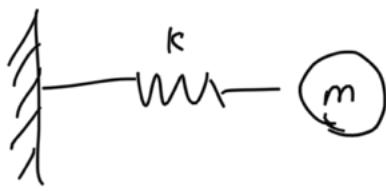


Wave Lecture 1 (20210831)

Lec 1



① Newtonian mechanics. $F = ma \Rightarrow m\ddot{x} + kx = 0$.

② Lagrangian mechanics. based on Hamilton principle

Hamilton principle

[The path of a particle, $x(t)$, is determined such that the function $I(x, \dot{x}) = \int_{t_1}^{t_2} L(t, x, \dot{x}) dt$ has an extremum]

For I to have extremum, $(L = T - V)$.

$$\boxed{\frac{\partial L}{\partial x} - \frac{\partial}{\partial t} \left(\frac{\partial L}{\partial \dot{x}} \right) = 0} : \text{Euler-Lagrange equation}$$

$$\underline{L = T - V} ; T = \frac{1}{2} m(\dot{x})^2, V = \frac{1}{2} kx^2$$

$$L = \frac{1}{2} m \dot{x}^2 - \frac{1}{2} kx^2$$

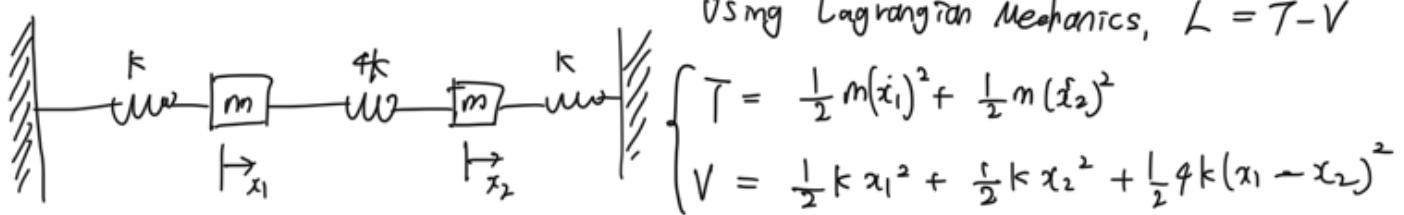
$$m\ddot{x} + kx = 0$$

$$\begin{aligned} -\nabla V &= \text{force.} \\ \Rightarrow -\frac{dV}{dx} &= -kx \\ \Rightarrow V &= \frac{1}{2} kx^2 + C. \end{aligned}$$

—

Wave Lecture 2 (20190902)

Lec 2 <Review of "Vibration">



⇒ E.O.M by Lagrangian Mechanics. (Euler-Lagrange Eq.)

$$\left. \frac{\partial L}{\partial x_i} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{x}_i} \right) = 0 \right|_{i=1,2} \Rightarrow \left. \begin{array}{l} -kx_1 - 4k(x_1 - x_2) - \frac{d}{dt}(m\dot{x}_1) = 0 \\ -kx_2 - 4k(x_2 - x_1) - \frac{d}{dt}(m\dot{x}_2) = 0 \end{array} \right\}$$

$$\Rightarrow \left. \begin{array}{l} -5kx_1 + 4kx_2 - m\ddot{x}_1 = 0 \\ -5kx_2 + 4kx_1 - m\ddot{x}_2 = 0 \end{array} \right\} \Rightarrow \underbrace{\ddot{\vec{x}} + \left(\sqrt{\frac{k}{m}} \right)^2 (\sqrt{A})^2 \vec{x}}_{?} = 0 \quad A = \begin{pmatrix} 5 & -4 \\ -4 & 5 \end{pmatrix}$$

< Functions of Matrices > (\sqrt{A} ?)

* characteristic polynomial of A : $P_A(\lambda) = \det(\lambda I - A)$.

Suppose $\underbrace{\sqrt{\lambda} = f(\lambda)}_{\text{Our Goal}} = \underbrace{P_A(\lambda)}_{\text{ }} \cdot \underbrace{g(\lambda)}_{\text{ }} + \underbrace{r(\lambda)}_{\text{ }}$

Cayley-Hamilton Theorem : $P_A(A) = \vec{0}$

$$\Rightarrow \underbrace{\sqrt{A} = f(A) = r(A)}_{\text{ }}$$

E.g.: $A = \begin{pmatrix} 5 & -4 \\ -4 & 5 \end{pmatrix}$ $\sqrt{I} = f(I) = \cancel{A(I)}^0 g(I) + (a \cdot \lambda + b) \Big|_{\lambda=1}$
 $\sqrt{9} = f(9) = \cancel{A(9)}^0 g(9) + (a \cdot 9 + b) \Big|_{\lambda=9}$

* $r(\lambda)$ is 1st order $\therefore P_A(\lambda)$ is 2nd order

$$\Rightarrow r(\lambda) = \frac{1}{4}\lambda + \frac{3}{4} \Rightarrow \sqrt{A} = \frac{1}{4}A + \frac{3}{4} \cdot I = \begin{pmatrix} 2 & -1 \\ -1 & 2 \end{pmatrix}$$

< Homework #1 >

what is $\sin\begin{pmatrix} 0 & 0 \\ 0 & 0 \end{pmatrix}$ and $\cos\begin{pmatrix} 0 & 0 \\ 0 & 0 \end{pmatrix}$? $A = \begin{pmatrix} 0 & 0 \\ 0 & 0 \end{pmatrix}$

① sin

$$P_A(\lambda) = \lambda^2 \Rightarrow \sin\lambda = f(\lambda) = P_A(\lambda)g(\lambda) + r(\lambda) = \lambda^2 g(\lambda) + C\lambda + D$$
$$\Rightarrow \cos\lambda = 2\lambda g(\lambda) + \lambda^2 g'(\lambda) + C$$

$$\Rightarrow D=0, C=1 \Rightarrow f(A) = \sin\begin{pmatrix} 0 & 0 \\ 0 & 0 \end{pmatrix} = \begin{pmatrix} 0 & 0 \\ 0 & 0 \end{pmatrix}$$

② cos

$$P_A(\lambda) = \lambda^2 \Rightarrow \cos\lambda = f(\lambda) = P_A(\lambda)g(\lambda) + r(\lambda) = \lambda^2 g(\lambda) + C\lambda + D$$
$$\Rightarrow -\sin\lambda = 2\lambda g(\lambda) + \lambda^2 g'(\lambda) + C$$
$$\Rightarrow C=0, D=1 \Rightarrow f(A) = \cos\begin{pmatrix} 0 & 0 \\ 0 & 0 \end{pmatrix} = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} = I$$

$$\text{Solution form of given example. : } \vec{X}(t) = \cos \underbrace{\begin{pmatrix} 2w_0 t & -w_0 t \\ -w_0 t & 2w_0 t \end{pmatrix}}_{B} \begin{pmatrix} \alpha_1 \\ \alpha_2 \end{pmatrix}$$

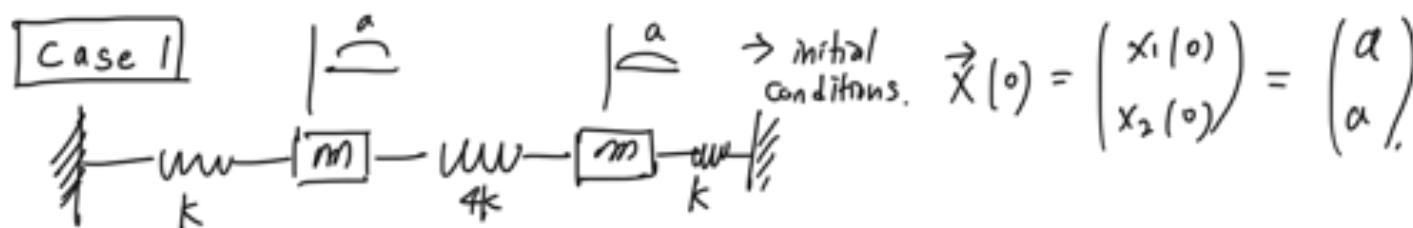
$$P_B(\lambda) = \det(\lambda I - B) = (\lambda - w_0 t)(\lambda - 3w_0 t)$$

$$\cos \lambda = f(\lambda) = P_B(\lambda) g(\lambda) + r(\lambda) = (\lambda - w_0 t)(\lambda - 3w_0 t) g(\lambda) + p\lambda + q$$

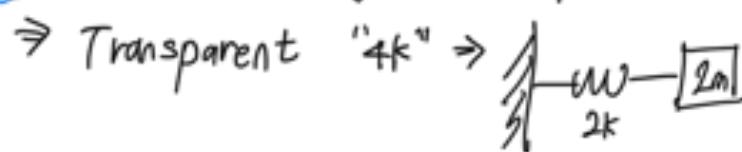
$$\Rightarrow \cos w_0 t = w_0 t \cdot p + q \Rightarrow p = \frac{\cos 3w_0 t - \cos w_0 t}{2w_0 t}$$

$$\cos 3w_0 t = 3w_0 t \cdot p + q \quad q = \frac{1}{2} (3\cos w_0 t - \cos 3w_0 t)$$

Wave Lecture 3 (20210907)



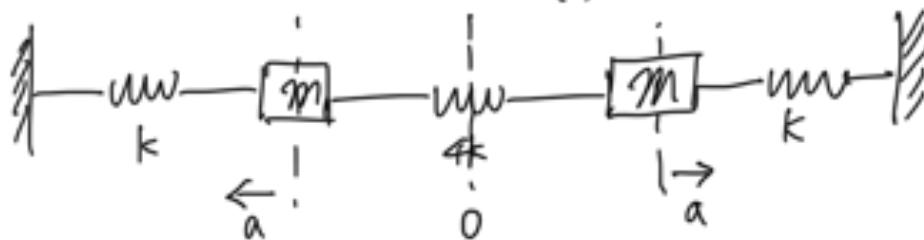
⇒ Intuition: No force by "4k" spring. (two masses synchronized)



< In-phase movement >

⇒ Frequency = $\omega_1 = \sqrt{k/m} = \omega_0$

Case 2 : $x_1(0) = a, x_2(0) = -a$



< out of phase movement >

⇒ Intuition: Symmetric movement via point "O"



⇒ Frequency = $\omega_2 = \sqrt{(4k+2k)/m} = 3\sqrt{k/m} = 3\omega_0$

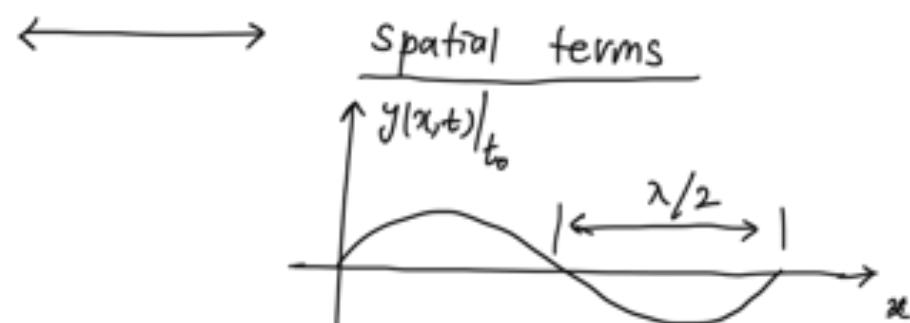
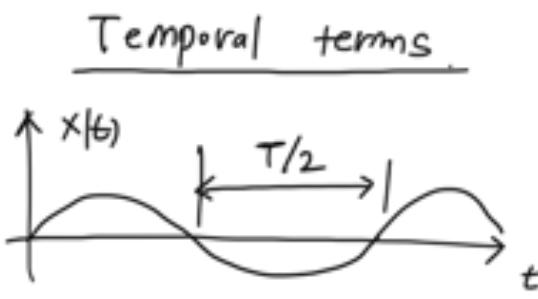
HW

Q) Can we realize higher frequencies just by adjusting Initial Conditions?

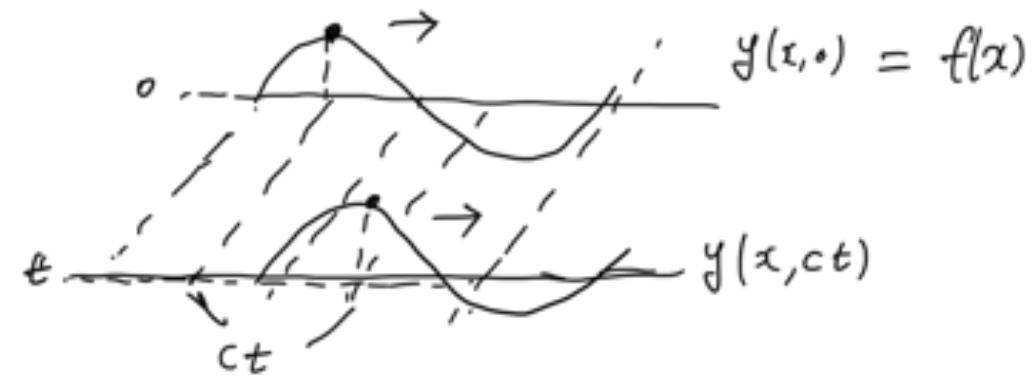
A) No. Why?

∞ DOF : lattice system.

• Terminologies. :



$$1) \quad T \text{ (period)} \longleftrightarrow \lambda \text{ (wavelength)}$$



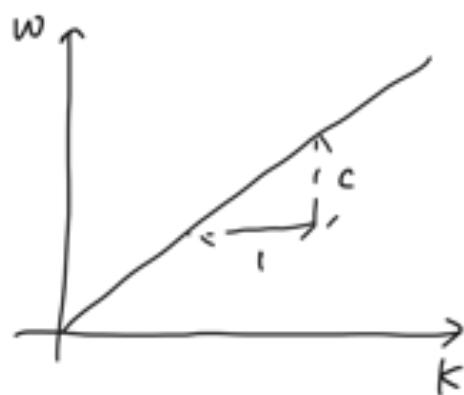
$$\Rightarrow y(x,ct) = y(x-ct,0) = \underline{f(x-ct)}$$

"Phase" $\left\{ \begin{array}{l} f(x-ct) : \vec{x} \text{ direction propagation} \\ f(x+ct) : -\vec{x} \text{ " " } \end{array} \right.$

$$c = \frac{\lambda}{T} = \frac{\omega}{2\pi} \cdot \lambda = \omega \cancel{k}$$

$$2) \quad \omega \text{ (angular frequency)} \longleftrightarrow \boxed{k} \text{ is \# of wave in } 2\pi \text{ (unit) length}$$

$k = 2\pi/\lambda$



"k-w curve": Dispersion Curve.



Wave Lecture 4 (20210909)

- 1D Wave Equation

① For $f(kx - \omega t)$: right going

$$\frac{\partial f}{\partial t} = \frac{\partial \phi}{\partial t} \frac{\partial f}{\partial \phi} = (-\omega) f' \Rightarrow k f' c - \omega f' = 0$$

$$\frac{\partial f}{\partial x} = \frac{\partial \phi}{\partial x} \frac{\partial f}{\partial \phi} = k f' \Rightarrow \left[\frac{\partial}{\partial t} + c \frac{\partial}{\partial x} \right] f = 0$$

② For $f(kx + \omega t)$: left going.

$$\frac{\partial f}{\partial t} = \omega f' \Rightarrow k f' c - \omega f' = 0$$

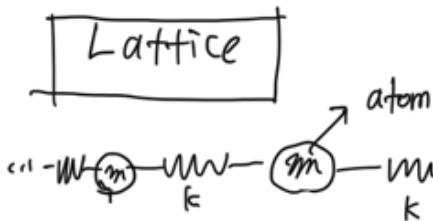
$$\frac{\partial f}{\partial x} = k f' \Rightarrow \left[\frac{\partial}{\partial t} - c \frac{\partial}{\partial x} \right] f = 0$$

From ① and ②,

$$\left(\frac{\partial}{\partial t} + c \frac{\partial}{\partial x} \right) \left(\frac{\partial}{\partial t} - c \frac{\partial}{\partial x} \right) f = 0$$

$$\Rightarrow \left(\frac{\partial^2}{\partial t^2} - c^2 \frac{\partial^2}{\partial x^2} \right) f = 0 \Leftrightarrow \boxed{\left(\frac{\partial^2}{\partial x^2} - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} \right) f = 0}$$

1 Dimensional Wave Equation.

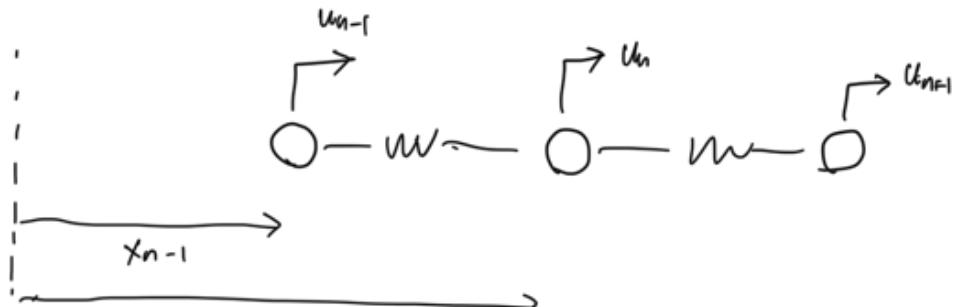


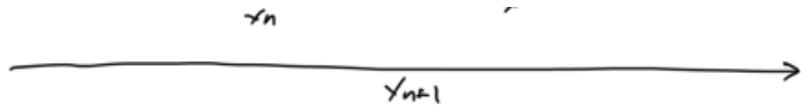
... - m - k - m - k - m - k - m - ... (lattice)

< Monoatomic lattice >

types of mass

1. Mono
2. Di
3. Tri





E.O.M $m \ddot{u}_n = +k(u_{n+1} - u_n) - k(u_n - u_{n-1}) = -k(2u_n - u_{n-1} - u_{n+1})$

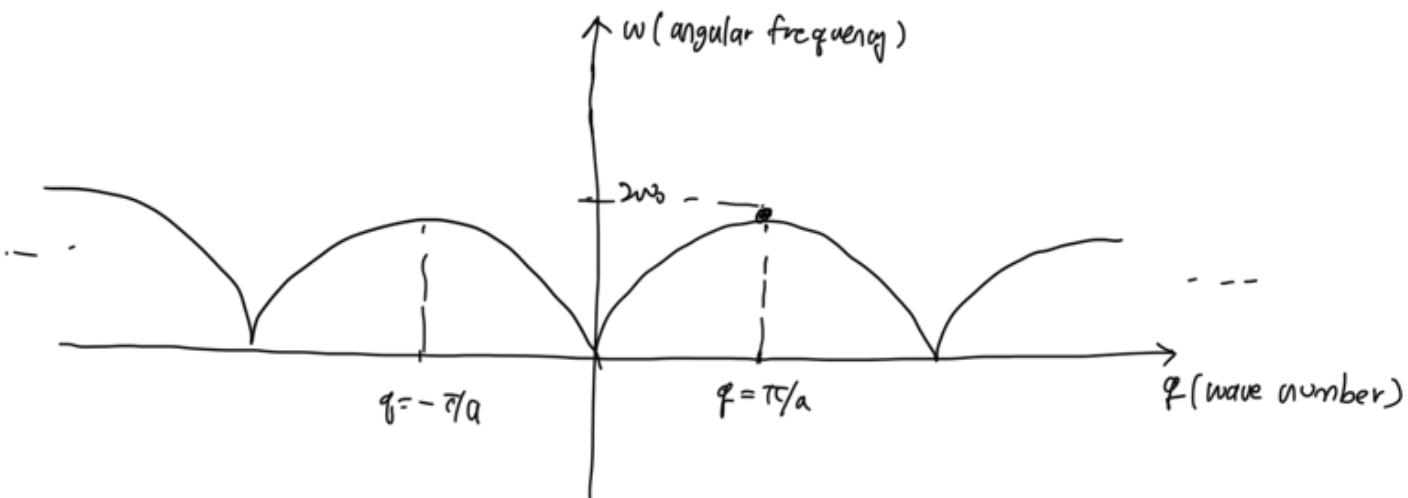
Let $u_n = A e^{i(qx_n - wt)}$ (q = wavenumber, A is same for all \because monatomic).

Since $x_n(t) = x_n + u_n t$, where x_n is equilibrium constant, $x_n = na$

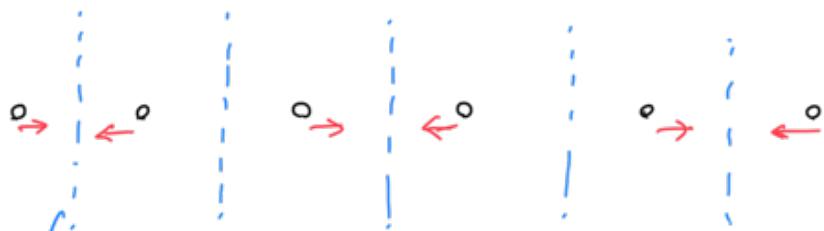
$$\Rightarrow -mw^2 e^{iqna} = +k(e^{iqna} \cdot 2 - e^{iq(n-1)a} - e^{iq(n+1)a})$$

$$\Rightarrow mw^2 = k(2 - 2\cos qa) = 4k(1 - \cos qa) = 4k \sin^2(qa/2)$$

$$\Rightarrow w = 2\sqrt{\frac{k}{m}} \left| \sin\left(\frac{qa}{2}\right) \right| = 2\omega_0 \left| \sin\left(\frac{qa}{2}\right) \right| \quad (\omega_0 = \sqrt{\frac{k}{m}})$$

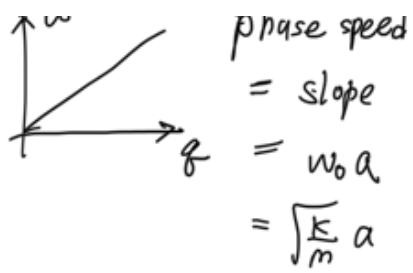


(1) when $q = \pi/a$, $u_n = A e^{i(qna - wt)} \rightarrow \phi_n$
 $u_{n+1} = A e^{i(q(n+1)a - wt)} \rightarrow \phi_{n+1}$ $\Rightarrow \begin{cases} \phi_{n+1} - \phi_n = qa = \pi \\ u_n = -u_{n+1} \end{cases}$



nodal points. \rightarrow no transport of wave energy.

$$(2) \frac{d\omega}{dq} = 0 \Rightarrow \omega = 2\omega_0 \left| \sin\left(\frac{qa}{2}\right) \right| \approx q\omega_0 a.$$



$$(3) \max(\omega) = 2\omega_0 = \sqrt{4k/m} \quad Q) \text{ Why } 4k?$$

$$(4) \omega(q) = \omega(-q) \quad (\text{symmetry}) : \begin{bmatrix} \text{right \& left going waves has the} \\ \text{same information} \end{bmatrix}$$

Wave Lecture 5 (20210914)

Review of Compressible "Fluid Mechanics"

* Extensive & Intensive properties.

$B \xrightarrow{\beta}$
normalized by mass



	B	β
mass	m	1
momentum	$m\vec{v}$	\vec{v}
Energy	$E + \frac{1}{2}mv^2$	$e + \frac{1}{2}v^2$

internal kinetic.

* Conservation Laws.

• Reynolds Transport Theorem (RTT)

The rate of change of an extensive property (B)

= time rate of change of B within C.V. + net rate of flow B through C.S.

$$\Rightarrow \frac{d\beta}{dt} = \int_{\Omega} \frac{\partial}{\partial t} (\rho\beta) dV + \int_{\partial\Omega} (\rho\beta) \vec{v} \cdot \hat{n} dA.$$

\downarrow control volume \downarrow Control surface.



$$\Rightarrow \frac{d}{dt} \int_{\Omega} (\rho p) dV = \int_{\Omega} \frac{\partial}{\partial t} (\rho p) dV + \int_{\partial\Omega} (\rho\beta) \vec{v}_b \cdot \hat{n} dA + \int_{\partial\Omega} (\rho p) \vec{v}_r \cdot \hat{n} dA$$

\downarrow \downarrow \downarrow
∂Ω velocity \vec{v}_b fluid velocity w.r.t ∂Ω
 v_r

① Continuity ($B = m$)

$$\frac{d\beta}{dt} = \int_{\Omega} \frac{\partial}{\partial t} (\rho \cdot 1) dV + \int_{\partial\Omega} (\rho \cdot 1) \vec{u} \cdot \vec{n} dA = \int_{\Omega} \left(\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{u}) \right) dV$$

||

$$\frac{dm}{dt} = 0 \quad \left(\because \text{mass of system is conserved} \right) \quad \left(\begin{array}{l} \therefore \text{Gauss divergence theorem} \\ \int_{\Omega} \nabla \cdot \vec{F} dV = \int_{\partial\Omega} \vec{F} \cdot \vec{n} dA \end{array} \right)$$

$$\Rightarrow \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{u}) = 0 \quad \left(\because \text{if } \int_{\Omega} f dV = 0 \Rightarrow f = 0 \text{ by localization theorem} \right)$$

② Momentum. $\beta_i = m_i \vec{u}_i$, $\rho = \vec{u}$ $\vec{B} = (B_1, B_2, B_3)$

$$\frac{d\beta_i}{dt} = \int_{\Omega} \frac{\partial}{\partial t} (\rho \cdot u_i) dV + \int_{\partial\Omega} (\rho \cdot u_i) \vec{u} \cdot \vec{n} dA \quad \text{for } i=1, 2, 3$$

||

$$\frac{d\vec{p}}{dt} = \vec{F}$$

$$\left(\begin{array}{l} \text{net force} \\ \text{acting on } d\Omega \end{array} \right) = \left(\begin{array}{l} \text{normal force} \\ \text{shear force} \end{array} \right) \Rightarrow \int_{\Omega} \frac{\partial}{\partial t} (\rho u_i) dV + \int_{\partial\Omega} [\rho u_i \vec{u} \cdot \vec{n} + P \vec{e}_i \cdot \vec{n}] dA = 0$$

pressure is inwards

$$-\int_{\partial\Omega} P \vec{e}_i \cdot \vec{n} dA \Rightarrow \int_{\Omega} \left[\frac{\partial}{\partial t} (\rho u_i) + \nabla \cdot (\rho u_i \vec{u}) + \nabla \cdot (P \vec{e}_i) \right] dV = 0$$

$$\left\{ \begin{array}{l} \vec{e}_1 = (1, 0, 0) \\ \vec{e}_2 = (0, 1, 0) \\ \vec{e}_3 = (0, 0, 1) \end{array} \right. \Rightarrow \int_{\Omega} \frac{\partial}{\partial t} (\rho u_i) + u_i \nabla \cdot (\rho \vec{u}) + \rho \vec{u} \cdot \nabla u_i + \frac{\partial P}{\partial x_i} dV = 0$$

$\because \nabla \cdot (P \vec{e}_i) = \nabla \cdot (P, 0, 0) = \frac{\partial P}{\partial x_i}$

$$\frac{\partial \rho}{\partial t} u_i + \rho \frac{\partial u_i}{\partial t} + u_i \nabla \cdot (\rho \vec{u}) + \rho \vec{u} \cdot \nabla u_i = - \frac{\partial P}{\partial x_i}$$

\because continuity equation.

$$\Rightarrow - \frac{\partial P}{\partial x_i} = \rho \frac{\partial u_i}{\partial t} + \rho \vec{u} \cdot \nabla u_i = \rho \left(\frac{\partial u_i}{\partial t} + \vec{u} \cdot \nabla u_i \right)$$

③ State equation. (thermodynamic process)

$$\underline{P = P(\rho, T)} \quad \leftrightarrow \quad \rho = \rho(P, S)$$

$$\underline{P - P_0} = \frac{\partial P}{\partial \rho} \Big|_{S=S_0} (\rho - \rho_0) + \cancel{T \text{ for } \rightarrow^o} + \frac{\partial P}{\partial S} \Big|_{\rho=\rho_0} (S - S_0) + \cancel{T \text{ for } \rightarrow^o}$$

||

$$P' = \frac{\partial P}{\partial \rho} \Big|_{S_0} \rho' + \underbrace{\frac{\partial P}{\partial S} \Big|_{T_0} S'}_{=0 \text{ for isentropic process}} \Rightarrow P' = \frac{\partial P}{\partial \rho} \Big|_{S_0} \rho' \quad \textcircled{1}$$

For adiabatic process,

$$\frac{P}{\rho^\gamma} = \frac{P_0}{\rho_0^\gamma} \Rightarrow \frac{\partial P}{\partial \rho} = \frac{P}{\rho^\gamma} + \rho^{\gamma-1} = \left(\frac{P}{\rho^\gamma} \right) \cdot \frac{\rho^\gamma}{\rho^{\gamma-1}} = \frac{\gamma P}{\rho} = \frac{\gamma \rho R T}{\rho}$$

From ① $\Rightarrow \underbrace{P' = \gamma R T \rho'}_{k}$

Note: Isentropic process assumes ideal state from adiabatic processes.

