Lesson 03

Virtual Work, Calculus of Variation Hamilton's Principle

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1. Virtual Work – Work and Energy

- ❖ Work is the product of force and displacement in the direction of the force.
- The work done by the force in moving the particle from A to B is given by

$$W = \int_{A}^{B} F \cdot du$$

Total work done on the body is the sum of work done on all particles of the body.

$$W = \int_{V} F \cdot u \, dv$$

Energy is the capacity to do work. Measure of the capacity of all forces.

$$E = \iint_{t} F \cdot u \, dv \, dt$$

❖ Both work and energy are scalars (independent of the coordinate system).

1. Virtual Work - Strain Energy

Strain energy density.

- Complementary strain energy density.
- $U_0 = \int_{\varepsilon} \sigma_{ij} d\varepsilon_{ij}$ $U_0^* = \int_{\varepsilon} \varepsilon_{ij} d\sigma_{ij}$

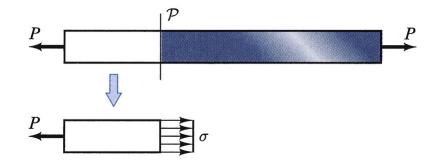
For linear elastic materials:

$$U_0 = U_0^*$$

Axially Loaded Bar Problem

Strain energy density.

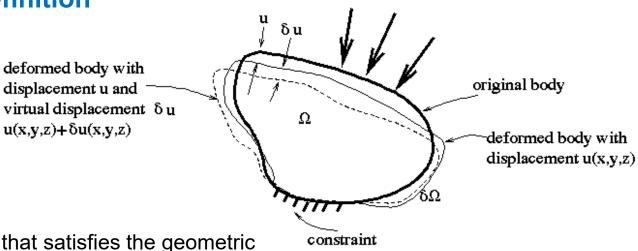
$$U_0 = \frac{1}{2}\sigma_x \varepsilon_x = \frac{1}{2}E\varepsilon^2 = \frac{1}{2}E\left(\frac{du}{dx}\right)^2$$



- ***** Strain energy. $U = \int_{V}^{L} \frac{1}{2} E\left(\frac{du}{dx}\right)^{2} dV = \int_{0}^{L} \int_{A}^{L} \frac{1}{2} E\left(\frac{du}{dx}\right)^{2} dA dx = \int_{0}^{L} \frac{EA}{2} \left(\frac{du}{dx}\right)^{2} dx$
- Complementary strain energy density. $U_0^* = \frac{1}{2}\sigma_x \varepsilon_x = \frac{1}{2}\frac{\sigma^2}{E} = \frac{1}{2E}\left(\frac{P}{A}\right)^2$
- $U^* = \int_{V} \frac{P^2}{2FA^2} dV = \int_{V} \frac{P^2}{2FA} dx$ Complementary strain energy.



1. Virtual Work — Definition



Load

- ** The set of configuration that satisfies the geometric constraints is called the set of admissible configurations.
- ** When mechanical system experiences such variations in its displacement configuration, it is said to undergo virtual displacements from its equilibrium configuration.
- ** The work done by the actual forces through a virtual displacement of the actual configuration is called virtual work.

$$\delta W = \int_{V} F \cdot \delta u \, dV$$

External work done subjected to body forces and surface forces.

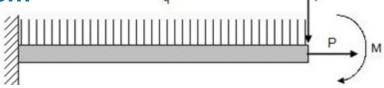
$$\delta W_E = -\int_V f_i \cdot \delta u_i \, dV - \int_{S_2} \hat{t}_i \cdot \delta u_i \, dS$$

 $\delta W_E = -\int\limits_V f_i \cdot \delta u_i \, dV - \int\limits_{S_2} \hat{t}_i \cdot \delta u_i \, dS$ Internal virtual work $\delta W_I = \int\limits_V \delta U_0 \, dV = \int\limits_V \delta \left(\int\limits_0^{\varepsilon_{ij}} \sigma_{ij} d\varepsilon_{ij}\right) dV = \int\limits_V \delta \left(\frac{1}{2} \sigma_{ij} \varepsilon_{ij}\right) dV = \int\limits_V \sigma_{ij} \delta \varepsilon_{ij} \, dV$



