

# Notes on regrasping as an underactuated pivot

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July 24, 2014

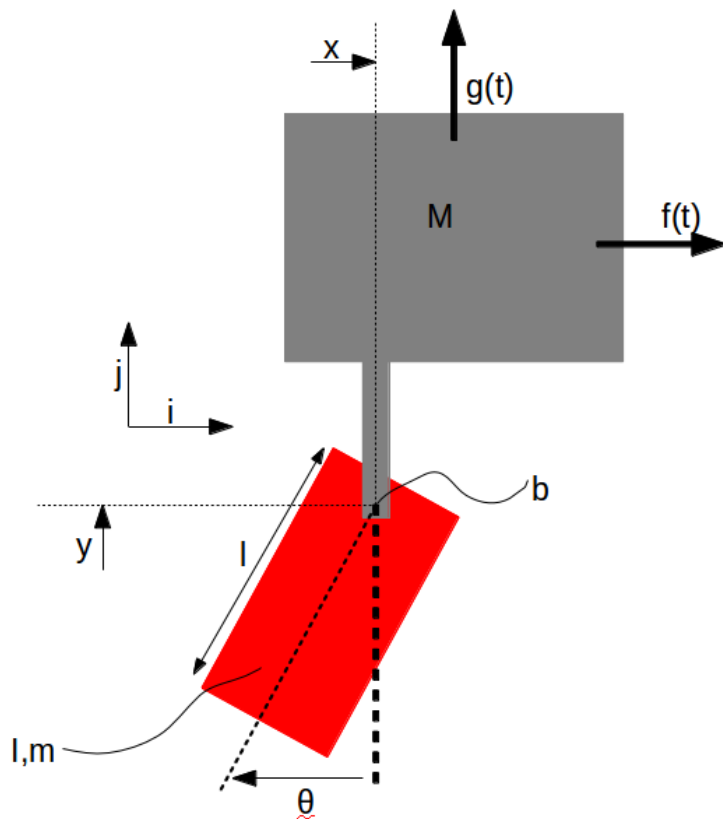


Figure 1: A rough sketch of the system. The hand is in gray with gripper coming down and the block in red.

As a first pass at the problem of pivoting a block into any angle using the dynamics of the system, I am approaching it as an underactuated system where the grasp acts as a pivot joint with a certain rotation damping due to the friction of the grasp,  $b$ . The block has a mass  $m$ , moment of inertia about the block's center of mass  $I$ , and a length  $l$ . The hand has a mass,  $M$  and its can move in the  $\hat{i}$  and  $\hat{j}$  directions as functions  $f(t)$  and  $g(t)$ .

# 1 Generalized Coordinate System and Forces

There are three degrees of freedom here (assuming no motion in the  $\hat{k}$  is relevant), which are  $x, y$ , and  $\theta$ . Positive  $x$  points to the right,  $y$  up, and  $\theta$  clockwise measured from the downward position.

$$\zeta_j : x, y, \theta$$

with the variation  $\zeta_j : \delta x, \delta y, \delta \theta$

The generalized forces,  $\Xi_j$  can be obtained from the work where

$$\delta W = \sum_{i=1}^n \mathbf{F}_i \cdot \delta \mathbf{r}_i = \sum_{j=1}^n \Xi_j \delta \zeta_j$$

Nonconservative forces from the inputs  $g(t)$  and  $f(t)$  and the damping  $b$  around the grasp result in,

$$\delta W = f(t)\delta x + g(t)\delta y - b\dot{\theta}\delta\theta$$

So we get:

$$\Xi_x = f(t)\Xi_y = g(t)\Xi_\theta = -b\dot{\theta}$$

## 2 Kinetic Energy

The kinetic energy of the hand (the cart in simple cases):

$$K_{hand} = \frac{1}{2}M\mathbf{v}^2$$

Where  $M$  is the mass of the hand and  $\mathbf{v}$  is a planar velocity vector of the hand (lets just assume  $x, y$  for now since movement in the same axis as the pivot axis doesnt do anything).

The kinetic energy for the block:

$$K_{block} = \frac{1}{2}m\mathbf{v}_c^2 + \frac{1}{2}I\omega^2$$

where  $v_c$  is the velocity of the center of mass of the block,  $m$  is the mass of the block,  $I$  is the moment of inertia around the block's center of mass, and  $\omega$  is the angular velocity.

