
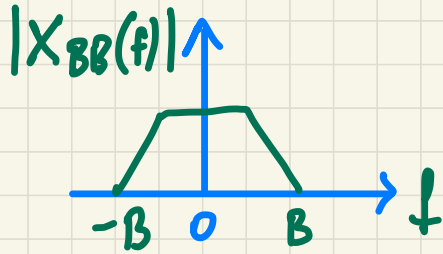


RF Circuit Design

L1

2020/21 

Communication Theory



Baseband
signal (information)

$\lambda/2$ physical dimension
Hertz dipole (antenna)

Carrier modulation

sinusoid
 $A_c \cos[\omega_c t]$
amplitude phase

"carries"
informat.

$$\lambda = \frac{c}{f_c}$$

$$c = 3 \cdot 10^8 \text{ m/s}$$

$$\lambda/2 \approx 15 \text{ cm}$$

$$\lambda \approx 30 \text{ cm}$$



$$f_c = 1 \text{ GHz}$$

AM modulation (amplitude modulation)

$$x(t) = A_c [1 + m \cdot \underbrace{x_{BB}(t)}_{\text{baseband signal}}] \cdot \underbrace{\cos \omega_c t}$$

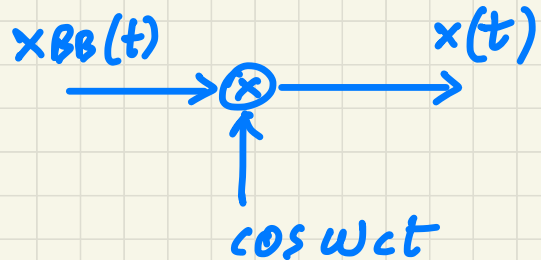
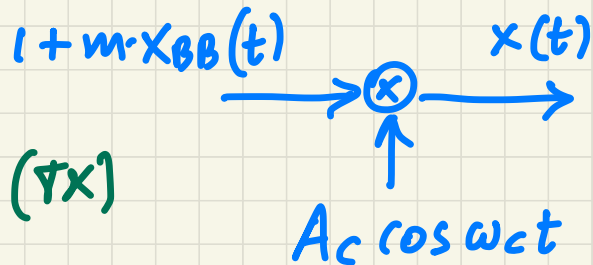
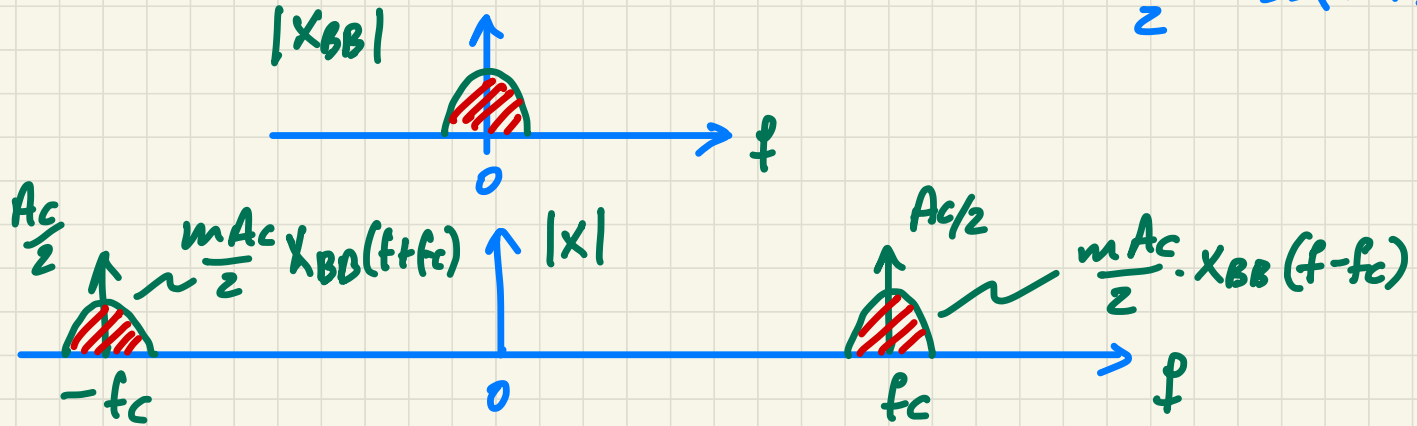
Spectrum : Fourier transform of $x(t)$

$$e^{\pm j\omega_c t} \leftrightarrow \delta(f \mp f_c) \quad X(f) \triangleq \int_{-\infty}^{+\infty} x(t) e^{-j2\pi f t} dt$$

$$x(t) = A_c [1 + m \cdot x_{BB}(t)] \cdot \frac{e^{j\omega_c t} + e^{-j\omega_c t}}{2}$$

