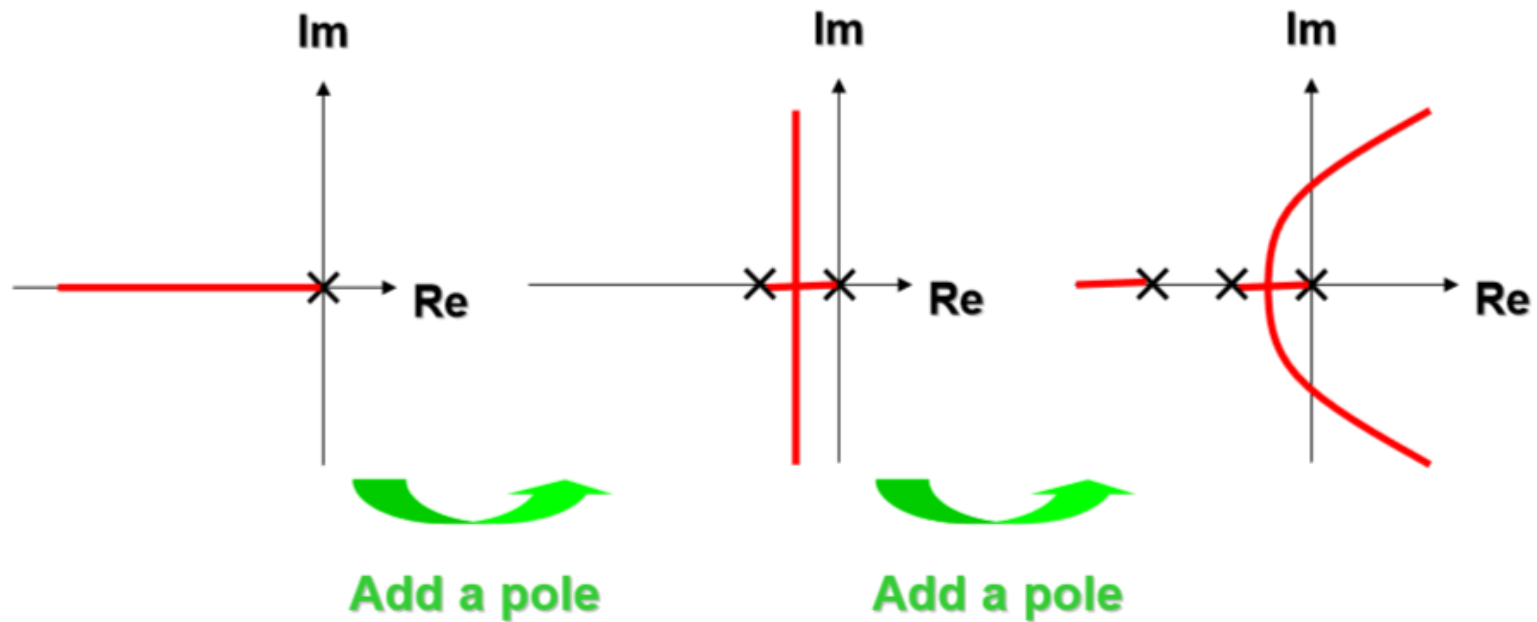


- Place closed-loop poles at desired locations
  - by tuning the gain  $C(s) = K$ . (for time domain specs)
- If root locus does not pass through the desired location, then **reshape** the root locus
  - by adding poles/zeros to  $C(s)$ . How?

*Compensation*

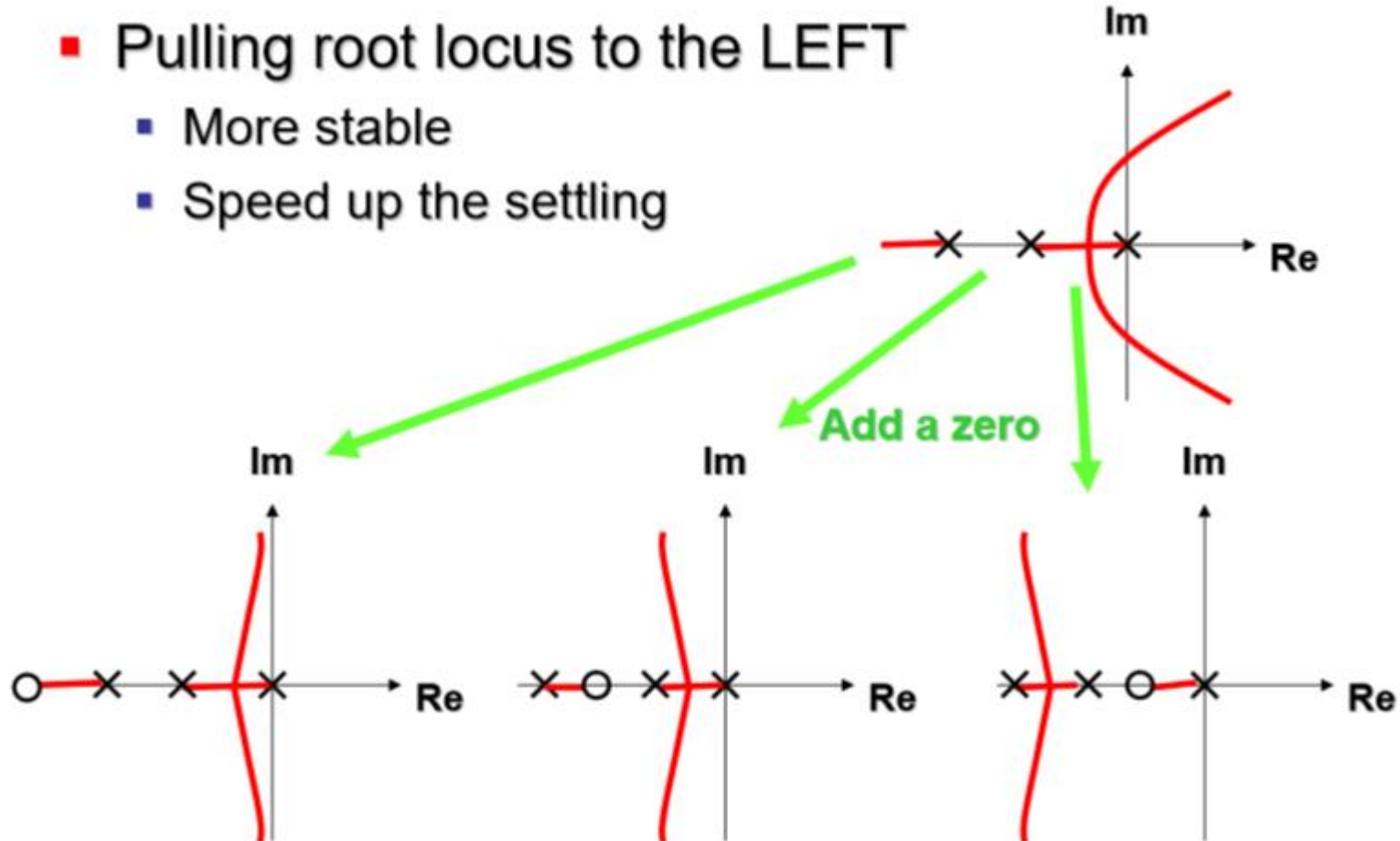
# General effect of addition of poles

- Pulling root locus to the RIGHT
  - Less stable
  - Slow down the settling



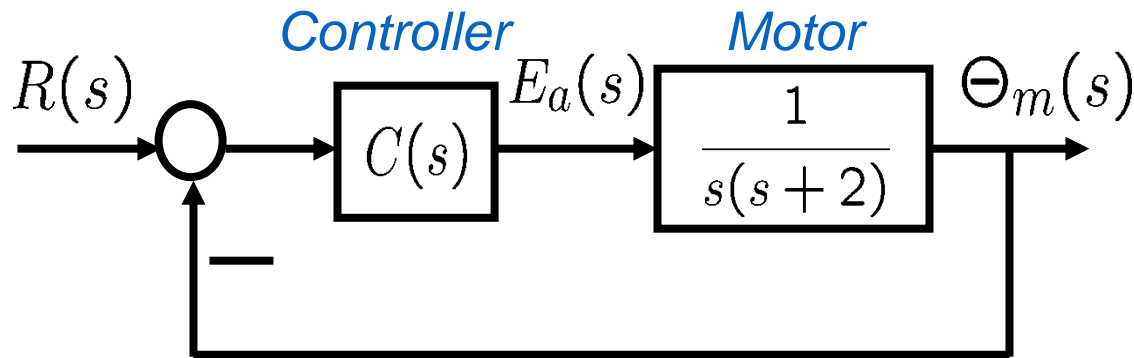
# General effect of addition of zeros

- Pulling root locus to the LEFT
  - More stable
  - Speed up the settling



# Example 1

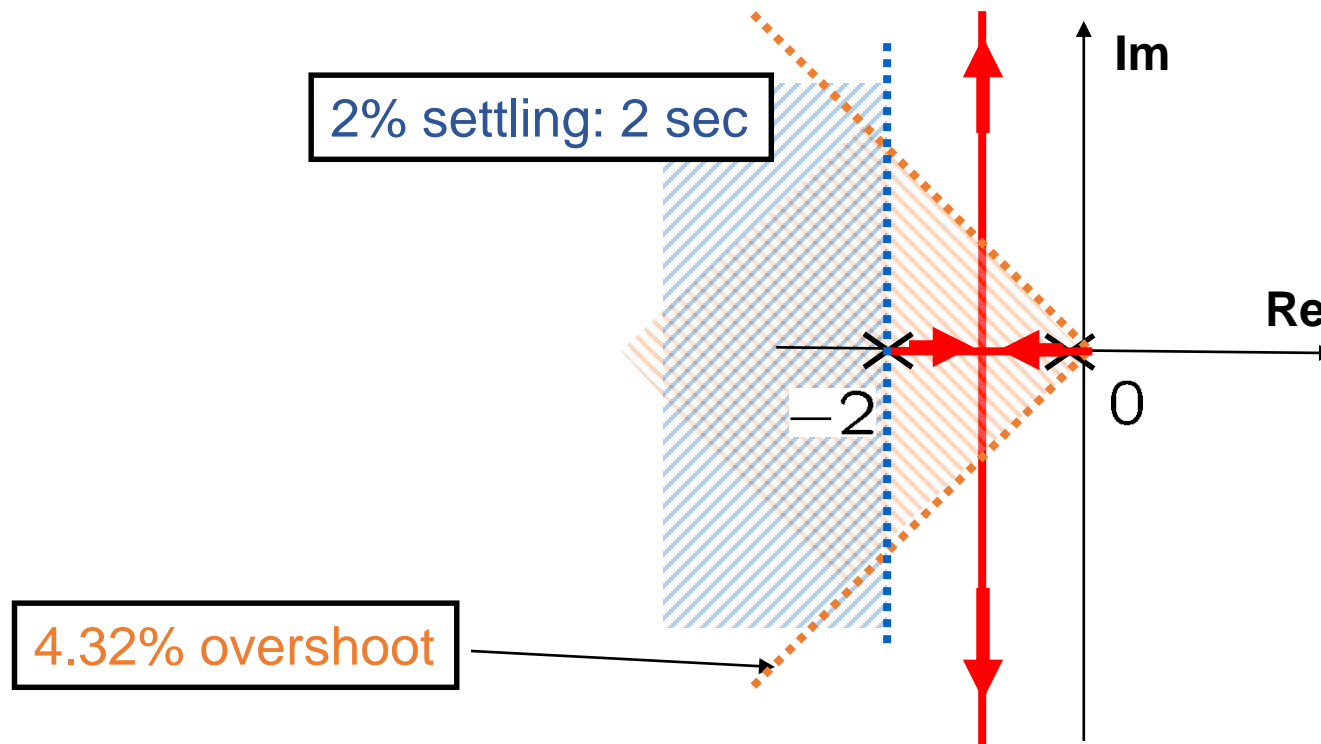
- A feedback system



- Design specifications
  - 2% settling time at most 2 seconds
  - Overshoot at most 4.32%
  - Steady state error
    - Zero for unit step  $r(t) = u(t)$
    - At most 0.05 for unit ramp  $r(t) = tu(t)$