Note: $\sqrt{\gamma R T} = \text{speed of sound (c)}$

Wave Lecture 6 (20210916)

• Summary

$$\textcircled{1} \quad \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho u) = 0$$

$$\textcircled{2} \quad \rho \left(\frac{\partial u}{\partial t} + u \cdot \nabla u \right) = -\nabla p$$

$$\textcircled{3} \quad p' = (\sqrt{\gamma RT})^2 \rho' \quad (\text{isentropic process})$$

$$\begin{array}{l} \text{Linearization} \\ \left\{ \begin{array}{l} \rho = \rho_0 + \rho' \\ u = u_0 + u' \end{array} \Rightarrow \right. \end{array}$$

〈Linearized〉. • 숙제 . 2주 주제

$$\frac{\partial \rho'}{\partial t} + \rho_0 \nabla \cdot u' = 0 \quad \textcircled{1}$$

$$\begin{array}{l} \left(\rho_0 + \rho' \right) \left(\frac{\partial u'}{\partial t} + u' \cdot \nabla u' \right) \approx \rho_0 \frac{\partial u'}{\partial t} = -\nabla p' \\ \underbrace{\qquad \qquad \qquad}_{T_0} \end{array} \quad \textcircled{2}$$

〈Speed of sound : Laplace〉 (Isentropic)

$$\frac{\partial \textcircled{1}}{\partial t} \Rightarrow \frac{\partial^2 \rho'}{\partial t^2} + \rho_0 \frac{\partial}{\partial t} \nabla \cdot u' = 0 \quad \Rightarrow \quad \nabla^2 p' - \frac{\partial}{\partial t^2} \left(\frac{1}{\sqrt{\gamma RT}} \right)^2 \rho' = 0 \quad \nabla \cdot \nabla = \nabla^2$$

$$\nabla \cdot \textcircled{2} \Rightarrow \underbrace{\rho_0 \nabla \cdot \frac{\partial}{\partial t} u'}_{= -\nabla \cdot (\nabla p')}$$

$$\Rightarrow \nabla^2 p' - \left(\frac{1}{\sqrt{\gamma RT}} \right)^2 \frac{\partial^2}{\partial t^2} \rho' = 0$$

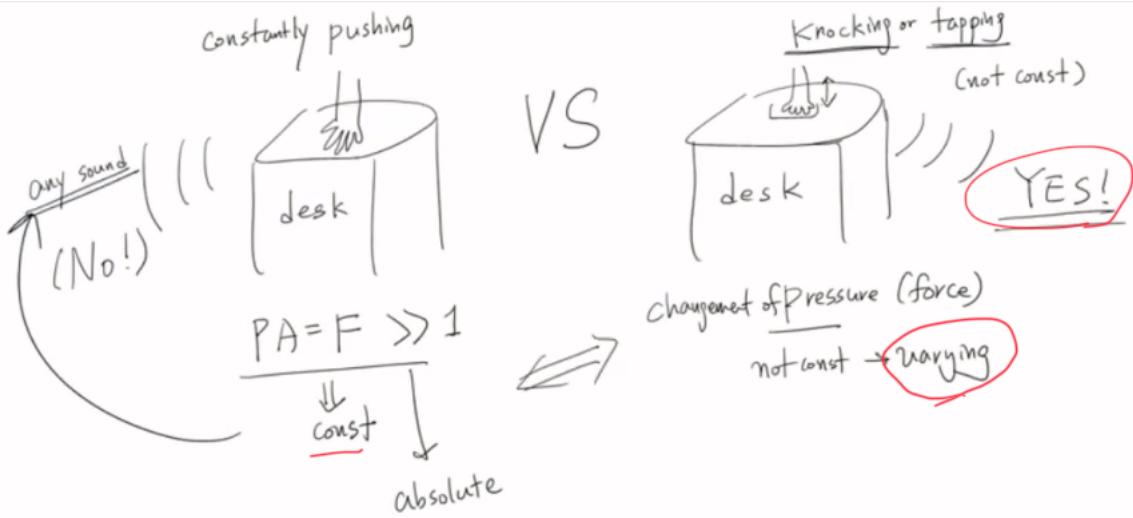
Waves in compressible fluid = "Sound" (Acoustics)

〈Speed of sound : Newton〉 (Isothermal)

$$p = p(\rho, T) \Rightarrow p' = \left. \frac{\partial p}{\partial \rho} \right|_{T_0} \rho' + \left. \frac{\partial p}{\partial T} \right|_{\rho_0} T' \Rightarrow p' = \left. \frac{\partial p}{\partial \rho} \right|_{T_0} \rho'$$

$$\text{since } p = \rho RT, \quad \frac{\partial p}{\partial \rho} = RT \Rightarrow p' = (\sqrt{\rho_0 T_0})^2 \rho' \quad \sqrt{\rho_0 T_0} \approx 290 \rightarrow \text{Wrong!}$$

Q1. What is Sound ?

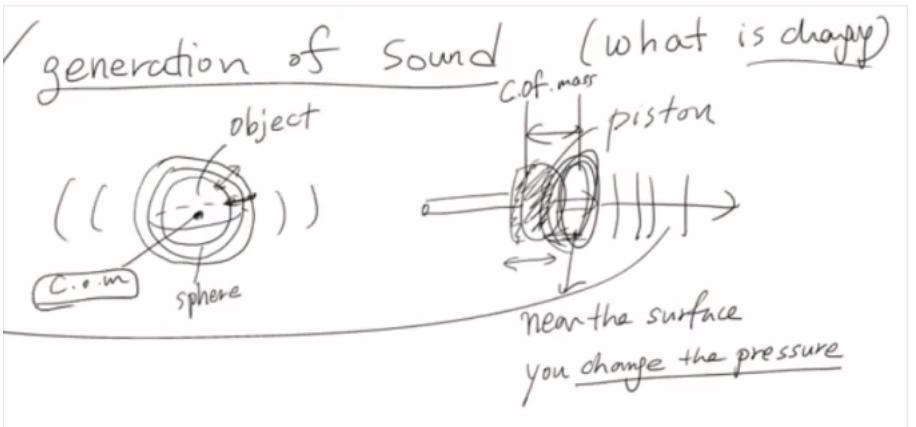


$$p = \underbrace{p_0}_{\text{mean}} + \underbrace{p'}_{\text{perturbed}} \rightarrow \text{Sound} = \text{Acoustic wave}$$

Q2. What Differential Equation governs the propagation of sound?

$$\left. \begin{array}{l} \text{Laplace's Eqn.} \\ \text{Lamé's Eqn.} \\ \text{state Eq. (isentropic)} \end{array} \right\} \Rightarrow \frac{\partial^2 p'}{\partial x^2} - \frac{1}{c^2} \frac{\partial^2 p'}{\partial t^2} = 0 \quad \text{Eq (1)}$$

Q3. How does the sound propagate? : Change.



Alternative way of expression.

$$\xi = x - ct \quad \text{and} \quad \eta = x + ct \quad (\text{for 1 dimension : } X \text{ axis}).$$

$$\begin{aligned}\frac{\partial}{\partial x} &= \frac{\partial \xi}{\partial x} \frac{\partial}{\partial \xi} + \frac{\partial \eta}{\partial x} \frac{\partial}{\partial \eta} = \frac{\partial}{\partial \xi} + \frac{\partial}{\partial \eta} \Rightarrow \frac{\partial^2}{\partial x^2} = \left(\frac{\partial}{\partial \xi} + \frac{\partial}{\partial \eta} \right) \left(\frac{\partial}{\partial \xi} + \frac{\partial}{\partial \eta} \right) \\ \frac{\partial}{\partial t} &= \frac{\partial \xi}{\partial t} \frac{\partial}{\partial \xi} + \frac{\partial \eta}{\partial t} \frac{\partial}{\partial \eta} = c \left(\frac{\partial}{\partial \eta} - \frac{\partial}{\partial \xi} \right) \Rightarrow \frac{\partial^2}{\partial t^2} = c \left(\frac{\partial}{\partial \eta} - \frac{\partial}{\partial \xi} \right) c \left(\frac{\partial}{\partial \eta} - \frac{\partial}{\partial \xi} \right) \\ \Rightarrow \frac{\partial^2}{\partial x^2} &= \frac{\partial^2}{\partial \xi^2} + 2 \frac{\partial^2}{\partial \xi \partial \eta} + \frac{\partial^2}{\partial \eta^2} \quad \text{and} \quad \frac{\partial^2}{\partial t^2} = c^2 \left(\frac{\partial^2}{\partial \eta^2} - 2 \frac{\partial^2}{\partial \xi \partial \eta} + \frac{\partial^2}{\partial \xi^2} \right)\end{aligned}$$

\Rightarrow From equation ①, assuming that $p'(x,t) = \tilde{p}(\xi, \eta)$,

$$\text{for 1 dimensional case, } \frac{\partial^2}{\partial x^2} p' = \frac{1}{c^2} \frac{\partial^2}{\partial t^2} p'$$

$$\Rightarrow \left(\frac{\partial^2}{\partial \xi^2} + 2 \frac{\partial^2}{\partial \xi \partial \eta} + \frac{\partial^2}{\partial \eta^2} \right) \tilde{p}(\xi, \eta) = \frac{1}{c^2} \cdot c^2 \left(\frac{\partial^2}{\partial \eta^2} - 2 \frac{\partial^2}{\partial \xi \partial \eta} + \frac{\partial^2}{\partial \xi^2} \right) \tilde{p}(\xi, \eta)$$

$$\Rightarrow 4 \frac{\partial^2}{\partial \xi \partial \eta} \tilde{p}(\xi, \eta) = 0 \Rightarrow \frac{\partial^2}{\partial \xi \partial \eta} \tilde{p}(\xi, \eta) = 0$$

Canonical form of
wave equation
Easy to solve PDE.

General solution form is, $\tilde{p}(\xi, \eta) = f(\xi) + g(\eta)$ (D'Alembert Solution).

Wave Lecture 7 (20210928)



Lec 07.

Waves in Compressible Fluids (air)

acoustic waves in the air
(sound)

D'Alembert solution of wave equation
in canonical form

original (1D)

$$\frac{\partial^2 p'}{\partial x^2} - \frac{1}{c^2} \frac{\partial^2 p'}{\partial t^2} = 0$$

where $p' = p'(x, t)$

canonical (1D)

$$\frac{\partial^2 \tilde{p}(s, \eta)}{\partial s^2} = 0 \quad (\text{PDE})$$

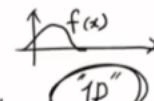
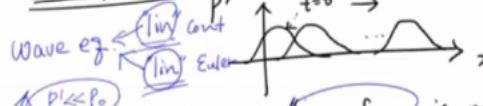
↓ benefit

$$(x, y) \rightarrow (s, \eta) \quad \begin{matrix} s \\ \parallel \\ x-ct \end{matrix} \quad \begin{matrix} \eta \\ \parallel \\ x+ct \end{matrix}$$

$$(x, t) \quad \tilde{p}(s, \eta) = f(s) + g(\eta)$$

for smooth (differentiable)
functions f & g .

interpretation (i) — for $f(\cdot)$



1D "nonlinear" wave
beyond the scope
of ME491 [Note]

same amplitude the wave-form is not changed in 1D propagation,
preserved (lossless medium)

[Note] Is the amplitude always preserved in 1D prop?
No, not always. "loss in the medium"

interpretation (2) D'Alembert soln

preparation (1) "acoustic potential" ϕ

Recall the velocity potential Φ .

For an irrotational velocity field,

There exists a scalar fn Φ such that $U_{\text{irrot}} = \nabla \Phi$ scalar fn.

$$\nabla \times U \equiv 0 \quad (\text{irrotational})$$

$$U = U_{\text{irrot}} + U_{\text{soln}}$$

By using a vector identity,

$$\begin{array}{c} \text{scalar fn} \\ \nabla \times \nabla \Phi \equiv 0 \\ \text{vector} \end{array}$$

$$0 \equiv \nabla \times U_{\text{irrot}} = \nabla \times \nabla \Phi \equiv 0$$

↓ single scalar fn → a vector field.

"what is changing"
perturbed quantity
 U' = scalar

↓ perturbed velocity potential
↓ acoustic potential

"preparation (2)" "wave eq" in terms of ϕ

(i) Linearized Euler eq.

$$\rho_0 \frac{\partial U'}{\partial t} = -\nabla P' \quad (U_0 \equiv 0)$$

$$U' = \nabla \phi$$

$$\rho_0 \frac{\partial}{\partial t} (\nabla \phi) = -\nabla P'$$

$$\nabla \left(\rho_0 \frac{\partial \phi}{\partial t} \right) = \nabla (-P')$$

$$\Rightarrow P' = -\rho_0 \frac{\partial \phi}{\partial t}$$

$$U' = \nabla \phi$$

relation btwn P' & ϕ

relation btwn U' & ϕ

solution ϕ

ϕ

P'

U'

∇^2

wave eq.

$$\nabla^2 P' - \frac{1}{c^2} \frac{\partial^2 P'}{\partial t^2} = 0$$

$$\frac{\partial P'}{\partial t} + \rho_0 \nabla \cdot U' = 0$$

$$\frac{1}{c^2} \frac{\partial^2 P'}{\partial t^2} + \rho_0 \nabla \cdot (\nabla \phi) = 0$$

$$\frac{1}{c^2} \frac{\partial^2 \phi}{\partial t^2} + \rho_0 \nabla^2 \phi = 0$$

$$\rightarrow \nabla^2 \phi - \frac{1}{c^2} \frac{\partial^2 \phi}{\partial t^2} = 0$$

wave eq.
in terms of ϕ

② Interpretation of D'Alembert solution (1D)

$$U' = \nabla \phi \quad \xrightarrow{\text{"1D"}} \quad \begin{cases} U' = \frac{\partial \phi}{\partial x} = \frac{\partial f(x-ct)}{\partial x} \\ P' = -\rho_0 \frac{\partial \phi}{\partial t} \end{cases}$$

Combining

$$-\rho_0 \frac{\partial f(x-ct)}{\partial t} \parallel \frac{\partial \phi}{\partial t} = -c$$

$$\frac{\partial f(x-ct)}{\partial x} = 1 \cdot f'(x)$$

$$\phi = \frac{f(x-ct)}{2} g(x+ct)$$

"right-going" wave
"left-going" wave

$$U' = f'(x) \quad P' = \rho_0 c f'(x)$$

$$\rho_0 \cdot c f'$$

HW: Find relation btw P', U' for left-going wave.

$$\begin{aligned} U' &= \frac{\partial \phi}{\partial x} = \frac{\partial f}{\partial x}(x+ct) \\ P' &= -\rho_0 \frac{\partial \phi}{\partial t} = -\rho_0 c f'(x+ct) \end{aligned} \quad \left. \frac{\partial h}{\partial t} = c \right\}$$

$$z = -\rho_0 c$$

$$\Rightarrow \frac{P'}{U'} = \frac{\rho_0 c}{2} \frac{U'}{f'(x+ct)}$$

phy. var. "material properties" phy. var.

recall $\frac{F}{U} = \text{mechanical impedance}$

$\frac{P'}{U'} = \frac{\rho_0 c}{2} \frac{U'}{f'(x+ct)} = \frac{\rho_0 c}{2} Z = \frac{Z}{2}$

area

acoustic impedance

how resistive

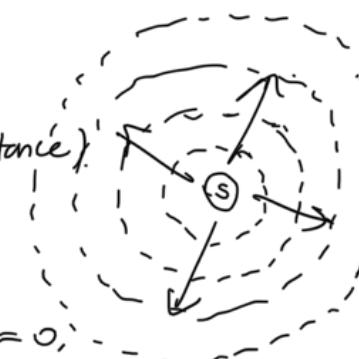
< Concentrate in sound propagation. >

① 1D propagation.

$$p'(x, t) = f(x - ct) + g(x + ct) \quad \text{and} \quad \phi(x, t) = f_1(x - ct) + g_1(x + ct)$$

② 3D propagation.

$$p'(r, \theta, \phi, t) = p'(r, t) : \text{function of } r, t \text{ (radial distance)}$$



$$\left(\nabla^2 - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} \right) p' = 0 \quad \xrightarrow{\text{Cartesian}} \left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} \right) p' = 0,$$

$\xrightarrow{\text{spherical}}$

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial}{\partial r} \right) p' + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial}{\partial \theta} \right) p' + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2}{\partial \phi^2} p' = 0.$$

< Homework > : derivation.

$$\text{W.E in 3 dim} : \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial}{\partial r} \right) p'(r, t) - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} p'(r, t) = 0,$$

$$\Rightarrow \frac{1}{r^2} \left(2r \frac{\partial}{\partial r} \right) p' + \frac{\partial^2}{\partial r^2} p' - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} p' = 0$$

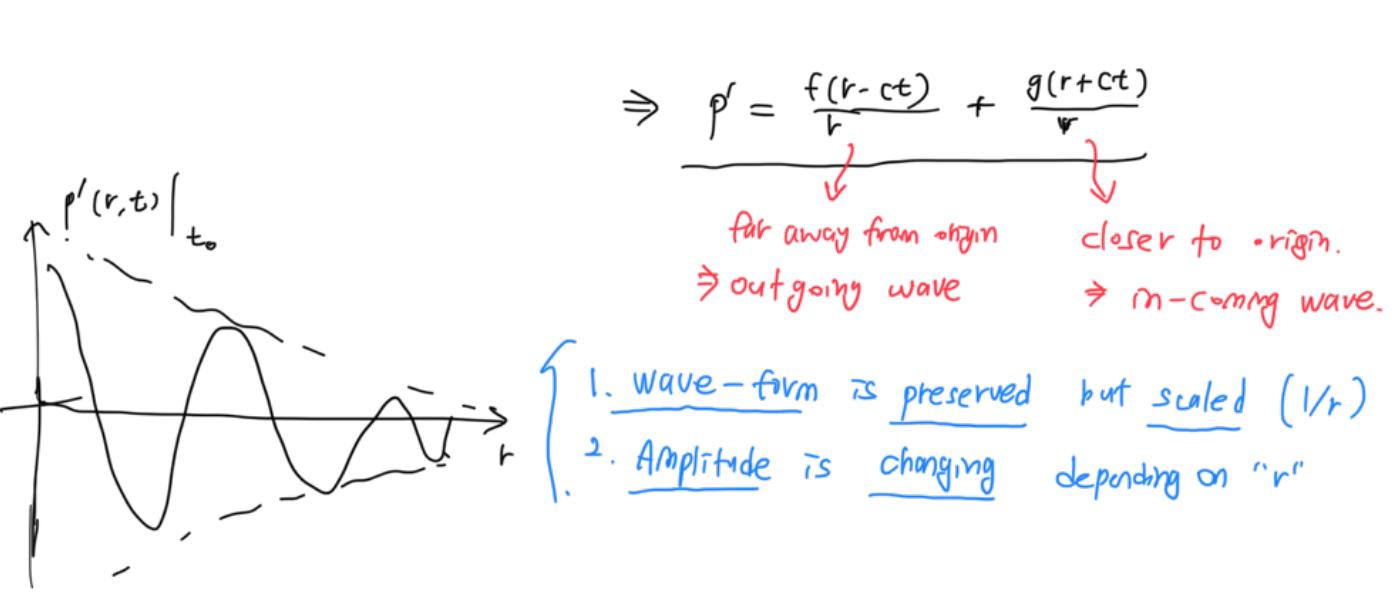
$$\Rightarrow \frac{\partial^2}{\partial r^2} p' + \frac{2}{r} \frac{\partial}{\partial r} p' - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} p' = 0$$

$$\Rightarrow \frac{1}{r} \left(r \frac{\partial^2}{\partial r^2} + 2 \frac{\partial}{\partial r} \right) p' - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} p' = 0$$

$$\Rightarrow \frac{1}{r} \frac{\partial}{\partial r} \left(\frac{\partial}{\partial r} (rp') \right) - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} p' = 0 \Rightarrow \underbrace{\frac{\partial^2}{\partial r^2} (rp')}_{\text{1 dimensional equation respect to } rp'} - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} (rp') = 0.$$

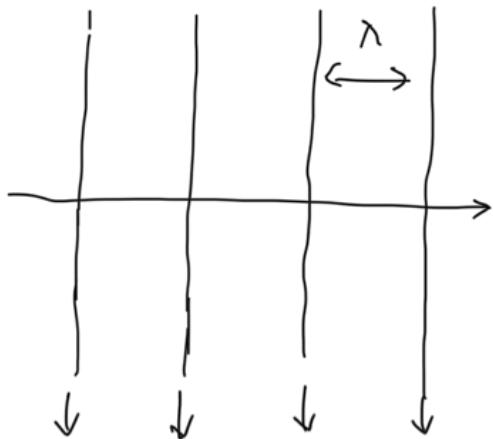
D'Alembert

$$\Rightarrow rp' = f(r - ct) + g(r + ct)$$

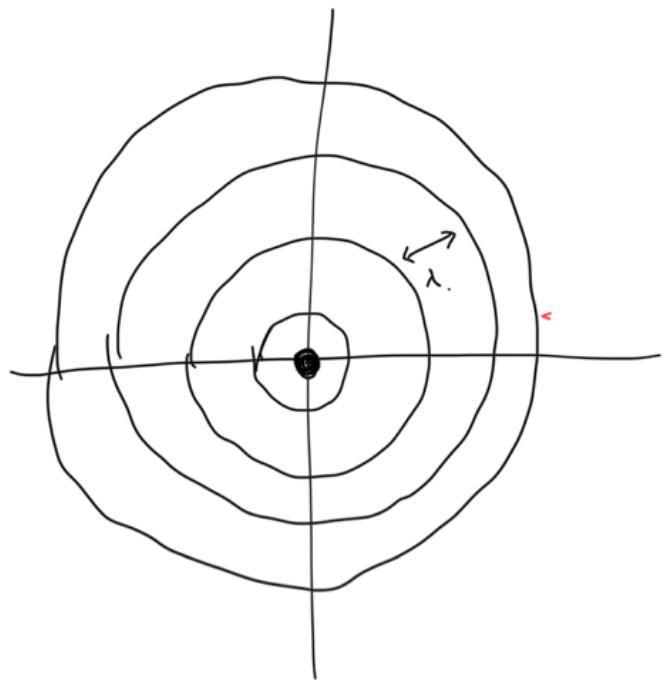


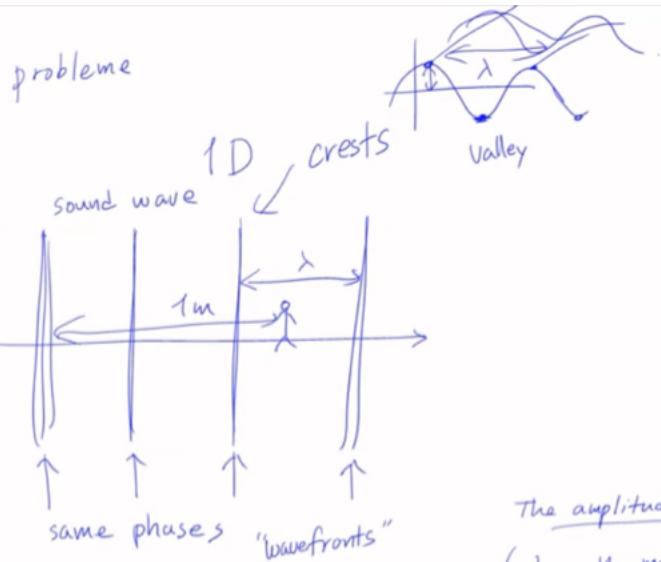
Problem

1D
sound wave.

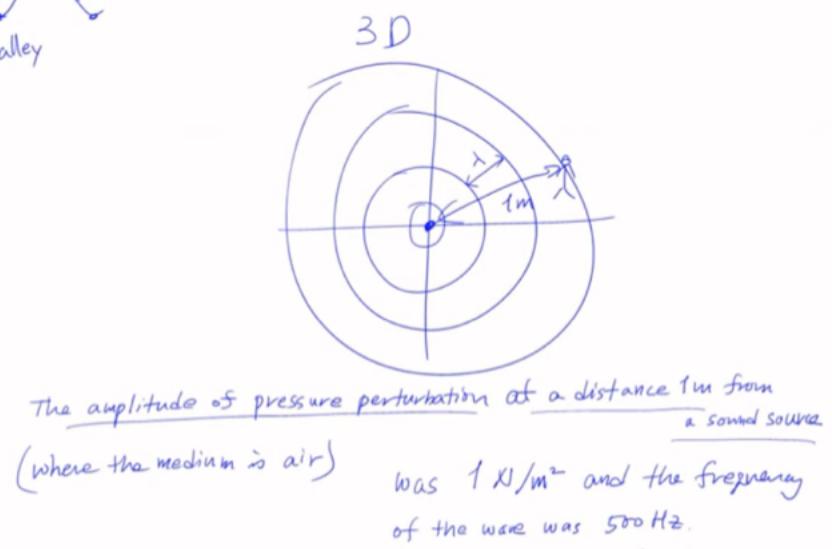


same phases : wavefronts.





same phases "wavefronts"



The amplitude of pressure perturbation at a distance 1m from a sound source (where the medium is air) was 1 N/m^2 and the frequency of the wave was 500 Hz.

Calculate the amplitude of particle velocity at 0.1 m from the source

$$\underbrace{\phi = \frac{f(r-ct)}{r} + \frac{g(r+ct)}{r}}_{\text{Linearized equations}} \quad p' = \underbrace{\frac{h(r-ct)}{r}}_{\text{form.}}$$

$$\frac{\partial \phi}{\partial t} + \rho_0 \nabla \cdot u = 0 \quad (\text{continuity})$$

$$\begin{cases} p' = -\rho_0 \frac{\partial \phi}{\partial t} \\ u' = \nabla \phi \end{cases} \Rightarrow \frac{1}{c^2} \frac{\partial p'}{\partial t} + \rho_0 \nabla \cdot (\nabla \phi) = 0$$

$$\Rightarrow \underbrace{\nabla^2 \phi - \frac{1}{c^2} \frac{\partial \phi}{\partial t}}_{\parallel} = 0$$

$$u' = \nabla \left(\frac{f(r-ct)}{r} \right) \quad \text{and} \quad p' = -\rho_0 \frac{\partial}{\partial t} \left(\frac{f(r-ct)}{r} \right) \quad (\text{assume right-going wave})$$

$$\Rightarrow u' = \frac{\partial}{\partial r} \left(\frac{f(r-ct)}{r} \right) \hat{r} \quad (\text{no components in } \theta, \varphi).$$

$$= \frac{f'(r-ct) \cdot r - f(r-ct)}{r^2} \hat{r} = \frac{r}{r} \frac{\partial f(r-ct)}{\partial r} - \frac{1}{r^2} f(r-ct).$$

$$p' = -\rho_0 \frac{1}{r} (-c) f'(r-ct) = \frac{\rho_0 c}{r} \frac{\partial}{\partial t} f(r-ct)$$

$$\textcircled{1} \text{ Since } f(x) = e^{ikx} \text{ so that } f(r-ct) = \underbrace{e^{i[k(r-ct)]}}_{kc = \omega}$$

$$\Rightarrow u' = \frac{1}{r} jk f(r-ct) - \frac{1}{r^2} f(r-ct) \text{ and } p' = \frac{\rho_0 c}{r} jk f(r-ct)$$

$$\Rightarrow \underbrace{z}_{\substack{\downarrow \\ \text{Acoustic impedance}}} = \frac{p'}{u'} = \frac{\frac{1}{r} \cdot k \cdot \rho_0 c \cdot j}{-\frac{1}{r^2} + \frac{1}{r} \cdot k \cdot j} \frac{\cancel{f(r-ct)}}{\cancel{f(r-ct)}} = \left\{ \frac{rk \cdot j}{-1 + rk \cdot j} \right\} \rho_0 c$$

Acoustic impedance.

$$\Rightarrow |z| = \frac{|p'|}{|u'|} = \frac{rk}{\sqrt{1 + (rk)^2}} \rho_0 c = \frac{rw}{\sqrt{c^2 + (rw)^2}} \rho_0 c$$

Since $|p'| = 1 \text{ N/m}^2$ and $f = 500 \text{ Hz}$

Since waveform does not change, $|p'|$ at $0.1 \text{ m} = 10 \text{ N/m}^2$ with same angular frequency $f = 500 \text{ Hz} \Rightarrow \omega = 2\pi \cdot 500 \text{ rad/s}$

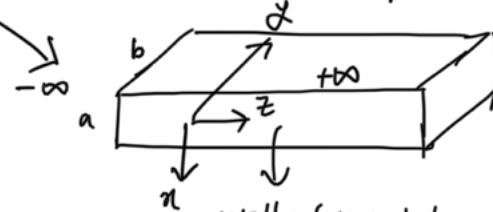
$$\Rightarrow |z| = \frac{|10|}{|u'|_{r=0.1m}} = \frac{0.1 \cdot 2\pi \cdot 500}{\sqrt{(343 \text{ m/s})^2 + (0.1 \cdot 2\pi \cdot 500)^2}} \frac{(1.225)(343)}{\text{kg/m}^3 \text{ m/s}} = 283.796$$

$$\Rightarrow |u'|_{r=0.1m} = 0.035 \text{ (m/s)} = \underline{\underline{35.24 \text{ (mm/s)}}}$$

Wave Lecture 8 (20210930)

3D sound propagation

free-space (spherical symmetric) $\Rightarrow p'(r,t)$



E.g. Rectangular, uniform cross section,

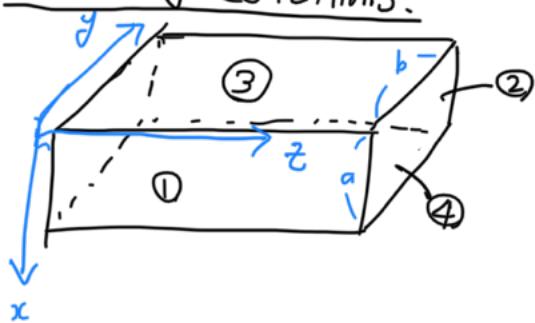
walls (rigid boundary): non-penetration condition

$$u_{,n} = 0 \quad \downarrow = 0$$

① G.E. (Governing Equation)

$$\nabla^2 \phi - \frac{1}{c^2} \frac{\partial^2 \phi}{\partial t^2} = 0 \quad (\vec{u}' = \nabla \phi)$$

② Boundary Conditions.



$$\left. \begin{array}{l} \text{① } u'_y \Big|_{y=0} = 0 \\ \text{② } u'_y \Big|_{y=b} = 0 \end{array} \right\} \begin{array}{l} 0 \leq x \leq a \\ -\infty < z < \infty \end{array} \quad \left. \begin{array}{l} \text{③ } u'_x \Big|_{x=0} = 0 \\ \text{④ } u'_x \Big|_{x=a} = 0 \end{array} \right\} \begin{array}{l} 0 \leq y \leq b \\ -\infty < z < \infty \end{array}$$

Note: $u'_x = \frac{\partial \phi}{\partial x}$ $u'_y = \frac{\partial \phi}{\partial y}$ $\Rightarrow \left. \begin{array}{l} \text{① } \frac{\partial \phi}{\partial y} \Big|_{y=0,b} = 0 \\ \text{② } \frac{\partial \phi}{\partial x} \Big|_{x=0,a} = 0 \end{array} \right\} \begin{array}{l} (0 \leq x \leq a) \\ (0 \leq y \leq b) \end{array} \quad 4 \text{ B.C.s.}$

Solve

$$\phi(x, y, z, t) = X(x) Y(y) Z(z) e^{-j\omega t}$$

$$\left\{ X'' Y Z + X Y'' Z + X Y Z'' - \frac{1}{c^2} (-j\omega)^2 X Y Z \right\} e^{-j\omega t} = 0$$

$\underbrace{\frac{\omega^2}{c^2} = k^2}_{\text{if}}$

$$\Rightarrow \underbrace{\frac{X''}{X} + \frac{Y''}{Y} + \frac{Z''}{Z} + k^2}_{\text{linear}} = 0$$

$$(1) \frac{X''}{X} = -\frac{Y''}{Y} - \frac{Z''}{Z} - k^2 = -\mu^2 \quad (\because \text{to get sinusoidal form, we set negative})$$

negative!