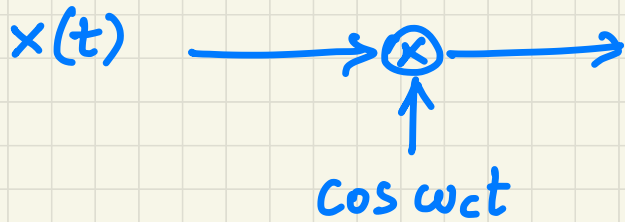
$$X(f) = \frac{A_c}{2} \delta(f - f_c) + \frac{A_c}{2} \delta(f + f_c) + \frac{m A_c}{2} \cdot X_{BB}(f) * \delta(f + f_c) + \frac{m A_c}{2} X_{BB}(f) * \delta(f - f_c)$$

$$X(f) = \frac{A_c}{2} \delta(f - f_c) + \frac{A_c}{2} \delta(f + f_c) + \frac{mA_c}{2} X_{BB}(f - f_c) + \frac{mA_c}{2} X_{BB}(f + f_c)$$



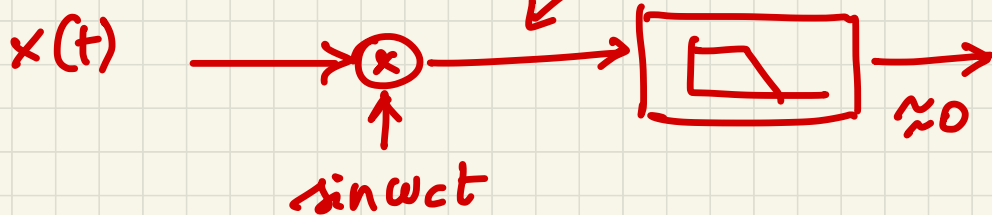
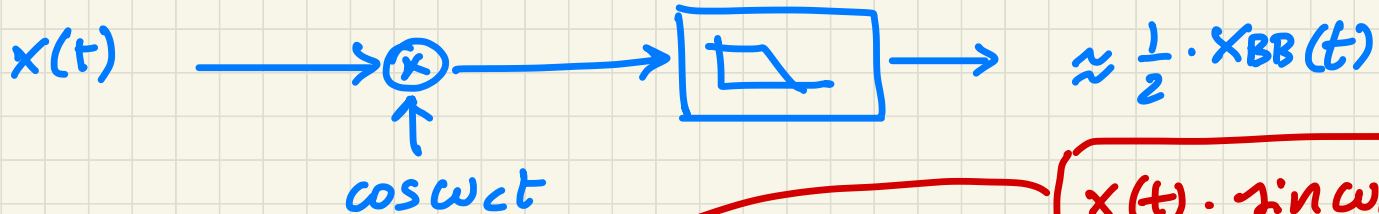
- AM modulation with transmitted carrier
- AM without transmitted c.

Coherent demodulation (Rx)



$$\begin{aligned} x(t) \cdot \cos \omega_c t &= \\ &= x_{BB}(t) \cdot \cos^2 \omega_c t = \\ &= x_{BB}(t) \cdot \frac{1 + \cos 2\omega_c t}{2} \end{aligned}$$

$$x(t) = x_{BB}(t) \cdot \cos \omega_c t$$



$$\begin{aligned} x(t) \cdot \sin \omega_c t &= \\ &= x_{BB}(t) \sin \omega_c t \cos \omega_c t \\ &= x_{BB}(t) \cdot \frac{1}{2} \sin 2\omega_c t \end{aligned}$$