1. Virtual Work - Cantilever Beam Problem

Displacements
$$u = u_0 - z \frac{dw_0}{dx}$$
; $w = w_0$



$$\mathcal{E}_{x} = \frac{\partial u}{\partial x} = \frac{du_{0}}{dx} - z \frac{d^{2}w_{0}}{\partial x^{2}} \qquad \rightarrow \qquad \delta \mathcal{E}_{x} = \frac{d\delta u_{0}}{dx} - z \frac{d^{2}\delta w_{0}}{\partial x^{2}}$$

• Stress resultants
$$N = \int_A \sigma_x dA$$
 $M = \int_A \sigma_x z dA$

External virtual work

$$\delta W_{E} = -\int_{V} f_{i} \cdot \delta u_{i} \, dV - \int_{S_{2}} \hat{t}_{i} \cdot \delta u_{i} \, dS = -\int_{0}^{L} \int_{A} (f \delta u + q \delta w) dA \, dx - P \delta u(L) - F \delta w(L)$$

$$= -\int_{0}^{L} (f \delta u_{0} + q \delta w_{0}) \, dx - P \delta u_{0}(L) - F \delta w_{0}(L)$$

Internal virtual work

$$\delta W_{I} = \int_{V} \sigma_{ij} \delta \varepsilon_{ij} \, dV = \int_{0}^{L} \int_{A} \sigma_{x} \delta \varepsilon_{x} dA \, dx = \int_{0}^{L} \int_{A} \sigma_{x} \left(\frac{d \delta u_{0}}{dx} - z \frac{d^{2} \delta w_{0}}{\partial x^{2}} \right) dA \, dx = \int_{0}^{L} \left[N \frac{d \delta u_{0}}{dx} - M \frac{d^{2} \delta w_{0}}{\partial x^{2}} \right] dx$$

Total virtual work

$$\delta W = \delta W_I + \delta W_E = \int_0^L \left[N \frac{d\delta u_0}{dx} + M \left(\frac{-d^2 \delta w_0}{\partial x^2} \right) - f \delta u_0 - q \delta w_0 \right] dx - P \delta u_0(L) - F \delta w_0(L)$$



1. Virtual Work - Complementary Virtual Work

The work done by the virtual forces through an actual displacement is called complementary virtual work.

$$\delta W^* = \int_V \delta F \cdot u \, dV$$

External work done subjected to body forces and surface forces.

$$\delta W_E^* = -\int_V \delta f_i \cdot u_i \, dV - \int_{S_1} \delta t_i \cdot \hat{u}_i \, dS$$

Internal Complementary Virtual Work

$$\delta W_I^* = \int_V \delta U_0^* dV = \int_V \delta \left(\int_0^{\sigma_{ij}} \varepsilon_{ij} d\sigma_{ij} \right) dV = \int_V \delta \left(\frac{1}{2} \sigma_{ij} \varepsilon_{ij} \right) dV = \int_V \varepsilon_{ij} \delta \sigma_{ij} dV$$

2. Calculus of Variation — Definition

- Calculus of variations is a field of mathematical analysis that deals with maximizing or minimizing functionals, which are mappings from a set of functions to the real numbers.
- The interest is in extremal functions that make the functional attain a maximum or minimum value or stationary functions those where the rate of change of the functional is zero.
- A simple example of such a problem is to find the curve of shortest length connecting two points. If there are no constraints, the solution is obviously a straight line between the points. However, if the curve is constrained to lie on a surface in space, then the solution is less obvious, and possibly many solutions may exist.