# Example 1 (cont'd)

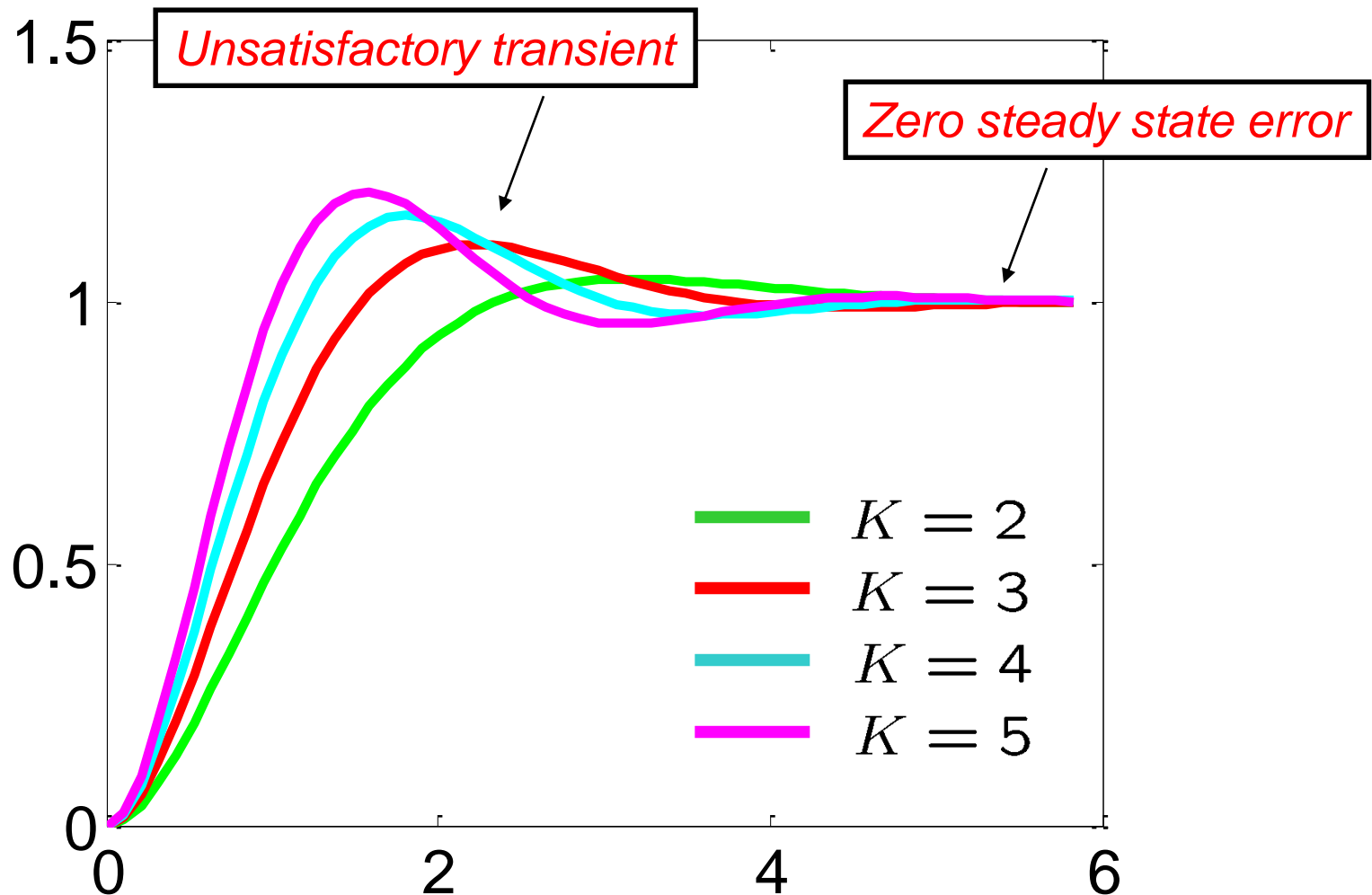
- Root locus for gain controller  $C(s) = K > 0$



*We cannot achieve the design specs  
with the gain feedback controller!*

# Example 1: Step responses for gain controllers

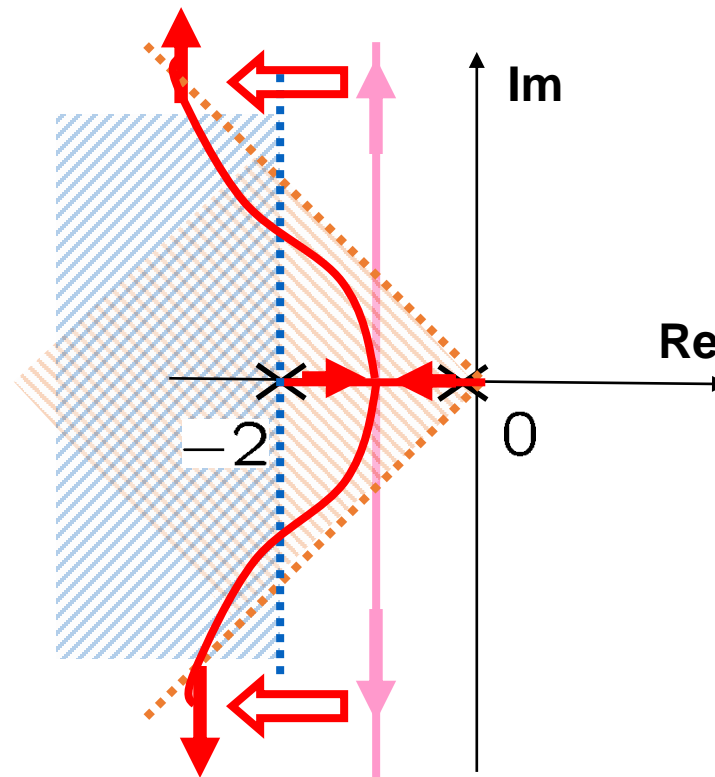
$C(s) = K > 0$



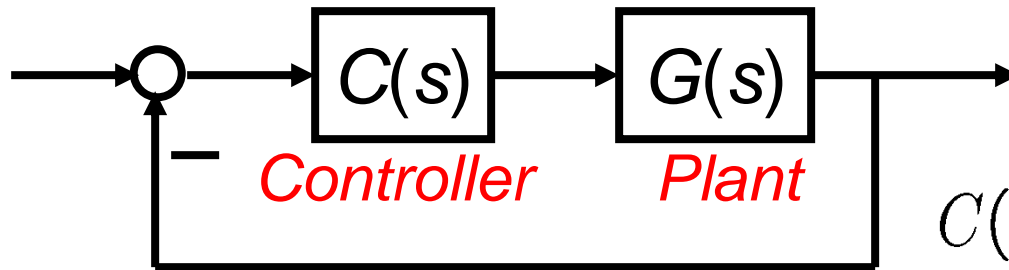


# Example 1 (cont'd)

- We **reshape** the root locus so that it passes through the allowable region.

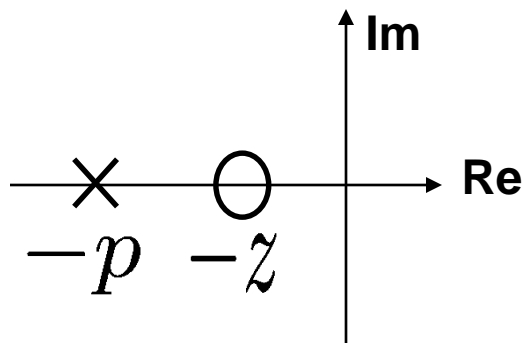


# Lead and lag compensators

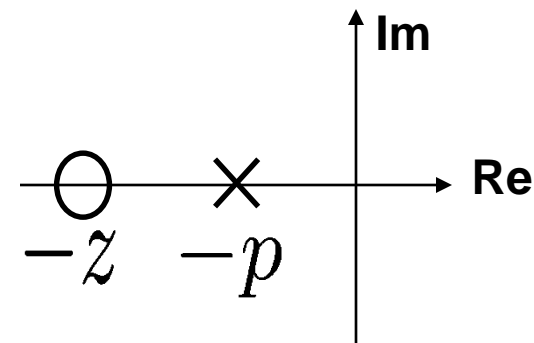


$$C(s) = K \frac{s + z}{s + p}, \quad (z > 0, p > 0)$$

- **Lead** compensator



- **Lag** compensator



The reason why these are called “lead” and “lag” will be explained in frequency response approach (later in this course).

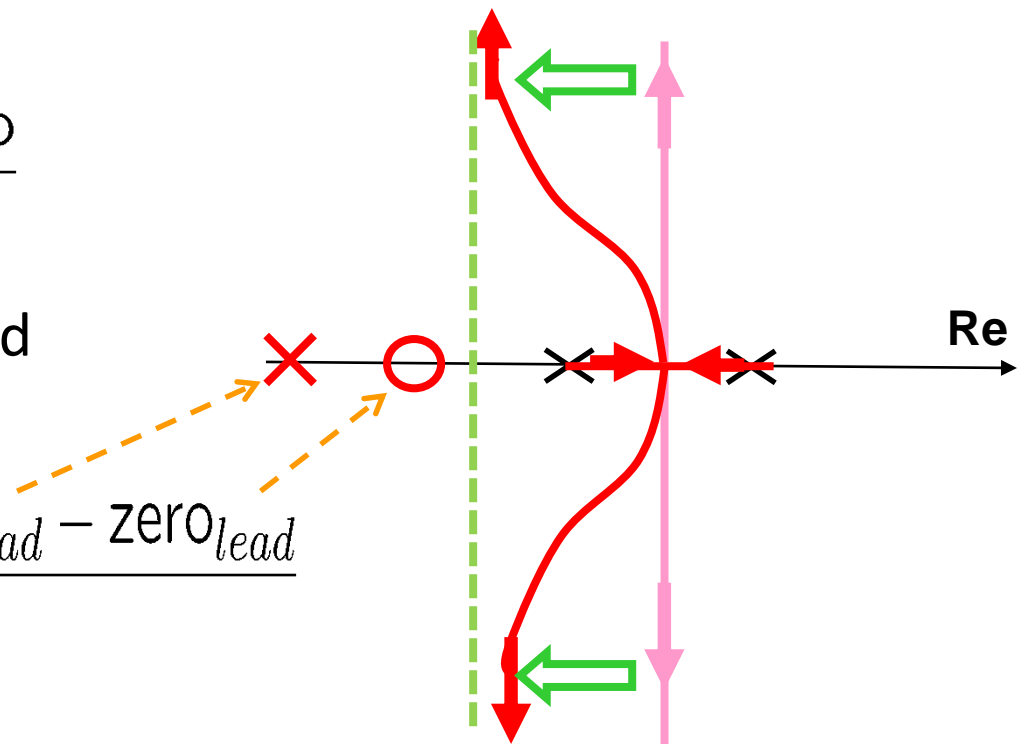
# Reshaping root locus by lead compensators

- Lead compensators move the intersection of asymptotes (the centroid) to the **left**.
  - With plant only

$$\frac{\sum \text{pole} - \sum \text{zero}}{r}$$

- With plant and lead

$$\frac{\sum \text{pole} - \sum \text{zero} + \text{pole}_{lead} - \text{zero}_{lead}}{r}$$



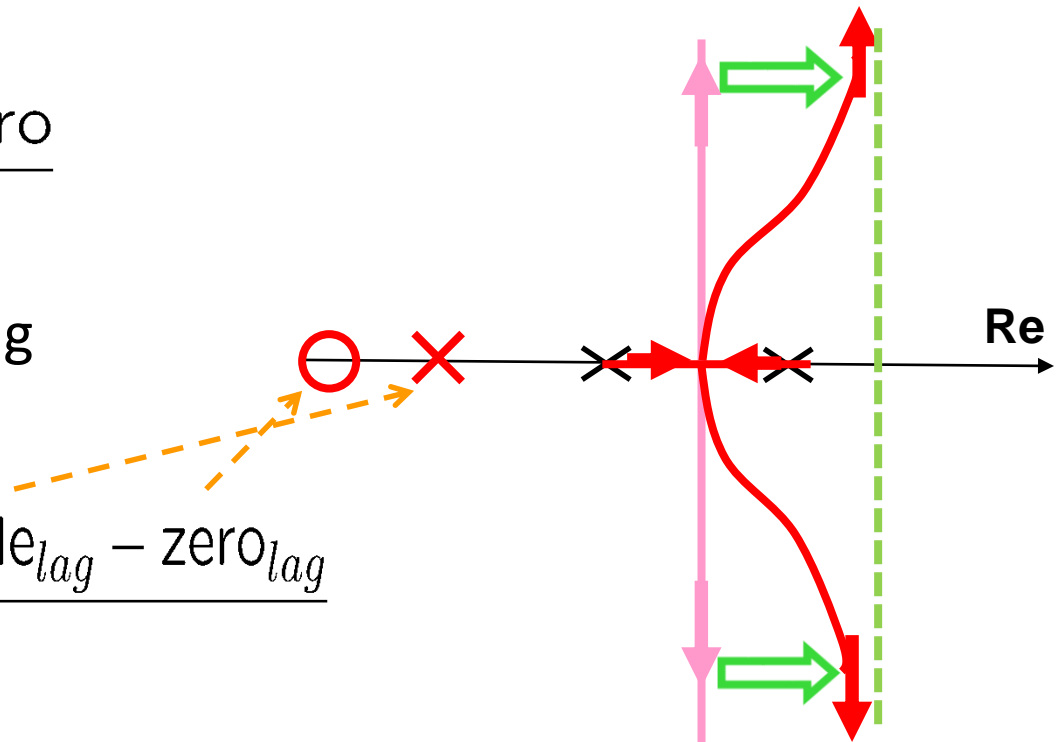
# Reshaping root locus by lag compensators