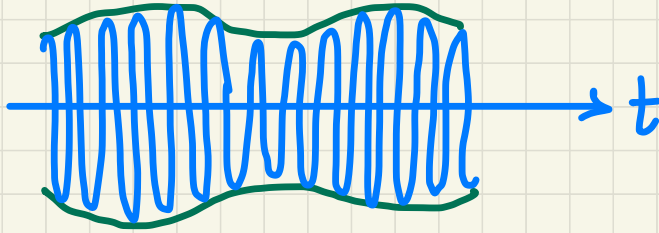
Non-coherent demodulation

$$x(t) = A_c [1 + m x_{BB}(t)] \cos \omega_c t$$

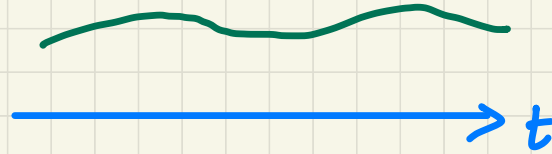
AM with TX carrier

$$m x_{BB} < 1$$

$x(t)$

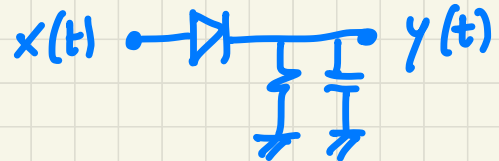


$y(t)$

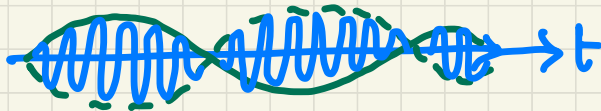


AM without TX'd carrier

$$x(t) = x_{BB}(t) \cdot \cos \omega_c t$$



$x(t)$



$y(t)$



Phasor representation of a sinusoidal AM

$$x_{BB}(t) = A_m \cos \omega_m t$$

$$\begin{aligned} \cos x \cos y &= \\ &= \frac{1}{2} \cos(x-y) + \\ &\quad + \frac{1}{2} \cos(x+y) \end{aligned}$$

$$x(t) = A_c [1 + m x_{BB}(t)] \cos \omega_c t =$$

$$= A_c \cdot \cos \omega_c t + m A_m A_c \cdot \cos \omega_c t \cdot \cos \omega_m t =$$

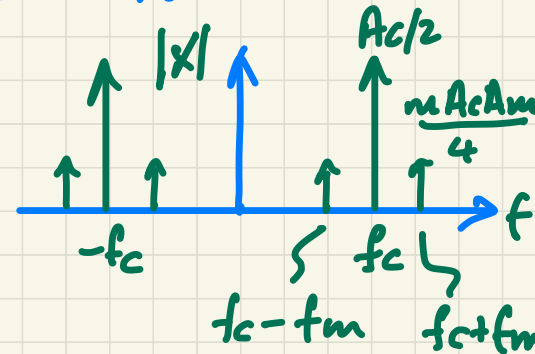
$$= A_c \cdot \cos \omega_c t + \frac{m A_m A_c}{2} \cos(\omega_c - \omega_m)t +$$

$$+ \frac{m A_m A_c}{2} \cos(\omega_c + \omega_m)t$$

$$x(t) = \text{Re} \{ \bar{X}(t) \cdot e^{j\omega_c t} \}$$

Phasor

$$e^{j\omega_c t} = \cos \omega_c t + j \sin \omega_c t$$

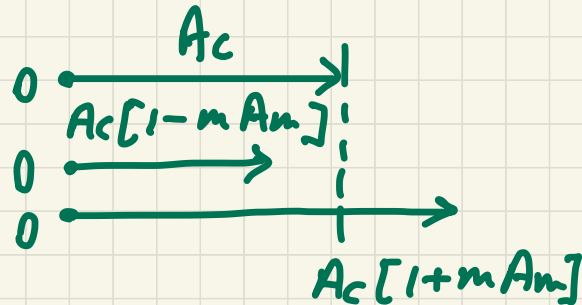
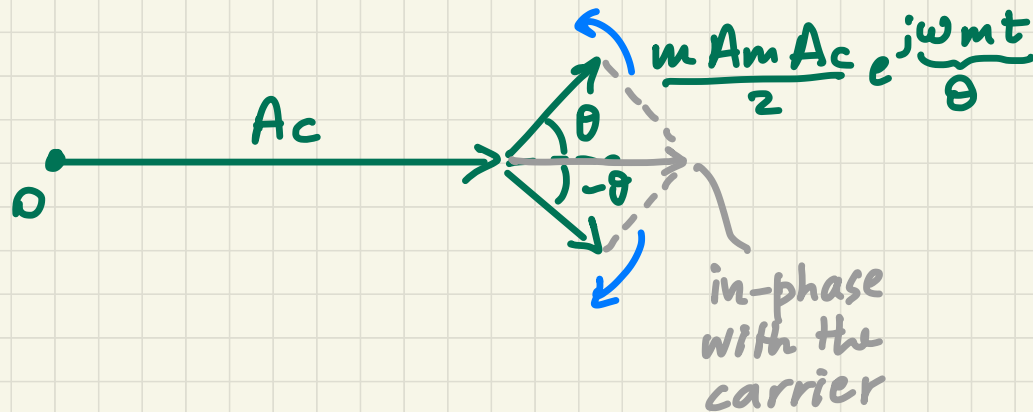