$X'' = 0 \rightarrow$ linear $B=0 \text{ or } \mu=0$

$\mu_n = n\pi \quad (n=0, 1, 2, \dots)$

$\mu_n = \frac{n\pi}{a}$

$\left. \begin{array}{l} \text{y-only} \\ \text{x-only} \end{array} \right\} \Rightarrow \underbrace{X'' + \mu^2 X = 0}_{\text{DDE}} \Rightarrow X(x) = A \cos(\mu x) + B \sin(\mu x)$

$+ \text{B.C. wrt } x \quad \left. \frac{\partial \phi}{\partial x} \right|_{x=0, a} = 0 \quad \text{for any } 0 \leq y \leq b$

$\left. \frac{\partial X}{\partial x} \right|_{x=0, a} = 0 \quad \Rightarrow -A\mu \sin(\mu a) + B\mu \cos(\mu a) \Big|_{x=0} = 0$

$\left. \frac{\partial X}{\partial x} \right|_{x=a} = 0 \quad \Rightarrow -A\mu \sin(\mu a) + B\mu \cos(\mu a) \Big|_{x=a} = 0$

$$\therefore X(x) = \sum_m A_m \cos\left(\frac{m\pi}{a}x\right) \quad \therefore \frac{\partial^2}{\partial x^2} X(x) \Big|_{x=0, a} = 0$$

$$(2) \frac{Y''}{Y} = -\frac{Z''}{Z} + \mu_m^2 - k^2 = -V^2 \Rightarrow Y(y) = \sum_n B_n \cos\left(\frac{n\pi}{b}y\right)$$

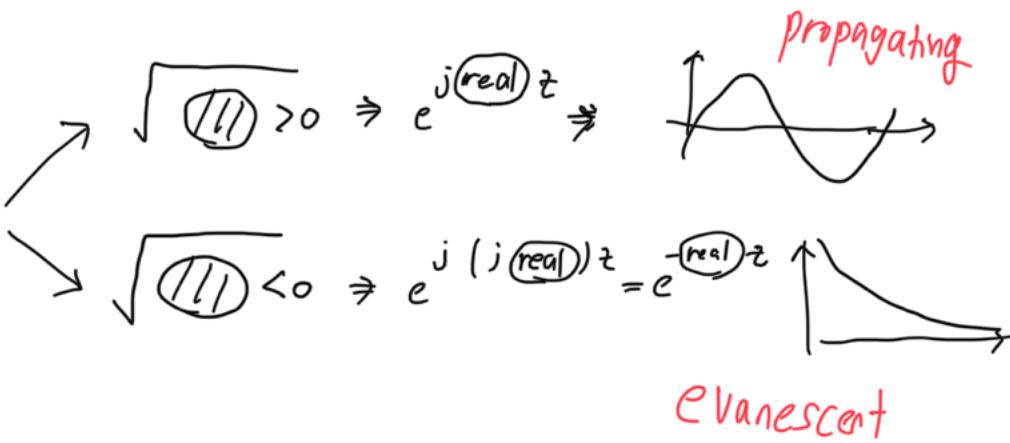
$$(3) \frac{Z''}{Z} = \mu_m^2 + V^2 - k^2 = -d_{mn}^2 \Rightarrow Z(z) = \sum_m \sum_n \left[C_{mn} e^{j d_{mn} z} + D_{mn} e^{-j d_{mn} z} \right]$$

From (1), (2), (3),

$$\phi(x, y, z, t) = \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} \cos\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) \left\{ C_{mn} e^{j d_{mn} z} + D_{mn} e^{-j d_{mn} z} \right\}$$

* Physical Interpretation.

$$d_{mn} = \pm \sqrt{\left(\frac{\omega}{c}\right)^2 - \pi^2 \left(\frac{m^2}{a^2} + \frac{n^2}{b^2}\right)}$$



$$\left(\frac{\omega}{c}\right)^2 - \pi^2 \left(\frac{m^2}{a^2} + \frac{n^2}{b^2}\right) > 0 : \text{Propagating} \\ < 0 : \text{Evanescent.}$$

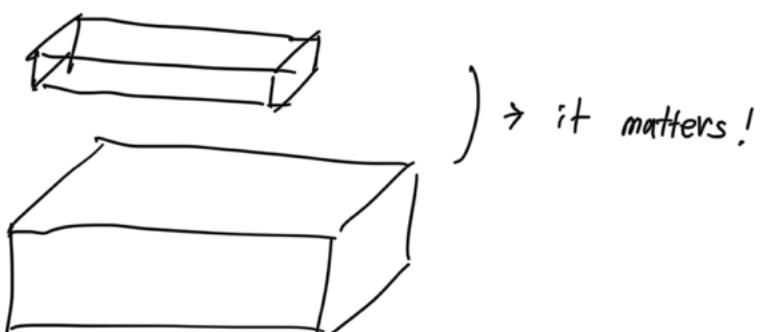
① $(m, n) = (0, 0)$: Plane wave mode



② Plane wave \rightarrow always propagation inside waveguide.

For higher modes, it can become evanescent waves.

③ $(a, b) \rightarrow$ size of duct.



Note: These are all ⁱⁿ compressible fluids.

Wave Lecture 9 (20211005)

• Review of Incompressible Fluid Mechanics → Water waves.

$$\textcircled{1} \text{ cont: } \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{u}) = 0 \xrightarrow{\rho = \rho_0 \text{ (constant)}} \underline{\nabla \cdot \vec{u} = 0}$$

if irrotational flow, $\vec{u} = \nabla \phi \Rightarrow \nabla^2 \phi = 0$

$$\textcircled{2} \text{ Euler Eq.: } \rho \left(\frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \nabla \vec{u} \right) = -\nabla p - \rho g \vec{e}_z$$

$$\Rightarrow \frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} = -\nabla \left(\frac{p}{\rho} \right) - g \vec{e}_z$$

Since $\nabla(\vec{A} \cdot \vec{B}) = (\vec{A} \cdot \nabla) \vec{B} + (\vec{B} \cdot \nabla) \vec{A} + \vec{A} \times (\nabla \times \vec{B}) + \vec{B} \times (\nabla \times \vec{A})$
 $(\vec{A} = \vec{B} = \vec{u} = \nabla \phi) \rightarrow$

$$\Rightarrow \nabla(\nabla \phi \cdot \nabla \phi) = 2 \cdot (\nabla \phi \cdot \nabla) \nabla \phi + 2 \cdot \nabla \phi \times (\nabla \times \nabla \phi) \xrightarrow{0}$$

$$\Rightarrow \nabla(\vec{u} \cdot \vec{u}) = 2(\vec{u} \cdot \nabla) \vec{u}$$

$$\Rightarrow \frac{\partial \vec{u}}{\partial t} + \frac{1}{2} \nabla |\vec{u}|^2 + \nabla \left(\frac{p}{\rho} \right) + g \vec{e}_z = 0$$

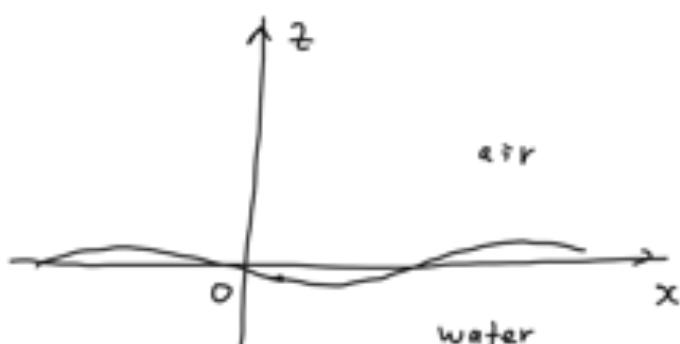
$$\Rightarrow \nabla \left(\frac{\partial \phi}{\partial t} + \frac{1}{2} |\nabla \phi|^2 + \frac{p}{\rho} \right) = -\nabla(g z)$$

$$\Rightarrow \nabla \left(\frac{\partial \phi}{\partial t} + \frac{1}{2} |\nabla \phi|^2 + \frac{p}{\rho} + g z \right) = 0$$

HW #2. $\nabla \times \nabla \phi = 0$ prove it!

$$\begin{aligned} \nabla \times \nabla \phi &= \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \frac{\partial \phi}{\partial x} & \frac{\partial \phi}{\partial y} & \frac{\partial \phi}{\partial z} \end{vmatrix} \\ &= 0\hat{i} + 0\hat{j} + 0\hat{k} = \vec{0}. \end{aligned}$$

$$\Rightarrow \frac{\partial \phi}{\partial t} + \frac{1}{2} |\nabla \phi|^2 + \frac{p}{\rho} + g z = \text{Const.}$$



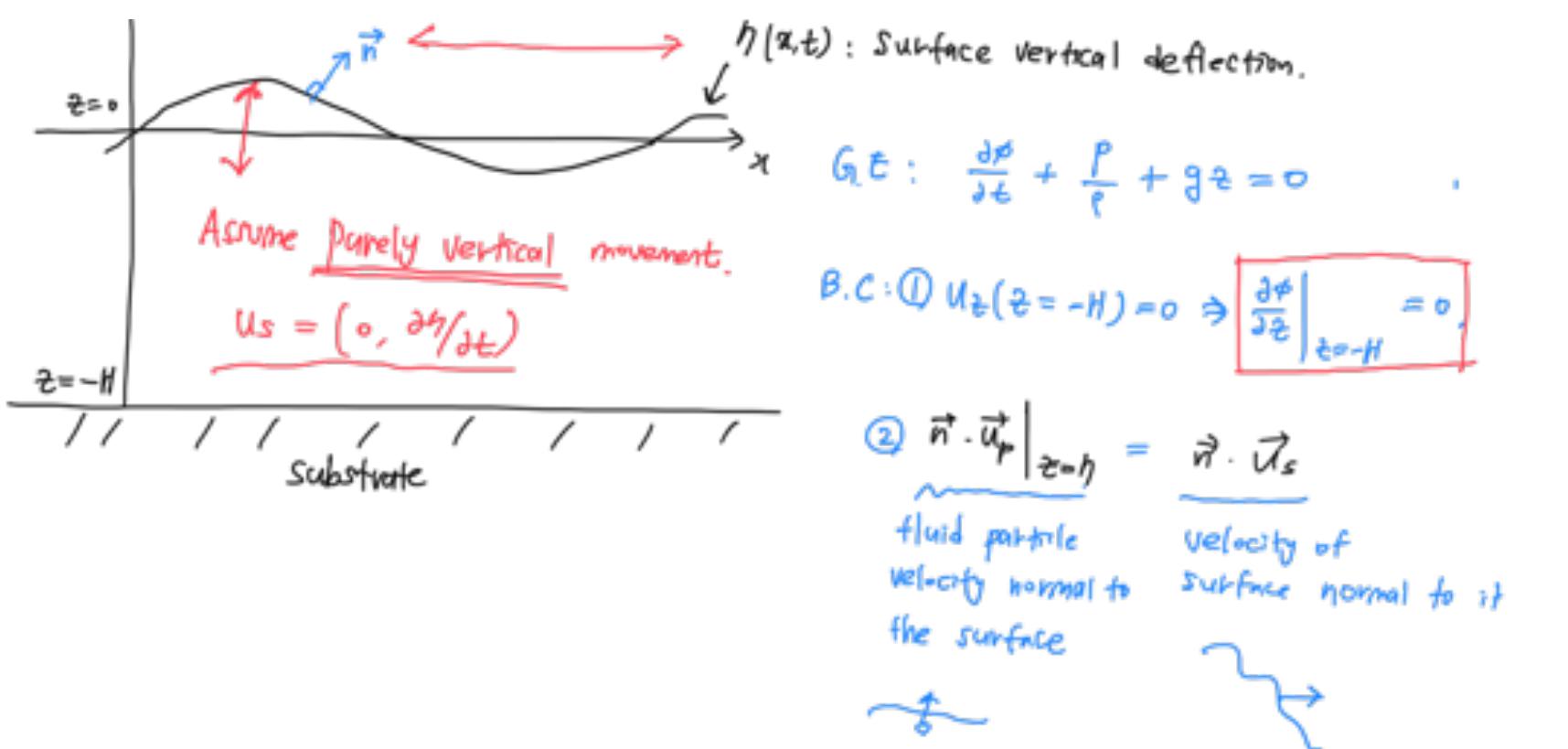
At $\rho = \rho_{\text{ambient}}$, undisturbed, neglect slope $\Rightarrow \frac{P_{\text{amb}}}{\rho} = \text{Constant.}, |\nabla \phi|^2 \sim 0$.

$$\Rightarrow \frac{\partial \phi}{\partial t} + \frac{1}{2} |\nabla \phi|^2 + \frac{P_{\text{absolute}}}{\rho} + g z = \frac{P_{\text{ambient}}}{\rho}$$

$$\Rightarrow \frac{\partial \phi}{\partial t} + \frac{P_{\text{gauge}}}{\rho} + g z = 0$$

Surface gravity wave.

Long wavelength $\xrightarrow{\frac{\partial h}{\partial x} \ll 1}$



$$③ \Rightarrow \text{Surface } f(x, z, t) = 0 \Rightarrow z - h(x, t) = 0$$

$$\left. \vec{n} = \frac{\nabla f}{\|\nabla f\|} = \left(-\frac{\partial h}{\partial x}, 1 \right) \right\} \Rightarrow \vec{n} \cdot \vec{u} \Big|_{z=h} = \vec{n} \cdot \vec{u}_s \quad \text{Q) what if we don't neglect } \vec{x} \text{ direction of surface?}$$

$$\Rightarrow \left(-\frac{\partial h}{\partial x}, 1 \right) \cdot (u, w) = \left(-\frac{\partial h}{\partial x}, 1 \right) \cdot \left(0, \frac{\partial h}{\partial t} \right)$$

$$\Rightarrow -\frac{\partial h}{\partial x} u + w = \frac{\partial h}{\partial t} \quad \left(w = \frac{\partial \phi}{\partial z} \Big|_{z=h} = \frac{\partial \phi}{\partial z} \Big|_{z=0} + \underbrace{\gamma \frac{\partial^2 \phi}{\partial z^2} + \dots}_{\text{Higher order...}} \right)$$

$$\Rightarrow \frac{\partial \phi}{\partial z} \Big|_{z=0} = \frac{\partial h}{\partial t} + \underbrace{\frac{\partial h}{\partial x} \cdot \frac{\partial \phi}{\partial x}}_{\ll 1} \Rightarrow \boxed{\frac{\partial \phi}{\partial z} \Big|_{z=0}} = \frac{\partial h}{\partial t}$$

Neglect $\rightarrow 0$
↓
Q) what if we include all higher order terms?

Q) what if γ is small?

④ at $z=h$, gauge pressure at interface $= 0$ (surface tension $\propto \gamma$)

$$\frac{\partial \phi}{\partial t} + \cancel{\frac{\rho \gamma}{\rho}} + g z = 0 \Rightarrow \frac{\partial \phi}{\partial t} \Big|_{z=h} = \frac{\partial \phi}{\partial t} \Big|_{z=0} = -gh$$

$$\Rightarrow \boxed{\frac{\partial \phi}{\partial t} \Big|_{z=0} = -gh}$$

Problem: $\phi(x, z, t) = \underbrace{f(z)}_{\text{depth term}} \sin(kx - \omega(k, t) t)$

Initial condition: $h(x, t=0) = a \cos kx$

① From continuity, $\nabla^2 \phi = 0 \Rightarrow \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial z^2} = 0 \Rightarrow \frac{\partial^2 f}{\partial z^2} - k^2 f = 0$

$$\Rightarrow f(z) = A e^{kz} + B e^{-kz}$$

$$\Rightarrow \phi(x, z, t) = \underbrace{(A e^{kz} + B e^{-kz})}_{\text{sin}(kx - \omega(k)t)}$$

$$\textcircled{1} \frac{\partial \phi}{\partial z} \Big|_{z=-H} = 0 \Rightarrow A k e^{-kH} - B k e^{+kH} = 0 \Rightarrow A = B e^{2kH} \rightarrow \textcircled{1}$$

$$\textcircled{2} \frac{\partial \phi}{\partial z} \Big|_{z=0} = \frac{\partial \eta}{\partial t} \Rightarrow (A k e^{kz} - B k e^{-kz}) \Big|_{z=0} \cancel{\sin(kx - \omega(k)t)} = \frac{A+B}{g} w(k)^2 \cancel{\sin(kx - \omega(k)t)} \quad (\text{by } \textcircled{3})$$

$$\Rightarrow (A-B)k = \frac{A+B}{g} \{w(k)\}^2$$

$$\Rightarrow w(k) = \sqrt{gk \frac{A-B}{A+B}} = gk \frac{e^{2kH}-1}{e^{2kH}+1} = \sqrt{gk \frac{e^{kH}-e^{-kH}}{e^{kH}+e^{-kH}}}$$

$$\textcircled{3} \frac{\partial \phi}{\partial t} \Big|_{z=0} = -gh \Rightarrow (A e^{kz} + B e^{-kz}) \Big|_{z=0} \cancel{-\omega(k) \cos(kx - \omega(k)t)} = -gh$$

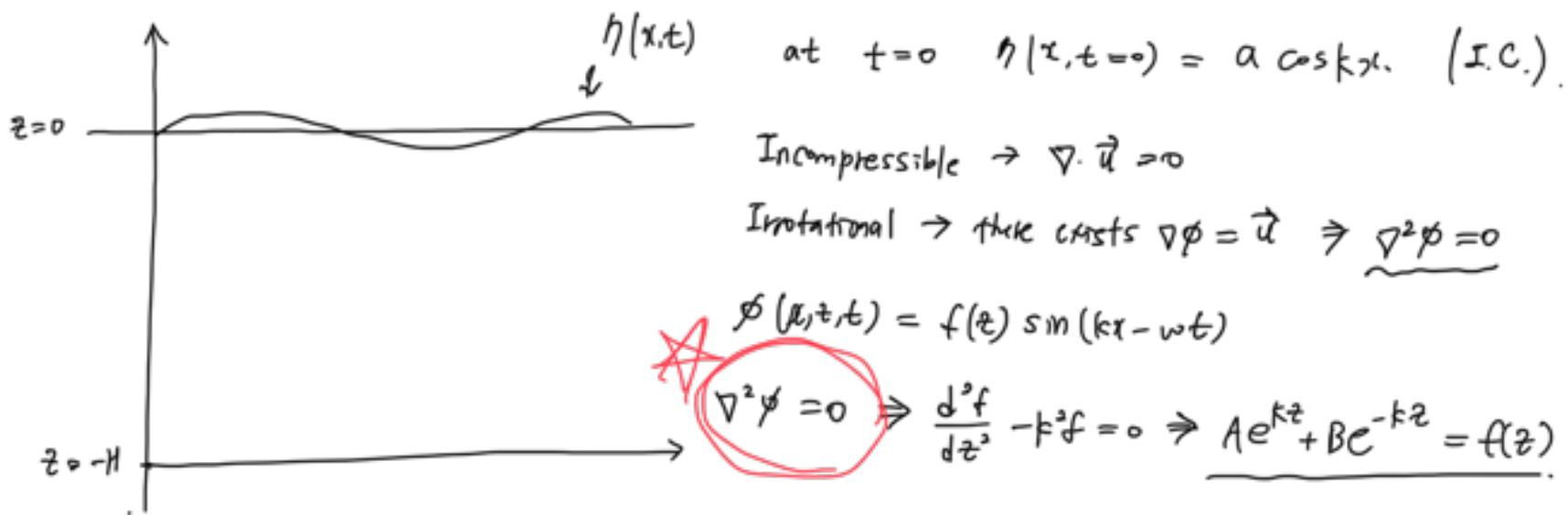
$$\Rightarrow gh = (A+B) w(k) \cos(kx - \omega(k)t)$$

$$\Rightarrow h = \frac{A+B}{g} w(k) \cos(kx - \omega(k)t) \rightarrow \textcircled{3}$$

From \textcircled{2}, $\omega(k) = \underbrace{\sqrt{gk \tanh(kH)}}$



Wave Lecture 10 (2021007)



$$\textcircled{1} \quad z = -H, \quad \frac{\partial \phi}{\partial z} \Big|_{z=-H} = 0 \quad (\because u_z \Big|_{bottom} = 0).$$

$$\Rightarrow \frac{\partial f}{\partial z} \sin(kx - \omega t) = 0 \Rightarrow \frac{\partial f}{\partial z} \Big|_{z=-H} = 0 \Rightarrow k(Ae^{-kH} - Be^{kH}) = 0 \Rightarrow \underline{A = Be^{2kH}}$$

$$\textcircled{2} \quad z = 0, \quad \frac{\partial \phi}{\partial z} \Big|_{z=0} = \frac{\partial h}{\partial t}, \quad \text{Note that } h(x,t) = a \cos(kx - \omega t) \quad \text{--- (1)}$$

$$\Rightarrow \frac{\partial h}{\partial t} = (Ak - Bk) \sin(kx - \omega t) \Rightarrow a(-\sin(kx - \omega t))(-\omega) = (Ak - Bk) \sin(kx - \omega t)$$

$$\Rightarrow \underline{k(A-B) = aw} \Rightarrow \underline{A = \frac{aw}{k} \frac{1}{1-e^{-2kH}}}, \quad \underline{B = \frac{aw}{k} \frac{e^{-2kH}}{1-e^{-2kH}}}$$

$$\Rightarrow A = \frac{aw}{k} \frac{e^{kH}}{e^{kH} - e^{-kH}} = \frac{aw}{k} \frac{e^{kH}}{2 \sinh kH}$$

$$B = \frac{aw}{k} \frac{e^{-kH}}{e^{kH} - e^{-kH}} = \frac{aw}{k} \frac{e^{-kH}}{2 \sinh kH}$$

$$\begin{aligned} \Rightarrow f(z) &= e^{kz} \frac{aw}{k} \frac{e^{kH}}{2 \sinh kH} + e^{-kz} \frac{aw}{k} \frac{e^{-kH}}{2 \sinh kH} \\ &= \frac{aw}{k} \frac{e^{k(z+H)} + e^{-k(z+H)}}{\sinh(kH) \cdot 2} = \frac{aw}{k} \frac{\cosh k(z+H)}{\sinh kH} \end{aligned}$$

cosh k(z+H).

$$\Rightarrow \phi(x, z, t) = \frac{aw}{k} \frac{\cosh k(z+H)}{\sinh kH} \sin(kx - \omega t) \quad \text{--- (2)}$$

$$\textcircled{3} \quad \frac{\partial \phi}{\partial t} \Big|_{z=0} = -gh \quad \text{from (1) and (2),}$$

$$\Rightarrow -\frac{aw^2}{k} \frac{\cos k(0+H)}{\sinh kH} \cancel{\cos(kx - \omega t)} = -g \cancel{d} \cos(kx - \omega t)$$

$$\Rightarrow \omega^2 = gk \frac{\sinh kH}{\cosh kH} \Rightarrow \omega = \sqrt{gk \tanh(kH)}.$$

* Properties.

$$\left\{ \begin{array}{l} V_p = w/k = \sqrt{\frac{g}{k}} \sqrt{\tanh(kH)} = \sqrt{gh \left[\frac{\tanh(kH)}{kh} \right]} \\ V_g = \partial w / \partial k = \frac{1}{2} \sqrt{\frac{g}{k}} \sqrt{\tanh(kH)} = \frac{1}{2} \sqrt{gh \left[\frac{\tanh(kH)}{kh} \right]}. \end{array} \right.$$

$\left(\frac{H}{\lambda} \gg 1 \Rightarrow kh \gg 1 \right)$	$\left(\frac{H}{\lambda} \ll 1 \Rightarrow kh \ll 1 \right)$
c_p for deep water ($H \gg \lambda$)	c_p for shallow water ($H \ll \lambda$)
$\lim_{kh \rightarrow \infty} \tanh kh = 1 \Rightarrow c_p \equiv \sqrt{\frac{g}{k}}$	$\lim_{kh \rightarrow 0} \frac{\tanh kh}{kh} = 1 \Rightarrow c_p = \sqrt{gh}$.
$\lambda \uparrow \quad k \downarrow \quad c_p \uparrow$	$H \uparrow \quad c_p \uparrow$

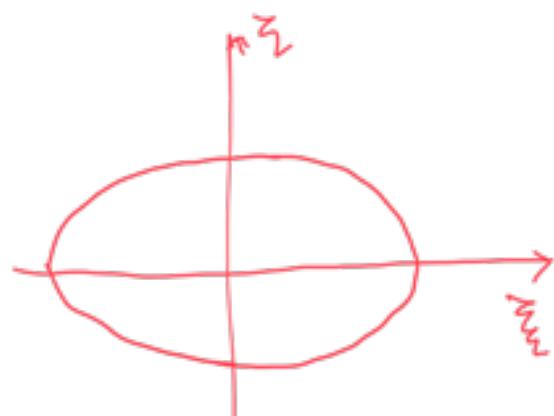
* Trajectory of particles.

$$\vec{x}_p(t) = x_p(t) \vec{a}_x + z_p(t) \vec{a}_z$$

$$\begin{aligned} x_p(t) &= x_0 + \xi(t) \Rightarrow \frac{dx_p}{dt} = \frac{d\xi}{dt} = \frac{\partial \xi}{\partial t} = \frac{\omega}{k} \frac{\cosh k(t+H)}{\sinh kH} \cos(kx - \omega t) \\ z_p(t) &= z_0 + \zeta(t) \quad \frac{dz_p}{dt} = \frac{d\zeta}{dt} = \frac{\partial \zeta}{\partial t} = \frac{\omega}{F} \end{aligned}$$

$$\left\{ \begin{array}{l} \xi(t) = -a \frac{\cosh k(t+H)}{\sinh kH} \sin(kx - \omega t) + "O" \\ \zeta(t) = a \frac{\sinh k(t+H)}{\sinh kH} \cos(kx - \omega t) \end{array} \right. \quad \because \xi \text{ and } \zeta \text{ means perturbation.}$$

$$\Rightarrow \left\{ \frac{\xi(t)}{-a \frac{\cosh k(t+H)}{\sinh kH}} \right\}^2 + \left\{ \frac{\zeta(t)}{+a \frac{\sinh k(t+H)}{\sinh kH}} \right\}^2 = 1 \quad \text{Ellipse!}$$



Note $-H < z < \infty \Rightarrow \cosh k(z+H) \propto e^{\square} + e^{-\square} > \sinh k(z+H) \propto e^{\square} - e^{-\square}$

\downarrow
strict!

HW #2 prob 5.