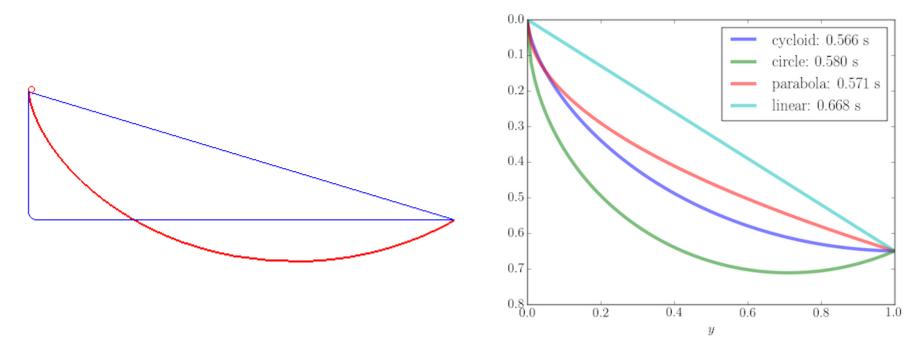
Historical Review

- Johann Bernoulli (1696): Raised Brachistochrone curve
- Leonhard Euler (1733): Elaborate the subject for Brachistochrone curve
- Joseph Louis Lagrange (1811): Euler-Lagrange Equation
- Simeon Poisson (1831): Contributes
- William Rowan Hamilton (1834): Hamilton's principle



2. Calculus of Variation - Brachistochrone curve

In mathematics, a brachistochrone curve, meaning shortest time, or curve of fastest descent, is the curve that would carry an idealized point-like body, starting at rest and moving along the curve, without friction, under constant gravity, to a given end point in the shortest time. For a given starting point, the brachistochrone curve is the same as the tautochrone curve.



The curve of fastest descent is not a straight or polygonal line (blue) but a cycloid (red).



2. Calculus of Variation - Variational Operator

- The first variation of u: δu
- Consider a function of dependent variable u and its derivative u'(x): F = F(x, u(x), u'(x))
- Consider the change in F for fixed x

$$\Delta F = F(x, u + \delta u, u' + \delta u') - F(x, u, u')$$

$$= F + \frac{\partial F}{\partial u} \delta u + \frac{\partial F}{\partial u'} \delta u' + \frac{1}{2!} \frac{\partial^2 F}{\partial u^2} (\delta u)^2 + \frac{1}{2!} \frac{\partial^2 F}{\partial u \partial u'} (\delta u) (\delta u') + \frac{1}{2!} \frac{\partial^2 F}{\partial u'^2} (\delta u')^2 + \dots - F$$

$$= \frac{\partial F}{\partial u} \delta u + \frac{\partial F}{\partial u'} \delta u' \left(+ \dots H.O.T \right)$$

• Comparison between δF and dF

$$\delta F = \frac{\partial F}{\partial u} \delta u + \frac{\partial F}{\partial u'} \delta u'$$

$$dF = \frac{\partial F}{\partial x} dx + \frac{\partial F}{\partial u} du + \frac{\partial F}{\partial u'} du'$$

 \bullet acts link d with respect to dependent variable (i.e., u(x) and u'(x)) when independent variable (i.e., x) is fixed.

2. Calculus of Variation — What is a Functional?

Functional: Functions of dependent variables, also function of other parameters

$$I(u) = \int_{a}^{b} F(x, u, u') dx$$

- Mathematically, functional *I(u)* is a mapping from a vector space *u* into the real number field; operator *I* mapping *u* into scalar.
- First variation of a functional $\delta I(u) = \delta \int_{a}^{b} F(x, u, u') dx = \int_{a}^{b} \delta F dx = \int_{a}^{b} \left[\frac{\partial F}{\partial u} \delta u + \frac{\partial F}{\partial u'} \delta u' \right] dx$
- ❖ A functional I(u) is said to have a minimum at u_0 if and only if $I(u) \ge I(u_0)$
- From elementary calculus, we know that a differentiable function f(x) has an extremum at a point xo only if (necessary condition): $\frac{df}{dx}\Big|_{x=x}$
- The sufficient condition for maximum: $\frac{d^2f}{dx^2} < 0$
- The sufficient condition for minimum: $\frac{d^2f}{dr^2} > 0$
- The functional I(u) is said to have a minimum at $u=u_0$ if it first variation $\delta I(u)=0$ and its second variation $\delta^2 I(u)$ is strongly positive at $u=u_0$.