$$x(t) = A_c \cdot \cos \omega_c t + \frac{m A_m A_c}{2} \cos(\omega_c - \omega_m)t + \frac{m A_m A_c}{2} \cos(\omega_c + \omega_m)t$$

$$x(t) = \text{Re} \{ \bar{X}(t) \cdot e^{j\omega_c t} \}$$

Phasor

$$\bar{X}(t) = A_c + \frac{m A_m A_c}{2} \cdot e^{-j\omega_m t} + \frac{m A_m A_c}{2} e^{j\omega_m t}$$



Frequency Modulation (FM)

$$x(t) = A_c \cos \left[\omega_c t + m \underbrace{\int_{-\infty}^t x_{BB}(t') dt'}_{\varphi(t)} \right]$$

$$\begin{cases} \omega(t) = \frac{d\phi}{dt} \\ \phi(t) = \int_{-\infty}^t \omega(t') dt' \end{cases}$$

Relationship between
angular frequency ω and
phase ϕ of a periodic signal

Narrowband FM approximation (NBFM):

$$\varphi(t) = m \int_{-\infty}^t x_{BB}(t') dt' \ll 1 \text{ rad}$$

$$x(t) = A_c \cos [\omega_c t + \varphi(t)] =$$

$$= A_c \cos \omega_c t \cdot \cos [\varphi(t)] - A_c \sin \omega_c t \cdot \sin [\varphi(t)] =$$

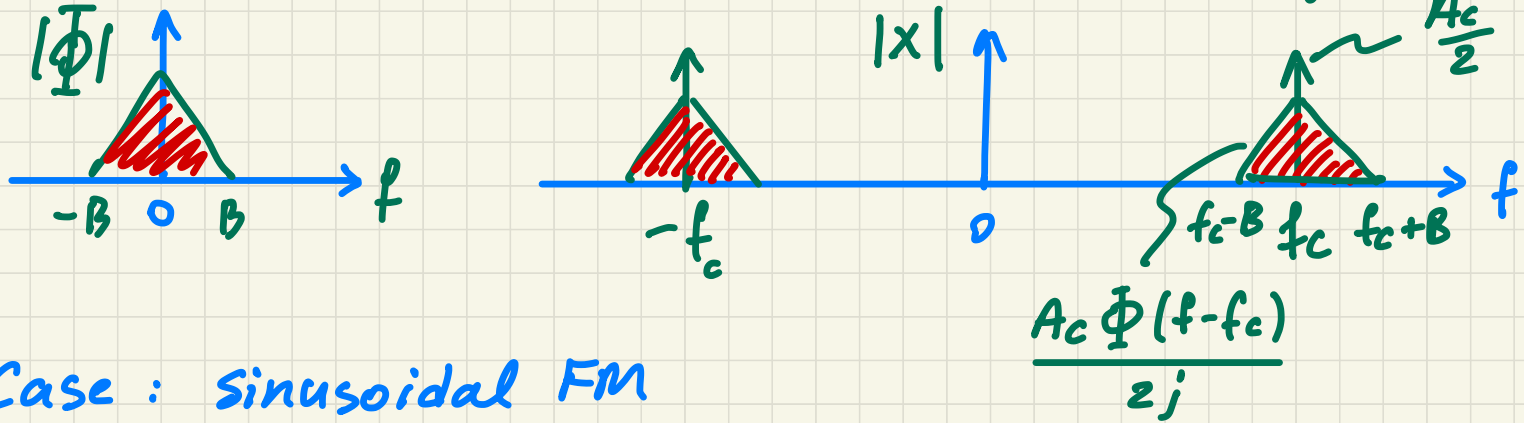
$$\approx A_c \cdot \cos \omega_c t \cdot 1 - A_c \cdot \sin \omega_c t \cdot \varphi(t) =$$

NBFM

$$= \underbrace{A_c \cos \omega_c t}_{\text{carrier}} - \underbrace{A_c \cdot \varphi(t) \cdot \sin \omega_c t}_{\text{AM modulation of the quadrature component of the carrier}} =$$

$$= A_c \cdot \frac{e^{j\omega_c t} + e^{-j\omega_c t}}{2} - A_c \varphi(t) \cdot \frac{e^{j\omega_c t} - e^{-j\omega_c t}}{2j}$$

$$x(t) = A_c \cdot \frac{e^{j\omega_c t} + e^{-j\omega_c t}}{2} - A_c \varphi(t) \cdot \frac{e^{j\omega_c t} - e^{-j\omega_c t}}{2j}$$