- Lag compensators move the intersection of asymptotes (the centroid) to the **right**.
  - With plant only

$$\frac{\sum \text{pole} - \sum \text{zero}}{r}$$

- With plant and lag

$$\frac{\sum \text{pole} - \sum \text{zero} + \text{pole}_{lag} - \text{zero}_{lag}}{r}$$



# Roles of lead & lag compensators

- **Lead compensator**
  - Improves transient response
  - Improves stability

$$C_{Lead}(s) = K \frac{s + z_{Lead}}{s + p_{Lead}}$$

- **Lag compensator**
  - Reduces steady state error

$$C_{Lag}(s) = \frac{s + z_{Lag}}{s + p_{Lag}}$$

- **Lead-lag compensator**
  - Takes into account both transient and steady state.

$$C_{LL}(s) = C_{Lead}(s)C_{Lag}(s)$$

# Analytical lead compensator design



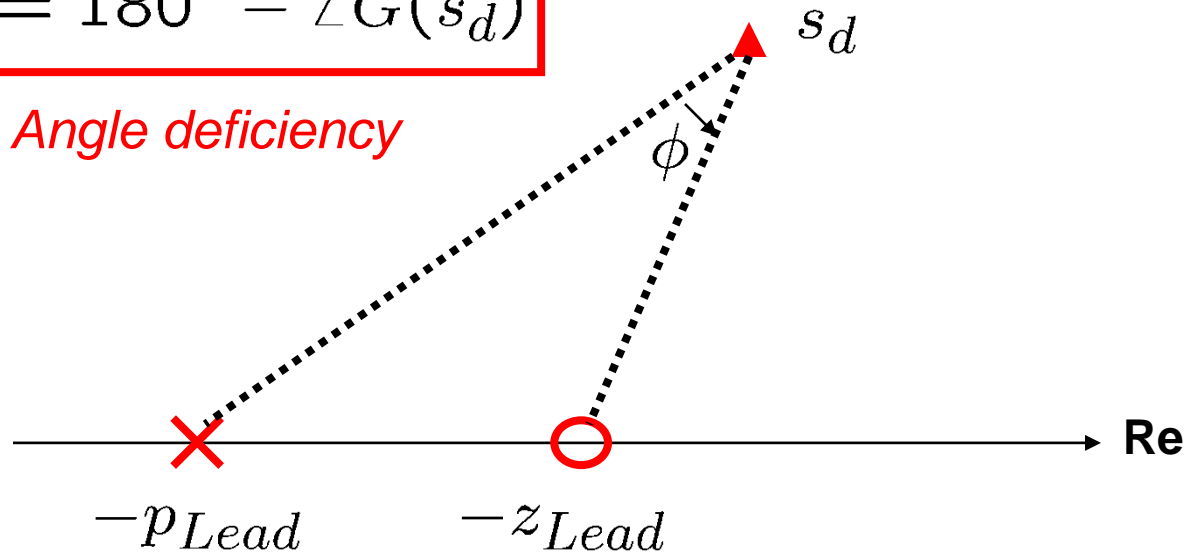
1. Select a desired pole in the allowable region. We aim at reshaping RL to pass through this pole.

# Analytical lead compensator design

2. Select pole/zero in  $C_{Lead}(s) = K \frac{s + z_{Lead}}{s + p_{Lead}}$  as

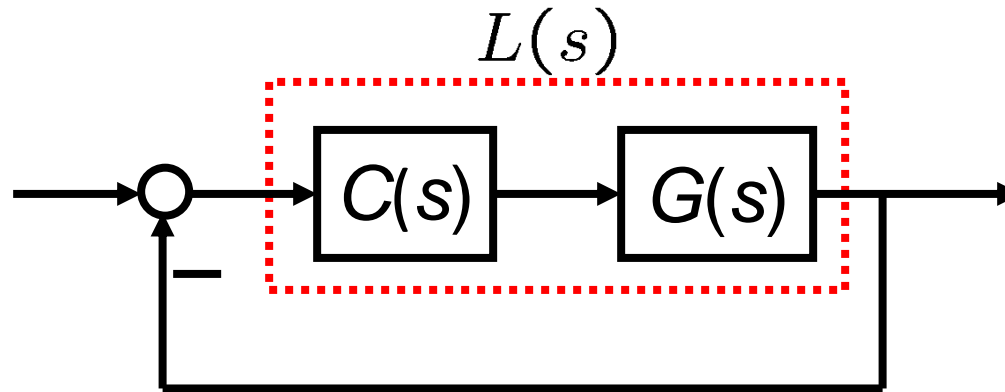
$$\phi = 180^\circ - \angle G(s_d)$$

*Angle deficiency*



# Angle and magnitude conditions

- For an open-loop transfer function  $L(s)$ ,



- A point  $s$  to be on root locus  $\leftrightarrow$  it satisfies
  - Angle condition**

$$\angle L(s) = 180^\circ \times (2k + 1), \quad k = 0, \pm 1, \pm 2, \dots$$

- For a point on root locus, gain  $K$  is obtained by
  - Magnitude condition**

$$|L(s)| = \frac{1}{K}$$

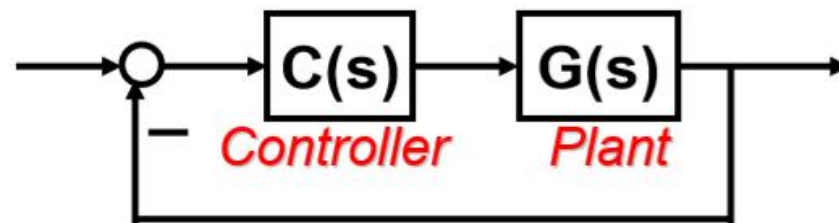


# Example 2

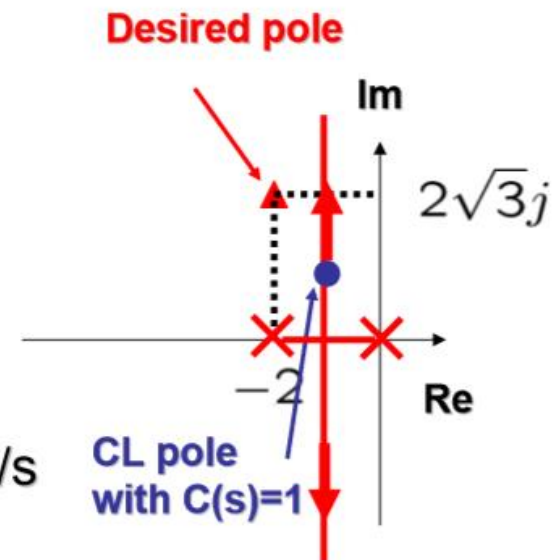
## Lead compensator design

- Consider a system

$$G(s) = \frac{4}{s(s+2)}$$



- Performance specification
  - Damping ratio  $\zeta=0.5$
  - Undamped natural freq.  $\omega_n=4$  rad/s



## Example 2 (cont'd)

### Lead compensator design (cont'd)

Evaluate  $G(s)$  at the desired pole.  $s_d = -\zeta\omega_n + j\omega_n\sqrt{1-\zeta^2}$

$$G(\underbrace{-2+2\sqrt{3}j}_{s_d}) = \frac{4}{(-2+2\sqrt{3}j)2\sqrt{3}j}$$

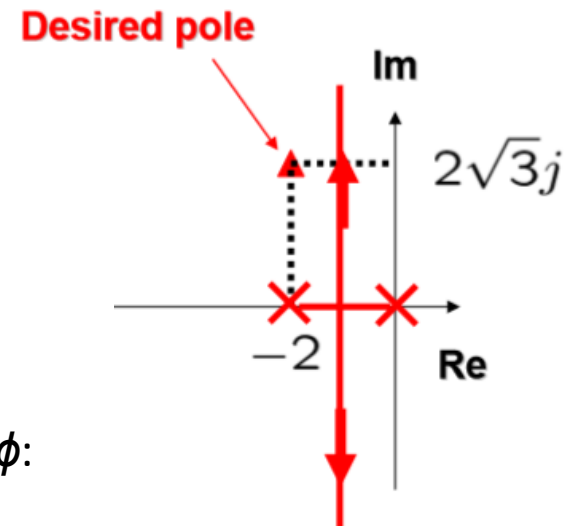
$$\begin{aligned}\angle G^*(s_d) &= \angle 4 - \angle(-2+2\sqrt{3}j) - \angle 2\sqrt{3}j \\ &= 0^\circ - \left( \tan^{-1} \left( \frac{2\sqrt{3}}{-2} \right) \right) - 90^\circ \\ &= -(+120^\circ) - 90^\circ = -210^\circ \rightarrow \\ \angle G^*(s_d) &= -210^\circ\end{aligned}$$

Convert “-210°” to an angle from +Re-axis:

$$360^\circ - 210^\circ = +150^\circ \rightarrow \angle G(s_d) = +150^\circ$$

Now, use the **angle deficiency formula** to calculate  $\phi$ :

$$\phi = 180^\circ - \angle G(s_d) \rightarrow \phi = 180^\circ - 150^\circ \rightarrow \phi = +30^\circ$$



## Example 2 (cont'd)

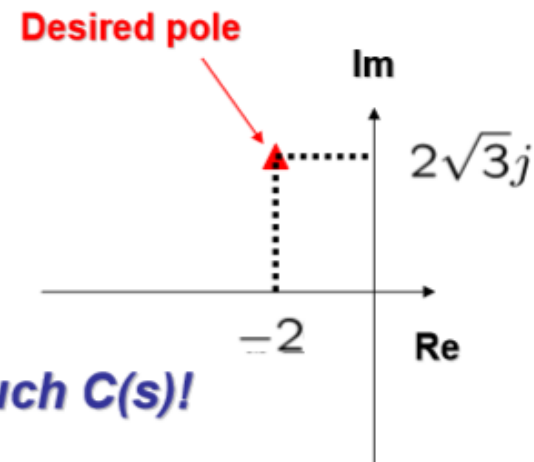
### Lead compensator design (cont'd)