2. Calculus of Variation – Euler-Lagrange Equations

- Determine the minimum of the functional $I(u) = \int_{a}^{b} F(x, u, u') dx$
- Subjected to the end conditions $u(a) = u_a, u(b) = u_b$
- Let $u = u_0 + \delta u$: $\delta u(a) = \delta u(b) = 0$
- ❖ Seek particular function *u* that makes the integral a minimum

$$0 = \delta I(u) = \int_{a}^{b} \left[\frac{\partial F}{\partial u} \delta u + \frac{\partial F}{\partial u'} \delta u' \right] dx = \int_{a}^{b} \left[\frac{\partial F}{\partial u} - \frac{d}{dx} \left(\frac{\partial F}{\partial u'} \right) \right] \delta u dx + \left[\frac{\partial F}{\partial u'} \delta u \right]_{a}^{b}$$

- Luler-Lagrange Equation $\frac{\partial F}{\partial u} \frac{d}{dx} \left(\frac{\partial F}{\partial u'} \right) = 0$ in a < x < b
- Essential Boundary Conditions (Displacement) Specifying dependent variables:

$$\delta u = 0 \ (u = \hat{u}) \ \text{at} \ x = a, b \ \text{thus} \ \frac{\partial F}{\partial u'}\Big|_{x=b} \delta u(b) - \frac{\partial F}{\partial u'}\Big|_{x=a} \delta u(a) = 0$$

Natural Boundary Conditions (Force) - Specifying the coefficients of dependent variables

$$\frac{\partial F}{\partial u'} = 0$$
 at $x = a, b$



2. Calculus of Variation – Euler-Lagrange Equations

- **.*** Either u(a) or $\frac{\partial F}{\partial u'}\Big|_{x=a}$ is specified.**.*** Either u(b) or $\frac{\partial F}{\partial u'}\Big|_{x=b}$ is specified.

Types of Boundary Value Problems

- All Essential Boundary Conditions: Dirichlet Boundary Value Problem
- All Natural Boundary Conditions: Neumann Boundary Value Problem
- Essential and Natural Boundary Conditions: Mixed Boundary Value Problem

2. Calculus of Variation - Axially-loaded Bar Problem

❖ Internal Energy (Strain Energy):

$$W_{I} = U = \int_{0}^{L} \frac{EA}{2} \left(\frac{du}{dx}\right)^{2} dx$$

***** External Energy: $W_E = -Pu(L)$

P P σ

• Total Work (Functional):
$$W = W_I + W_E = \int_0^L \frac{EA}{2} \left(\frac{du}{dx}\right)^2 dx - Pu(L) = I(u)$$

Minimization (first variation of a functional - mathematically or virtual work - physically)

$$\delta I(u) = \delta W = \int_{0}^{L} EA \frac{du}{dx} \frac{d\delta u}{dx} dx - P \delta u(L)$$

$$0 = -\int_{0}^{L} \frac{d}{dx} \left(EA \frac{du}{dx} \right) \delta u \, dx + \left[\left(EA \frac{du}{dx} - P \right) \delta u \right]_{x=L} + \left[\left(EA \frac{du}{dx} \right) \delta u \right]_{x=0}$$

• Euler Equations
$$-\frac{d}{dx} \left(EA \frac{du}{dx} \right) = 0$$

Boundary Conditions

At
$$x = 0$$
: $u = 0$ (EBC) $\rightarrow \delta u = 0 \rightarrow \left(EA\frac{du}{dx}\right)\delta u = 0$

At
$$x = L$$
: $u = unknown \rightarrow \delta u = arbitrary \rightarrow \left(EA\frac{du}{dx} - P\right)\delta u = 0 \rightarrow P = EA\frac{du}{dx}$ (NBC)



2. Calculus of Variation – Axial Bar with Spring Problem



An elastic bar fixed at the left end, spring supported at the right end, and subjected to distributed load. Total work is

$$\Pi(u) = \int_{0}^{L} \left[\frac{EA}{2} \left(\frac{du}{dx} \right)^{2} - fu \right] dx + \frac{k}{2} u (L)^{2}$$

The first variation is given by

$$\delta \Pi(u) = \int_{0}^{L} \left(EA \frac{du}{dx} \frac{d\delta u}{dx} - f \delta u \right) dx + ku(L) \delta u(L)$$