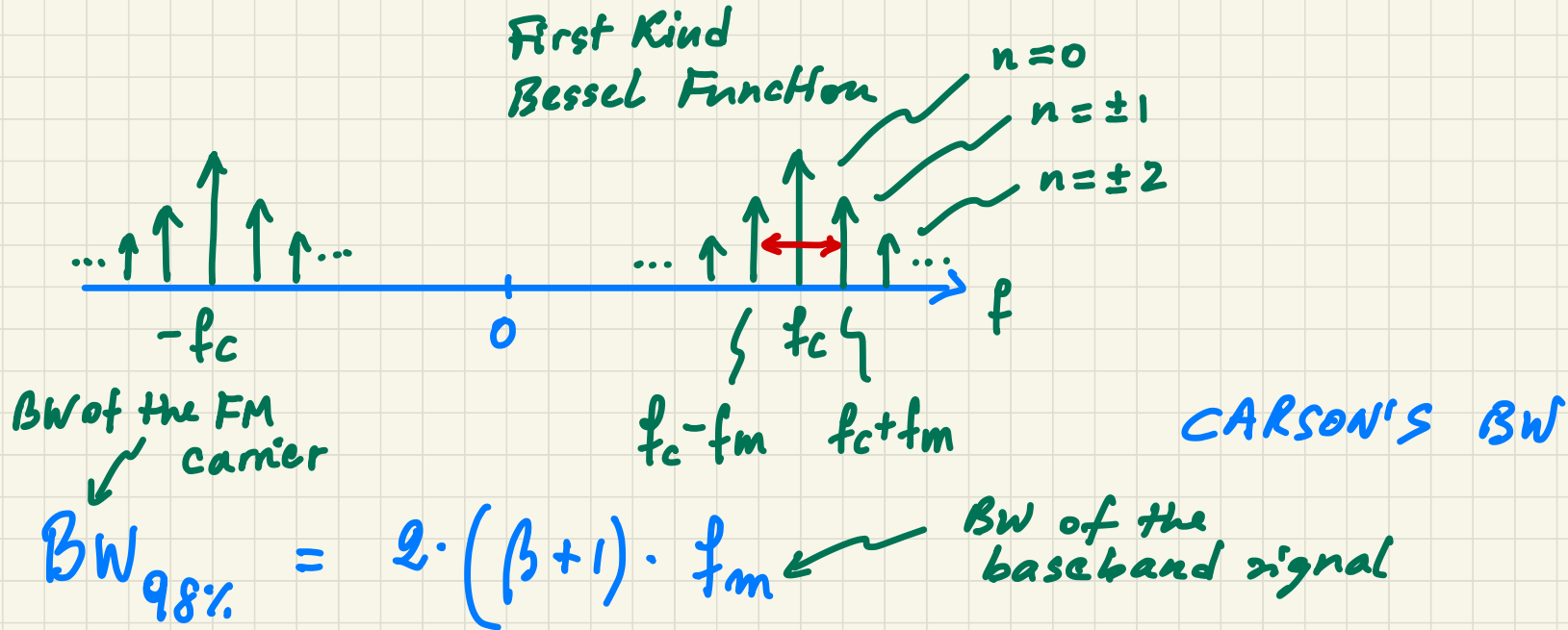
Case : Sinusoidal FM

$$x_{BB}(t) = A_m \cos \omega_m t$$

$$\begin{aligned} x(t) &= A_c \cos \left[\omega_c t + m \int_{-\infty}^t A_m \cos \omega_m t' dt' \right] = \\ &= A_c \cos \left[\omega_c t - \underbrace{\frac{m A_m}{\omega_m}}_{\beta} \underbrace{\sin \omega_m t}_{\varphi(t)} \right] = \end{aligned}$$

$$x(t) = A_c \cos \left[\omega_c t - \underbrace{\beta \cdot \sin \omega_m t}_{\varphi(t)} \right] =$$

$$= A_c \sum_{n=-\infty}^{+\infty} \underbrace{J_n(\beta)}_{\text{First Kind Bessel Function}} \cdot \cos [\omega_c + \underbrace{n}_{\text{modulation depth}} \omega_m t]$$