The position vector can then be written,

$$\mathbf{r}_c = (x - l \sin(\theta))\hat{i} + (y - l \cos(\theta))\hat{j}$$

$$\mathbf{v}_c = \frac{d\mathbf{r}_c}{dt} = (\dot{x} - l \cos(\theta)\dot{\theta})\hat{i} + (\dot{y} + l \sin(\theta)\dot{\theta})\hat{j}$$

Then,  $\omega = \dot{\theta}$

So plugging in we get,

$$\begin{aligned} K_{block} &= \frac{1}{2}m(\dot{x}^2 - 2\dot{x}l\cos(\theta)\dot{\theta} + l^2\cos^2(\theta)\dot{\theta}^2 + \dot{y}^2 + 2\dot{y}l\sin(\theta)\dot{\theta} + l^2\sin^2(\theta)\dot{\theta}^2) + \frac{1}{2}I\dot{\theta}^2 \\ &= \frac{1}{2}m(\dot{x}^2 - 2\dot{x}l\cos(\theta)\dot{\theta} + \dot{y}^2 + 2\dot{y}l\sin(\theta)\dot{\theta} + l^2\dot{\theta}^2) + \frac{1}{2}I\dot{\theta}^2 \end{aligned}$$

Then our total kinetic energy is,

$$K = K_{hand} + K_{block} = \frac{1}{2}M(\dot{x}^2 + \dot{y}^2) + \frac{1}{2}m(\dot{x}^2 - 2\dot{x}l\cos(\theta)\dot{\theta} + \dot{y}^2 + 2\dot{y}l\sin(\theta)\dot{\theta} + l^2\dot{\theta}^2) + \frac{1}{2}I\dot{\theta}^2$$

### 3 Potential Energy

$$P = -mg(y + l)\cos(\theta)$$

### 4 Lagrangian

From the kinetic and potential energies, the lagrangian is given by

$$L = K - P$$

which becomes

$$L = \frac{1}{2}M(\dot{x}^2 + \dot{y}^2) + \frac{1}{2}m(\dot{x}^2 - 2\dot{x}l\cos(\theta)\dot{\theta} + \dot{y}^2 + 2\dot{y}l\sin(\theta)\dot{\theta} + l^2\dot{\theta}^2) + \frac{1}{2}I\dot{\theta}^2 + mg(y + l)\cos(\theta)$$

#### 4.1 More Lagrange Shit

The equations for x,

$$\begin{aligned}\Xi_x &= \frac{d}{dt}\left(\frac{\partial L}{\partial \dot{x}}\right) - \frac{\partial L}{\partial x} \\ \frac{d}{dt}(M\dot{x} + m\dot{x} - ml\cos(\theta)\dot{\theta}) &= f(t) \\ (M + m)\ddot{x} - ml\cos(\theta)\ddot{\theta} + ml\sin(\theta)\dot{\theta}^2 &= f(t)\end{aligned}$$

The same for y,

$$\begin{aligned}\Xi_y &= \frac{d}{dt}\left(\frac{\partial L}{\partial \dot{y}}\right) - \frac{\partial L}{\partial y} \\ \frac{d}{dt}(M\dot{y} + m\dot{y} + ml\sin(\theta)\dot{\theta}) - mg\cos(\theta) &= g(t) \\ (M + m)\ddot{y} + ml\sin(\theta)\ddot{\theta} - ml\cos(\theta)\dot{\theta}^2 - mg\cos(\theta) &= g(t)\end{aligned}$$

And for  $\theta$ ,

$$\begin{aligned}\Xi_\theta &= \frac{d}{dt}\left(\frac{\partial L}{\partial \dot{\theta}}\right) - \frac{\partial L}{\partial \theta} \\ \frac{d}{dt}(-m\dot{x}l\cos(\theta) + m\dot{y}l\sin(\theta) + ml^2\dot{\theta} + I\dot{\theta}) - (ml\dot{x}\sin(\theta)\dot{\theta} + ml\dot{y}\cos(\theta)\dot{\theta} - mg\sin(\theta)) &= -b\dot{\theta} \\ (ml^2 + I)\ddot{\theta} - ml\dot{x}\cos(\theta) + ml\dot{x}\sin(\theta)\dot{\theta} + ml\ddot{y}\sin(\theta) + ml\dot{y}\cos(\theta)\dot{\theta} - (ml\dot{x}\sin(\theta)\dot{\theta} + ml\dot{y}\cos(\theta)\dot{\theta} - mg\sin(\theta)) &= -b\dot{\theta}\end{aligned}$$

where  $b$  is a rotational damping coefficient around the grasp.

Now we have to solve for  $f(t)$  (motion in the  $\hat{i}$  direction) and  $g(t)$  (motion in the  $\hat{j}$  direction)

$$(M + m)\ddot{x} - ml\cos(\theta)\ddot{\theta} + ml\sin(\theta)\dot{\theta}^2 = f(t) \tag{1}$$

$$(M + m)\ddot{y} + ml\sin(\theta)\ddot{\theta} - ml\cos(\theta)\dot{\theta}^2 - mg\cos(\theta) = h(t) \tag{2}$$

$$(ml^2 + I)\ddot{\theta} + b\dot{\theta} - ml\dot{x}\cos(\theta) + ml\ddot{y}\sin(\theta) + mg\sin(\theta) = 0 \tag{3}$$

## 5 Energy Regulation using PFLs

### 5.1 Collocated Partial Feedback Linearization (PFL)

Our goal is for  $\ddot{x} = \ddot{x}_d$  and  $\ddot{y} = \ddot{y}_d$ . We can solve for  $\ddot{\theta}$  using 3

$$\ddot{\theta} = \frac{1}{ml^2}(-mgs - mls\ddot{y} + mlc\ddot{x} - b\dot{\theta})$$

Where  $s = \sin(\theta)$  and  $c = \cos(\theta)$ .