Find the orientation. (direction of rotation)



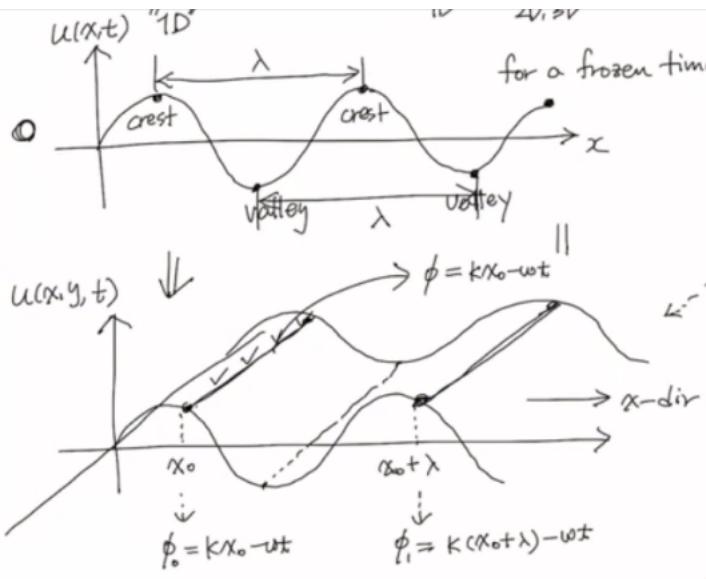
⇒ phove it!

Trajectory	✓ deep water $H \gg \lambda$	intermediate depth $\lambda \sim H$	shallow water $\lambda \gg H$
$(KH \gg 1)$			

recall
$$\left[\frac{\zeta}{a \frac{\cosh K(z+H)}{\sinh KH}} \right]^2 + \left[\frac{\zeta}{a \frac{\sinh K(z+H)}{\sinh KH}} \right]^2$$

Wave Lecture 11 (20211012)

- Wavefronts, Wavenumber, wave packets.



$$\phi_1 - \phi_0 = 2\pi$$

$$u(x,t) = f(kx - \omega t)$$

$$u = \sin(kx - \omega t) \rightarrow \text{phase}$$

all the points on each crest

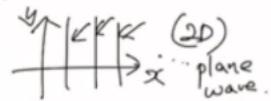
have the same phase, $\phi_0 = kx_0 - \omega t$ (frozen)
= const

The points form a "equi-phase" line
(iso-phase)

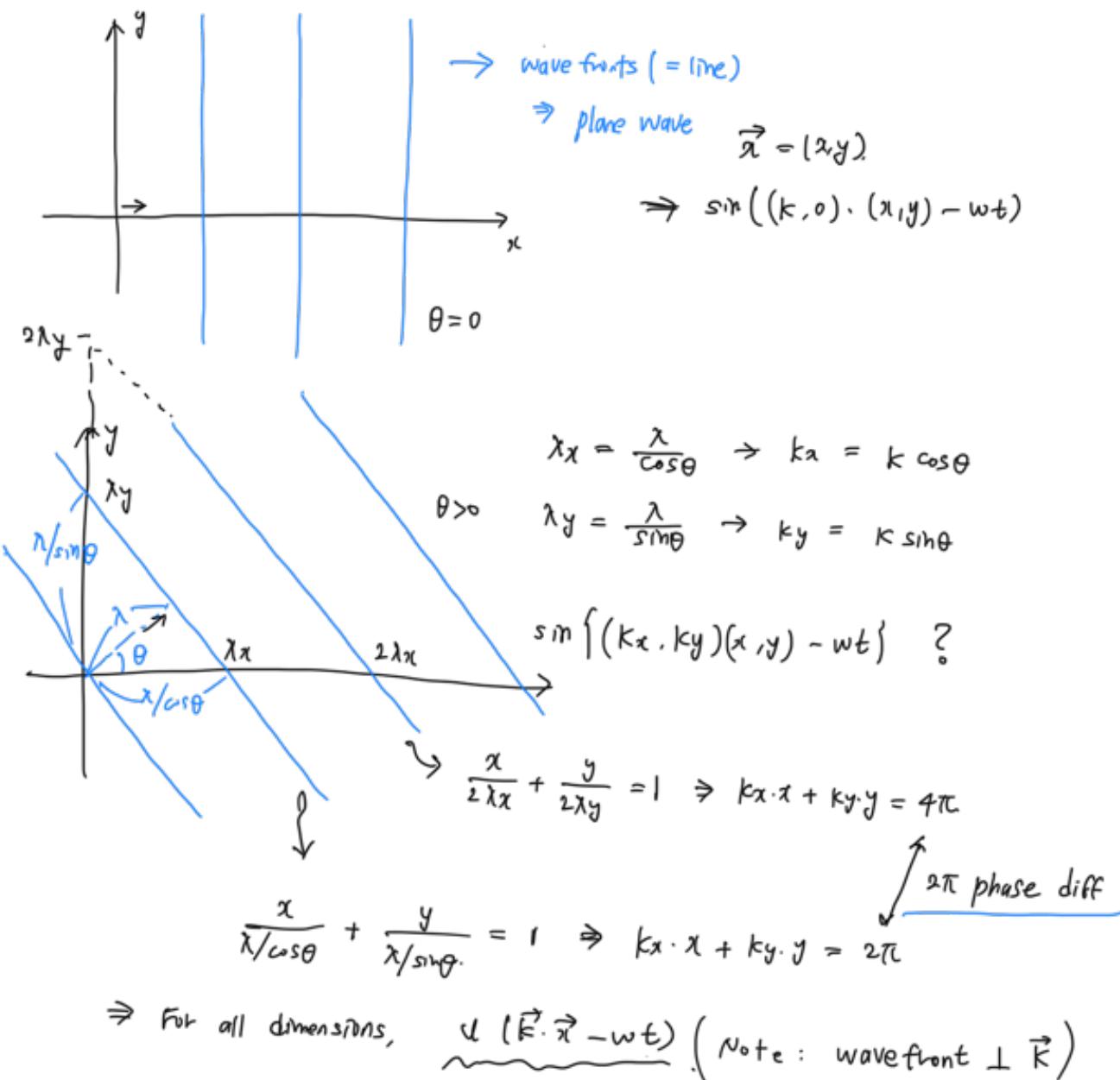
Then, we call it wavefront.

If a wavefront forms a line or a plane,
(2D) (3D)

we call it plane wave



< Top view of 2D wave p.p >

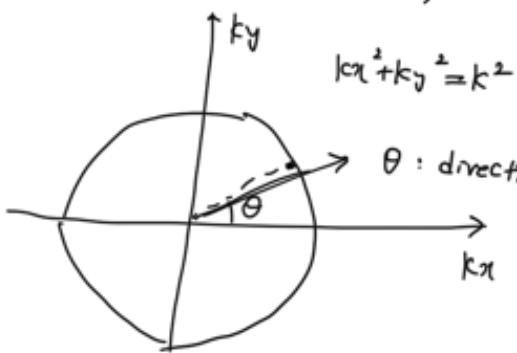


E.g.) Cylindrical wave

$$\vec{r} = (r \cos\theta, r \sin\theta), \vec{k} = (k \cos\theta, k \sin\theta)$$

$$u(\vec{k} \cdot \vec{r} - wt) = u(kr(\cos^2 + \sin^2) - wt) = u(kr - wt)$$

⟨ Wavenumber plane. (2D) ⟩



θ : direction of propagation

what if.

Q) $|k_x| > k$?

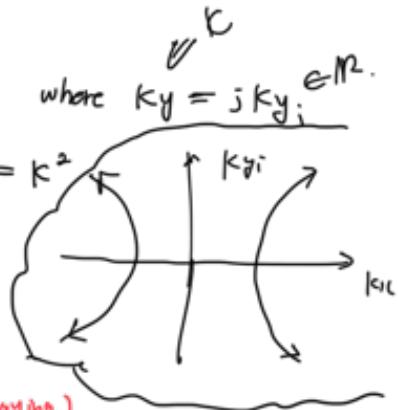
$$k_x^2 + k_y^2 = k^2 \text{ where } k_y = j k_y e^{j\pi/2}$$

$$\Rightarrow |k_x|^2 - |k_y|^2 = k^2$$

Note: $e^{j(R \cdot \vec{x} - \omega t)}$

$$= e^{jkx} e^{-kyj} e^{-j\omega t}$$

Evanescent (Decaying).



⟨ Wave packets ⟩ Superposition, phase velocity, group velocity.

$$f_1 = A \cos(k_1 x - \omega_1 t)$$

$$f_2 = A \cos(k_2 x - \omega_2 t)$$

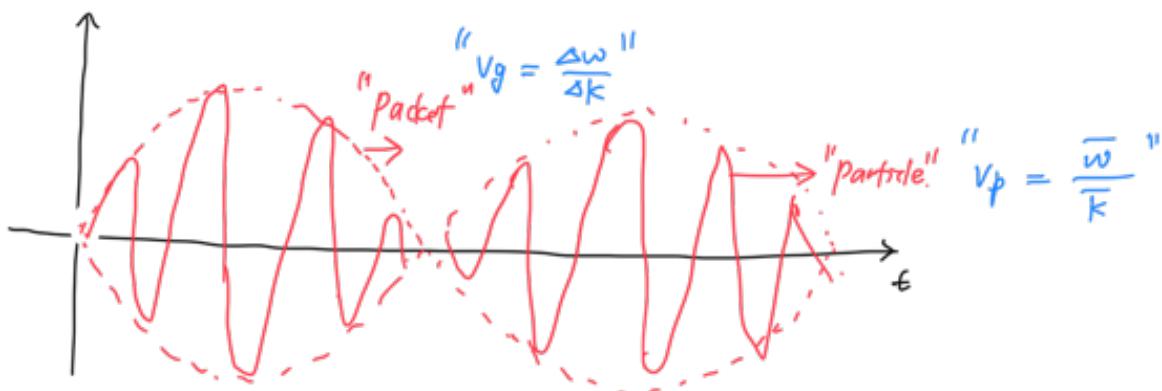
$\oplus \Rightarrow f_1 + f_2 = A \left[2 \cos\left(\frac{\alpha + \beta}{2}\right) \cos\left(\frac{\alpha - \beta}{2}\right) \right]$

$$\Rightarrow f_1 + f_2 = 2A \cos\left(\frac{k_1 + k_2}{2} x - \frac{\omega_1 + \omega_2}{2} t\right) \cos\left(\frac{k_1 - k_2}{2} x - \frac{\omega_1 - \omega_2}{2} t\right)$$

$$= 2A \cos(\bar{k} x - \bar{\omega} t) \cos(\Delta k x - \Delta \omega t)$$

Fastly oscillating slowly oscillating.

$$\Delta \omega \ll \bar{\omega} \quad \because \omega_1 \approx \omega_2, \quad k_1 \approx k_2$$



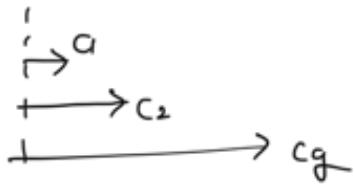
$$c_g = \frac{\Delta \omega}{\Delta k} \rightarrow \lim_{\Delta k \rightarrow 0, \Delta \omega \rightarrow 0} \frac{\Delta \omega}{\Delta k} \Rightarrow \left(\frac{\partial \omega}{\partial k} \right), \quad c_p = \left(\frac{\omega}{k} \right)$$

Q1. $k_1 \neq k_2$, $\omega_1 \neq \omega_2$, what's different?

Q2. $\frac{\omega_1}{k_1} < \frac{\omega_2}{k_2}$ and $k_1 < k_2$

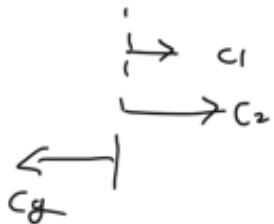
$$c_g = \frac{\omega_2 - \omega_1}{k_2 - k_1} > \frac{\omega_2 - k_1/k_2 \cdot \omega_2}{k_2 - k_1} = \frac{\omega_2}{k_2} = c_2$$

$\Rightarrow c_g > c_2 > c_1$ (Group velocity is the fastest among c_1 & c_2)



Q3. $\frac{\omega_1}{k_1} > \frac{\omega_2}{k_2}$ and $k_1 < k_2$ and $\omega_1 > \omega_2$

$$c_g = \frac{\omega_2 - \omega_1}{k_2 - k_1} < 0 \quad (\text{wave packets move in the opposite direction})$$



Wave Lecture 12 (20211014)

Moving medium wave equation | $(\rho = \rho_0 + \rho', u = u_0 + u', p = p_0 + p')$

$$\textcircled{1} \text{ cont: } \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{u}) = 0 \Rightarrow \frac{\partial \rho'}{\partial t} + \nabla \cdot (\rho_0 u' + \rho' u_0) = 0$$

$$\Rightarrow \underbrace{\frac{\partial \rho'}{\partial t} + \rho_0 \nabla \cdot \vec{u}'}_{\text{Stationary } (u_0 = 0)} + u_0 \cdot \nabla \rho' = 0.$$

Euler:

$$\textcircled{2} \quad \rho \left(\frac{\partial u}{\partial t} + u \cdot \nabla u \right) = -\nabla p \Rightarrow (\rho_0 + \rho') \left(\frac{\partial u'}{\partial t} + \underbrace{(u_0 + u') \nabla}_{\text{H.O.T.} \Rightarrow 0} \cdot \vec{u}' \right) = -\nabla p'$$

$$\Rightarrow \underbrace{\rho_0 \left(\frac{\partial u'}{\partial t} + u_0 \cdot \nabla u' \right)}_{\text{Stationary } (u_0 = 0)} = -\nabla p'$$

Stationary ($u_0 = 0$)

\textcircled{3} Isentropic ($S=0$) state.

$$\rho' = c^2 \rho' = (\gamma R T)^2 \rho'$$

$$\boxed{\begin{aligned} &\text{let } \frac{\partial}{\partial t} + u \cdot \nabla = \frac{D}{Dt} \\ &\frac{\partial}{\partial t} + u_0 \cdot \nabla = \frac{D_0}{Dt} \end{aligned}}$$

$$\Rightarrow \frac{D_0}{Dt} \rho' + \underbrace{\rho_0 \nabla \cdot \vec{u}'}_{\textcircled{1}} = 0 \quad \Rightarrow \frac{D_0}{Dt} \textcircled{1} - \nabla \cdot \textcircled{2}$$

$$\underbrace{\rho_0 \cdot \frac{D_0}{Dt} u'}_{\textcircled{2}} = -\nabla p' \quad \textcircled{2}$$

$$\Rightarrow \nabla^2 p' - \frac{1}{c^2} \frac{D_0^2}{Dt^2} p' = 0$$

$$\nabla^2 p' - \frac{1}{c^2} \left(\frac{D_0^2}{Dt^2} p' \right) = 0 \Rightarrow \nabla^2 p' - \frac{1}{c^2} \left(\frac{\partial^2}{\partial t^2} + 2 \vec{u}_0 \cdot \nabla \frac{\partial}{\partial t} + (\vec{u}_0 \cdot \nabla)^2 \right) p' = 0.$$

$$\underline{\underline{p'(x,t) = \tilde{p}(\vec{x}) e^{-j\omega t}}}$$

Note that \vec{x} is vector ($\vec{x} = (x, y)$)

$$\textcircled{1} \quad \frac{\partial^2 p'}{\partial t^2} = (-j\omega)^2 \tilde{p}(\vec{x}) e^{-j\omega t} = \underline{\underline{-\omega^2 \tilde{p}(\vec{x}) e^{-j\omega t}}}$$

$$\textcircled{2} \quad 2\vec{u}_0 \cdot \nabla \frac{\partial}{\partial t} p' = 2\vec{u}_0 \cdot \nabla (-j\omega) \tilde{p}(x) e^{-j\omega t} = -2j\omega u_{00} \frac{\partial \tilde{p}}{\partial x} e^{-j\omega t}$$

$$= -2j\omega (u_{0x}, u_{0y}) \cdot \left(\frac{\partial \tilde{p}}{\partial x}, \frac{\partial \tilde{p}}{\partial y} \right) e^{-j\omega t}.$$

(for $u_x, u_y, u_x + u_{0x}$)

$\therefore \text{Assume } \vec{u}_0 = (u_{00}, 0) \text{ in } \mathbb{R}^2$

$$\Rightarrow \vec{u}_0 \cdot \nabla = (u_{00}, 0) \left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y} \right) = u_{00} \frac{\partial}{\partial x}.$$

$$\textcircled{3} \quad u_0 \cdot \nabla = u_{00} \frac{\partial}{\partial x} \Rightarrow \left(u_{00} \frac{\partial}{\partial x} \right)^2 p' = u_{00}^2 \frac{\partial^2 \tilde{p}'}{\partial x^2}$$

$$u_0 \cdot \nabla = (u_x, u_y) \cdot \left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y} \right) = u_x \frac{\partial}{\partial x} + u_y \frac{\partial}{\partial y} \Rightarrow \text{square} \Rightarrow u_{0x}^2 \frac{\partial^2 \tilde{p}}{\partial x^2} + 2u_x u_y \frac{\partial^2 \tilde{p}}{\partial x \partial y} + u_{0y}^2 \frac{\partial^2 \tilde{p}}{\partial y^2}$$

$$\Rightarrow \left[\gamma^2 \tilde{p}(\vec{x}) - \frac{1}{c^2} \left\{ -\omega^2 \tilde{p}(\vec{x}) - 2j\omega u_{00} \frac{\partial \tilde{p}}{\partial x} + u_{00}^2 \frac{\partial^2 \tilde{p}'}{\partial x^2} \right\} \right] e^{-j\omega t} = 0$$

$$\Rightarrow \frac{\partial^2 \tilde{p}}{\partial x^2} + \frac{\partial^2 \tilde{p}}{\partial y^2} + \left(\frac{\omega}{c} \right)^2 \tilde{p} + 2j \left(\frac{\omega}{c} \right) \left(\frac{u_{00}}{c} \right) \frac{\partial \tilde{p}}{\partial x} - \left(\frac{u_{00}}{c} \right)^2 \frac{\partial^2 \tilde{p}'}{\partial x^2} = 0$$

$$\Rightarrow \frac{\partial^2 \tilde{p}}{\partial x^2} + \frac{\partial^2 \tilde{p}}{\partial y^2} + k^2 \tilde{p} + 2jkM \frac{\partial \tilde{p}}{\partial x} - M^2 \frac{\partial^2 \tilde{p}'}{\partial x^2} = 0$$

$$\begin{pmatrix} M = \frac{u_{00}}{c} : \text{Mach \#} \\ k = \frac{\omega}{c} : \text{wave \#} \end{pmatrix} \quad \begin{array}{l} M=1 : \text{Sonic} \\ M>1 : \text{Super Sonic} \end{array}$$

$$\Rightarrow \boxed{(1-M^2) \frac{\partial^2 \tilde{p}}{\partial x^2} + \frac{\partial^2 \tilde{p}}{\partial y^2} + 2jkM \frac{\partial \tilde{p}}{\partial x} + k^2 \tilde{p} = 0}$$

$$\text{if } M=0, \quad \gamma^2 \tilde{p} + k^2 \tilde{p} = 0$$

\Rightarrow Helmholtz Eq.

< In 1-Dimension >

$$\Rightarrow (1-M^2) \frac{\partial^2 \tilde{p}}{\partial x^2} + 2jkM \frac{\partial \tilde{p}}{\partial x} + k^2 \tilde{p} = 0 \quad \text{set } \tilde{p} = e^{jkmx}$$

(note: $k \neq km$)

$$\Rightarrow (1-M^2)(-km^2) + 2jkM(jkm) + k^2 = 0$$

$$\Rightarrow \underbrace{(1-M^2)km^2 + 2kkm \cdot M - k^2}_{=0} = 0 \Rightarrow km = \frac{-km \pm \sqrt{k^2 m^2 + k^2 (1-M^2)}}{1-M^2}$$

$$\Rightarrow km = \frac{-km \pm k}{(1-M)(1+M)} \cdot \frac{k}{1-M}$$

$$\Rightarrow \tilde{p}(x) = \begin{cases} e^{j\frac{k}{1+M}x} & : \text{right-going} \quad \lambda_r = (1+M)\lambda \\ e^{-j\frac{k}{1-M}x} & : \text{left-going} \quad \lambda_l = (1-M)\lambda \end{cases}$$

\Rightarrow Modulation of wavelength
due to the flow.

< Prandtl - Glauert Transformation ($p - G_1$ trans) >

$$(1-M^2) \frac{\partial^2 \tilde{p}}{\partial x^2} + \frac{\partial^2 \tilde{p}}{\partial y^2} + 2jkM \frac{\partial \tilde{p}}{\partial x} + k^2 \tilde{p} = 0$$

$$\tilde{z} = \frac{x}{\sqrt{1-M^2}} \quad \text{and} \quad h = y \quad \text{and} \quad \psi = \tilde{p} e^{-j\alpha \tilde{z}}$$

\Rightarrow ? 4th Calibration.

\hookrightarrow $(1-M^2)$ 상체에 대한 증가 및 감소

$$\Rightarrow (1-M^2) \cancel{\frac{1}{1-M^2} \frac{\partial^2}{\partial z^2} (\psi e^{j\alpha z})} + \frac{\partial^2}{\partial \eta^2} (\psi e^{j\alpha z}) + 2jkM \frac{\partial}{\partial x} (\psi e^{j\alpha z}) + k^2 \psi e^{j\alpha z} = 0$$

$$\Rightarrow \cancel{\frac{\partial^2 \psi}{\partial z^2} e^{j\alpha z}} + 2(j\alpha) \cancel{\frac{\partial \psi}{\partial z} e^{j\alpha z}} + (j\alpha)^2 \psi \cancel{e^{j\alpha z}} + \cancel{\frac{\partial^2 \psi}{\partial \eta^2} e^{j\alpha z}} + \cancel{\frac{2jkM}{\sqrt{1-M^2}} \left(\frac{\partial \psi}{\partial z} + j\alpha \psi \right) e^{j\alpha z}} + k^2 \psi \cancel{e^{j\alpha z}} = 0$$

$$\Rightarrow \frac{\partial^2 \psi}{\partial z^2} + \frac{\partial^2 \psi}{\partial \eta^2} + 2j \left(\alpha + \frac{kM}{\sqrt{1-M^2}} \right) \frac{\partial \psi}{\partial z} + \psi \left\{ k^2 - \alpha^2 - \frac{2kM\alpha}{\sqrt{1-M^2}} \right\}$$

Set $\alpha = \frac{-kM}{\sqrt{1-M^2}}$ to eliminate $\frac{\partial \psi}{\partial z}$ term!

$$\Rightarrow \nabla^2 \psi + \psi \left\{ k^2 - \frac{k^2 M^2}{1-M^2} + \frac{2k^2 M^2}{1-M^2} \right\} \Rightarrow \boxed{\nabla^2 \psi + \psi \left\{ \frac{k^2}{1-M^2} \right\} = 0}$$

Wave Lecture 13 (20211026)

Lec. "Part II"-①

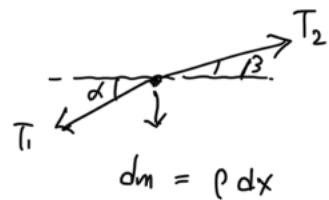
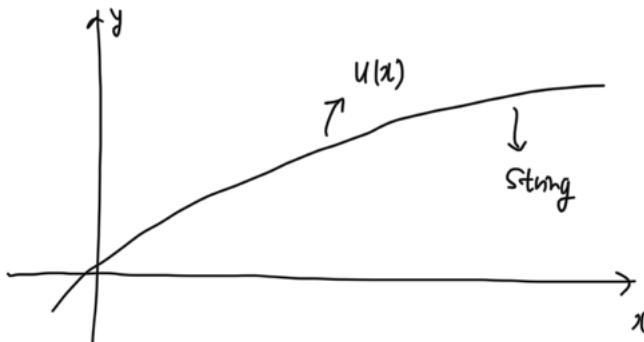
basis: 1DOF/2DOF vib.) infinite lattice (mm/s)
in fluids gas(air) / liquid (water)
Compressible incompressible
black C# or D# D# or Eb F# or G# A# or B#
C D E F G A B C D E
1-octave 12 steps C → C (1-octave)
 $f(C) = f_0$
 $f(C_1) = 2f_0$
 $(12 \text{ steps}) \quad (x 2^{\frac{1}{12}})^2 = 2^{\frac{1}{6}} = \sqrt[6]{2}$
 $f(C^\#) = 2^{\frac{1}{12}} \cdot f_0$
 $f(D) = (2^{\frac{1}{12}})^2 f_0 = 2^{\frac{1}{6}} f_0$

midterm final
basis: waves in string (1D) & membrane (2D)
in Solids infinite solid beams/plates

Waves in String (1D)
Math & Phys of Guitar (Violin, cello, etc)

6 strings
finger \Rightarrow tune
lower higher
Guitar how many octaves?
2 octaves
why the thin string have
does high tone?

Waves in String



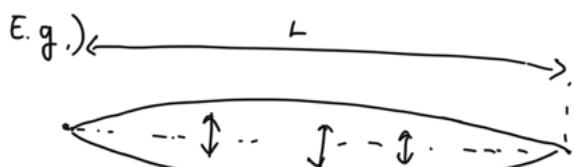
$$1) x : -T_1 \cos \alpha + T_2 \cos \beta = 0 \Rightarrow T_1 \approx T_2 = T.$$

$$2) y : T_2 \sin \beta - T_1 \sin \alpha = dm \ddot{u} \Rightarrow T (\tan \beta - \tan \alpha) = dm \ddot{u} = \rho \partial x \ddot{u}$$

$$\Rightarrow \tan \beta = \left. \frac{\partial u}{\partial x} \right|_{x=x_0 + \Delta x} \quad \text{and} \quad \tan \alpha = \left. \frac{\partial u}{\partial x} \right|_{x=x_0}$$

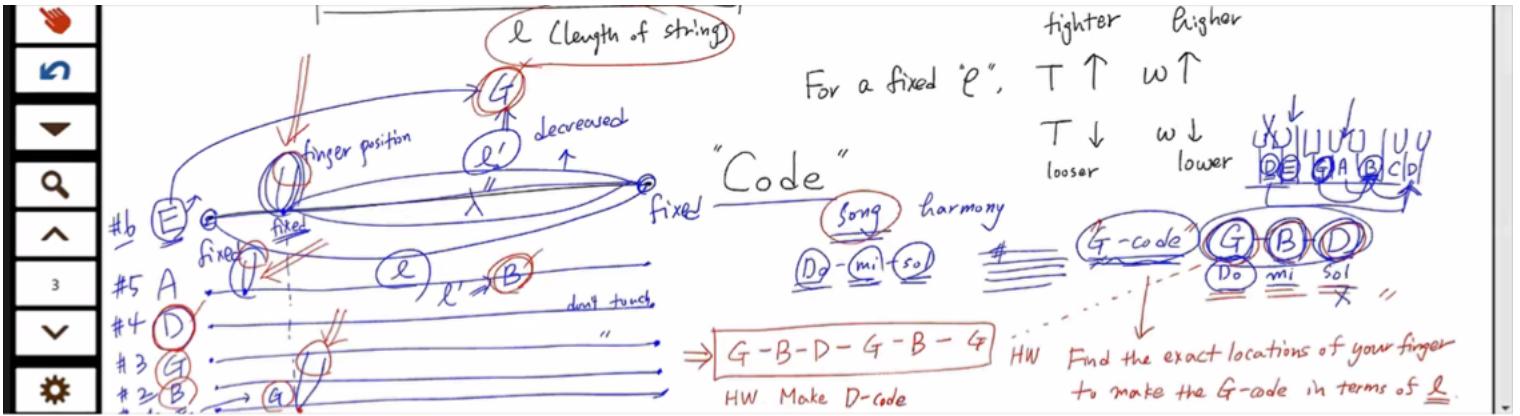
$$\Rightarrow T \left(\left. \frac{\partial u}{\partial x} \right|_{x=x_0 + \Delta x} - \left. \frac{\partial u}{\partial x} \right|_{x=x_0} \right) = T \left(\cancel{\left. \frac{\partial u}{\partial x} \right|_{x_0}} + \frac{\partial}{\partial x} \left. \frac{\partial u}{\partial x} \right|_{x_0} \Delta x + H.o.T - \cancel{\left. \frac{\partial u}{\partial x} \right|_{x_0}} \right)$$

$$\Rightarrow T \frac{\partial^2 u}{\partial x^2} = \rho \cdot \cancel{\Delta x} \cancel{\frac{\partial^2 u}{\partial t^2}} \Rightarrow \boxed{\frac{\partial^2 u}{\partial x^2} - \frac{1}{c_s^2} \frac{\partial^2 u}{\partial t^2} = 0} \quad (c_s = \sqrt{T/\rho})$$



$$\omega = kc = \frac{\pi}{L} \cdot \sqrt{\frac{T}{\rho}}$$

$$\lambda = 2L \rightarrow k = \frac{2\pi}{\lambda} = \frac{\pi}{L}$$



$$\begin{aligned} D &: D - F^{\#} - A \\ A &: A - C^{\#} - E \end{aligned} \quad \left. \right\}, \quad \text{Ex. GDC code 77m1ch5}$$

Next Class : String G.E using Lagrangian Mechanics. (continuum system)

Not lattice!

Wave Lecture 14 (20211028)

Waves in Strings (Lagrangian)

• $T = \int_{x_1}^{x_2} \frac{1}{2} (\rho dx) \left(\frac{du}{dt} \right)^2$, $V =$ Work done in "stretching" the string away from equilibrium.