To compensate angle deficiency,  
design a lead compensator  $C(s)$

$$C(s) = K \frac{s + z}{s + p}$$

satisfying

$$\angle C(-2 + 2\sqrt{3}j) = 30 = \phi$$



*There are many ways to design such  $C(s)$ !*

## Example 2 (cont'd)

### How to select pole and zero?

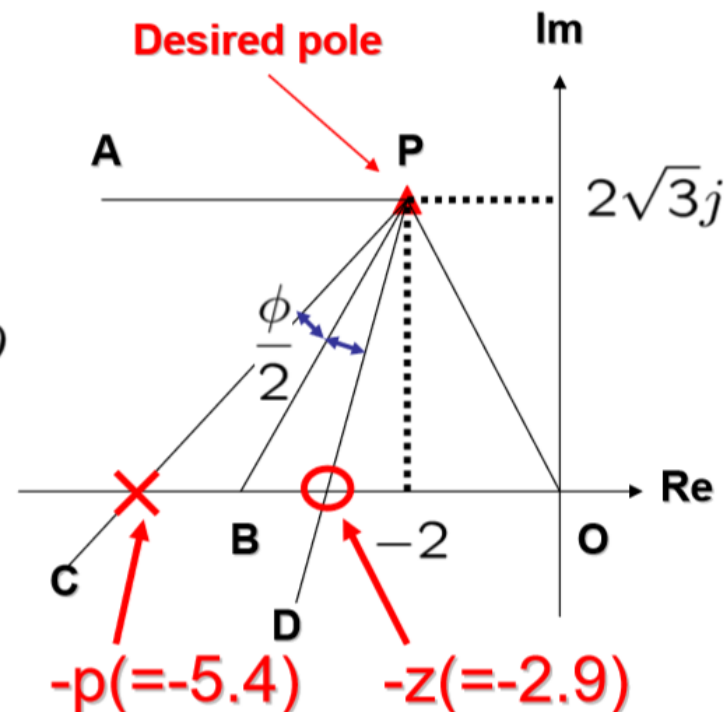
- Draw horizontal line PA
- Draw line PO
- Draw bisector PB

$$\angle APB = \angle BPO = \frac{1}{2} \angle APO$$

- Draw PC and PD

$$\angle CPB = \angle BPD = \frac{\phi}{2}$$

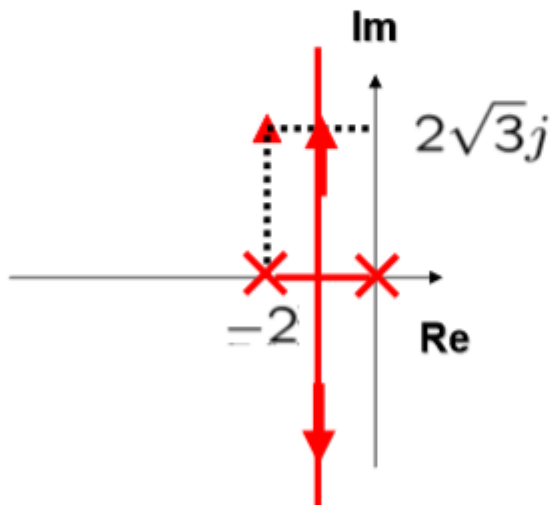
- Pole and zero of C(s) are shown in the figure.



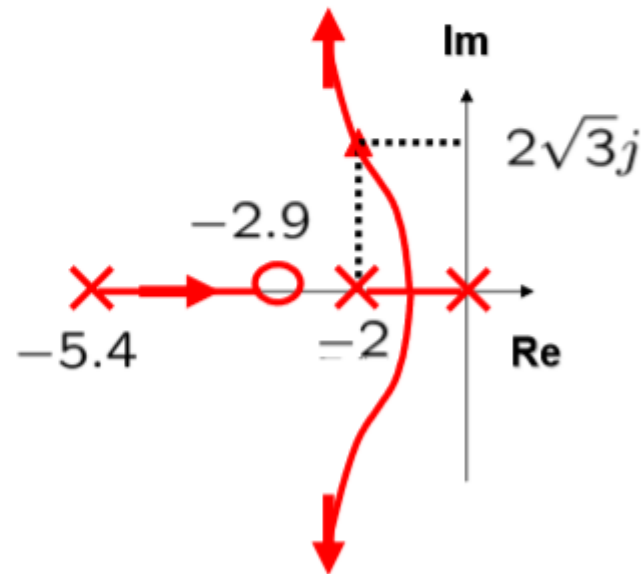
## Example 2 (cont'd)

### Comparison of root locus

■  $G(s)$



■  $G(s)C(s)$



**Improved stability!**

## Example 2 (cont'd)

### How to design the gain K?

- Lead compensator

$$C(s) = K \frac{s + 2.9}{s + 5.4}$$

- Open loop transfer function

$$G(s)C(s) = K \frac{4(s + 2.9)}{s(s + 2)(s + 5.4)}$$

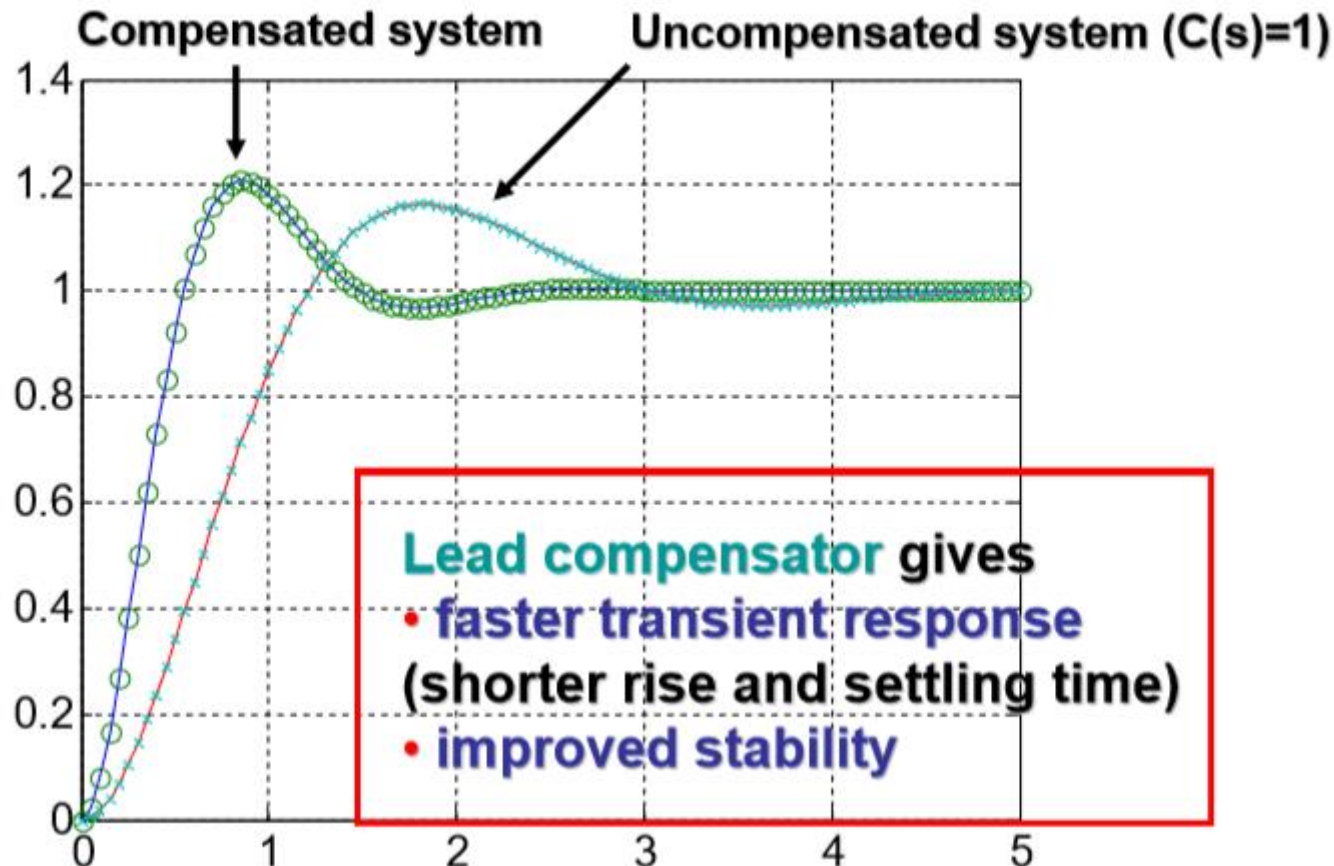
- Magnitude condition

$$K \left| \frac{4(s + 2.9)}{s(s + 2)(s + 5.4)} \right|_{s=-2+2\sqrt{3}j} = 1 \quad \rightarrow \quad K = 4.675$$

$$\rightarrow G(s)C(s) = \frac{4}{s(s + 2)} \cdot \frac{4.675(s + 2.9)}{s + 5.4}$$

## Example 2 (cont'd)

### Comparison of step responses





## Example 2 (cont'd)

### Error constants

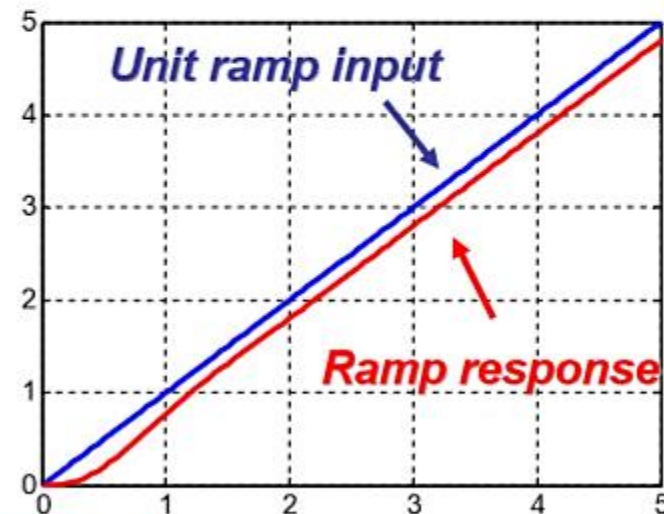
$$G(s)C(s) = \frac{4}{s(s+2)} \cdot \frac{4.675(s+2.9)}{s+5.4}$$

- Step-error constant

$$K_p = \lim_{s \rightarrow 0} G(s)C(s) = \infty$$

- Ramp-error constant

$$K_v = \lim_{s \rightarrow 0} sG(s)C(s) = 5.02$$



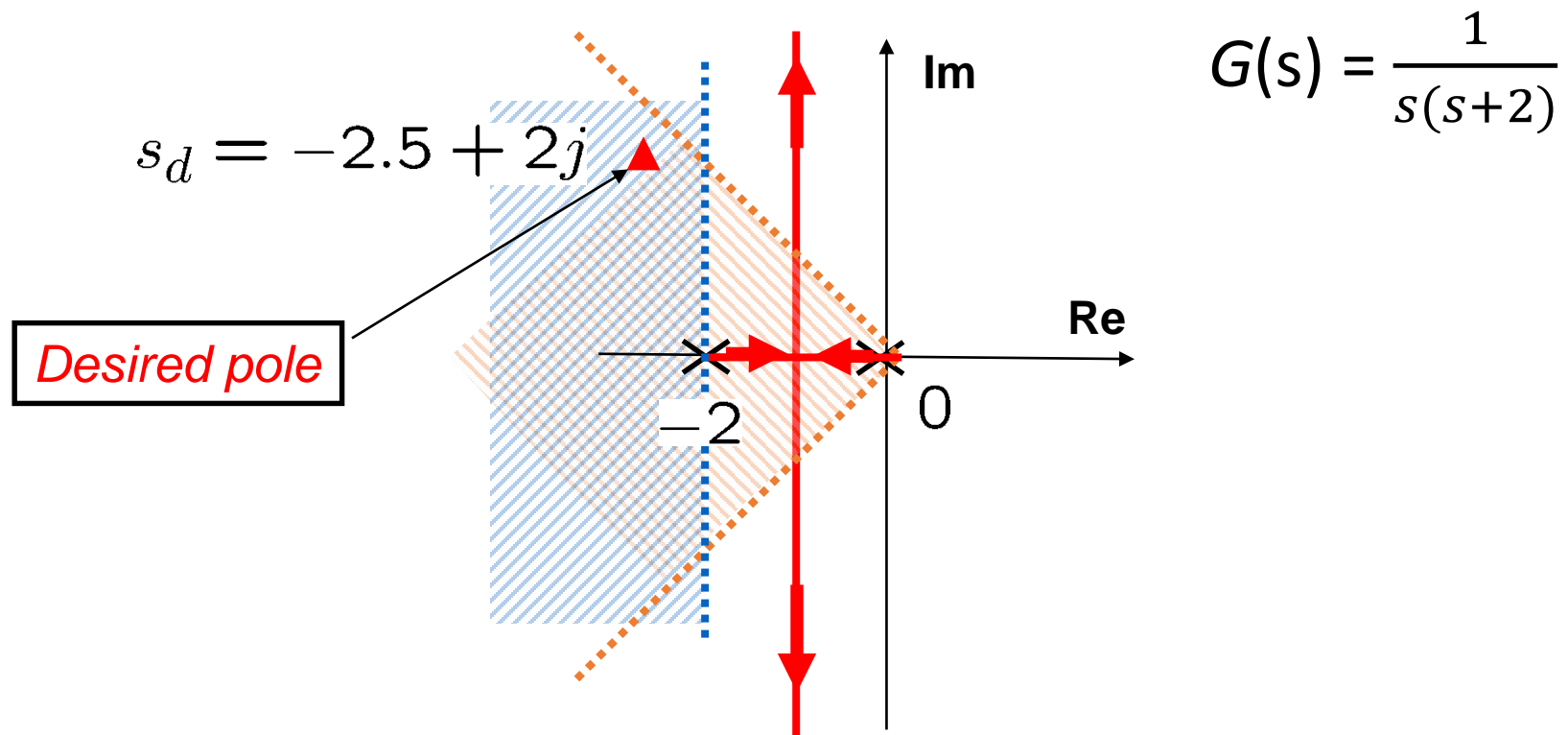
*Lag compensator can be used to reduce steady-state error.*

This will be shown soon.



