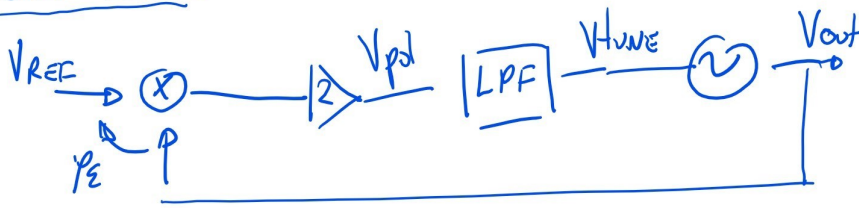


## • LOCK RANGE



$$\begin{cases} \omega_{out} = \omega_{REF} \\ \quad = \omega_{REF} + K_{VCO} V_{tune} \\ \langle V_{pd} \rangle = V_{tune} = K_{pd} \sin(\phi_e) \end{cases}$$

$$\langle V_{pd} \rangle^{max} = \pm 1$$

$$\omega_{out}^{max} = \omega_{REF} + K_{VCO} (+1)$$

$$\omega_{out}^{min} = \omega_{REF} + K_{VCO} (-1)$$

IN OUR CASE:

$$\omega_{REF} = \omega_0$$

$$\omega_{REF} = \omega_0 + \Delta\omega$$

INPUT STEP

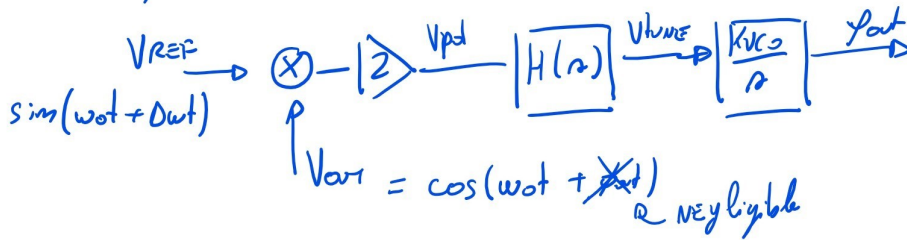
MAXIMUM

INPUT STEP:

$$\Delta\omega^{max} = K_{VCO} (\pm 1V) = 2 \frac{rad/s}{V} = 2 \frac{rad/s}{V}$$

## • CAPTURE RANGE

• APPLY AN input frequency step  $\Delta\omega$



$$V_{pd} = 2 \left[ \frac{1}{2} \sin(\Delta\omega t) + \frac{1}{2} \sin(2\omega_0 t + \Delta\omega t) \right]$$

FILTERED BY LPF

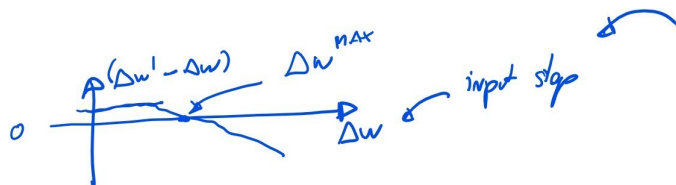
This signal is @  $\Delta\omega$  freq with amplitude  $K_{pd}$  so it is partially filtered by LPF.



• The PLL can REACH LOCK if

$$\Delta\omega' = K_{pd} |H(j\Delta\omega)| K_{VCO} \geq \Delta\omega$$

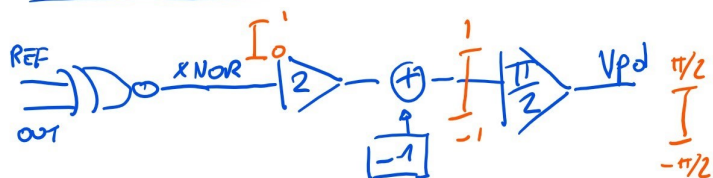
GRAPHICAL SOLUTION:



SEE MATLAB SCRIPT

$$\Delta\omega^{max} = \text{CAPTURE RANGE}$$

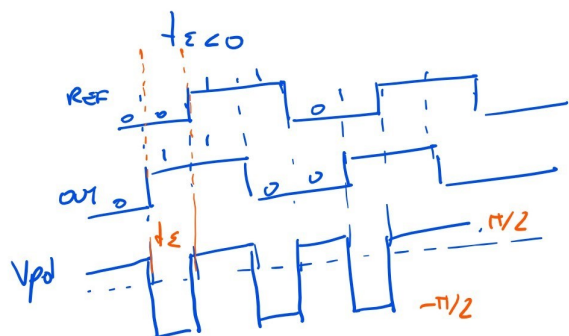
# NXOR PHASE DETECTOR



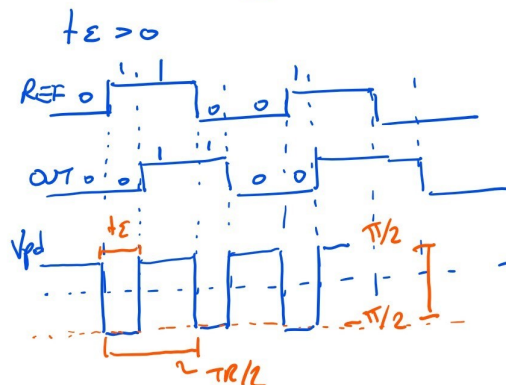
• DERIVING THE LINEARIZED AVERAGED MODEL IN PHASE DOMAIN

NXOR

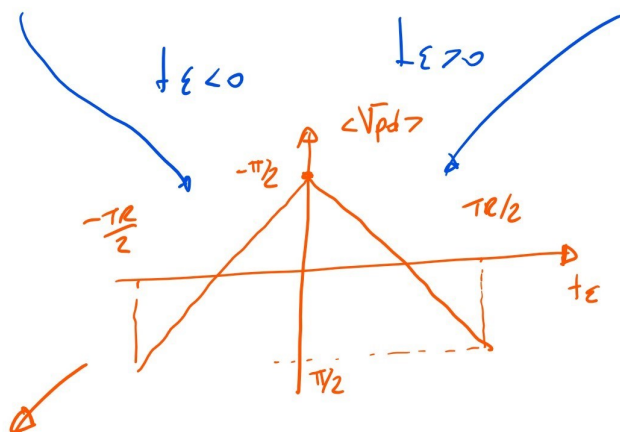
REF	OUT	XNOR
0	0	1
0	1	0
1	0	0
1	1	1



$$\langle \bar{V}_{pd} \rangle = -\frac{\pi}{2} + 2\pi \frac{tE}{T_R}$$



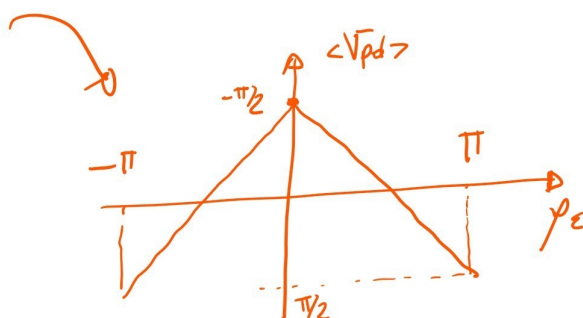
$$\begin{aligned} \langle \bar{V}_{pd} \rangle &= -\frac{\pi}{2} + \pi \frac{(T_R/2 - tE)}{T_R/2} \\ &= -\frac{\pi}{2} + \pi - 2\pi \frac{tE}{T_R} \\ &= \frac{\pi}{2} - 2\pi \frac{tE}{T_R} \end{aligned}$$



in PHASE DOMAIN

$$\phi_E = \frac{2\pi}{T_R} tE \sim tE = \gamma_E \frac{T_R}{2\pi}$$

$$\langle \bar{V}_{pd} \rangle = \frac{\pi}{2} - (\gamma_E \text{ V/nm})$$



$\phi_E < 0$ :

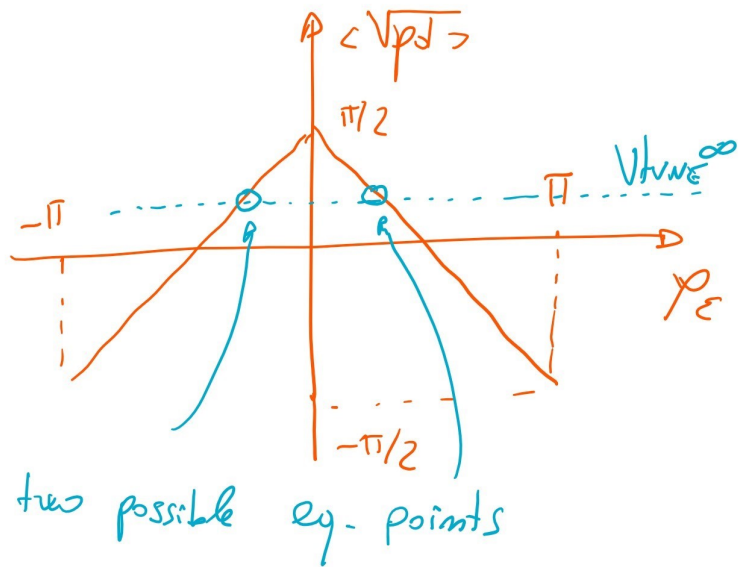
$$K_{pd} = \frac{\partial \langle \bar{V}_{pd} \rangle}{\partial \phi_E} = 1$$

$\phi_E > 0$ :

$$K_{pd} = \frac{\partial \langle \bar{V}_{pd} \rangle}{\partial \phi_E} = -1$$

## PLL EQ POINT:

$$\begin{cases} \omega_{out} = \omega_{ref} \\ = \omega_{ref} + K_{VCO} V_{tune} \\ V_{tune} = \angle \sqrt{p_d} = K_{pd} \phi_E^\infty \\ V_{tune}^\infty = \frac{\omega_{ref} - \omega_{ref}}{K_{VCO}} = \frac{d\omega}{K_{VCO}} = 0.1V \\ \phi_E^\infty = \frac{V_{tune}^\infty}{K_{pd}} = \pm 0.1 \text{ rad} \end{cases}$$