Tension: $K \Rightarrow \Delta V = K \cdot \Delta l \Rightarrow \Delta l = \sqrt{(dx)^2 + (du)^2} - dx$

$$\Rightarrow \Delta l = dx \sqrt{1 + \left(\frac{du}{dx} \right)^2} - 1 \approx dx \int \left(1 + \frac{1}{2} \left(\frac{du}{dx} \right)^2 - 1 \right) = \frac{1}{2} \left(\frac{du}{dx} \right)^2 dx \quad \left(\because u \ll 1, u_x, u_t \ll 1 \right)$$

$$V = \int_{x_1}^{x_2} \Delta V = \int_{x_1}^{x_2} K \frac{1}{2} \left(\frac{du}{dx} \right)^2 dx$$

$$L = T - V = \int_{x_1}^{x_2} \left[\frac{1}{2} \rho \left(\frac{\partial u}{\partial t} \right)^2 - \frac{1}{2} K \left(\frac{\partial u}{\partial x} \right)^2 \right] dx \quad L = L(t, x, u, u_t, u_x)$$

\Rightarrow Euler-Lagrange Eq. can't be used.

\Rightarrow Generalized Euler-Lagrange Eq.: $\frac{\partial L}{\partial u} - \frac{\partial}{\partial t} \left(\frac{\partial L}{\partial u_t} \right) - \frac{\partial}{\partial x} \left(\frac{\partial L}{\partial u_x} \right) = 0$

$$\begin{cases} \textcircled{1} \quad \frac{\partial L}{\partial u} = 0 \\ \textcircled{2} \quad \frac{\partial L}{\partial u_t} = \rho \frac{\partial u}{\partial t} \\ \textcircled{3} \quad \frac{\partial L}{\partial u_x} = -K \frac{\partial u}{\partial x} \end{cases} \Rightarrow \begin{cases} -\rho \frac{\partial^2 u}{\partial t^2} + K \frac{\partial^2 u}{\partial x^2} = 0 \\ \frac{\partial^2 u}{\partial t^2} - \frac{K}{\rho} \frac{\partial^2 u}{\partial x^2} = 0 \end{cases}$$

Wave Eq. for string.

Solving Equation.

$$\frac{\partial^2 u}{\partial t^2} - c^2 \frac{\partial^2 u}{\partial x^2} = 0 \Rightarrow u(x, t) = X(x)T(t) \Rightarrow TX - c^2 T''X = 0 \Rightarrow \frac{1}{c^2} \frac{T''}{T} = \frac{X''}{X} = -\mu^2$$



$$u(0) = 0$$

$$X(0) = 0$$

$$u(L) = 0$$

$$X(L) = 0$$

$$X(x) = A \cos \mu x + B \sin \mu x,$$

$$A = 0, \mu L = m\pi \Rightarrow \underline{\mu_m = \frac{m\pi}{L}} \quad (m=1, 2, \dots)$$

$$X(x) = \sum_{m=1}^{\infty} B_m \sin \left(\frac{m\pi}{L} x \right)$$

$$T(t) = A' \cos(c\mu t) + B' \sin(c\mu t) \Rightarrow u(x, t) = \sum_{m=1}^{\infty} \sin\left(\frac{m\pi}{L}x\right) \left[C_m \cos\left(c \cdot \frac{m\pi}{L}t\right) + D_m \sin\left(c \cdot \frac{m\pi}{L}t\right)\right]$$

C_m, D_m ?

$$\begin{aligned} u(x, 0) &= f(x) \\ u_t(x, 0) &= g(x) \end{aligned} \quad \begin{aligned} \Rightarrow \sum_{m=1}^{\infty} \sin\left(\frac{m\pi}{L}x\right) C_m &= f(x) \quad \text{--- 1.} \\ \Rightarrow \sum_{m=1}^{\infty} \sin\left(\frac{m\pi}{L}x\right) \cdot c \cdot \frac{m\pi}{L} \cdot D_m &= g(x) \quad \text{--- 2.} \end{aligned}$$

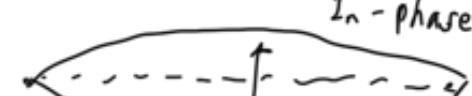
$$\textcircled{1} \quad \int_0^{2L/m} \sin\left(\frac{m\pi}{L}x\right) \cdot \sum_{m=1}^{\infty} \sin\left(\frac{m\pi}{L}x\right) \cdot C_m dx = \int_0^{2L/m} \sin\left(\frac{m\pi}{L}x\right) \cdot f(x) dx$$

\textcircled{2} In the same way as \textcircled{1}.

physics

$$u(x, t) = \sum_{m=1}^{\infty} \sin\left(\frac{m\pi}{L}x\right) (\text{Temporal terms}) = \sum \textcircled{1} + \textcircled{2} + \textcircled{3} + \dots$$

\textcircled{1} $m=1$



1st mode / fundamental mode.

\textcircled{2} $m=2$



2nd mode. Node / Nodal point.

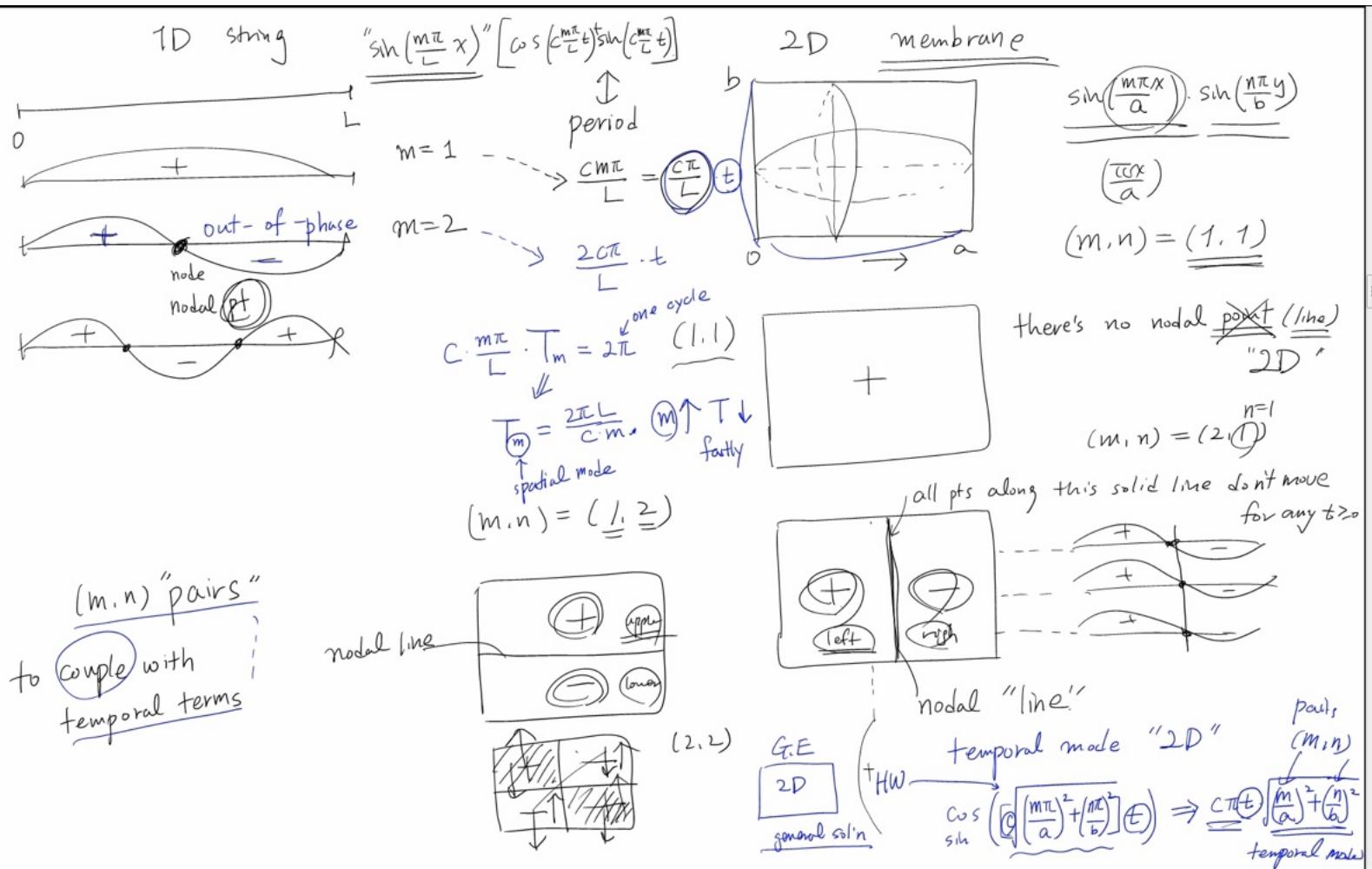
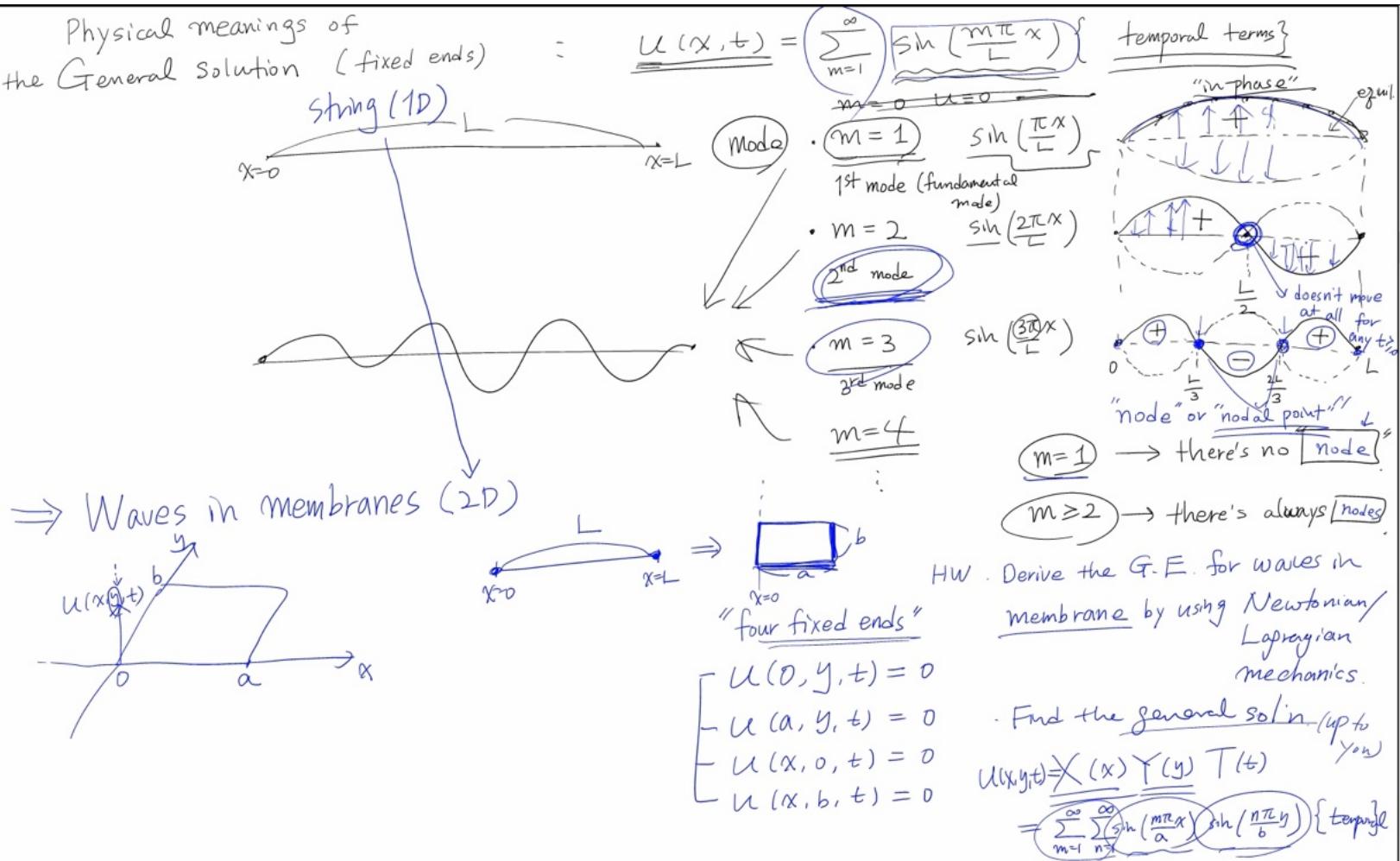
\textcircled{3} $m=3$



$m=1 \rightarrow$ no node

$m \geq 2 \rightarrow$ always node,

Wave Lecture 15 (20211102)



C. F. Gauss

Crown of math

[Number Theory]

* multiplication of two prime numbers

of $(4n+1)$ can be expressed by

"Summation" between two squares

$$P^2 + Q^2$$

$$\text{ex. } (5) \cdot (13) = \underline{\underline{65}} = 1^2 + 8^2$$

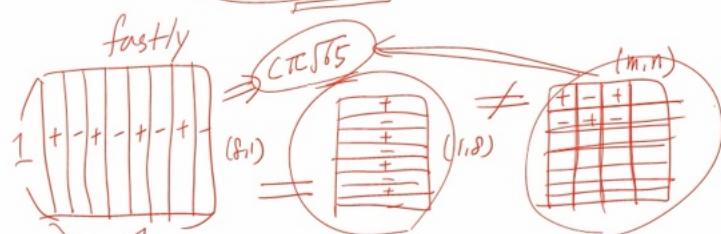
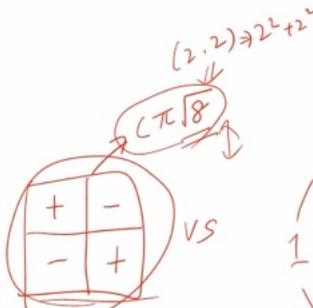
$$= 8^2 + 1^2$$

$$= 4^2 + 7^2$$

$$= 7^2 + 4^2$$

$$\left\{ \begin{array}{l} \underline{\underline{5}} = 4 \cdot 1 + 1 \\ \underline{\underline{13}} = 4 \cdot 3 + 1 \\ \underline{\underline{17}} = 4 \cdot 4 + 1 \\ \cancel{\underline{\underline{21}}} = 4 \cdot 5 + 1 \end{array} \right.$$

String
membrane



$$\textcircled{1} \quad u_{12} \quad u_{21}$$

$$\sin(\pi x) \sin(2\pi y) + \sin(2\pi x) \sin(\pi y)$$

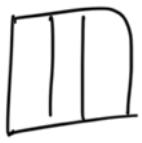


$$\textcircled{2} \quad \frac{1}{2} \sin(\pi x) \sin(2\pi y) + \sin(2\pi x) \sin(\pi y)$$



$$\textcircled{3} \quad u_{13} \quad u_{31}$$

$$\sin(\pi x) \sin(3\pi y) + \sin(3\pi x) \sin(\pi y)$$

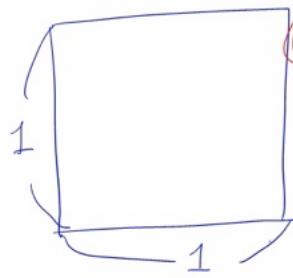


$$\textcircled{4} \quad \cos \pi x + \cos \pi y = 0$$

membrane motion

$$(m, n) \text{ pairs} \rightarrow C \pi t \sqrt{m^2 + n^2}$$

Let $a = b = 1$. (square membrane)



Q Find all pairs of (m, n) corresponding to

$$\underline{\underline{65}} = C \pi \sqrt{65}$$

$$\cos(\underline{\underline{65}} t)$$

$$\sin(\underline{\underline{65}} t)$$

$$C \pi \sqrt{m^2 + n^2} = C \pi \sqrt{65}$$

$$m^2 + n^2 = \underline{\underline{65}} \Leftarrow \underline{\underline{(2, 1) or (1, 8)}} \Leftarrow \underline{\underline{(4, 7) or (7, 4)}}$$

$$2 \sin \pi x \sin \pi y \cos \pi y + 2 \sin \pi x \cos \pi x \sin \pi y$$

$$= 2 \sin \pi x \sin \pi y (\underbrace{\cos \pi x + \cos \pi y}_{!!}) = 0$$

$$\sin \pi x \sin \pi y \cos \pi y + 2 \sin \pi x \cos \pi x \sin \pi y$$

$$= \sin \pi x \sin \pi y (\underbrace{\cos \pi y + 2 \cos \pi x}_{!!}) = 0$$

$$\sin \pi x (3 \sin \pi y - 4 \sin^3 \pi y)$$

$$+ \sin \pi y (3 \sin \pi x - 4 \sin^3 \pi x).$$

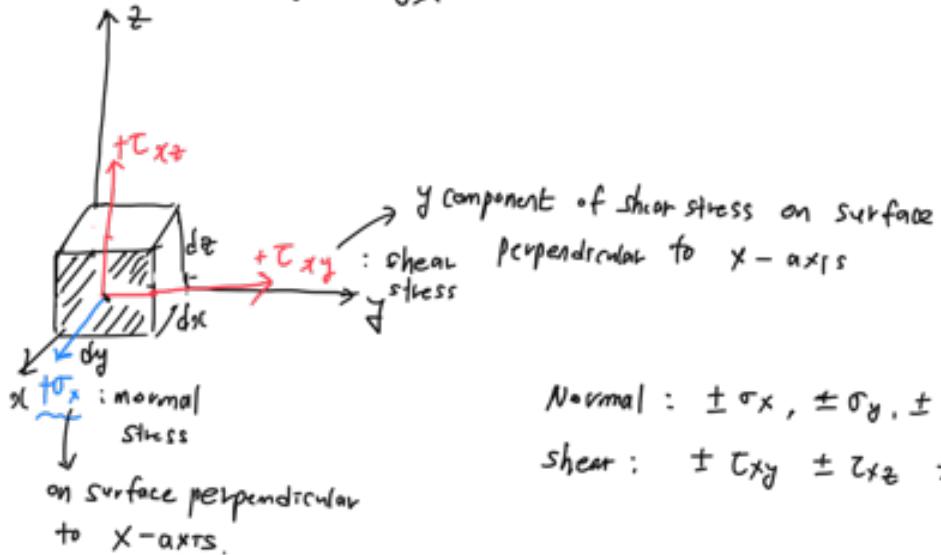
$$= 3 \sin \pi x \sin \pi y (\underbrace{6 - 4 \sin^2 \pi x - 4 \sin^2 \pi y}_{!!}) = 0$$

$$\cos \pi x + \frac{1}{2} \cos \pi y = 0$$

Wave Lecture 16 (20211104)

Elastodynamics: Dynamic theory of elasticity.

① Stress: Contact force / Unit area of an infinitesimal element.
≠ body force (e.g. gravity).



- Basic background.
- 1) Stress
- 2) Strain
- 3) Displacement
- 4) modulus E (Young's)
 G (shear)
- 5) Poisson ratio ν
- 6) Hooke's law: $\sigma_x = E \epsilon_x$
- 7) Cauchy, Lamé'

$$\left(\begin{array}{lll} \sigma_x = \sigma_{11} & \sigma_y = \sigma_{22} & \sigma_z = \sigma_{33} \\ \tau_{xy} = \sigma_{12} & \tau_{yz} = \sigma_{23} & \tau_{zx} = \sigma_{31} \\ \tau_{xz} = \sigma_{13} & \tau_{yx} = \sigma_{21} & \tau_{zy} = \sigma_{32} \end{array} \right)$$

$$\Rightarrow \begin{pmatrix} \sigma_x & \tau_{xy} & \tau_{xz} \\ \tau_{yx} & \sigma_y & \tau_{yz} \\ \tau_{zx} & \tau_{zy} & \sigma_z \end{pmatrix} = \begin{pmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{pmatrix}$$

stress tensor.

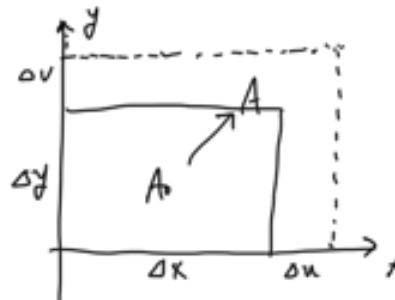
$\sigma_{ij} = \text{normal } (i=j)$
 $\text{shear } (i \neq j)$

HW) prove $\tau_{xy} = \tau_{yx}$ (State condition for equality).

$$T_z = I_z \cdot \alpha = a \tau_{xy} - b \tau_{yx}$$

$$\Rightarrow \tau_{xy} = \tau_{yx} \quad (\underbrace{\alpha = b}_{\text{Condition}})$$

② Dilatation (2D)



Dilatation
(scalar)

$$A_0 = \Delta x \Delta y$$

$$A = (\Delta x + \Delta u)(\Delta y + \Delta v) \approx \Delta x \Delta y + \Delta x \Delta v + \Delta y \Delta u$$

$$\Rightarrow A - A_0 = \Delta x \Delta v + \Delta y \Delta u$$

$$\text{Relative change : } \frac{A - A_0}{A_0} = \frac{\Delta u}{\Delta x} + \frac{\Delta v}{\Delta y}$$

$$\underline{\epsilon} = \lim_{\Delta x, \Delta y \rightarrow 0} R = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = \left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y} \right) \cdot (u, v) = \underline{\nabla} \cdot \vec{d}$$

\vec{d} displacement vector
Divergence of displacement.

Note that $\frac{\partial u}{\partial x} = \epsilon_x$ and $\frac{\partial v}{\partial y} = \epsilon_y$ (strain)

$$\frac{\partial w}{\partial z} = \epsilon_z \Rightarrow \epsilon_{2D} = \epsilon_x + \epsilon_y \Rightarrow \underline{\epsilon_{3D}} = \epsilon_x + \epsilon_y + \epsilon_z$$

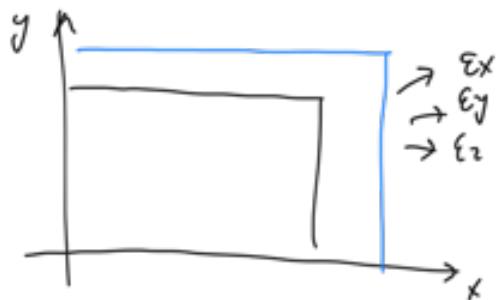
Strain : Tensor

$$\begin{pmatrix} \epsilon_x & \gamma_{xy} & \gamma_{xz} \\ \gamma_{yx} & \epsilon_y & \gamma_{yz} \\ \gamma_{zx} & \gamma_{zy} & \epsilon_z \end{pmatrix}$$

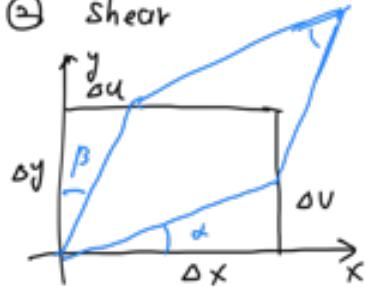
③ Strain - Displacement Relation.

$$\vec{d} = (u, v, w) = u \hat{i} + v \hat{j} + w \hat{k} = (u_1, u_2, u_3)$$

① Normal



② Shear



$$\gamma_{xy} = \alpha + \beta \approx \tan \alpha + \tan \beta$$

$$= \lim \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} = \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y}$$

$$\text{Suppose } (\)_{,i} = \frac{\partial}{\partial x_i} (\)$$

$$\Rightarrow \gamma_{xy} = u_{2,1} + u_{1,2}$$

$$\gamma_{12} = u_{1,2} + u_{2,1} \Rightarrow \gamma_{12} = \gamma_{21}$$

$$\gamma_{21} = u_{3,1} + u_{1,3} \quad (\underbrace{\gamma_{12} = \gamma_{21}}_{\gamma_{xy} = \gamma_{yx}})$$

French mathematician.

Cauchy) let $\epsilon_{ij} = \frac{1}{2}(u_{i,j} + u_{j,i}) \rightarrow \epsilon_{11} = \frac{1}{2} \cdot 2 u_{1,1} = \epsilon_x$

$$\gamma_{12} = u_{1,2} + u_{2,1} = 2 \epsilon_{12}$$

$$\begin{pmatrix} \epsilon_x & \gamma_{12} & \gamma_{13} \\ \gamma_{21} & \epsilon_y & \gamma_{23} \\ \gamma_{31} & \gamma_{32} & \epsilon_z \end{pmatrix} \Rightarrow \begin{pmatrix} \epsilon_{11} & 2\epsilon_{12} & 2\epsilon_{13} \\ 2\epsilon_{21} & \epsilon_{22} & 2\epsilon_{23} \\ 2\epsilon_{31} & 2\epsilon_{32} & \epsilon_{33} \end{pmatrix} \rightarrow \text{strain tensor.}$$

Summary : $\left. \begin{array}{l} 6 \text{ stresses} \\ 6 \text{ strains} \\ 3 \text{ displacements} \end{array} \right\} 15 \text{ unknowns}$

$$\epsilon_{ij} = \frac{1}{2}(u_{i,j} + u_{j,i}) \quad | \quad 6 \text{ Equations.}$$

9 More equations needed!

Wave Lecture 17 (20211109)

~ Previous class.

① stress \rightarrow 3 normal, 3 shear \rightarrow (6) unknowns.

② dilation \rightarrow 3 " " \rightarrow (6) "

③ relation ($\sigma \sim \varepsilon$) \rightarrow 6 relations.

$\nabla \cdot \vec{d} = \text{dilation}$ 15 unknowns!

(3) unknowns

Equation of motion | $\vec{f} = d\vec{F} = dm \cdot \vec{a} = \rho dx dy dz \cdot \frac{d^2 \vec{d}}{dt^2}$ (\vec{d} : displacement vector)

$$f = (f_x, f_y, f_z)$$

↓ ↓ ↓
1 normal " 2 shear " " "

$$\begin{aligned} & \text{① } \sigma_x + \frac{\partial \sigma_x}{\partial x} dx \\ & \text{② } \tau_{yx} + \frac{\partial \tau_{yx}}{\partial y} dy \\ & \text{③ } \tau_{zx} + \frac{\partial \tau_{zx}}{\partial z} dz \end{aligned}$$

\hookrightarrow A 면 가중가장.

From ①, ②, ③, we get.

$$f_x = \left(\sigma_x + \frac{\partial \sigma_x}{\partial x} dx - \tau_{yx} \right) dy dz + \left(\tau_{yx} + \frac{\partial \tau_{yx}}{\partial y} dy - \tau_{zx} \right) dx dz$$

$$+ \left(\tau_{zx} + \frac{\partial \tau_{zx}}{\partial z} dz - \tau_{xy} \right) dx dy$$

$$\Rightarrow f_x = \left(\frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} \right) dx dy dz$$

i) x direction.

$$f_x = \left(\frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} \right) dx dy dz = \rho dx dy dz \cdot \frac{d^2 u}{dt^2} \quad (\because \vec{d} = u, v, w)$$

$$\Rightarrow \frac{\partial \sigma_{11}}{\partial x_1} + \frac{\partial \sigma_{21}}{\partial x_2} + \frac{\partial \sigma_{31}}{\partial x_3} = \sigma_{11,1} + \sigma_{21,2} + \sigma_{31,3} = \rho \ddot{u}_1$$

ii) y direction $\Rightarrow \sigma_{12,1} + \sigma_{22,2} + \sigma_{32,3} = \rho \ddot{u}_2$

iii) z direction $\Rightarrow \sigma_{13,1} + \sigma_{23,2} + \sigma_{33,3} = \rho \ddot{u}_3$

$\sigma_{ii,j} = \rho \ddot{u}_i$

for $i=1, 2, 3$

j : summation index

Hw) Derive (ii) and (iii). for exercise!

$$\text{Cauchy : } \varepsilon_{ij} = \frac{1}{2} (u_{i,j} + u_{j,i}) \quad i,j = 1, 2, 3. \quad \begin{matrix} & 6 \text{ Equations.} \\ \rightarrow & \text{strain-displacement} \end{matrix}$$

$$\text{Navier : } \sigma_{ji,j} = \rho \ddot{u}_i \quad \text{for } i = 1, 2, 3. \quad \begin{matrix} & 3 \text{ Equations.} \\ \rightarrow & \text{stress-displacement.} \end{matrix}$$

Lame' : strain-stress via Hooke's law ($\sigma_x = E \varepsilon_x$) $\begin{matrix} <1D> \\ 6 \text{ Equations.} \end{matrix}$

$$\text{Note : } \sigma_x = \frac{E}{(1+\nu)(1-2\nu)} [\varepsilon_x(1-\nu) + (\varepsilon_y + \varepsilon_z)\nu] \quad \begin{matrix} <3D> \\ \end{matrix}$$

$$\Rightarrow \sigma_x = \frac{E}{(1+\nu)(1-2\nu)} [\varepsilon_x(1-2\nu) + (\varepsilon_x + \varepsilon_y + \varepsilon_z)\nu] \\ = \varepsilon.$$

$$= \frac{E\nu}{(1+\nu)(1-2\nu)} \varepsilon + \frac{E}{1+\nu} \varepsilon_x \quad \begin{matrix} & \text{G.} \\ & // \\ \text{Independent of direction.} & \end{matrix}$$

$$\text{and } \sigma_{xy} = \frac{E}{2(1+\nu)} \gamma_{xy}$$

Can we unify these two?

$$\varepsilon_x = \varepsilon_{11} \quad \text{let } \frac{E}{2(1+\nu)} = \mu \quad \text{and } \frac{E\nu}{(1+\nu)(1-2\nu)} = \lambda.$$

$\gamma_{xy} = 2\varepsilon_{12}$ Lame's 2nd const

Lame's 1st const

Rewriting equations,

$$\left. \begin{array}{l} \sigma_{11} = \lambda \varepsilon + 2\mu \varepsilon_{11} \\ \sigma_{22} = \lambda \varepsilon + 2\mu \varepsilon_{22} \\ \sigma_{33} = \lambda \varepsilon + 2\mu \varepsilon_{33} \end{array} \right| \quad \left. \begin{array}{l} \sigma_{12} = \mu 2\varepsilon_{12} \\ \sigma_{23} = \mu 2\varepsilon_{23} \\ \sigma_{31} = \mu 2\varepsilon_{31} \end{array} \right| \quad \left. \begin{array}{l} \sigma_{xy} \\ \parallel \\ \sigma_{xy} \\ \parallel \\ \gamma_{xy} \end{array} \right| \quad \left. \begin{array}{l} \tau_{xy} \\ \parallel \\ \tau_{xy} \\ \parallel \\ \tau_{xy} \end{array} \right| \quad \left. \begin{array}{l} \Rightarrow \sigma_{ij} = 2\mu \varepsilon_{ij} + \delta_{ij} \lambda \varepsilon \\ \text{where } \delta_{ij} \rightarrow \text{Kronecker delta. func.} \\ \delta_{ij} = \begin{cases} 0 & i \neq j \\ 1 & i = j \end{cases} \end{array} \right|$$

Since $\varepsilon = \varepsilon_{11} + \varepsilon_{22} + \varepsilon_{33} = \varepsilon_{kk}$ (ε_{kk} : Einstein summation tensor)

$$\Rightarrow \boxed{\sigma_{ij} = \lambda \varepsilon_{kk} \delta_{ij} + 2\mu \varepsilon_{ij}}$$

Lame' Einstein. Kronecker Cauchy.