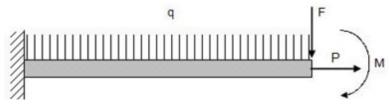
Euler Equation (after using the integration by parts)

$$-\frac{d}{dx}\left(EA\frac{du}{dx}\right) - f = 0, \quad 0 < x < L$$

Natural Boundary Condition (NBC)

$$EA\frac{du}{dx} + ku(L) = 0$$
 at $x = L$

2. Calculus of Variation — Cantilever Beam Problem



First variation of the functional (refer to page 5)

$$\delta W = \int_{0}^{L} \left[N \frac{d\delta u}{dx} + M \left(\frac{-d^{2}\delta w}{\partial x^{2}} \right) - f \delta u - q \delta w \right] dx - P \delta u(L) - F \delta w(L) = 0$$

u and w now represent mid-plane displacements.

- Stress resultants $N = \int_A \sigma_x dA = EA \frac{du}{dx}; \qquad M = \int_A \sigma_x z dA = -EI \frac{d^2w}{dx^2}$
- Integration by parts

$$\delta W = -\int_{0}^{L} \left[\frac{d}{dx} \left(EA \frac{du}{dx} \right) \delta u + \frac{d}{dx} \left(EI \frac{d^{2}w}{dx^{2}} \right) \frac{d\delta w}{dx} + f \delta u + q \delta w \right] dx$$

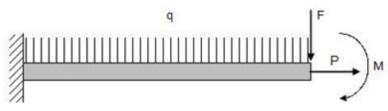
$$+ \left[\left(EA \frac{du}{dx} \right) \delta u \right]_{0}^{L} + \left[\left(EI \frac{d^{2}w}{dx^{2}} \right) \frac{d\delta w}{dx} \right]_{0}^{L} - P \delta u(L) - F \delta w(L) = 0$$

$$\delta W = -\int_{0}^{L} \left[\frac{d}{dx} \left(EA \frac{du}{dx} \right) \delta u - \frac{d^{2}}{dx^{2}} \left(EI \frac{d^{2}w}{dx^{2}} \right) \delta w + f \delta u + q \delta w \right] dx$$

$$+ \left[\left(EA \frac{du}{dx} \right) \delta u + \left(EI \frac{d^{2}w}{dx^{2}} \right) \frac{d\delta w}{dx} - \frac{d}{dx} \left(EI \frac{d^{2}w}{dx^{2}} \right) \delta w \right]_{0}^{L} - P \delta u(L) - F \delta w(L) = 0$$



2. Calculus of Variation — Cantilever Beam Problem



Euler Equations

$$\frac{d}{dx}\left(EA\frac{du}{dx}\right) + f = 0$$
$$-\frac{d^2}{dx^2}\left(EI\frac{d^2w}{dx^2}\right) + q = 0$$

Boundary Conditions

At
$$x = 0$$

Either
$$\left(EA\frac{du}{dx}\right)$$
 or δu

Either
$$\left(EI\frac{d^2w}{dx^2}\right)$$
 or $\frac{d\delta w}{dx}$

Either
$$\frac{d}{dx} \left(EI \frac{d^2 w}{dx^2} \right)$$
 or δw

At x = L

Either
$$\left(EA\frac{du}{dx}\right) - P$$
 or δu

Either
$$\left(EI\frac{d^2w}{dx^2}\right)$$
 or $\frac{d\delta w}{dx}$

Either
$$\frac{d}{dx} \left(EI \frac{d^2 w}{dx^2} \right) + F$$
 or δw

3. Hamilton's Principle - Principle of Virtual Displacements

A continuous body is in equilibrium if and only if the virtual work of all forces acting on the body is zero in virtual displacement.

$$\delta W = \delta W_I + \delta W_E = 0$$

Applicable to any continuous bodies (elastic and inelastic)

$$\int_{V} \sigma_{ij} \cdot \delta \varepsilon_{ij} \, dV - \int_{V} f_{i} \cdot \delta u_{i} \, dV - \int_{S_{2}} \hat{t}_{i} \cdot \delta u_{i} \, dS = 0$$