## Example 3

Design a lead compensator controller by using the given desired pole in the allowable region.



We aim at reshaping RL to pass through the desired pole.

## Example 3: One possible $C_{Lead}$

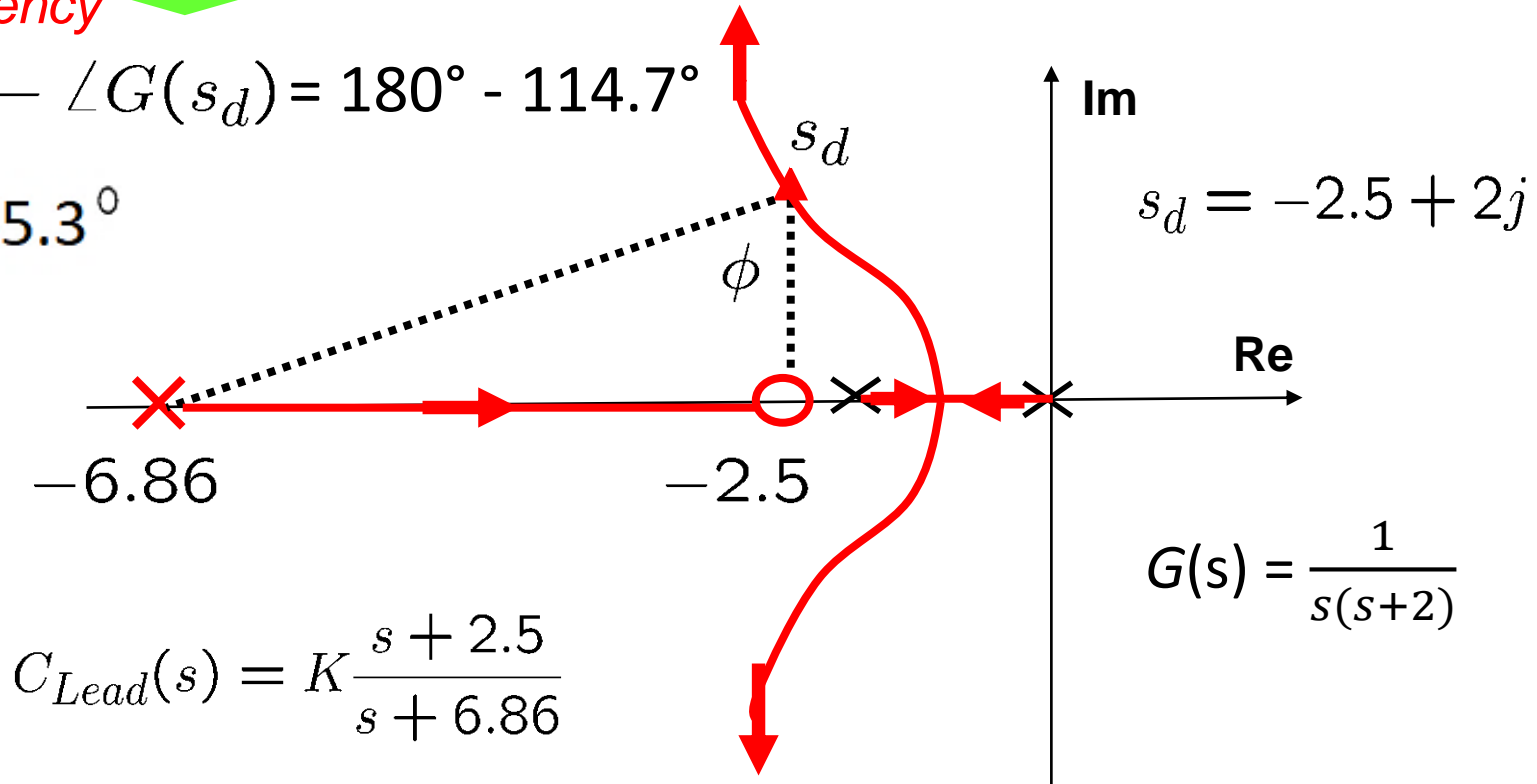
$$\angle G^*(s_d) = \angle \frac{1}{s_d(s_d + 2)} = -245.3^\circ \rightarrow 360^\circ - 245.3^\circ = 114.7^\circ$$

$$\rightarrow \angle G(s_d) = 114.7^\circ$$

Angle deficiency

$$\phi = 180^\circ - \angle G(s_d) = 180^\circ - 114.7^\circ$$

$$\phi = 65.3^\circ$$



## Example 3: Design of pole/zero in $C_{Lead}$

- Lead compensator

$$C_{Lead}(s) = K \frac{s + 2.5}{s + 6.86}$$

- Open-loop transfer function

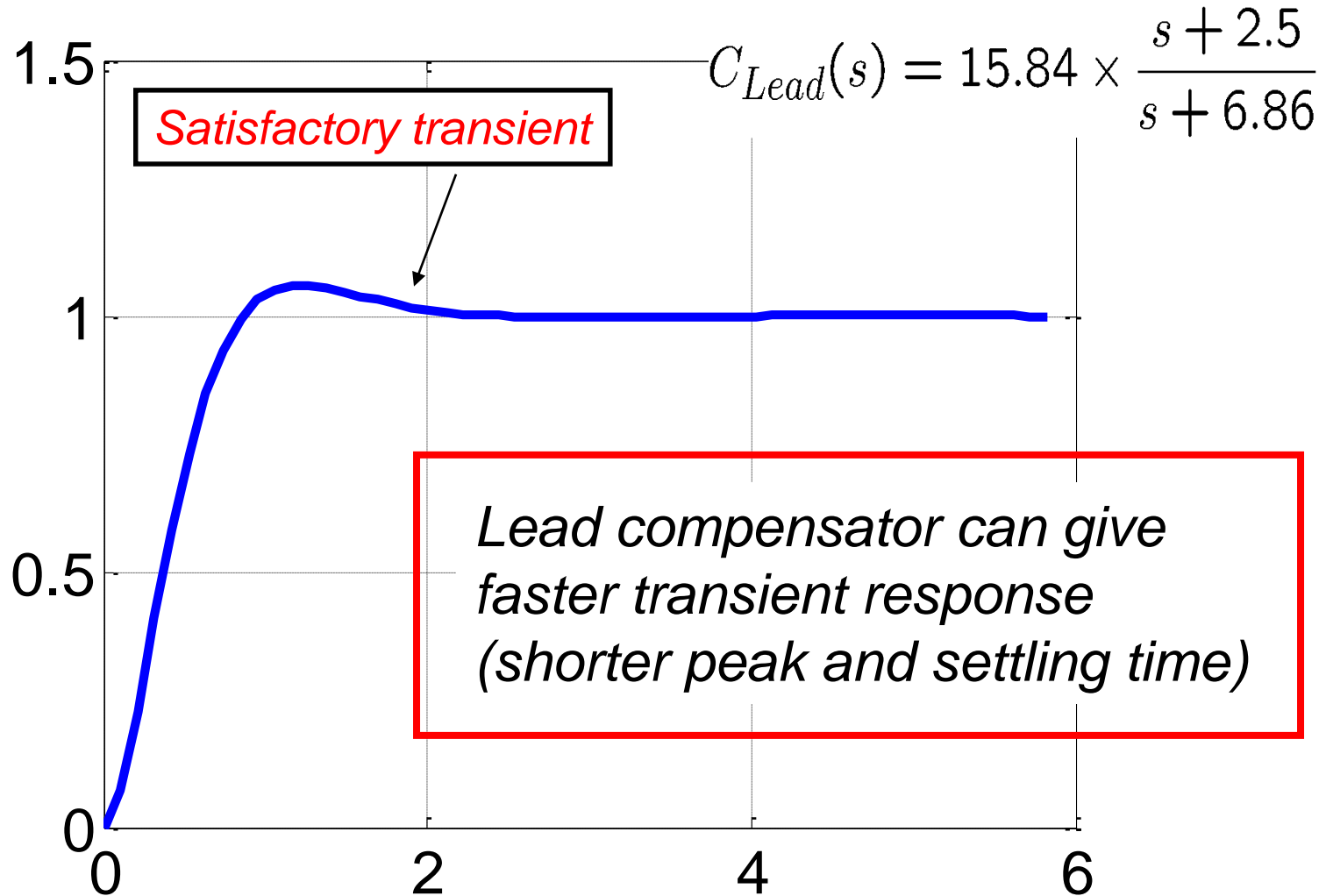
$$G(s)C_{Lead}(s) = K \frac{s + 2.5}{\underbrace{s(s + 2)(s + 6.86)}_{L_0(s)}}$$

- Gain computation

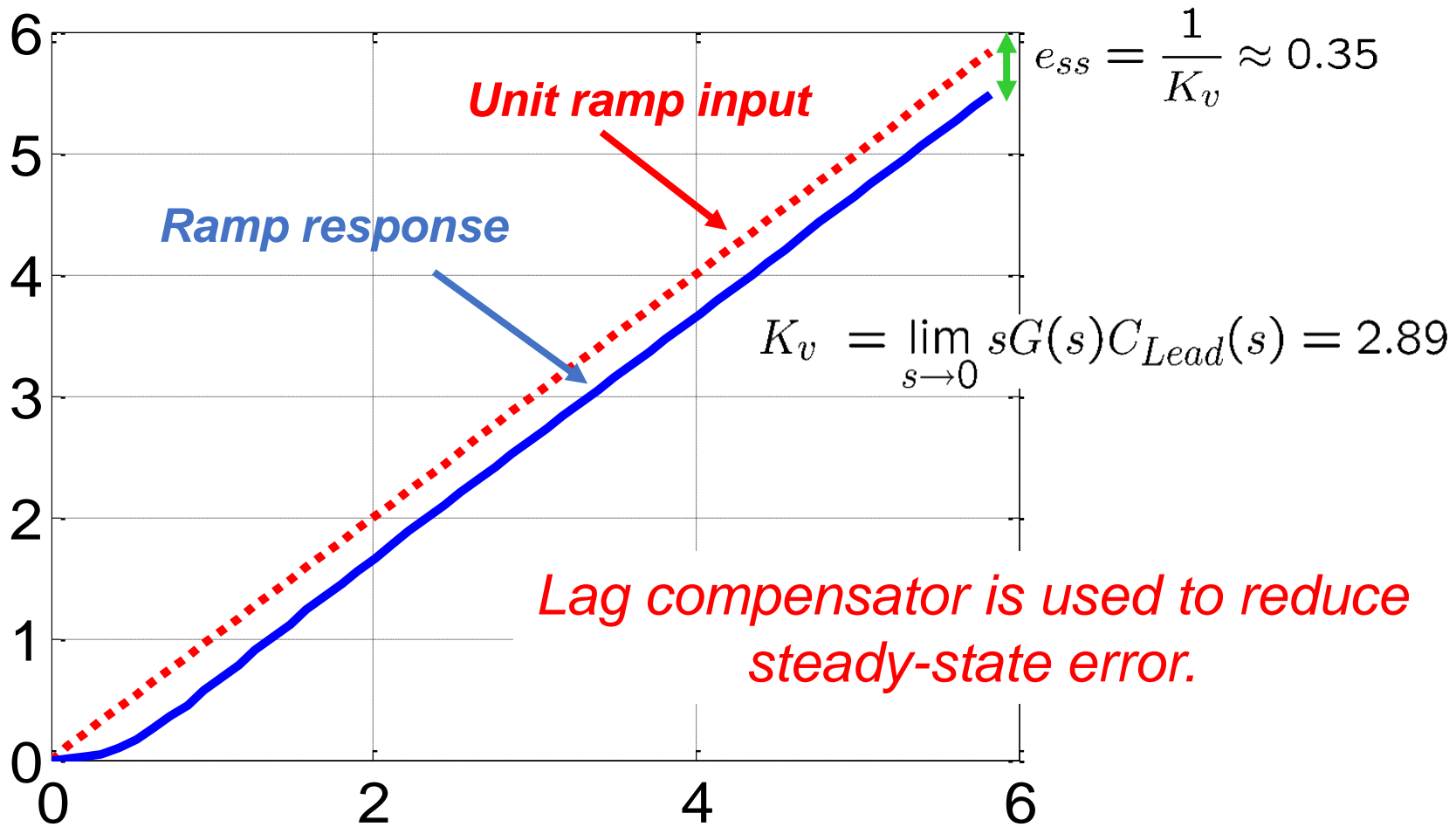
$$K = - \left. \frac{1}{L_0(s)} \right|_{s=s_d} = \dots = 15.84 \quad \rightarrow$$