$$BW_{98\%} = 2(\beta + 1) \cdot f_m \approx \underbrace{2 \cdot f_m}$$

NB FM

$$\varphi \ll 1 \text{ rad}$$

$$\Rightarrow \beta \ll 1 \text{ rad}$$

Phasor Representation

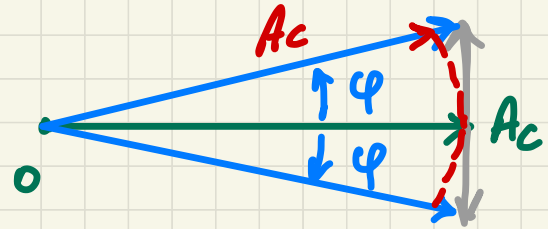
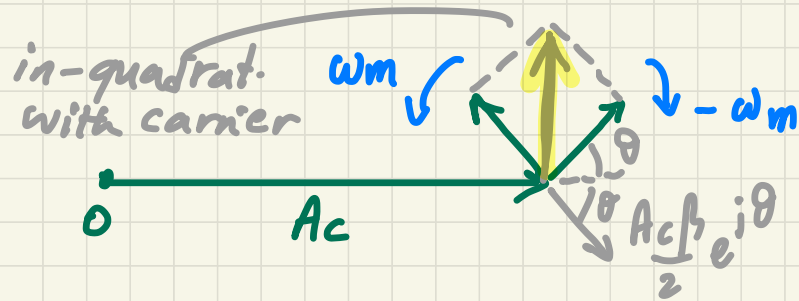
$$x(t) = A_c \cos[\omega_c t + \varphi(t)] \approx A_c \cos \omega_c t - A_c \cdot \varphi(t) \cdot \sin \omega_c t$$

$$= A_c \cos \omega_c t - A_c \cdot \sin \omega_c t \cdot [-\beta \sin \omega_m t] =$$

$$= A_c \cos \omega_c t + \frac{A_c \beta}{2} \cos(\omega_c - \omega_m)t - \frac{A_c \beta}{2} \cos(\omega_c + \omega_m)t$$

$$\Rightarrow \bar{X}(t) = A_c + A_c \beta / 2 \cdot e^{-j \underbrace{\omega_m t}_0} - A_c \beta / 2 \cdot e^{j \underbrace{\omega_m t}_0}$$

$$\bar{X}(t) = A_c + A_c \beta / 2 \cdot e^{-j \underbrace{\omega_m t}_\theta} - A_c \beta / 2 \cdot e^{j \underbrace{\omega_m t}_\theta}$$



PM (or FM) is equivalent to amplitude modulat. of the quadrature component of the carrier

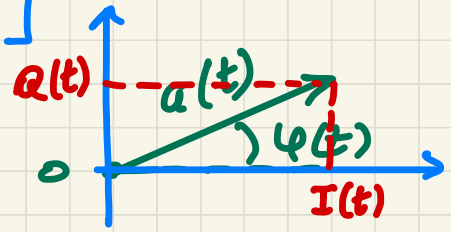
Why is not a pure PM modulation?

The equivalence holds only under NBFM approximation
 $\beta \ll 1 \text{ rad}$ (or $\phi \ll 1 \text{ rad}$)

AM and PM modulation (Quadrature modulation)

- $x(t) = a(t) \cdot \cos[\omega_c t + \varphi(t)]$

Phasor $\bar{x}(t) = a(t) \cdot e^{j\varphi(t)}$



$$\text{Re}\{x(t) \cdot e^{j\omega_c t}\} = \text{Re}\{a(t) \cos[\omega_c t + \varphi] + j a(t) \sin[\omega_c t + \varphi]\}$$

- $x(t) = I(t) \cdot \cos \omega_c t - Q(t) \sin \omega_c t =$

$$= I(t) \frac{e^{j\omega_c t} + e^{-j\omega_c t}}{2} + j Q(t) \cdot \frac{e^{+j\omega_c t} - e^{-j\omega_c t}}{2j} =$$

$$= \frac{1}{2} [\underbrace{I(t) + jQ(t)}_{\bar{x}}] \cdot e^{j\omega_c t} + \frac{1}{2} [I(t) - jQ(t)] e^{-j\omega_c t}$$

$$= \frac{1}{2} \bar{x} e^{j\omega_c t} + \frac{1}{2} \bar{x}^* e^{-j\omega_c t} = \frac{1}{2} \text{Re}\{\bar{x} e^{j\omega_c t}\}$$