• Divergence theorem $\int_{\Omega} \nabla \cdot \mathbf{A} \, d\Omega = \oint_{\Gamma} \hat{\mathbf{n}} \cdot \mathbf{A} \, ds$

$$\int_{V} \sigma_{ij} \delta \varepsilon_{ij} dV = \int_{V} \sigma_{ij} \delta u_{i,j} dV = -\int_{V} \sigma_{ij,j} \delta u_{i} dV + \int_{V} (\sigma_{ij} \delta u_{i})_{,j} dV = -\int_{V} \sigma_{ij,j} \delta u_{i} dV + \oint_{S} n_{j} \sigma_{ij} \delta u_{i} dS$$

The boundary integral can be expressed as the sum of two integral, one on S1 (EBC) and the other on S2 (NBC). The integral on S1 is zero.

$$-\int_{V} \left(\sigma_{ij,j} + f_{i}\right) \delta u_{i} dV + \oint_{S_{2}} \left(n_{j} \sigma_{ij} - \hat{t}_{i}\right) \delta u_{i} dS = 0$$

Equilibrium Equations and Stress Boundary Conditions

$$\sigma_{ii,j} + f_i = 0$$
 in V

$$n_i \sigma_{ii} - \hat{t}_i = 0$$
 in S_2



3. Hamilton's Principle – Principle of Virtual Forces

The strains and displacements in a deformable body are compatible and consistent with the constraints if and only if the total complementary virtual work is zero

$$\delta W^* = \delta W_I^* + \delta W_E^* = 0$$

Applicable to any continuous bodies (elastic and inelastic)

$$\int_{V} \varepsilon_{ij} \cdot \delta \sigma_{ij} \, dV - \int_{V} \delta f_{i} \cdot u_{i} \, dV - \int_{S_{1}} \delta t_{i} \cdot \hat{u}_{i} \, dS = 0$$

• Equilibrium Equations and Stress BCs (page 17) $\delta f_i = -\delta \sigma_{ij,j}$; $\delta t_i = n_j \delta \sigma_{ji}$

$$\int_{V} \varepsilon_{ij} \delta \sigma_{ij} dV + \int_{V} \delta \sigma_{ij,j} u_{i} dV - \int_{S_{1}} \delta \sigma_{ji} n_{j} \hat{u}_{i} dS = 0$$

Integration by parts
$$\leftrightarrow \int_{V} \varepsilon_{ij} \delta \sigma_{ij} \, dV + \int_{V} \left(\delta \sigma_{ij} u_{i} \right)_{,j} \, dV - \int_{V} \delta \sigma_{ij} u_{i,j} \, dV - \int_{S_{1}} \delta \sigma_{ji} n_{j} \hat{u}_{i} \, dS = 0$$

Divergence theorem
$$\leftrightarrow \int_{V_{\Sigma}} \mathcal{E}_{ij} \delta \sigma_{ij} dV + \int_{S_1} \delta \sigma_{ij} u_i n_j dS - \int_{V} \delta \sigma_{ij} u_{i,j} dV - \int_{S_1} \delta \sigma_{ji} n_j \hat{u}_i dS = 0$$

Symmetry feature
$$\leftrightarrow \int_{V}^{V} \left[\varepsilon_{ij} - \frac{1}{2} \left(u_{i,j} + u_{j,i} \right) \right] \delta \sigma_{ij} dV + \int_{S_1} \left(u_i - \hat{u}_i \right) n_j \delta \sigma_{ij} dS = 0$$

Strain-displacement Equations and Displacement Boundary Conditions

$$\varepsilon_{ij} - \frac{1}{2} \left(u_{i,j} + u_{j,i} \right) = 0 \quad \text{in} \quad V$$

$$u_i - \hat{u}_i = 0 \quad \text{on} \quad S_1$$



3. Hamilton's Principle – Principle of Potential Energy

Principle of Total Potential Energy

A special case of the principle of virtual work that deals with elastic bodies is known as the principle of total potential energy.

$$\delta \Pi = \delta U + \delta V = 0$$

with

$$\delta U = \delta W_I, \quad \delta V = \delta W_E$$

Principle of Complementary Potential Energy

A special case of the principle of complementary virtual work that deals with elastic bodies is known as the principle of complementary potential energy.

$$\delta \Pi^* = \delta U^* + \delta V^* = 0$$

with

$$\delta U^* = \delta W_I^*, \quad \delta V^* = \delta W_E^*$$

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