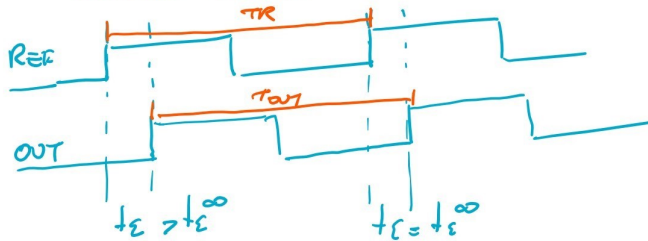


## WHICH IS THE STABLE EQ POINT?

### METHOD 1: APPLY PERTURBATION

#### CASE $\phi_E > 0$

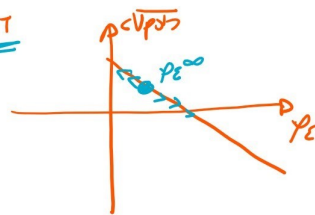
suppose  $\phi_E > \phi_E^\infty$



CASE  $\phi_E > 0$

IF I APPLY A PERTURBATION  $\phi_E > \phi_E^\infty$   
to reach  $\phi_E = \phi_E^\infty$  the PLL needs  
to set  $T_{out} < T_R$  (INCREASE FREQUENCY)

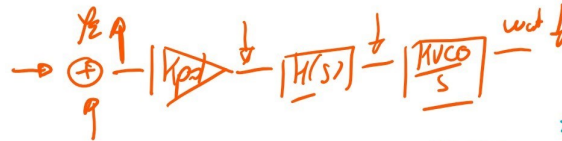
BUT



FOR  $\phi_E > 0$

IF I HAVE  $\phi_E > \phi_E^\infty$

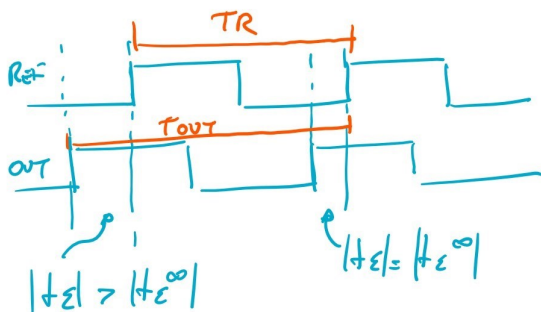
the PLL DECREASES  
THE OUTPUT FREQUENCY



UNSTABLE EQ. POINT.

#### CASE $\phi_E < 0$

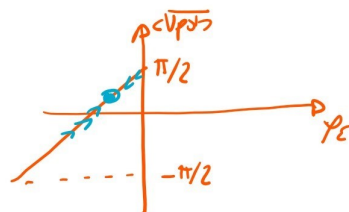
suppose  $|\phi_E| > \phi_E^\infty$



CASE  $\phi_E < 0$

IF I APPLY A PERTURBATION  $|\phi_E| > \phi_E^\infty$

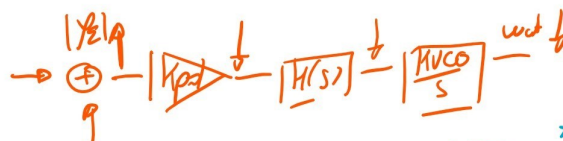
to reach  $|\phi_E| = \phi_E^\infty$  the PLL needs  
to set  $T_{out} > T_R$  (DECREASE FREQUENCY)



FOR  $\phi_E < 0$

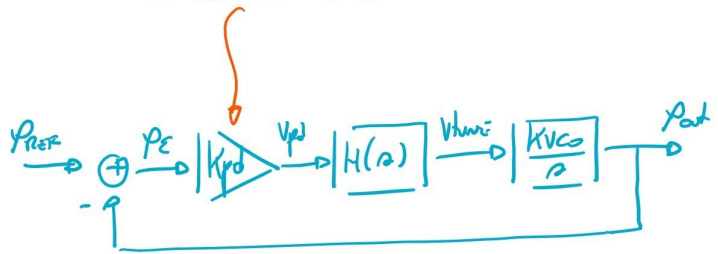
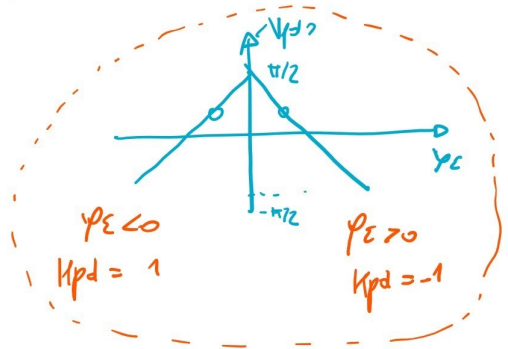
IF I HAVE  $|\phi_E| > \phi_E^\infty$

the PLL DECREASES  
THE OUTPUT FREQUENCY



STABLE EQ. POINT.

• METHOD 2: LOOP GAIN SIGN



to have  $G_{loop} < 0 \rightarrow K_{pd} > 0 \rightsquigarrow p_e^+$  in  $p_e < 0$  stable eq point.