Conclusion

$$\textcircled{1} \quad \varepsilon_{ij} = \frac{1}{2} (u_{i,j} + u_{j,i}) \quad i,j = 1, 2, 3 \quad \begin{matrix} & 6 \text{ strain-displacement.} \\ & \end{matrix}$$

$$\textcircled{2} \quad \sigma_{ji,j} = \rho \ddot{u}_i \quad i = 1, 2, 3 \quad \begin{matrix} & 3 \text{ stress-displacement.} \\ & \end{matrix}$$

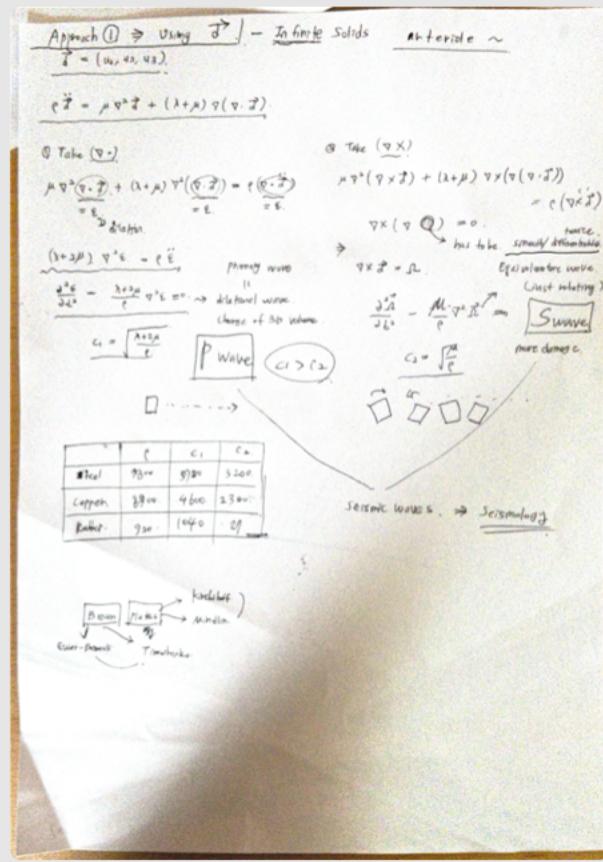
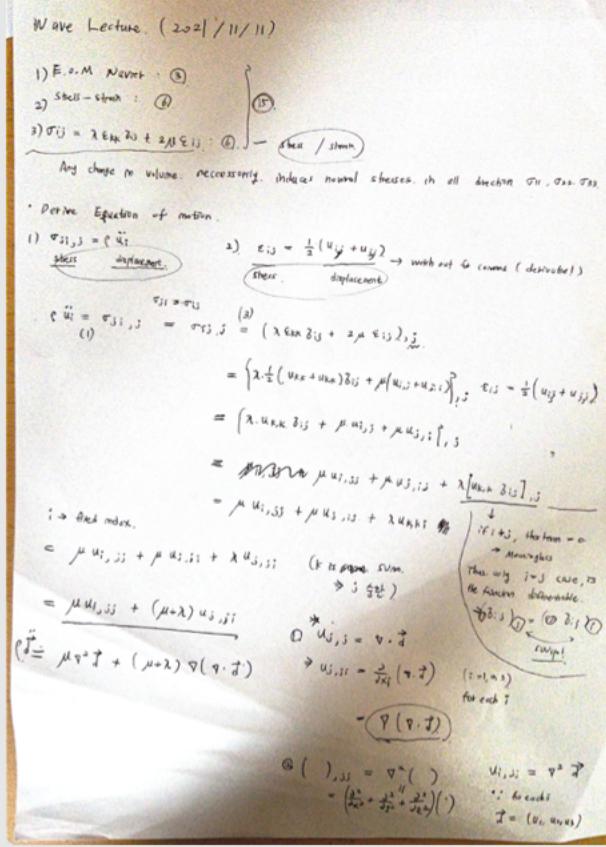
$$③ \quad \sigma_{ij} = \lambda \epsilon_{kk} \delta_{ij} + 2\mu \epsilon_{ij} \quad i,j = 1,2,3$$

6 Stress-strain

- | | | | |
|----|-----------------------------------|---|--------------|
| 1) | ϵ_{ij} ($i,j = 1,2,3$) | 6 | strain |
| 2) | σ_{ij} ($i,j = 1,2,3$) | 6 | stress |
| 3) | u_i ($i = 1,2,3$) | 3 | displacement |

Wave Lecture 18 (20211111)

스캔된 문서



$$\textcircled{1} \quad \sigma_{ji,j} = \rho \ddot{u}_i \quad \textcircled{2} \quad \varepsilon_{ij} = \frac{1}{2}(u_{i,j} + u_{j,i}) \quad \textcircled{3} \quad \sigma_{ij} = \lambda \varepsilon_{kk} \delta_{ij} + 2\mu \varepsilon_{ij}$$

$$\rho \ddot{u}_i = \sigma_{i,j,j} = (\lambda \varepsilon_{kk} \delta_{ij} + 2\mu \varepsilon_{ij}),_j = \left\{ \lambda \cdot \frac{1}{2} (u_{k,k} + u_{k,k}) \delta_{ij} + 2\mu \varepsilon_{ij} \right\},_j$$

$$= \left\{ \underbrace{\lambda u_{k,k} \delta_{ij}}_{\text{cancel}} + \mu (u_{i,j} + u_{j,i}) \right\},_j = \underbrace{\lambda u_{k,k} }_{\text{cancel}} + \mu (u_{i,j} + u_{j,i}),_j$$

$$(\lambda u_{k,k} \delta_{ij}),_j = \lambda u_{k,k,j} = \lambda u_{k,k} \quad \left(\begin{array}{l} \because \delta_{ij} = 0 \text{ if } i \neq j \Rightarrow \text{meaningless.} \\ \text{Consider only } i=j \text{ case} \Rightarrow \delta_{ij} = 1 \end{array} \right)$$

$$\Rightarrow \rho \ddot{u}_i = \lambda u_{k,k} + \mu u_{i,j,j} + \mu u_{j,i,j} = \lambda u_{j,ji} + \mu u_{i,jj} + \underbrace{\mu u_{j,ji}}_{\text{cancel}}$$

$$\Rightarrow \rho \ddot{u}_i = \mu u_{i,jj} + (\mu + \lambda) u_{j,ji} \quad \textcircled{1} \quad u_{j,j} = \nabla \cdot \vec{d} \Rightarrow u_{j,ji} = \nabla \cdot (\nabla \cdot \vec{d})$$

$$\textcircled{2} \quad u_{i,jj} = \left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} \right) u_i = \nabla^2 u_i$$

$$\Rightarrow \rho \ddot{\vec{d}} = \mu \nabla^2 \vec{d} + (\mu + \lambda) \nabla (\nabla \cdot \vec{d})$$

Note that $\nabla^2 f = \nabla \cdot (\nabla f)$ is
 conventionally used for scalar
 field f only.
~~Notation~~
 Here Laplacian ∇^2 is for
 each component u_1, u_2, u_3 .

\textcircled{1} $(\nabla \cdot \cdot)$ operator

\textcircled{2} $(\nabla \times \cdot)$ operator.

$$\rho \underbrace{\nabla \cdot \vec{d}}_{\text{cancel}} = \mu \nabla^2 \underbrace{(\nabla \cdot \vec{d})}_{\text{cancel}} + (\mu + \lambda) \nabla^2 \underbrace{(\nabla \cdot \vec{d})}_{\text{cancel}} \quad \rho \underbrace{(\nabla \times \vec{d})}_{\text{cancel}} = \mu \nabla^2 \underbrace{(\nabla \times \vec{d})}_{\text{cancel}} + (\mu + \lambda) \nabla \times \underbrace{\nabla (\nabla \cdot \vec{d})}_{\text{cancel}}$$

$$\Rightarrow \frac{\partial^2 w}{\partial t^2} - \frac{2\mu + \lambda}{\rho} \nabla^2 w = 0$$

$$\Rightarrow \frac{\partial^2 \Omega}{\partial t^2} - \frac{\mu}{\rho} \nabla^2 \Omega = 0$$

$$\underbrace{c_p}_{\text{cancel}} = \sqrt{\frac{2\mu + \lambda}{\rho}}$$

$$\underbrace{c_s}_{\text{cancel}} = \sqrt{\frac{\mu}{\rho}}$$

\rightarrow Bulk modulus

$\nabla \cdot \vec{d}$: compression : P wave



$\nabla \times \vec{d}$: spin/twist : S wave



Seismic Waves.

Note : These results are for infinitely long solids.

Wave Lecture 19 (20211116)

String/membrane

Infinite elastic solids.

Beams. (Euler - Bernoulli: \Rightarrow Timoshenko)

Plate (Kirchhoff \Rightarrow Mindlin)

⇒ Approximate theory. of elastic wave motions

\therefore Elastic wave motions related to "Vibrations" \rightarrow noise heat

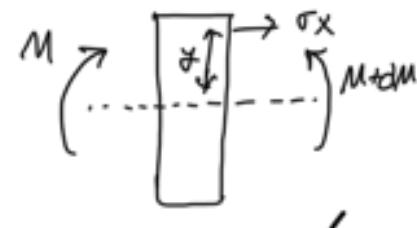
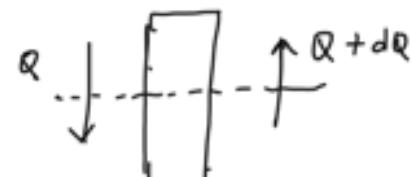
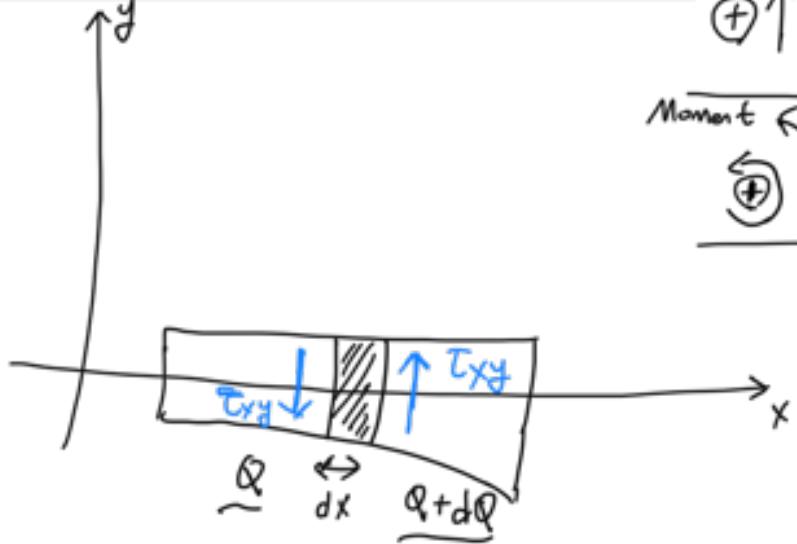
1. Euler - Bernoulli beam theory

$$Q = \int_A T_{xy} dA$$

$$\text{Moment } \leftarrow \textcircled{+} M = \int_A -r_x \cdot y \, dA$$

Effect of T_{xy} to M

will be concerned later.



* Nomenclature (명명법)

① $w(x, t)$: transverse deflection of an infinitesimal element.

② $\theta(r,t)$: rotation angle / slope of centroidal axis. (ccw : +)

③ $Q(x,t)$: shear force

$M(x,t)$: bending moment

④ ρ : density / E : Young's modulus

$$\textcircled{5} \quad A(x) : \text{cross-sectional area} \quad / \quad I(x) = \text{moment of inertia of area} = \int y^2 dA.$$

$$J(x) = \text{rotational inertia} = \int r^2 dm$$



Assumptions

Timoshenko.

② Material is elastic / isotropic / homogeneous / continuous

$$E_x = E_y = E$$

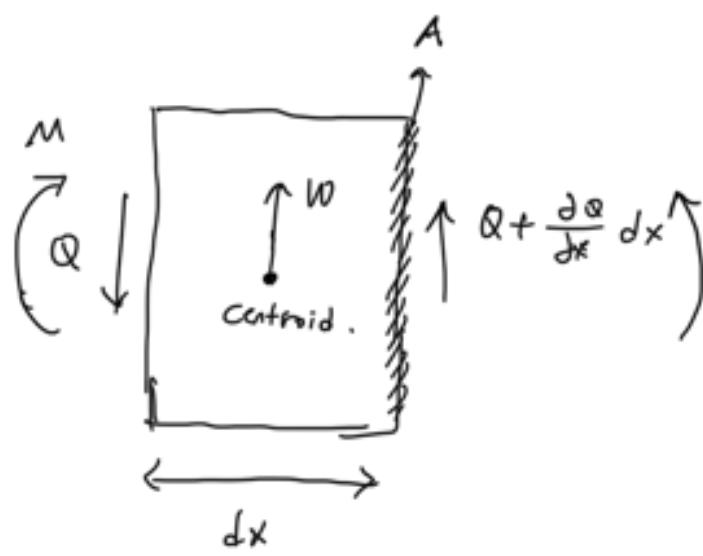
= no holes.

③ Transverse deflections are small ($w \ll 1$) \rightarrow Linearization!

- E.B.
- ④ Transverse deflections are close to purely translational motion in y direction.
(Thus, rotational inertia can be neglected)
 $J\ddot{\theta} = 0$
- ⑤ Cross sections remain plane/perpendicular to x -axis during/after deformation.
(not distorted) (Neglect shear deformation.)

Discard ④, ⑤ \Rightarrow Timoshenko Beam

Equations



$$\left. \begin{aligned} ① \quad I F_y &= d_m \frac{d^2 w}{dt^2} \\ \Rightarrow Q + \frac{d\theta}{dx} dx - Q &= \rho A dx \frac{d^2 w}{dt^2} \\ \Rightarrow \frac{dQ}{dx} &= \rho A \frac{d^2 w}{dt^2} \end{aligned} \right\}$$

$$\left. \begin{aligned} ② \quad I M &= J \frac{d^2 \theta}{dt^2} = 0. \quad (\text{for E.B. beams}) \\ \Rightarrow M + \frac{dM}{dx} dx - M + \left(Q + \frac{dQ}{dx} dx\right) \frac{dx}{2} + Q \cdot \frac{dx}{2} &= 0 \\ \Rightarrow \frac{dM}{dx} &= -Q \quad (\because (dx)^2 \ll 1) \end{aligned} \right\}$$

Recall that $M = E \cdot I \frac{d^2 w}{dx^2}$

$$\Rightarrow \rho A \frac{d^2 w}{dt^2} = \frac{dQ}{dx} = -\frac{d^2 M}{dx^2} = -\frac{d^2}{dx^2} \left(E \cdot I \frac{d^2 w}{dx^2} \right).$$

$$\Rightarrow \underline{\underline{\rho A \frac{d^2 w}{dt^2} + \frac{d^2}{dx^2} \left(E \cdot I \cdot \frac{d^2 w}{dx^2} \right)}} = 0 \quad (\text{Euler-Bernoulli beam equation.})$$

Boundary conditions. (w, θ, Q, M) at $x=0$:

① Simply supported. (ss) $w=0, M=0$

② Free end. $w=0, M=0$

② Free (F)  $\alpha = 0, M = 0$

③ Clamped (C)  $\omega = 0, \theta = 0$

choose. $\binom{4}{2} = 6 \rightarrow 4 \text{ B.C.s} / 1 \text{ beam}$

④ Sliding (S)  $\theta = 0, \alpha = 0$

Wave Lecture 20 (20211118)

$$\boxed{\text{Waves in Solids (E-B beam)}} : \frac{\partial^2 w}{\partial t^2} + \underbrace{\frac{EI}{\rho A}}_{\text{constant for prismatic beam.}} \frac{\partial^4 w}{\partial x^4} = 0 \quad \checkmark$$

For prismatic beam)

$$\text{B.C.s} : \begin{cases} S.S. : w=0, M=0 \rightarrow w=0, w''=0 \\ F : Q=0, M=0 \rightarrow w'''=0, w''=0 \\ C : w=0, \theta=0 \rightarrow w=0, w'=0 \\ S : \theta=0, Q=0 \rightarrow w'=0, w'''=0 \end{cases} \quad \begin{aligned} M &= EI w'' \\ Q &= -\frac{\partial M}{\partial x} = -EI w''' \end{aligned}$$

Note that for acoustic perturbation,

$$1) \frac{\partial^2 p'}{\partial t^2} - c^2 \frac{\partial^2 p'}{\partial x^2} = 0 \Leftrightarrow 2) \frac{\partial^2 w}{\partial t^2} + \frac{EI}{\rho A} \frac{\partial^4 w}{\partial x^4} = 0$$

$$1) p' = A e^{j(kx - \omega t)} \Rightarrow A e^{j(kx - \omega t)} \left\{ (-j\omega)^2 - c^2(jk)^2 \right\} = 0 \Rightarrow \omega = ck \Rightarrow Cp = c$$

$$2) w = W e^{j(kx - \omega t)} \Rightarrow (-j\omega)^2 + \frac{EI}{\rho A} (jk)^4 = 0 \Rightarrow \underbrace{w = \sqrt{\frac{EI}{\rho A}} k^2}_{\text{constant in all frequencies } (\omega)}$$

< Dispersion Relation in E.B. beam >

$$\begin{array}{l} \omega \uparrow : c_B \uparrow \xrightarrow{\text{MV}} \\ \omega \downarrow : c_B \downarrow \xrightarrow{\sim} \end{array} \left[\begin{array}{l} \text{phase speed of elastic waves in E-B is} \\ \text{depending on frequency.} \end{array} \right] \Rightarrow c_B = \sqrt[4]{\frac{EI}{\rho A}} \cdot \sqrt{\omega} \quad c_B \sim \sqrt{\omega}$$

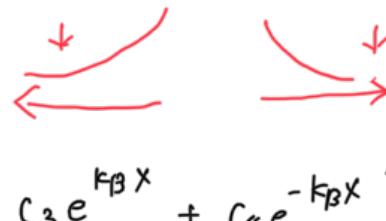
$$k^4 = \frac{\rho A}{EI} \omega^2 \Rightarrow k = \pm k_B, \pm jk_B \Rightarrow w(x,t) = \left\{ C_1 e^{jk_B x} + C_2 e^{-jk_B x} + C_3 e^{-k_B x} + C_4 e^{k_B x} \right\} e^{-j\omega t}$$

\$k_B\$ is called "Bending wavenumber" General solution

* General solution.

$$w(x,t) = \left\{ C_1 e^{jk_B x} + C_2 e^{-jk_B x} + \frac{C_3 e^{k_B x} + C_4 e^{-k_B x}}{\text{Evanescent wave}} \right\} e^{-j\omega t}$$

Travelling (propagating) waves



No exponentially "growing" allowed

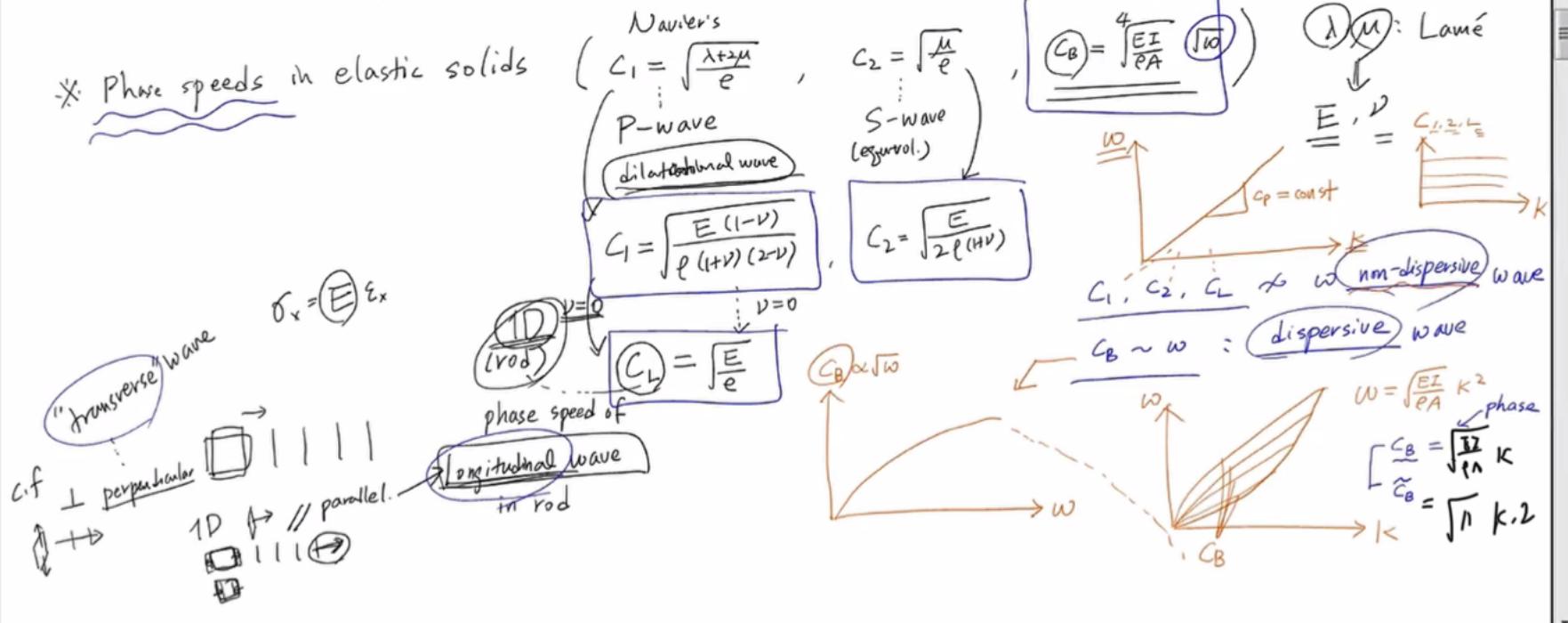
■ Recall speeds in elastic solids

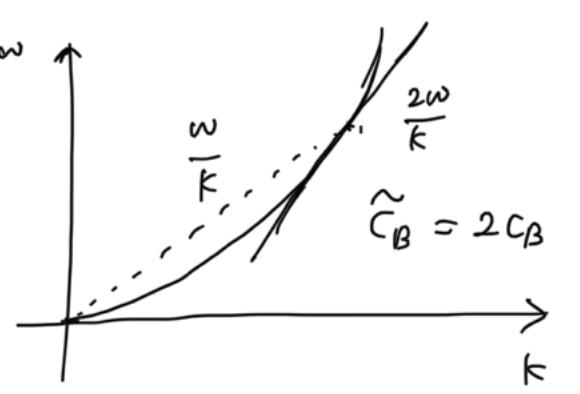
$$c_1 = \sqrt{\frac{\lambda + 2\mu}{\rho}}, \quad c_2 = \sqrt{\frac{\mu}{\rho}}, \quad c_B = \sqrt[4]{\frac{EI}{\rho A}} \omega$$

Express in \$E, v\$

P wave	S wave
$c_1 = \sqrt{\frac{E(1-v)}{\rho(1+v)(2-v)}}$	$c_2 = \sqrt{\frac{E}{2\rho(1+v)}}$

* Phase speeds in elastic solids





Ex)  \Rightarrow 

$\therefore C_B \sim w$) \Rightarrow waveform
 $\tilde{C}_B \sim 2w$, not preserved

↓

Dispersive

- * Prismatic beam of length "L"



$$G.E. \frac{\partial^2 w}{\partial t^2} + \frac{EI}{PA} \frac{\partial^4 w}{\partial x^4} = 0 \Rightarrow \begin{cases} C_1 e^{j\omega t} + C_2 e^{-j\omega t} + C_3 e^{jk_B x} + C_4 e^{-jk_B x} \\ b_1 \cos k_B x + b_2 \sin k_B x + b_3 \cosh k_B x \\ + b_4 \sinh k_B x \end{cases}$$

$$\text{B.C. } w(0,t) = 0 \quad w'(0,t) = 0$$

$$\omega(L, t) = 0 \quad \omega'(L, t) = 0$$

$$\Rightarrow w(0) = b_1 + b_3 = 0$$

$$\omega'(.) = k_{p,b_2} + k_{i_3,b_4} = 0$$

$$\omega(\zeta) = \overbrace{\hspace{10em}}^{\text{---}}$$

$$\omega'(t) = \text{wavy line} \equiv 0$$

$$\Rightarrow \begin{pmatrix} 1 & 0 & 1 & 0 \\ 0 & 1 & 0 & 1 \\ \cos k_B L & \sin k_B L & \cos h k_B L & \sin h k_B L \\ -\sin k_B L & \cos k_B L & \sin h k_B L & \cos h k_B L \end{pmatrix} \begin{pmatrix} b_1 \\ b_2 \\ b_3 \\ b_4 \end{pmatrix} = \vec{0}$$

Since $b_1 = b_2 = b_3 = b_4 = 0$ is not considered, $\text{let } E(A) = 0$

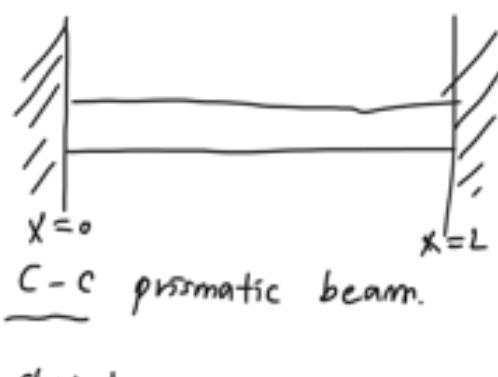
$$\det(A) = \left\{ (\cosh^2 k_B L - \sinh^2 k_B L) + \sin k_B L \sinh k_B L - \cos k_B L \cosh k_B L \right\}. 1$$

$$+ \int (\cos^2 k_0 L + \sin^2 k_0 L - \sin k_0 L \sinh k_0 L - \cos k_0 L \cosh k_0 L) \cdot 1 = 0,$$

$$\Rightarrow 2 - 2 \cos k_B L \cosh k_B L = 0 \quad \Rightarrow \quad \boxed{\cos k_B L \cosh k_B L = 1}$$

Wave Lecture 21 (20211123)

Waves in E-B beam.



$$\cos k_B L \cosh k_B L = 1$$

where $k_B = \sqrt{\frac{pA}{EI}} \sqrt{\omega}$

$$\Rightarrow k_B L = 4.93 \dots$$

$$7.85 \dots$$

$$10.99 \dots$$

$$14.13 \dots$$

From previous.

Equations of motion /

$$b_1 + b_3 = 0, \quad b_2 + b_4 = 0$$

$$b_1 (\cos k_B L - \cosh k_B L) + b_2 (\sin k_B L - \sinh k_B L) = 0$$

$$\Rightarrow b_3 = -b_1, \quad b_4 = -b_2, \quad \left. \begin{array}{l} b_2 = \frac{\cos k_B L - \cosh k_B L}{\sin k_B L - \sinh k_B L} b_1 \\ \hline \end{array} \right\} \rightarrow \sigma \rightarrow \sigma_n$$

$$\Rightarrow W(x,t) = b_1 \left[\cos k_B L - \sigma \sin k_B L - \cosh k_B L + \sigma \sinh k_B L \right] e^{-j\omega t}$$

$\downarrow \quad \downarrow \quad \downarrow \quad \downarrow \quad \downarrow$
 $b_{1,n} \quad k_{B,n} \quad k_{B,n} \quad k_{D,n} \quad k_{D,n}$

$$\Rightarrow w(x,t) = \sum_{n=1}^{\infty} w_n(x,t)$$

"Temporal" Eigenfrequency

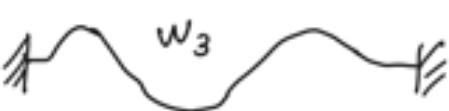
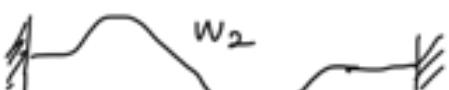
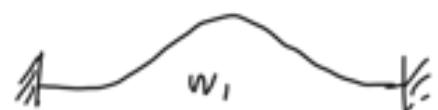
$$f_1 = \frac{4.93^2}{2\pi} \sqrt{\frac{EI}{pA}}$$

$$f_2 = \frac{7.85^2}{2\pi} \sqrt{\frac{EI}{pA}}$$

$$f_3 = \frac{10.99^2}{2\pi} \sqrt{\frac{EI}{pA}}$$

:
geometric features
material properties $\Rightarrow f$

"Spectral" mode shape



string (1D) \neq Beam (1D).