$$G(s)C_{Lead}(s) = 15.84 \frac{s + 2.5}{s(s + 2)(s + 6.86)}$$

## Example 3: Step response with $C_{Lead}$



## Example 3: Steady state error for $r(t) = tu(t)$



# Roles of lead & lag compensators

- Lead compensator
  - Improves transient response
  - Improves stability

$$C_{Lead}(s) = K \frac{s + z_{Lead}}{s + p_{Lead}}$$

- Lag compensator
  - Reduces steady state error

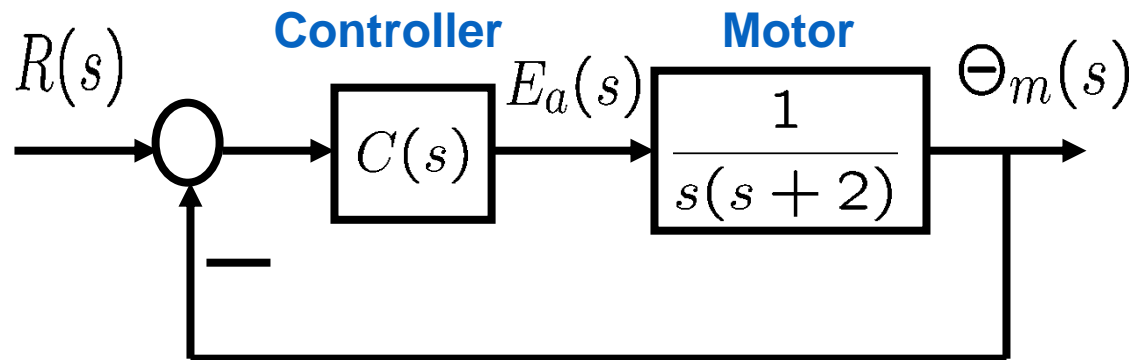
$$C_{Lag}(s) = \frac{s + z_{Lag}}{s + p_{Lag}}$$

- Lead-lag compensator
  - Takes into account both transient and steady state.

$$C_{LL}(s) = C_{Lead}(s)C_{Lag}(s)$$

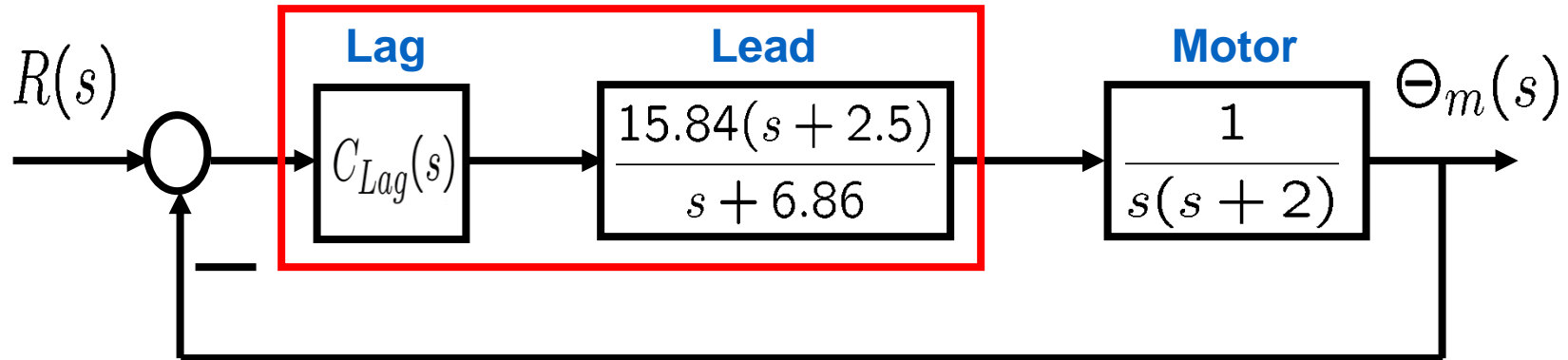
## Example 4 (restated)

- A feedback system



- Design specifications
  - 2% settling time at most 2 seconds
  - Overshoot at most 4.32%
  - Steady state error
    - Zero for unit step  $r(t) = u(t)$
    - At most 0.05 for unit ramp  $r(t) = tu(t)$   $\Rightarrow K_v > 20$

## Example 4: After $C_{Lead}$ design



- For a designed  $C_{Lead}$ , design  $C_{Lag}$  so that
  - Steady state error for unit ramp  $r(t)$  is reduced ( $e_{ss}$  should be less than 0.02).
  - Transient is maintained. That is, we do not want to lose the satisfactory transient property achieved by the lead compensator.



## Example 4: Design of $C_{Lag}(s) = \frac{s + z_{Lag}}{s + p_{Lag}}$

- We would like to reduce the steady state error, i.e., to increase ramp-error constant

$$K_v = \lim_{s \rightarrow 0} sG(s)C_{Lead}(s)C_{Lag}(s) = 2.89 \times \frac{z_{Lag}}{p_{Lag}} > 20$$

Take, for example,  $z_{Lag} = 10p_{Lag}$

$$\frac{z_{Lag}}{p_{Lag}} > 6.92$$

- Also, we want to maintain the transient property,

$$|p_{Lag}| : \text{small}$$

- We still want our RL to pass through  $s_d$ , despite modifying our  $L(s)$ .

$$\left. \begin{array}{l} 1 + G(s_d)C_{Lead}(s_d) = 0 \\ C_{Lag}(s_d) \approx 1 \end{array} \right\} \rightarrow 1 + G(s_d)C_{Lead}(s_d)C_{Lag}(s_d) \approx 0$$

# Why should $p_{Lag}$ be small?

$p_{Lag}$  : small



$$z_{Lag} = 10p_{Lag}$$

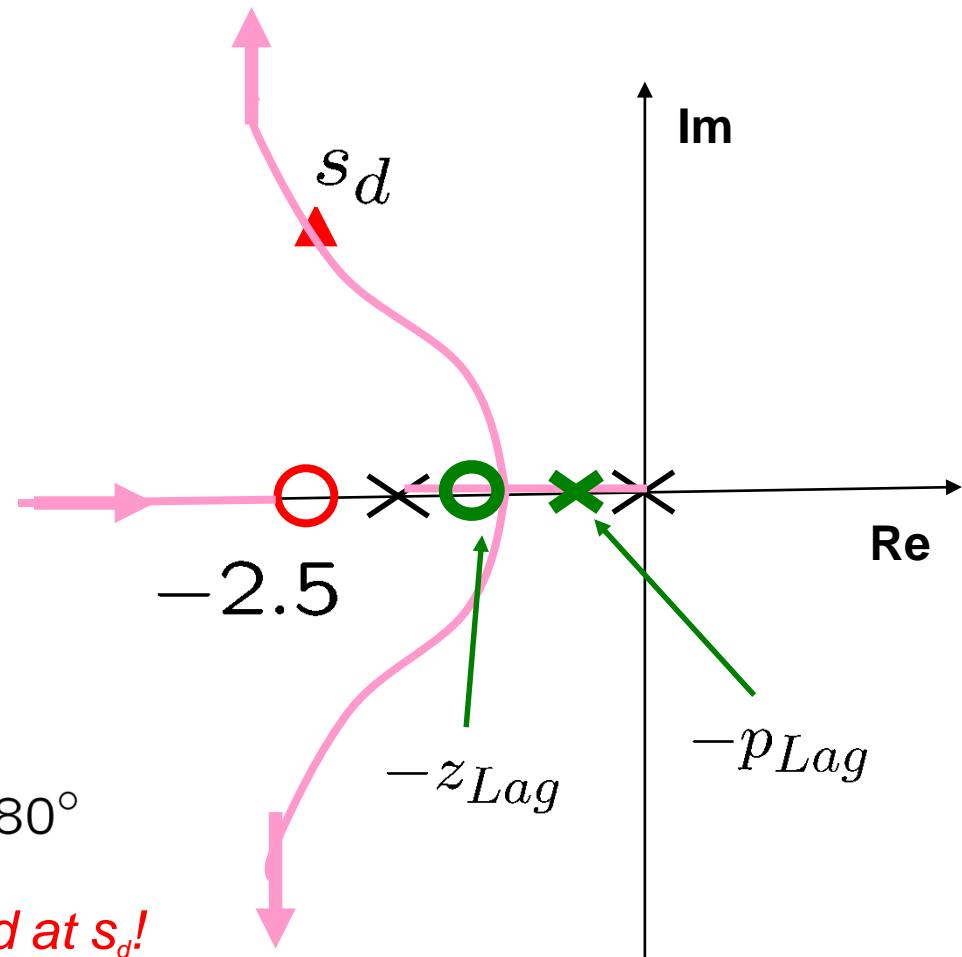


$$C_{Lag}(s_d) = \frac{s_d + z_{Lag}}{s_d + p_{Lag}} \approx 1$$



$$\angle G(s_d)C_{Lead}(s_d)C_{Lag}(s_d) \approx 180^\circ$$

*Angle condition: almost satisfied at  $s_d$ !*



## Example 4: $C_{Lag}$ design

- In design projects, we assume a small  $p_{Lag}$  and use trial-and-error! Here,  $p_{Lag}$  will be given to you.

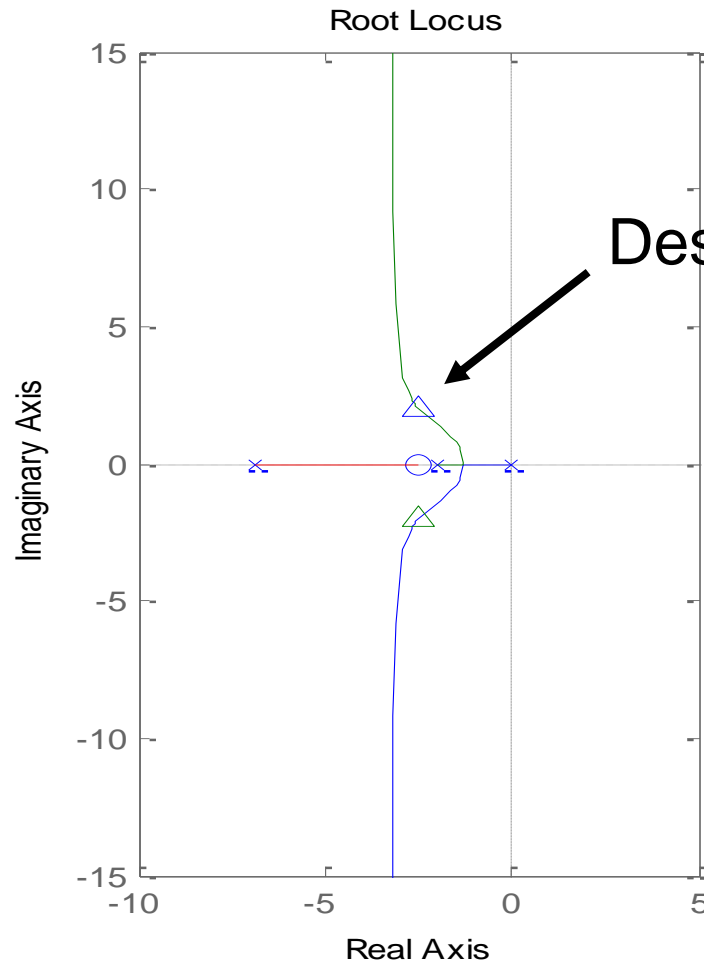
$$p_{Lag} = 0.005 \quad \longrightarrow \quad z_{Lag} = 0.05$$