HW) Compare eigenfrequencies of string & beam, for same length

$$h=1 \rightarrow f_{beam} = \text{ (1/1)} \quad f_{string} = \frac{1}{2L} \cdot c = \frac{1}{2L} \sqrt{T/\mu}$$

Questions! for E-B beams.



No upper bound $\lim_{\omega \rightarrow \infty} c_B = \infty ?$

• Limitation of E-B beam theory

From the assumptions of

- ✓ 4) rotational inertia neglected
- ✓ 5) shear deformation neglected. $J\ddot{\theta} = 0$

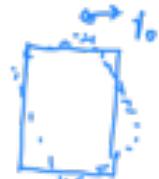
Timoshenko theory

$$\mathcal{I} F_y = \rho A \frac{d}{dx} \frac{d^2 w}{dt^2} = Q + \frac{dQ}{dx} - \alpha \Rightarrow \frac{dQ}{dx} = \rho A \frac{d^2 w}{dt^2} \quad (1)$$

$$\mathcal{I} M = \frac{dM}{dx} dx + Q dx = \underbrace{\rho I dx}_{= J} \frac{d^2 \psi}{dt^2} \quad \begin{cases} \psi : \text{total angle} / \gamma_0 = \text{shear angle} (=0 \text{ for E.B. beam}) \\ \psi = \frac{dw}{dx} - \gamma_0 \end{cases} \quad (2)$$

$$Q = \int_A t_{xy} dA = G \int_A \gamma_{xy} dA = k G A \gamma_0$$

$$\Rightarrow Q = k G A (\frac{dw}{dx} - \psi) \quad (5)$$



correcting factor $\begin{cases} k(\text{rectangular}) : \frac{10(1+\nu)}{12+11\nu} \\ k(\text{circular}) : \frac{6(1+\nu)}{7+6\nu} \end{cases}$

$$(1) \frac{dQ}{dx} = \rho A \frac{d^2 w}{dt^2}$$

$$(1), (5) \frac{d}{dx} \left(k G A (\frac{dw}{dx} - \psi) \right) = \rho A \frac{d^2 w}{dt^2} \quad (1)$$

$$(2) \frac{dM}{dx} + Q = \rho I \frac{d^2 \psi}{dt^2}$$

$$(2), (3), (5) \frac{d}{dx} \left(EI \frac{d\psi}{dx} \right) + k G A (\frac{dw}{dx} - \psi) = \rho I \frac{d^2 \psi}{dt^2} \quad (2)$$

$$(3) M = EI \frac{d\psi}{dx}$$

"Timoshenko" beam equation (2 vars., 2 eqns.)

$$(4) \psi = \frac{dw}{dx} - \gamma_0$$

HW) $\textcircled{1}$ Set $\rho I \frac{d^2 \psi}{dt^2} \rightarrow 0$ derive E.B. beam.
 $\textcircled{2}$ Set $\gamma_0 \rightarrow 0$

Prismatic Timoshenko beam theory ($EI = \text{const.}, A = \text{const.}$)

$$\textcircled{1} \underbrace{\frac{d\psi}{dx}}_{= \frac{d^2 w}{dx^2}} = \frac{d^2 w}{dx^2} - \frac{1}{kG} \frac{d^2 w}{dt^2}$$

$$\textcircled{2} EI \frac{d^2 \psi}{dx^2} + k G A \left(\frac{dw}{dx} - \psi \right) = \rho I \frac{d^2 \psi}{dt^2}$$

$$\Rightarrow EI \frac{d^3 \psi}{dx^3} + k G A \left(\frac{d^2 w}{dx^2} - \frac{d\psi}{dx} \right) = \rho I \frac{d}{dx} \frac{d^2 \psi}{dt^2}$$

$\Rightarrow \psi$ w/ $\textcircled{1}$ & $\textcircled{2}$ \rightarrow Calculations ...

$$\Rightarrow \underbrace{\frac{EI}{\rho A} \frac{d^4 w}{dx^4} + \frac{d^2 w}{dt^2}}_{\text{E.B. beam}} - \underbrace{\frac{I}{A} \left(1 + \frac{E}{GK} \right) \frac{d^4 w}{dx^2 dt^2}}_{\text{Rotational inertia}} + \underbrace{\frac{\rho I}{kAG} \frac{d^4 w}{dt^4}}_{\text{Shear deformation.}} = 0$$

↑
Rotational inertia

↑
Shear deformation.

Q) Which is more important?

Dispersion relation $w = A e^{j(\gamma x - \omega t)}$

$$\frac{EI}{\rho A} \gamma^4 - \omega^2 - \frac{J}{A} \left(1 + \frac{E}{GK}\right) \gamma^2 \omega^2 + \frac{\rho I}{KA G} \omega^4 = 0$$

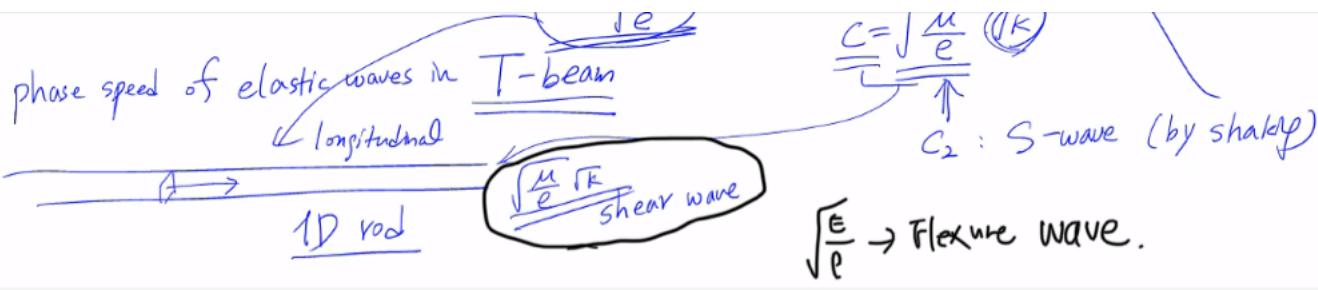
$c_B \sim \sqrt{\omega}$ (Using $\omega = c_f$)

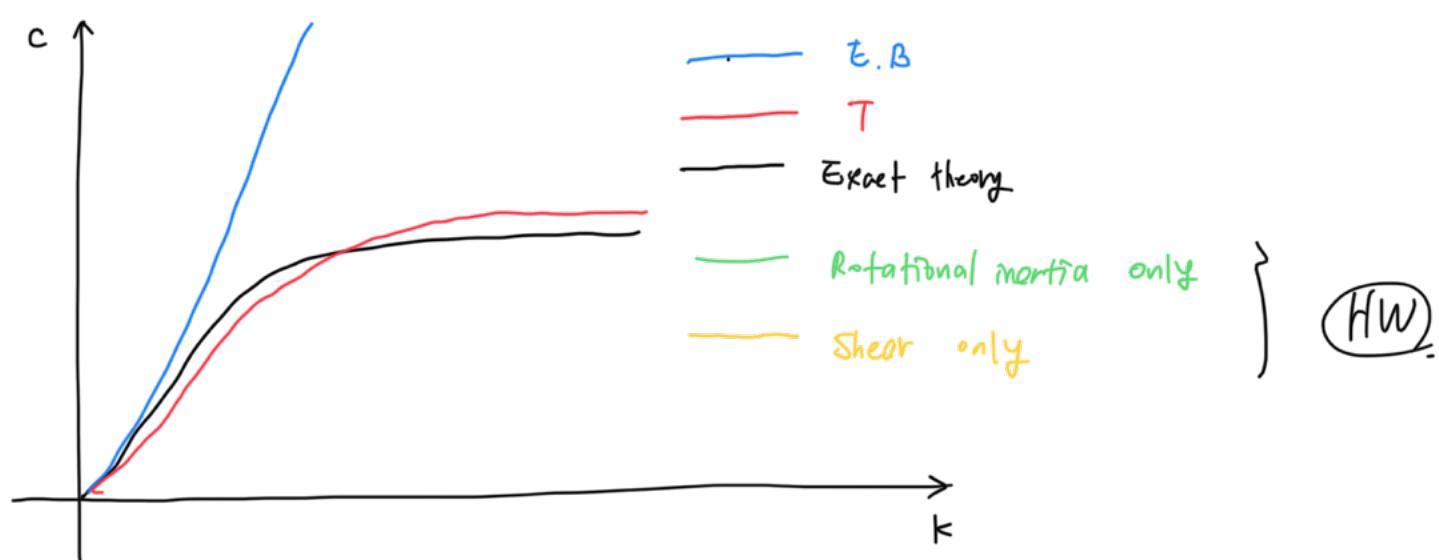
Tedious derivation
(math)

$$\Rightarrow \bar{c}^4 - \left(1 + \frac{GK}{E}\right) \bar{c}^2 + \frac{GK}{E} = 0 \quad \left(\bar{c} = \frac{c}{c_L}, \quad c_L = \sqrt{\frac{E}{\rho}} \right)$$

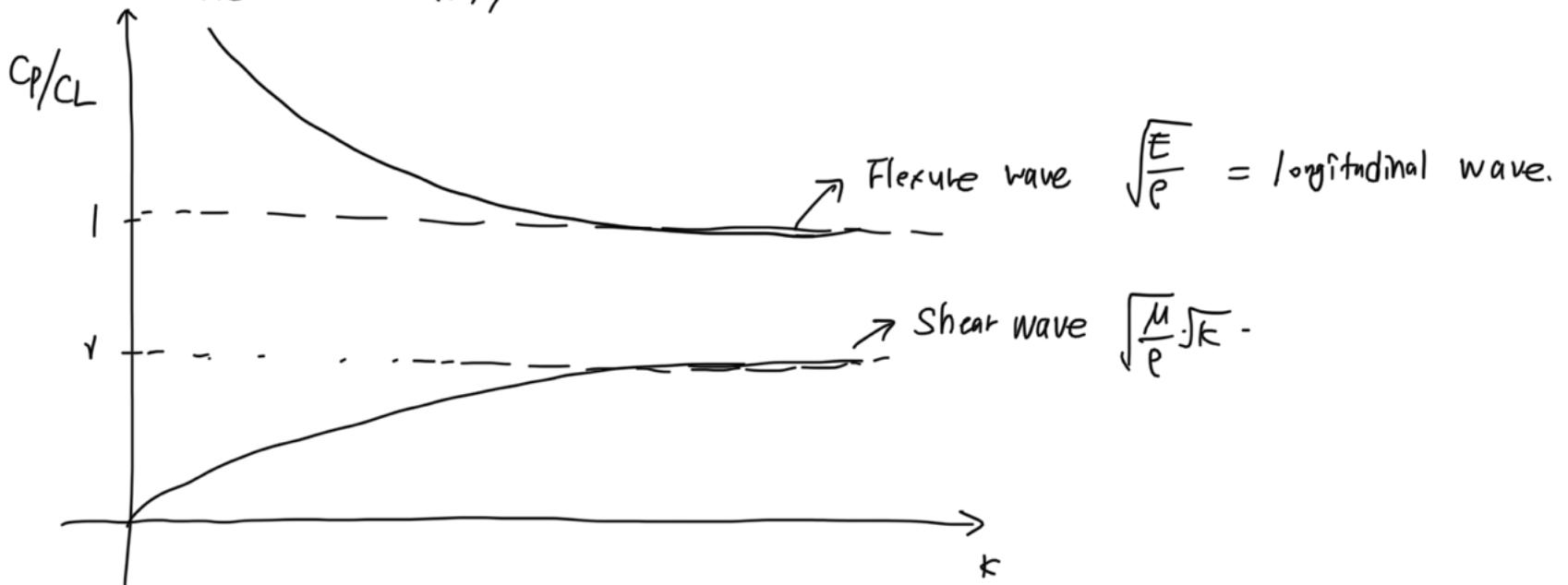
$$\Rightarrow \bar{c} = 1 \quad \text{or} \quad \bar{c} = \sqrt{\frac{GK}{E}} \quad \Rightarrow \quad c = c_L \quad \text{or} \quad c = \sqrt{\frac{GK}{E}} \sqrt{\frac{E}{\rho}} = \sqrt{\frac{GK}{\rho}},$$

$\parallel \frac{E/\rho}{}$.





< Timoshenko Beam >



< Rayleigh Beam > : only considers rotational inertia (not shear strain)

$$\underbrace{1) \rho I \frac{\partial^2 \psi}{\partial t^2}}_{1)} \quad \underbrace{2) \psi = \frac{\partial w}{\partial x} - v_0 = \frac{\partial w}{\partial x}}_{2)}$$

$$① - \frac{\partial}{\partial x} ② \Rightarrow \frac{\partial^2}{\partial x^2} \left(EI \frac{\partial^2 w}{\partial x^2} \right) + \rho A \frac{\partial^2 w}{\partial t^2} - \frac{\partial}{\partial x} \left(\rho I \frac{\partial^2}{\partial t^2} \frac{\partial w}{\partial x} \right) = 0$$

For prismatic Rayleigh beam, EI , ρA , ρI are constants.

$$\Rightarrow \underbrace{EI \frac{\partial^4 w}{\partial x^4} - \rho I \frac{\partial^4 w}{\partial x^2 \partial t^2} + \rho A \frac{\partial^2 w}{\partial t^2}}_{1)} = 0 \rightarrow w = D e^{j(kx - \omega t)} \rightarrow \text{See/ue!}$$

$$\Rightarrow \tilde{w}^2 = \frac{\tilde{k}^4}{1 + \tilde{k}^2} \quad \left(\text{where } \tilde{w} = \frac{w \cdot \sqrt{I/A}}{\sqrt{E/\rho}} \quad \tilde{k} = \sqrt{I/A} \cdot k \right)$$

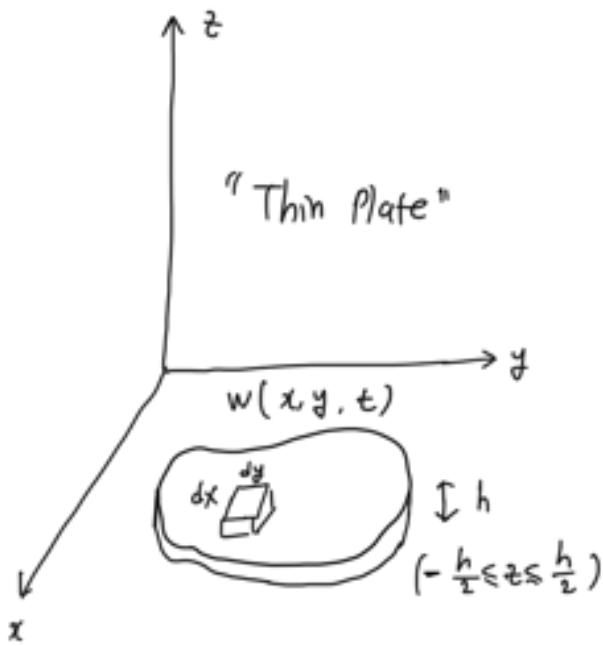
Wave Lecture 22 (20211125)

Waves in Plates

Kirchhoff plate
Mindlin plate.

- ① Rotational inertia
- ② Shear deformation.

Euler-B
Timoshenko

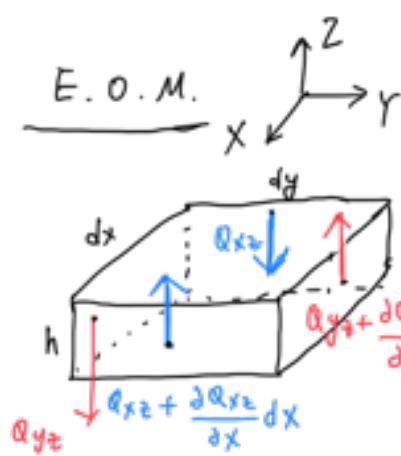


Assumptions

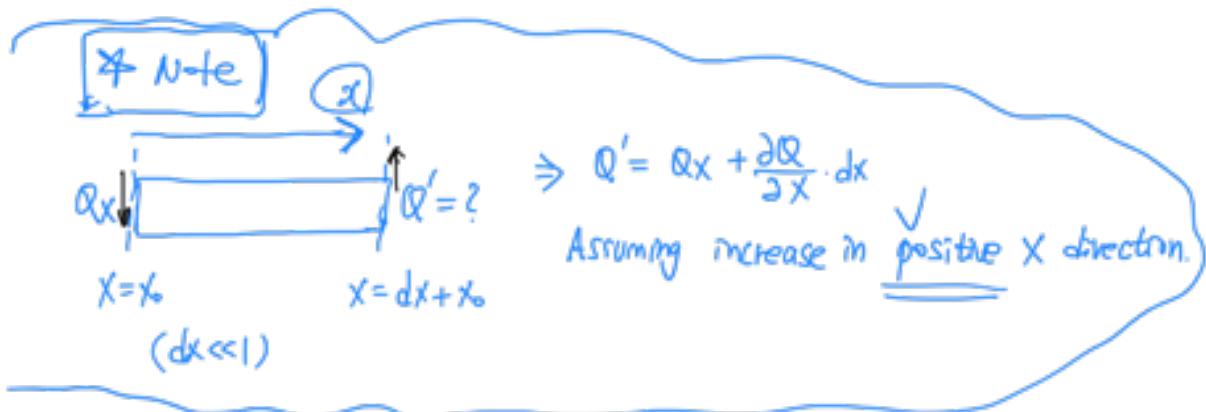
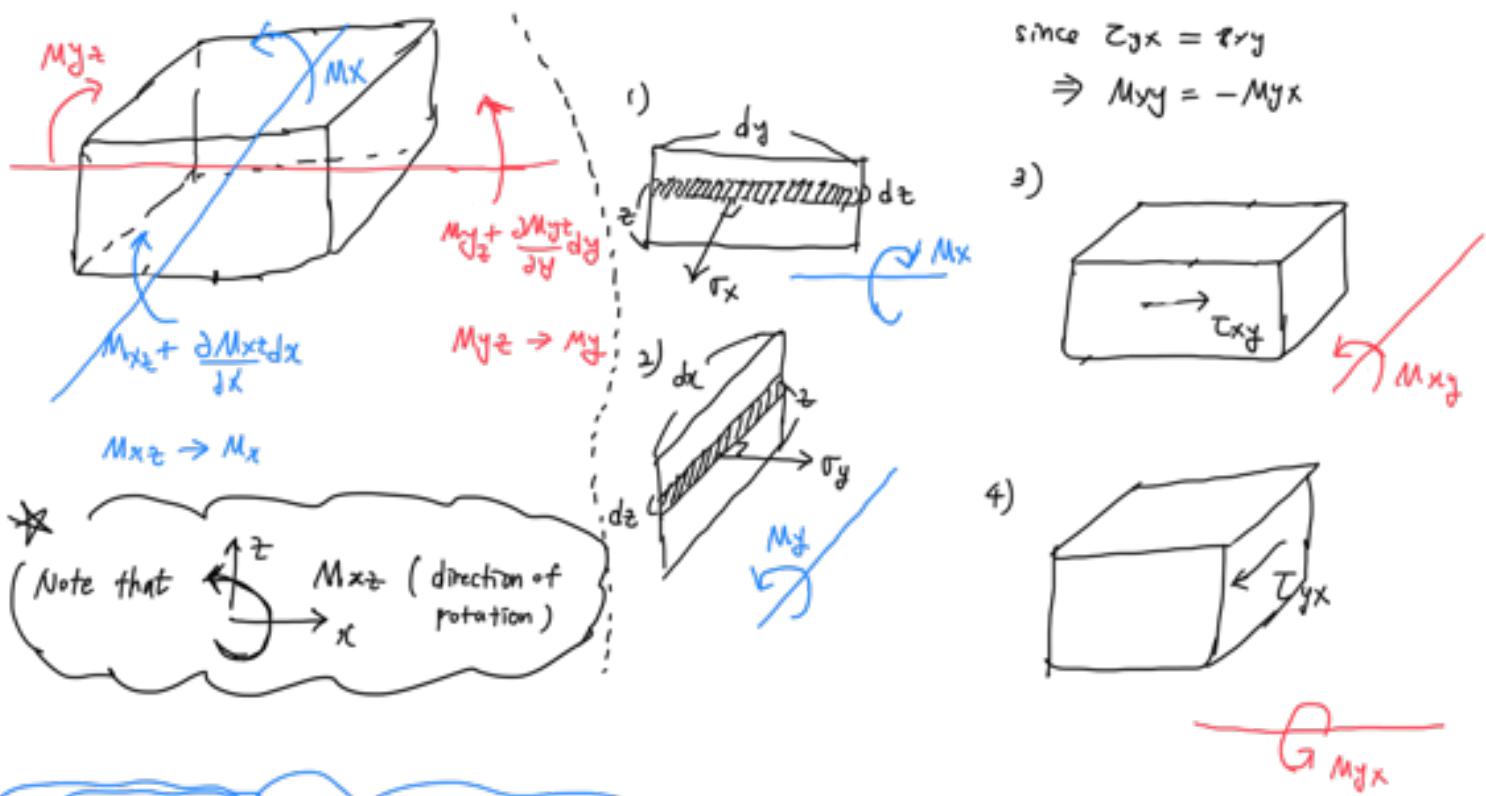
- 1) Plate has a "flat" mid-plane denoted as "xy plane"
- 2) Material : Elastic, Isotropic, Homogeneous, and Continuous.
- 3) Transverse deflection $w(x, y, t)$ small ($w \ll 1$)
 \Rightarrow Linear theory.

Only for Kirchhoff

- 4) Deflection due to a purely translational motion in z -axis (rotational inertia \times)
- 5) Line elements perpendicular to the mid-plane remain straight & perpendicular to the mid-plane during / after deformation.
- 6) Line elements do not change "Length" ($\epsilon_{zz} = 0$)



Internal bending moment per length	Internal twisting moment per length.
$M_x dy = - \int_{-\frac{h}{2}}^{\frac{h}{2}} z \sigma_x dy dz$	$M_{xy} = - \int_{-\frac{h}{2}}^{\frac{h}{2}} \tau_{xy} \pm dz$
$M_y dx = - \int_{-\frac{h}{2}}^{\frac{h}{2}} z \sigma_y dx dz$	$M_{yx} = + \int_{-\frac{h}{2}}^{\frac{h}{2}} \tau_{yx} \pm dz$



① Net force (z)

$$\underbrace{\left(Q_x + \frac{\partial Q_x}{\partial x} dx - Q_x \right) dy + \left(Q_y + \frac{\partial Q_y}{\partial y} dy - Q_y \right) dx}_{\text{per unit length}} = \rho dx dy h \frac{\partial^2 w}{\partial t^2}$$

$$\Rightarrow \underbrace{\frac{\partial Q_x}{\partial x} + \frac{\partial Q_y}{\partial y}}_{\text{per unit length}} = \rho h \frac{\partial^2 w}{\partial t^2} - ①$$

② Net moment

$$\begin{aligned} & \cancel{\left(M_y + \frac{\partial M_y}{\partial y} dy - M_y \right) dx} + \left(M_{xy} + \frac{\partial M_{xy}}{\partial x} dx - M_{xy} \right) dy \\ & \quad + \left(Q_y + \frac{\partial Q_y}{\partial y} dy + Q_y \right) \frac{dx}{2} dy = J_x = 0. \end{aligned}$$

$$\begin{array}{c} \cancel{M_y} \\ \downarrow \quad \uparrow Q_y + dQ_y \\ \hline \end{array} \Rightarrow \underbrace{\frac{\partial M_y}{\partial y} + \frac{\partial M_{xy}}{\partial x} + Q_y}_{\text{per unit length}} = 0 - ②$$

③ Net moment

$$\begin{aligned} & - \left(M_x + \frac{\partial M_x}{\partial x} - M_x \right) dy + \left(M_{yx} + \frac{\partial M_{yx}}{\partial y} dy - M_{yx} \right) dx \\ & \quad - \left(Q_x + \frac{\partial Q_x}{\partial x} dx + Q_x \right) \frac{1}{2} dy \cdot dx = J_y = 0 \end{aligned}$$

$$\Rightarrow \underbrace{-\frac{\partial M_x}{\partial x} + \frac{\partial M_{yx}}{\partial y} - Q_x}_{\text{per unit length}} = 0 - ③$$

③ \rightarrow ① \Rightarrow Q equation
 ② \rightarrow ①

$$\Rightarrow \frac{\partial}{\partial x} \left(-\frac{\partial M_x}{\partial x} + \frac{\partial M_{xy}}{\partial y} \right) + \frac{\partial}{\partial y} \left(-\frac{\partial M_y}{\partial y} - \frac{\partial M_{xy}}{\partial x} \right) = \rho h \frac{\partial^2 w}{\partial t^2}$$

$$\Rightarrow -\frac{\partial^2 M_x}{\partial x^2} - \frac{\partial^2 M_y}{\partial y^2} - 2 \frac{\partial^2 M_{xy}}{\partial x \partial y} = \rho h \frac{\partial^2 w}{\partial t^2} \quad (\because M_{xy} = -M_{yx})$$

Note : Moment - Curvature Constitutive Eqs.

Just before, we obtained

$$-\frac{\partial^2 M_x}{\partial x^2} - \frac{\partial^2 M_y}{\partial y^2} - 2 \frac{\partial^2 M_{xy}}{\partial x \partial y} = \rho h \frac{\partial^2 w}{\partial t^2}$$

* moment - curvature constitute equations

$$M_x = \int_{-\frac{h}{2}}^{\frac{h}{2}} z \sigma_x dz$$

$$\sigma_x = \frac{E}{1-\nu} (\varepsilon_x + \varepsilon_y \nu)$$

under plane stress condition

$$M_y = - \int_{-\frac{h}{2}}^{\frac{h}{2}} z \sigma_y dz \quad " \quad \sigma_y = \frac{E}{1-\nu} (\varepsilon_y + \varepsilon_x \nu)$$

$$M_{xy} = - \int_{-\frac{h}{2}}^{\frac{h}{2}} z \tau_{xy} dz \quad " \quad \tau_{xy} = \frac{E}{2(1+\nu)} \gamma_{xy}$$

$$\sigma = \begin{pmatrix} \sigma_x & \sigma_{xy} & 0 \\ \sigma_{yx} & \sigma_y & 0 \\ 0 & 0 & \sigma_z \end{pmatrix}$$

* stress vector in zero across a particular plane, π_{xy} -plane.
 (in our case)

relations btwn

here, $\varepsilon_x \equiv$

$$M_{x,y,xy} \sim w \Leftarrow$$

$$\gamma_{xy} \simeq -2z \frac{\partial^2 w}{\partial x \partial y}$$

$$\text{Then, } M_x = \int_{-\frac{h}{2}}^{\frac{h}{2}} z \frac{E}{1-\nu} \left(\frac{\partial^2 w}{\partial x^2} + \nu \frac{\partial^2 w}{\partial y^2} \right) dz$$

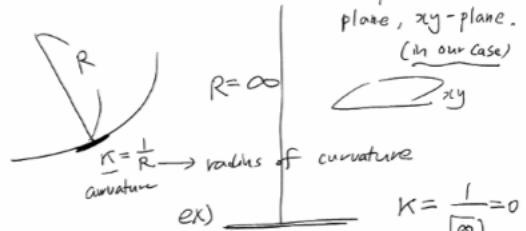
$$= \frac{E}{1-\nu} \left[\frac{2^2 w}{2x^2} \int_{-\frac{h}{2}}^{\frac{h}{2}} z^2 dz + \nu \frac{2^2 w}{2y^2} \int_{-\frac{h}{2}}^{\frac{h}{2}} z^2 dz \right]$$

$$\stackrel{(2)}{=} \int_0^{\frac{h}{2}} z^2 dz = \frac{2}{3} z^3 \Big|_0^{\frac{h}{2}} = \frac{2}{24} h^3 = \frac{h^3}{12}$$

$$= \frac{E h^3}{12(1-\nu)} \left(\frac{\partial^2 w}{\partial x^2} + \nu \frac{\partial^2 w}{\partial y^2} \right)$$

$$\text{Let } D = \frac{E h^3}{12(1-\nu)}$$

be "flexural stiffness"



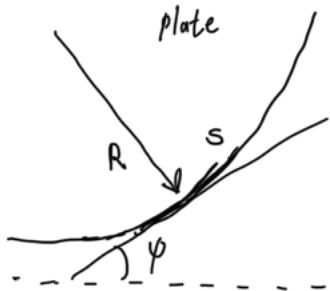
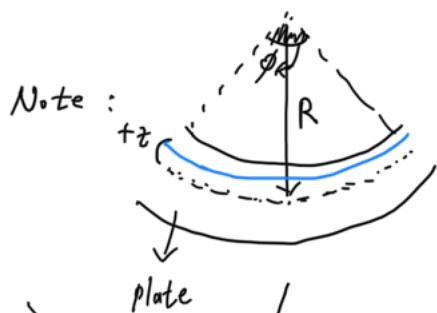
$$M_x = D \left(\frac{\partial^2 w}{\partial x^2} + \nu \frac{\partial^2 w}{\partial y^2} \right) \quad M_{xy} = (1-\nu) D \frac{\partial^2 w}{\partial x \partial y}$$

$$M_y = D \left(\nu \frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} \right)$$

$\frac{\partial^2 w}{\partial y^2}$
 ν
 B
 $\frac{\partial^2 w}{\partial x^2}$
 ν
 $x\nu = (1-\nu) D \frac{\partial^2 w}{\partial x \partial y}$
 Kirchhoff plate equation
 $\boxed{-D \nabla^4 w = \rho h \frac{\partial^2 w}{\partial t^2}}$

Let $D = \frac{E h^3}{12(1-\nu^2)}$ be "flexural stiffness"
 EoM: $-D \left(\frac{\partial^4}{\partial x^4} + \frac{\partial^4}{\partial y^4} + 2 \frac{\partial^4}{\partial x^2 \partial y^2} \right) w = \rho h \frac{\partial^2 w}{\partial t^2}$
 $\left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right)^2 w = \rho h \frac{\partial^2 w}{\partial t^2}$
 biharmonic operator
 $\boxed{\nabla^4}$

HW: Derive { $\epsilon_x, \epsilon_y, \gamma_{xy} \sim w$ relation }
 by yourself.



$$\epsilon_x = \frac{\Delta x}{L} = \frac{(R-z)\phi - R\phi}{R\phi} = -\frac{z}{R_x} \quad R = R_x$$

$$\epsilon_y = \frac{\Delta y}{L} = \frac{(R-z)\phi - R\phi}{R\phi} = -\frac{z}{R_y} \quad R = R_y.$$

$$d\psi \cdot R = ds \Rightarrow \underbrace{\frac{1}{R}}_{\tan \phi = \frac{dw}{dx}} = \frac{d\psi}{ds}$$

$$\frac{\tan \phi = \frac{dw}{dx}}{ds = \sqrt{1 + \left(\frac{dw}{dx}\right)^2} dx} \Rightarrow \sec^2 \phi \frac{d\psi}{ds} = \frac{d^2 w}{dx^2}$$

$$\Rightarrow \frac{d\psi}{ds} = \frac{d\psi}{dx} \frac{dx}{ds} = \frac{d^2 w}{dx^2} \cdot \frac{1}{\sqrt{1 + \left(\frac{dw}{dx}\right)^2}}$$

$$\Rightarrow \frac{d\psi}{ds} = f_{Rx} = \frac{1}{R_x} = \frac{d^2 w}{dx^2} \cdot \frac{1}{\sqrt{1 + \left(\frac{dw}{dx}\right)^2}}$$

$$= \frac{d^2 w}{dx^2} \cdot \underbrace{\frac{1}{\left[1 + \left(\frac{dw}{dx}\right)^2\right]^{3/2}}}_{\sim}$$

Thus, for ($\theta \ll 1 \Leftrightarrow dw/dx \ll 1$) case $\Rightarrow \frac{1}{R_x} = \frac{d^2 w}{dx^2}$ and $\frac{1}{R_y} = \frac{d^2 w}{dy^2}$.