$$\longrightarrow C_{Lag}(s) = \frac{s + 0.05}{s + 0.005}$$

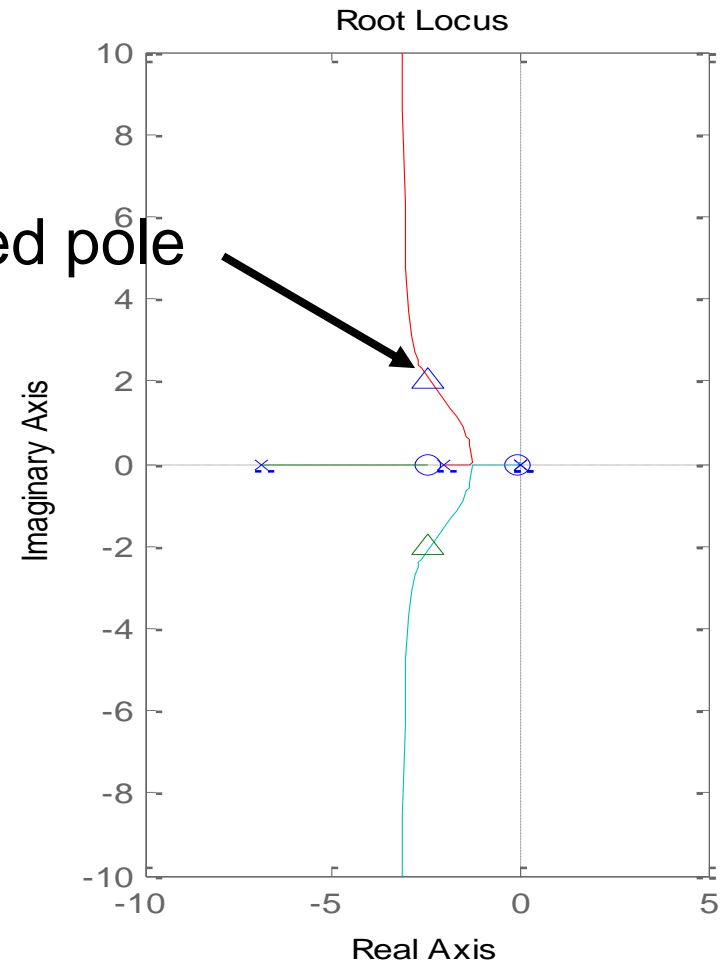
$$\longrightarrow C_{LL}(s) = \underbrace{\frac{15.84(s + 2.5)}{s + 6.86}}_{C_{Lead}(s)} \times \underbrace{\frac{s + 0.05}{s + 0.005}}_{C_{Lag}(s)}$$

# Example 4: Root locus

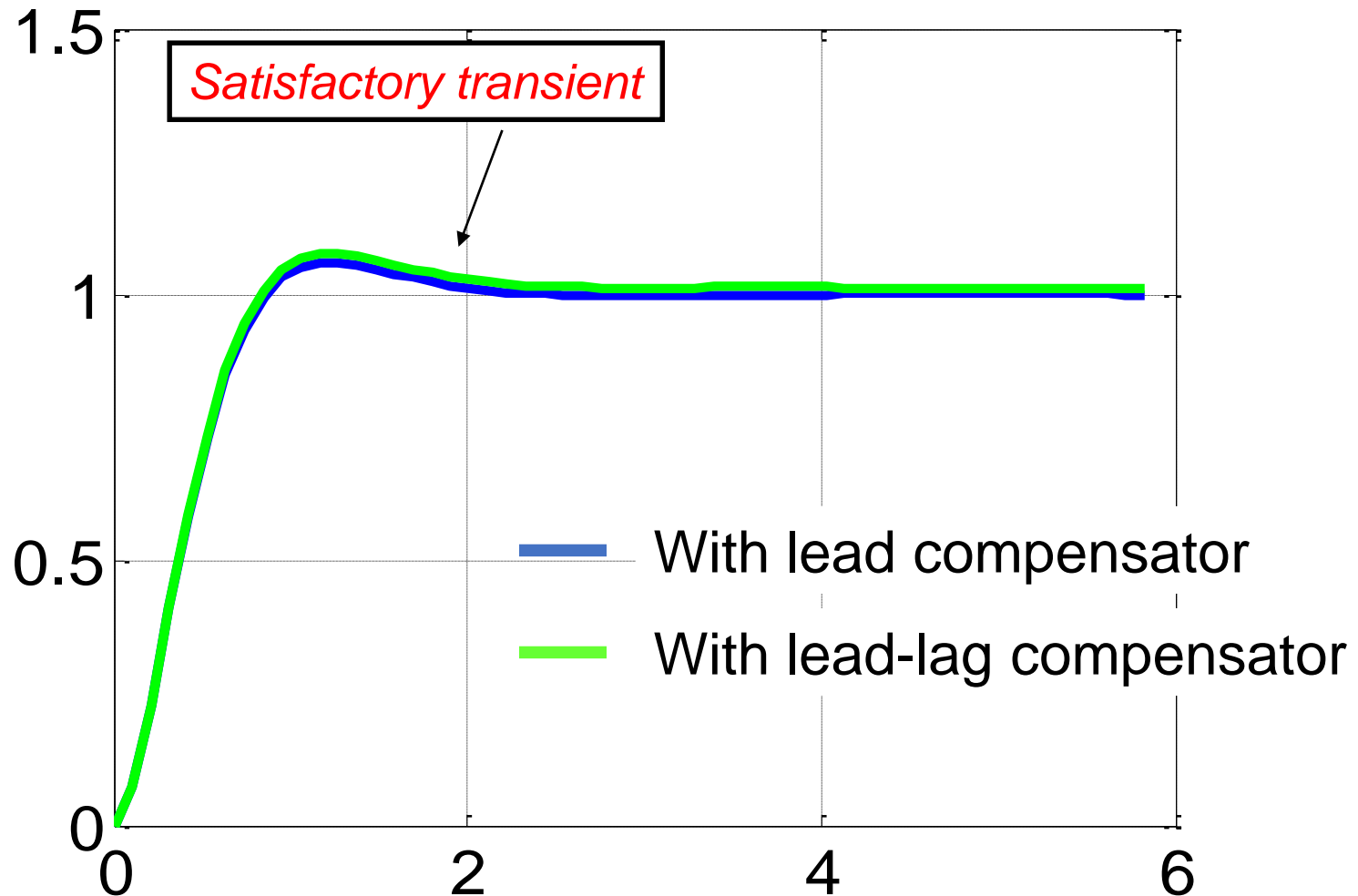
With lead compensator



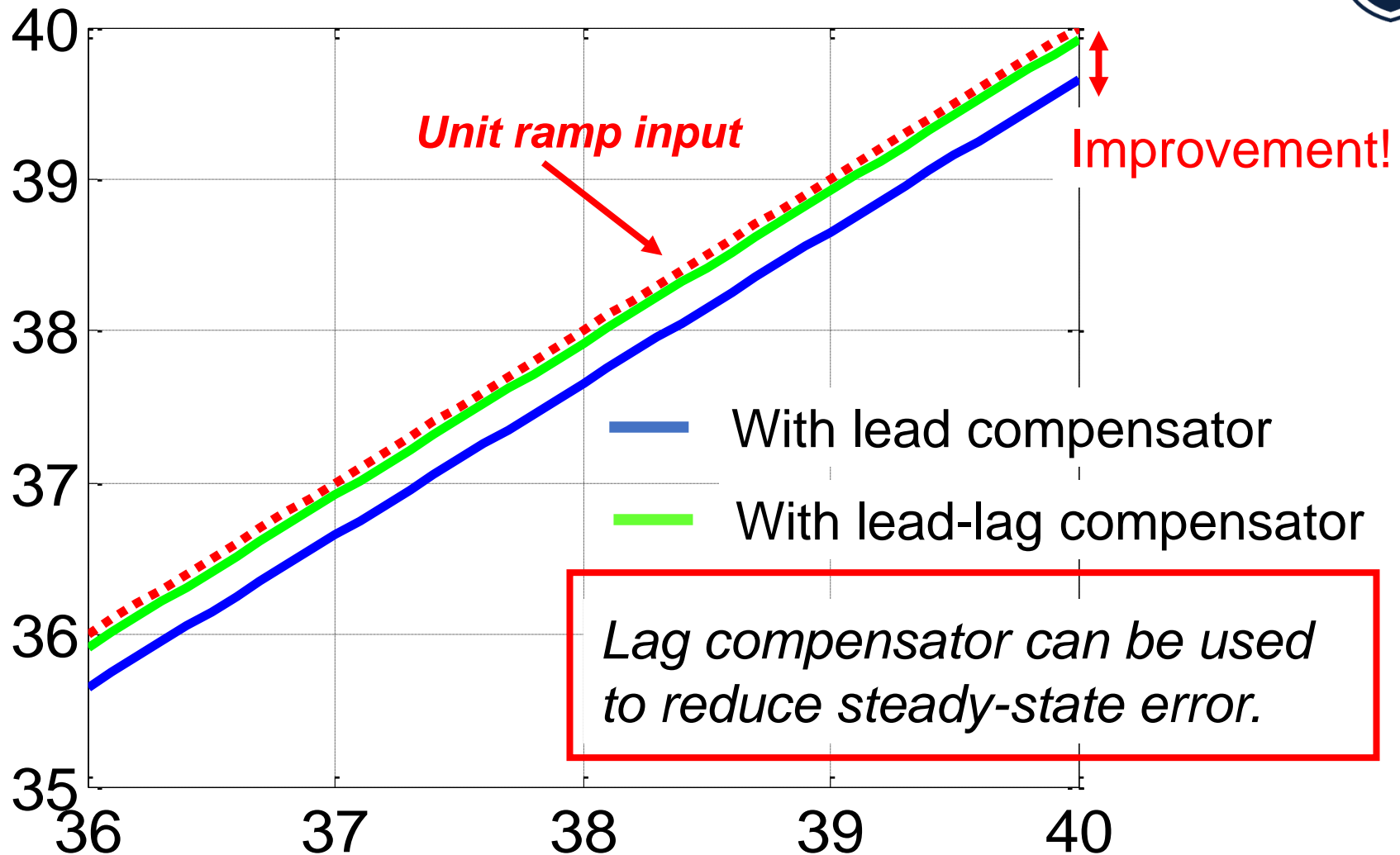
With lead-lag compensator



## Example 4: Comparison of step responses



## Example 4: Comparison of ramp responses



# Example 2 (revisited)

If we only use a lead compensator.

## Error constants

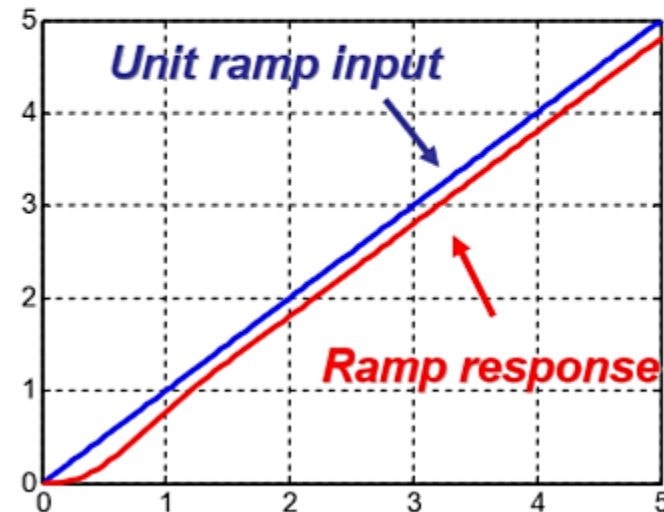
$$G(s)C(s) = \frac{4}{s(s+2)} \cdot \frac{4.675(s+2.9)}{s+5.4}$$

- Step-error constant

$$K_p = \lim_{s \rightarrow 0} G(s)C(s) = \infty$$

- Ramp-error constant

$$K_v = \lim_{s \rightarrow 0} sG(s)C(s) = 5.02$$



*Lag compensator can be used to reduce steady-state error.*

## Example 2 (revisited)

### How to design lag compensator

- Lag compensator  $C_{Lag}(s) = \frac{s + z}{s + p}$
- We want to increase ramp-error constant

$$e_{5s} < 0.02; \quad e_{ss} = \frac{R}{K_v}$$

$$\frac{1}{K_v} < 0.02 \rightarrow K_v > 50$$

$$K_v = \lim_{s \rightarrow 0} sG(s)C_{Lead}(s)C_{Lag}(s) = 5.02 \cdot \frac{z}{p} > 50$$

$$\frac{z_{Lag}}{p_{Lag}} > 9.96 \rightarrow \mathbf{z_{Lag} = 10p_{Lag}}$$

- We still want our RL to pass through  $s_d$ , despite modifying our  $L(s)$ .