How about γ_{xy} ?

Wave Lecture 23 (20211130)

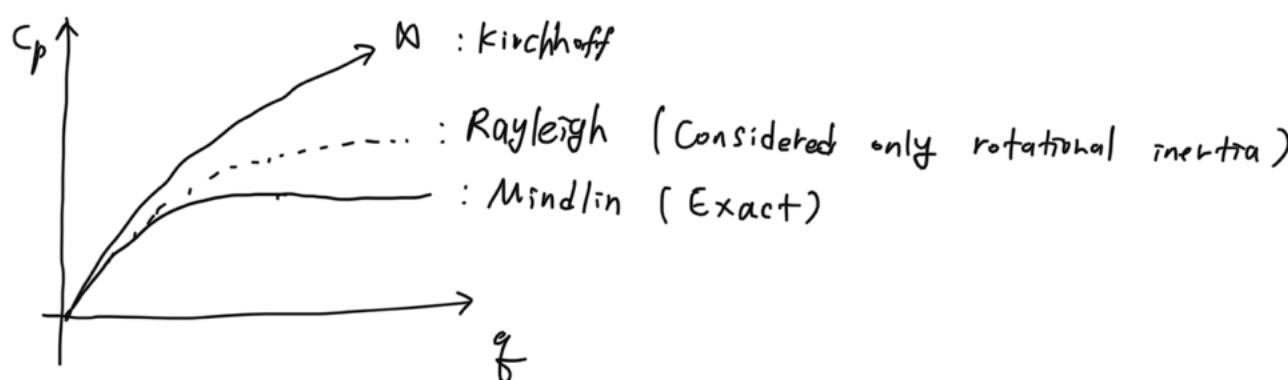
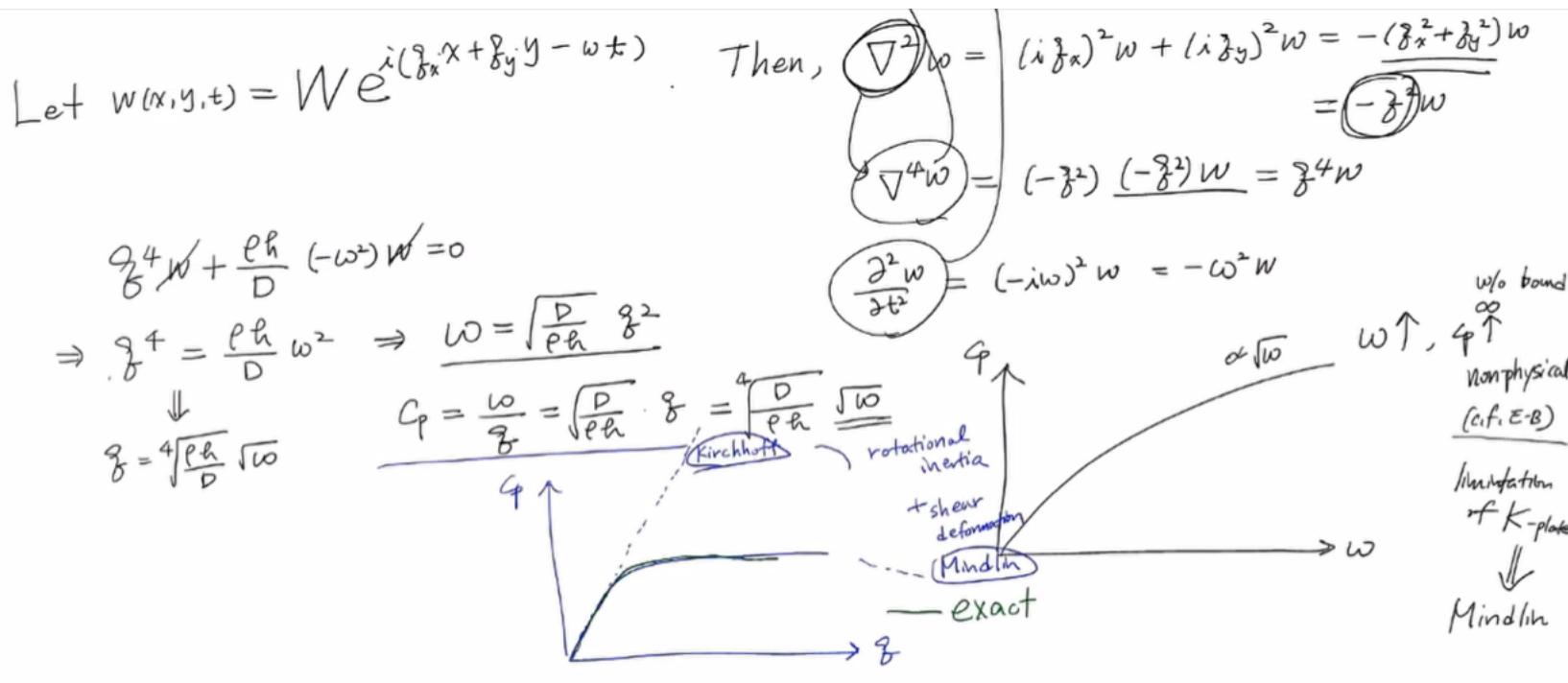
In Kirchhoff plate, $-D \nabla^4 w = \rho h \frac{\partial^2 w}{\partial t^2} \Rightarrow \nabla^4 w + \frac{\rho h}{D} \frac{\partial^2 w}{\partial t^2} = 0$

Flexural stiffness

$$\nabla^2 \nabla^2 = \frac{\partial^4}{\partial x^4} + \frac{\partial^4}{\partial y^4} + 2 \frac{\partial^4}{\partial x^2 \partial y^2}$$

Let $w(x, y, t) = W e^{j(\vec{q} \cdot \vec{x} - \omega t)}$ where $\vec{q} = (q_x, q_y)$: wave vector.

$$\Rightarrow q^4 W + \frac{\rho h}{D} (-\omega^2) W = 0 \Rightarrow \omega = \sqrt{\frac{D}{\rho h}} q^2 \Rightarrow c_p = \sqrt{\frac{D}{\rho h}} \sqrt{\omega}$$



\times Mindlin plate. (OUT OF SCOPE)

(iv) rotational inertia considered
(v) shear deformation

- i) (iv) rotational inertia is taken into account.
 $\overline{\overline{\omega}}$ Line elements perpendicular to the mid-plane remain straight but not necessarily perpendicular to the mid-plane during and after deformation.

Q: Check Contributions of \checkmark rotational inertia & \checkmark shear deformation.

\times Mindlin Plate Theory (w/o derivation)

c.f. Kirchhoff single PDE

E.o.M

(three PDES - coupled)

$$\begin{aligned} \frac{D}{2} \left\{ (1-\nu) \nabla^2 \psi_x + (1+\nu) \frac{\partial \bar{\psi}}{\partial x} \right\} - KGh (\psi_x + \frac{\partial w}{\partial x}) &= \frac{\rho h^3}{12} \frac{\partial^2 \psi_x}{\partial t^2} \\ \frac{D}{2} \left\{ (1-\nu) \nabla^2 \psi_y + (1+\nu) \frac{\partial \bar{\psi}}{\partial y} \right\} - KGh (\psi_y + \frac{\partial w}{\partial y}) &= \frac{\rho h^3}{12} \frac{\partial^2 \psi_y}{\partial t^2} \\ KGh (\nabla^2 w + \bar{\psi}) &= \rho h \frac{\partial^2 w}{\partial t^2} \end{aligned}$$

— transl. accel.

(iv) rotational inertia is taken into account.
 (v) Line elements perpendicular to the mid-plane remain straight but not necessarily perpendicular to the mid-plane during and after deformation.

where ψ_x : total angle in x-dir
 ψ_y : " in y-dir

$$\rightarrow \bar{\psi} = \frac{\partial \psi_x}{\partial x} + \frac{\partial \psi_y}{\partial y}$$

G : shear modulus

K: shear correction factor

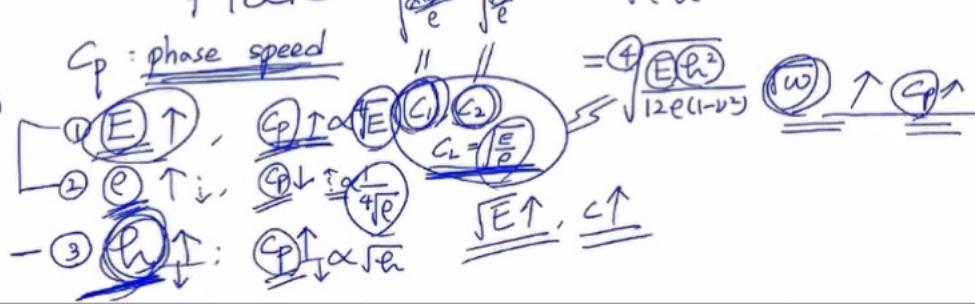
contributions of
 ✓ rot. inert
 ✓ shear def.

$$C_p = \sqrt[4]{Eh^3 / [12\rho(1-\nu^2)]} \sqrt{w} \dots$$

W:
modulus

correction factor

ρ, E, ν



SAW (Surface Acoustic Waves)

Helmholtz decomposition theorem.

Any smooth vector field can be decomposed into the summation of

solenoidal & irrotational field

(div - free)

(curl - free)

$$\left\{ \begin{array}{l} \nabla \cdot F_{\text{solen}} = 0 \\ \nabla \times F_{\text{irrot}} = 0 \end{array} \right.$$

vector identities:

$$\left\{ \begin{array}{l} \nabla \times (\nabla \phi) = 0 \\ \nabla \cdot (\nabla \times \psi) = 0 \end{array} \right.$$

$F_{\text{irrot}} = \nabla \phi \Rightarrow \text{There exist a scalar fn } \phi \text{ such that } \nabla \phi = F_{\text{irrot}}$
 curl-free

$F_{\text{solen}} = \nabla \times \psi \quad \text{"} \quad \text{vector valued fn } \psi \quad \text{"} \quad \nabla \times \psi = F_{\text{solen}}$

Σ P-wave (by pushing)
 dilatational wave

S-wave (by shaking)
 equivilometric

$$\Rightarrow \vec{d} = \underbrace{\nabla \phi}_{\text{Dilatational}} + \underbrace{\nabla \times \psi}_{\text{Equivolumetric}} \quad \text{Recall Navier's Eq.}$$

$$e \ddot{\vec{d}} = (\lambda + \mu) \nabla (\nabla \cdot \vec{d}) + \mu \nabla^2 \vec{d}$$

$$\textcircled{1} \quad \vec{d} = \nabla \phi \quad (\text{curl-free, dilatational})$$

$$\textcircled{2} \quad \vec{d} = \nabla \times \psi \quad (\text{div-free, equivolume})$$

$$e \nabla \dot{\phi} = (\lambda + \mu) \nabla (\nabla^2 \phi) + \mu \nabla \nabla^2 \phi$$

$$e \nabla \dot{\psi} = (\lambda + \mu) \nabla (\nabla \times \psi) + \mu \nabla^2 \nabla \times \psi$$

$$\Rightarrow \rho \cdot \dot{\phi} = (\lambda + 2\mu) \nabla^2 \phi : \text{P-wave Eq.}$$

$$\Rightarrow \rho \dot{\psi} = \mu \nabla^2 \psi : \text{S-wave Eq.}$$

B.C.s

\textcircled{1} No traction force

$$\sigma_{yy} = \sigma_{yx} = 0$$

\textcircled{2} No variation along z axis
(in-plane motion)

$$xy \text{ plane} \rightarrow \frac{\partial}{\partial z} = 0$$

$$\vec{d} = \nabla \phi + \nabla \times \psi$$

$$= \begin{pmatrix} \frac{\partial \phi}{\partial x} \\ \frac{\partial \phi}{\partial y} \\ \cancel{\frac{\partial \phi}{\partial z}} \end{pmatrix} + \begin{pmatrix} \frac{\partial \psi_x}{\partial y} - \frac{\partial \psi_y}{\partial z} \\ \cancel{\frac{\partial \psi_x}{\partial z}} - \frac{\partial \psi_z}{\partial x} \\ \frac{\partial \psi_y}{\partial x} - \frac{\partial \psi_x}{\partial y} \end{pmatrix}$$

$$= \begin{pmatrix} \frac{\partial \phi}{\partial x} + \frac{\partial \psi_z}{\partial y} \\ \frac{\partial \phi}{\partial y} - \frac{\partial \psi_z}{\partial x} \\ \cancel{\frac{\partial \psi_y}{\partial x}} - \cancel{\frac{\partial \psi_x}{\partial y}} \end{pmatrix} = \begin{pmatrix} u \\ v \\ w \end{pmatrix} \quad \left. \begin{array}{l} \text{Only } \phi, \psi_z \\ \text{are needed} \end{array} \right\}$$

From \textcircled{1}, \textcircled{2}, respectively.

$$\frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} = \frac{1}{c_1^2} \frac{\partial^2 \phi}{\partial t^2} \quad \left/ \frac{\partial^2 \psi_z}{\partial x^2} + \frac{\partial^2 \psi_z}{\partial y^2} = \frac{1}{c_2^2} \frac{\partial^2 \psi_z}{\partial t^2} \right.$$

Wave Lecture 24 (20211207)

• SAW

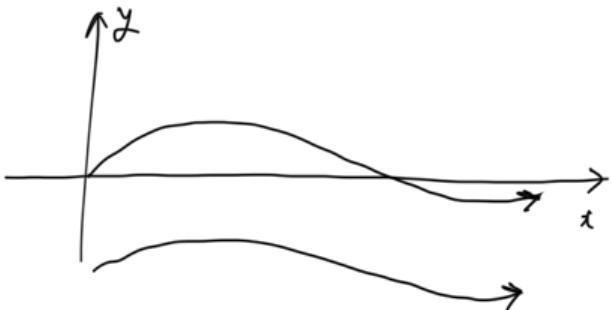
$$\rho \ddot{\vec{P}} = (\lambda + \mu) \nabla(\nabla \cdot \vec{P}) + \mu \nabla^2 \vec{P}$$

$$\begin{aligned} \text{H.D.T} & \quad \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} = \frac{1}{c_1^2} \frac{\partial^2 \phi}{\partial t^2} \quad (1) \\ \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} &= \frac{1}{c_2^2} \frac{\partial^2 \psi}{\partial t^2} \quad (2) \\ \vec{P} &= \nabla \phi + \nabla \times \psi \end{aligned}$$

B.C.s

$$1) \sigma_{xy} = \lambda \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right) + 2\mu \frac{\partial v}{\partial y}$$

$$2) \tau_{yx} = G \tau_{yx} = 2\mu \varepsilon_{yx} = \mu \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) \quad (4)$$



$$\begin{cases} u = \frac{\partial \phi}{\partial x} + \frac{\partial \psi}{\partial y} \\ v = \frac{\partial \phi}{\partial y} - \frac{\partial \psi}{\partial x} \end{cases}$$

$$\text{Assume } \phi(x, y, t) = f(y) e^{j(kx - \omega t)}$$

$$\psi(x, y, t) = g(y) e^{j(kx - \omega t)}$$

$$\begin{aligned} ① \Rightarrow -k^2 f + f'' &= -\frac{\omega^2}{c_1^2} f \Rightarrow f'' - \underbrace{\left(k^2 - \left(\frac{\omega}{c_1} \right)^2 \right)}_{=\zeta^2} f = 0 \quad \zeta^2 > 0 \\ ② \Rightarrow g'' - \underbrace{\left(k^2 - \left(\frac{\omega}{c_2} \right)^2 \right)}_{=\eta^2} g &= 0 \quad f(y) = A e^{-\zeta y} + B e^{\zeta y} \\ & g(y) = C e^{-\eta y} + D e^{\eta y} \end{aligned}$$

∵ if negative,
 $f = F(\cos, \sin)$
 $y \rightarrow -\infty \not\models f = 0$
 not possible

$$\Rightarrow \begin{cases} \phi = B e^{\zeta y} e^{j(kx - \omega t)} \\ \psi = D e^{\eta y} e^{j(kx - \omega t)} \end{cases}$$

$$\begin{aligned} \text{Note: } \zeta^2 &= k^2 - \frac{\omega^2}{c_1^2} = k^2 - \frac{\rho \omega^2}{\lambda + 2\mu} \\ \eta^2 &= k^2 - \frac{\omega^2}{c_2^2} = k^2 - \frac{\rho \omega^2}{\mu} \\ \Rightarrow (\lambda + 2\mu) \zeta^2 &= (\lambda + 2\mu) k^2 - \rho \omega^2 \\ \mu \eta^2 &= \mu k^2 - \rho \omega^2 \\ \Rightarrow (\lambda + 2\mu) \zeta^2 - \lambda k^2 &= \mu \eta^2 + \mu k^2 \quad — (*) \end{aligned}$$

$$\begin{aligned} \textcircled{3}: & (\lambda + 2\mu)(\zeta^2 - k^2)B - 2\mu(-k^2B + jkD\eta) = 0 \\ \Rightarrow & [(\lambda + 2\mu)\zeta^2 - \lambda k^2]\beta - 2jkD\mu\eta = 0 \Rightarrow \underbrace{\mu(\eta^2 + k^2)\beta - 2jk\mu\eta D}_{\therefore (\star)} = 0 \end{aligned}$$

$$\textcircled{4} \quad \mu(2\beta jk\zeta + \eta^2 D + k^2 D) = 0$$

$$\text{From } \textcircled{3}, \textcircled{4} \Rightarrow \underbrace{\begin{pmatrix} \eta^2 + k^2 & -2jk\eta \\ 2jk\zeta & \eta^2 + k^2 \end{pmatrix}}_A \begin{pmatrix} B \\ D \end{pmatrix} = 0 \Rightarrow \det(A) = 0$$

$$\boxed{(\eta^2 + k^2)^2 - 4k^2\zeta\eta = 0}$$

$$\text{Note that, } \eta^2 = k^2 - \frac{\omega^2}{C_2^2} = k^2 \left(1 - \frac{C_R^2}{C_2^2}\right) \text{ where } C_R = \frac{\omega}{k} \begin{pmatrix} \text{phase speed} \\ \text{of SAW} \end{pmatrix}$$

$$\zeta^2 = k^2 - \frac{\omega^2}{C_1^2} = k^2 \left(1 - \frac{C_R^2}{C_1^2}\right)$$

$$\Rightarrow \left(k^2 \left(1 - \frac{C_R^2}{C_2^2}\right) + k^2\right)^2 - 4k^2 \cdot k^2 \sqrt{1 - \frac{C_R^2}{C_1^2}} \sqrt{1 - \frac{C_R^2}{C_2^2}} = 0$$

$$\Rightarrow \boxed{\left(2 - \frac{C_R^2}{C_2^2}\right)^4 = 16 \left(1 - \frac{C_R^2}{C_1^2}\right) \left(1 - \frac{C_R^2}{C_2^2}\right)}$$

C_R is independent
of frequency (ω)

$$\therefore C_R = C_R(C_1, C_2)$$

Particle Trajectories

$$\text{Also, } D = \frac{-2jk\zeta}{\eta^2 + k^2} \cdot B$$

$$\text{Recall, } \begin{cases} \rho = Be^{\zeta y} \cdot e^{j(kx - \omega t)} \\ \psi_z = De^{\eta z} \cdot e^{j(kx - \omega t)} \end{cases}$$

$$\boxed{\psi_z = -\frac{2ik^2}{\eta^2+k^2} e^{iy} e^{i(kx-wt)}}$$

$$u = \frac{\partial \phi}{\partial x} + \frac{\partial \psi_z}{\partial y} = B \underbrace{i k \left[e^{iy} - \frac{2 \eta}{\eta^2+k^2} e^{iy} \right]}_a e^{i(kx-wt)}$$

$$v = \frac{\partial \phi}{\partial y} - \frac{\partial \psi_z}{\partial x} = B \underbrace{\bar{z} \left[e^{iy} - \frac{2k^2}{\eta^2+k^2} e^{iy} \right]}_b e^{i(kx-wt)}$$

$$\Rightarrow \left| \frac{u}{a} \right|^2 + \left| \frac{v}{b} \right|^2 = 1 \rightarrow \text{Ellipse.}$$

① oblate



② prolate



① cw

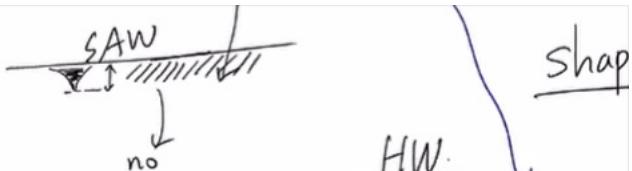
② ccw

Penetration Depth

depth ↓ ////////////////

$$\frac{u(y)}{u(0)} = \frac{e^{iy} - \frac{2\eta}{\eta^2+k^2} e^{iy}}{1 - \frac{2\eta}{\eta^2+k^2}} \ll 1$$

$$\frac{v(y)}{v(0)} = \frac{e^{iy} - \frac{2k^2}{\eta^2+k^2} e^{iy}}{1 - \frac{2k^2}{\eta^2+k^2}} \ll 1$$



$$\frac{U(y)}{U(0)} = \frac{e^{\eta y} - \frac{2\beta\eta}{\eta^2 + k^2} e^{\eta y}}{1 - \frac{2\beta\eta}{\eta^2 + k^2}}$$

$$\frac{V(y)}{V(0)} = \frac{e^{\eta y} - \frac{2k^2}{\eta^2 + k^2} e^{\eta y}}{1 - \frac{2k^2}{\eta^2 + k^2}}$$

Penetration Depth of Rayleigh Wave

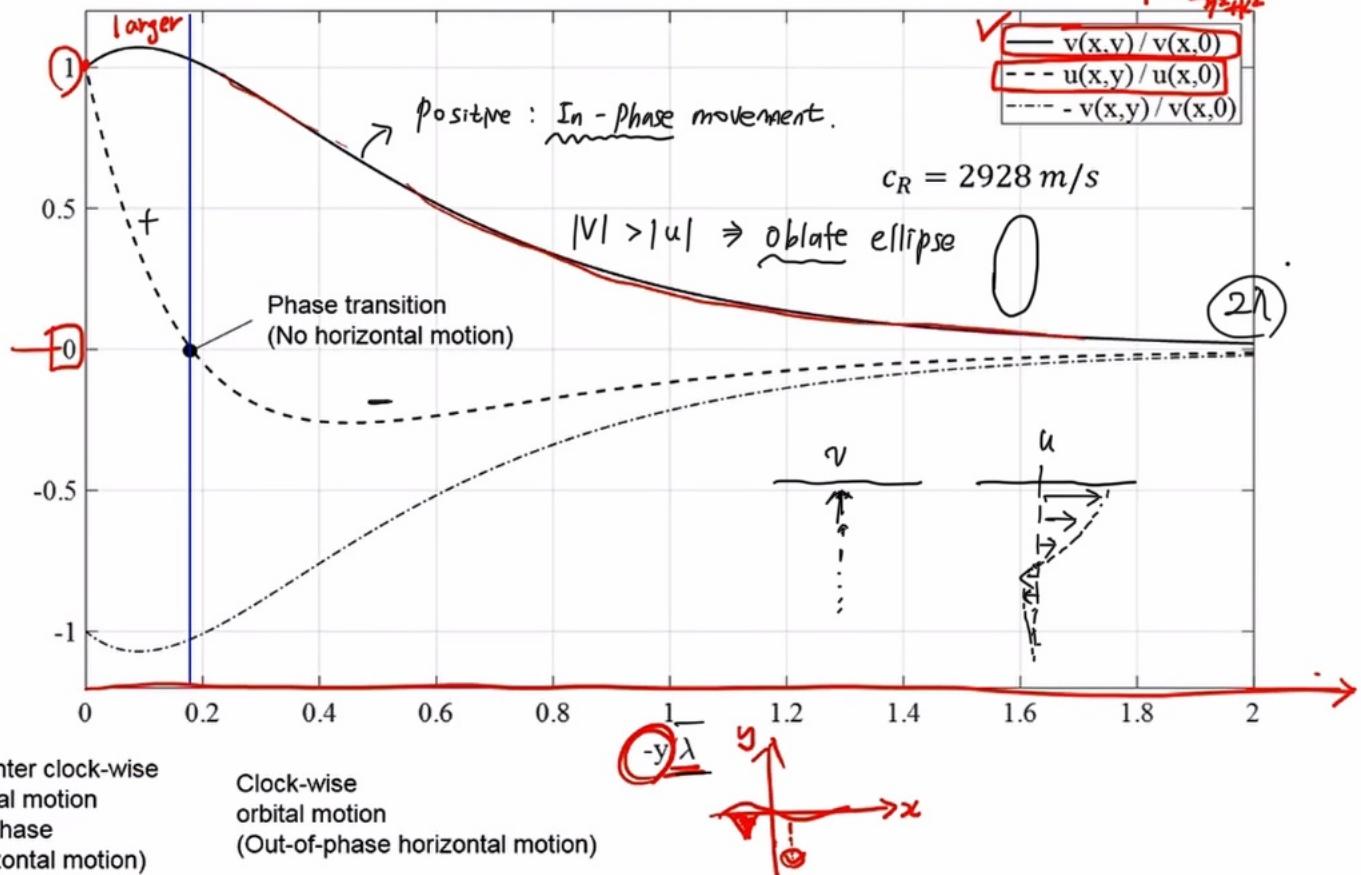


Rayleigh wave in Aluminum at 3000 Hz

$$\frac{U(x,y)}{U(x,0)} = \frac{e^{\eta y} - \frac{2\beta\eta}{\eta^2 + k^2} e^{\eta y}}{1 - \frac{2\beta\eta}{\eta^2 + k^2}}$$

$$\frac{V(x,y)}{V(x,0)} = \frac{e^{\eta y} - \frac{2k^2}{\eta^2 + k^2} e^{\eta y}}{1 - \frac{2k^2}{\eta^2 + k^2}}$$

$$c_R = 2928 \text{ m/s}$$



Aluminium vs Rubber @ 3000 Hz