$$\left. \begin{array}{l} 1 + G(s_d)C_{Lead}(s_d) = 0 \\ C_{Lag}(s_d) \approx 1 \end{array} \right\} \rightarrow 1 + G(s_d)C_{Lead}(s_d)C_{Lag}(s_d) \approx 0$$



## Example 2 (revisited)

- For the desired CL pole  $s_d = -2 + 2\sqrt{3}j$

$$C_{Lag}(s_d) \approx 1 \iff \left| \frac{s_d + 10p}{s_d + p} \right| \approx 1 \quad \angle \left( \frac{s_d + 10p}{s_d + p} \right) \approx 0$$

- Let us say  $p_{Lag}$  is given as 0.025:

$$\begin{aligned} z_{Lag} &= 10p_{Lag} \\ &= (10)(0.025) = 0.25 \end{aligned} \quad \longrightarrow \quad \left| \frac{s_d + 10p}{s_d + p} \right| = 0.97 \quad \angle \left( \frac{s_d + 10p}{s_d + p} \right) \approx -2.88^\circ$$

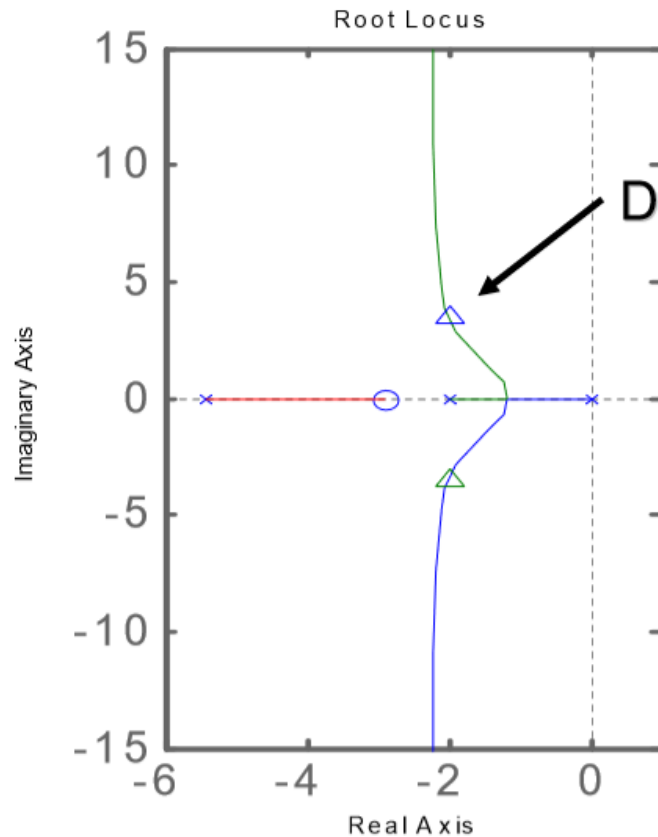
- Lead-lag controller

$$C_{LL}(s) = 4.675 \frac{s + 2.9}{s + 5.4} \cdot \frac{s + 0.25}{s + 0.025}$$

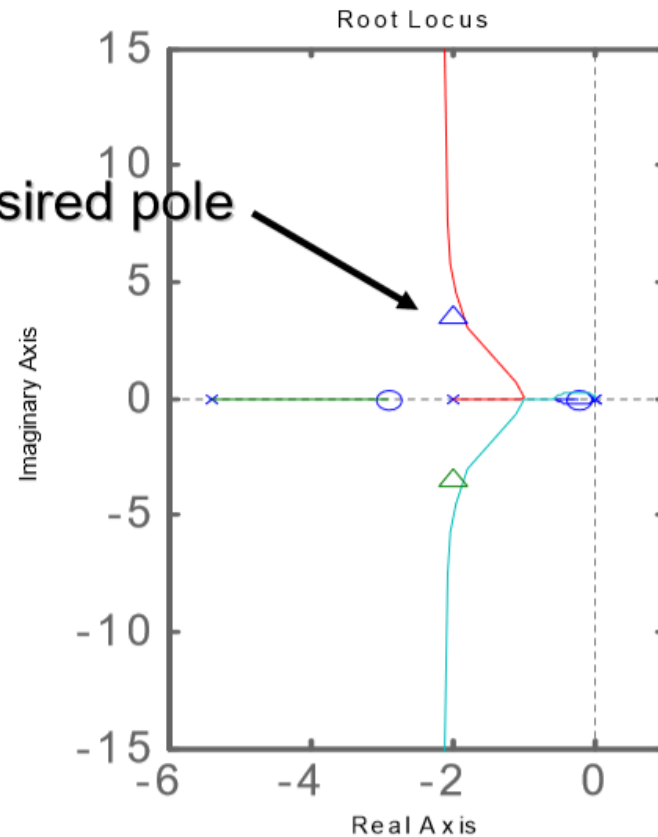
# Example 2 (revisited)

## Root locus

With lead compensator

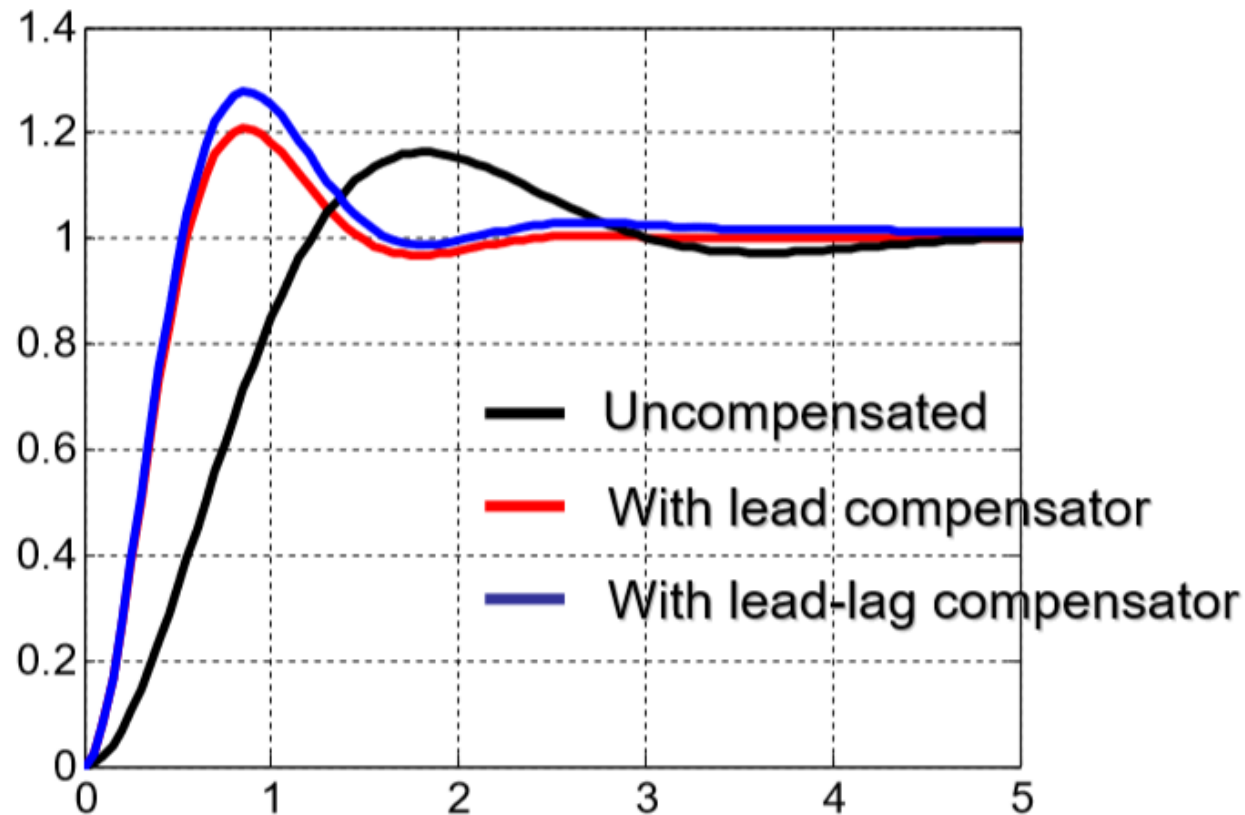


With lead-lag compensator



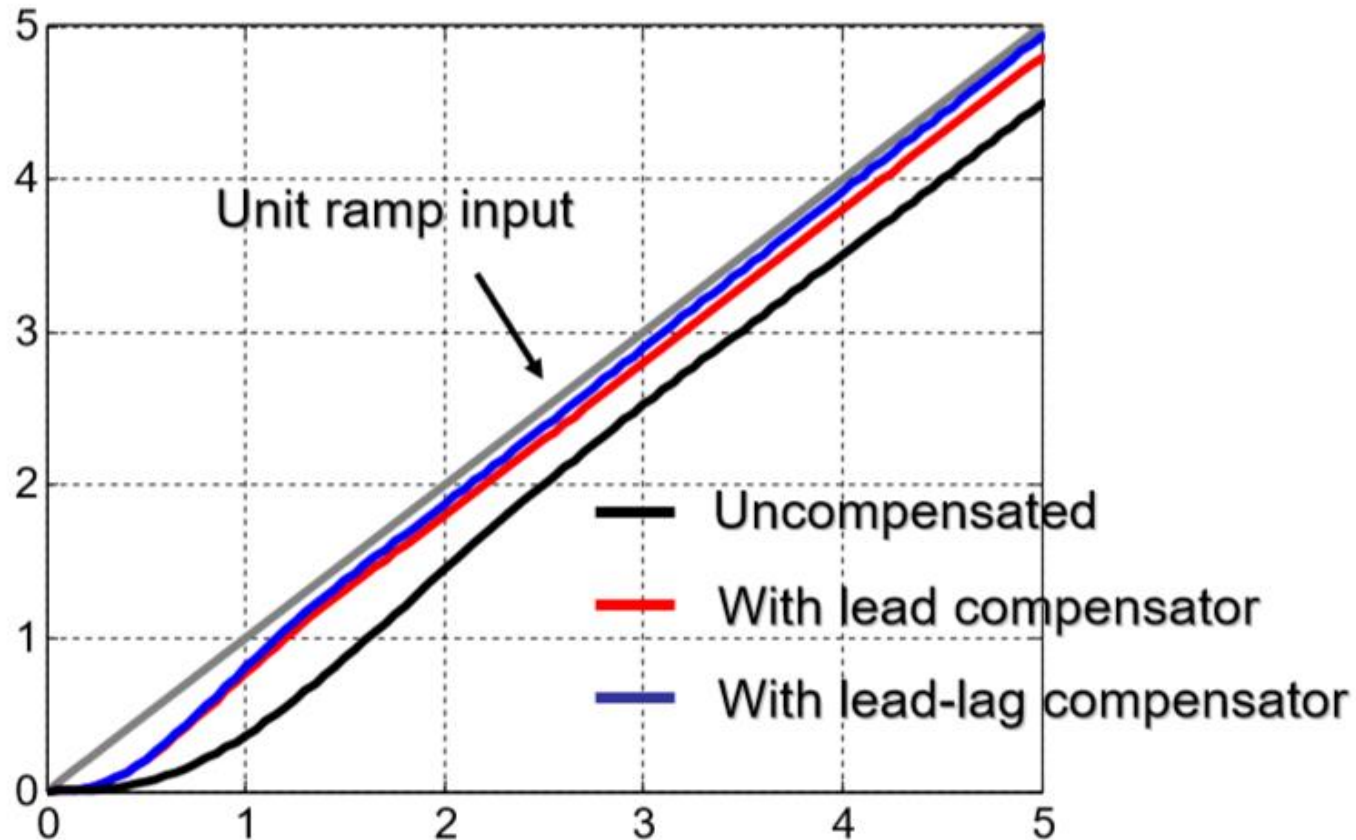
# Example 2 (revisited)

## Comparison of step responses



# Example 2 (revisited)

## Comparison of ramp responses



# Remarks on controller design

- Existence of a satisfactory controller is generally unknown before the design.
- When a satisfactory controller exists, such controller is not unique.
- Controller design methods are not unique either.
  - Different references explain controller design in a different way.
  - Different control engineers design controllers in a different way.

# Summary

- Controller design based on root locus
  - Lead compensator **to improve transient response.**
  - Lag compensator **to improve steady state error.**
  - Lead-lag compensator **to improve both transient and steady state responses.**
- Next
  - Lead-lag compensator in Matlab and PID Controller design