If we plug this into 2

$$(M + m)\ddot{y} + mls\left(\frac{1}{ml^2}(-mgs - mls\ddot{y} + mlc\ddot{x} - b\dot{\theta})\right) - mlc\dot{\theta}^2 - mgc = h(t)$$

$$(M + m)\ddot{y} + \frac{s}{l}(-mgs - mls\ddot{y} + mlc\ddot{x} - b\dot{\theta}) - mlc\dot{\theta}^2 - mgc = h(t)$$

$$\ddot{y} = \frac{1}{M + mc^2}\left(h(t) + \frac{mgs^2}{l} - msc\ddot{x} + \frac{bs\dot{\theta}}{l} + mlc\dot{\theta}^2 + mgc\right)$$

Then into 1

$$(M + m)\ddot{x} - ml\cos(\theta)\ddot{\theta} + ml\sin(\theta)\dot{\theta}^2 = f(t)$$

etc. etc. etc.

### 5.2 Energy Regulation

If  $\ddot{x} = \bar{u}$  and  $\ddot{y} = \bar{v}$ , then

$$\ddot{\theta} = \frac{1}{ml^2}(-mgs - mls\bar{v} + mlc\bar{u} - b\dot{\theta})$$

From before our energy is given by,

$$E = \frac{1}{2}ml^2\dot{\theta}^2 - mg(y + l)c$$

$$\dot{E} = ml^2\dot{\theta}\ddot{\theta} + mg(y + l)s\dot{\theta}$$

$$\dot{E} = ml^2\dot{\theta}\left(\frac{1}{ml^2}(-mgs - mls\bar{v} + mlc\bar{u} - b\dot{\theta})\right) + mg(y + l)s\dot{\theta}$$

$$\dot{E} = \dot{\theta}(-mgs - mls\bar{v} + mlc\bar{u} - b\dot{\theta}) + mg(y + l)s\dot{\theta}$$

So to increase the energy, we can chose and  $\bar{u}$  and  $\bar{v}$  to make this expression positive. For example,

$$\bar{u} = kmlc\dot{\theta}\bar{E}$$

$$\bar{v} = -kmls\dot{\theta}\bar{E}$$

Where  $\bar{E}$  is the difference between the desired energy and the actual energy.

### 5.3 now wat

We have two problems: we have no feedback for  $\dot{\theta}$ , and since our desired energy is not at an equilibrium point, it won't have zero kinetic energy, so we don't really know what  $\bar{E}$  is.

The first is easier to deal with. If we just put in just enough energy to get to  $\theta$  before it begins decreasing, we will be at zero velocity at the apex of a path arc at  $\theta$ . So our  $E_d = mg(y + l)\cos(\theta)$ .

To handle no feedback (which is inherent in this problem since the block is always connected at the fingertips where there is no sensing normally), we can predict what  $\theta$  is ideally doing based on the equations of motion.

Let's plug our expression for  $\ddot{\theta}$  into 1 (or we could use 2)

$$\ddot{\theta} = \frac{1}{ml^2}(-mgs - mls\bar{v} + mlc\bar{u} - b\dot{\theta})$$

We know that  $f(t) = \bar{u}$  and that  $\ddot{x} = \frac{f(t)}{m} = klc\dot{\theta}$ . Similarly for  $\ddot{y}$

$$\ddot{\theta} = \frac{1}{ml^2}(-mgs - mls(-kls\dot{\theta}) + mlc(klc\dot{\theta}) - b\dot{\theta})$$

$$\ddot{\theta} = \frac{1}{ml^2}(-mgs + kml^2\dot{\theta} - b\dot{\theta})$$

From 1,  $(M + m)\ddot{x} - ml \cos(\theta)\ddot{\theta} + ml \sin(\theta)\dot{\theta}^2 = f(t)$

$$(M + m)(klc\dot{\theta}) - ml \cos(\theta)(\frac{1}{ml^2}(-mgs + kml^2\dot{\theta} - b\dot{\theta})) + ml \sin(\theta)\dot{\theta}^2 = kmlc\dot{\theta}$$

$$(M - m)(klc\dot{\theta}) + \frac{cb\dot{\theta}}{l} + \frac{mgsc}{l} + mls\dot{\theta}^2 = 0 \quad (4)$$

From 2,  $(M + m)\ddot{y} + ml \sin(\theta)\ddot{\theta} - ml \cos(\theta)\dot{\theta}^2 - mg \cos(\theta) = h(t)$

$$(M + m)(-kls\dot{\theta}) + ml \sin(\theta)(\frac{1}{ml^2}(-mgs + kml^2\dot{\theta} - b\dot{\theta})) - ml \cos(\theta)\dot{\theta}^2 - mg \cos(\theta) = -kmls\dot{\theta}$$

$$(m - M)(kls\dot{\theta}) - \frac{bs\dot{\theta}}{l} - \frac{mgs^2}{l} - mls\dot{\theta}^2 - mgc = 0 \quad (5)$$

To solve for  $\theta$  and  $\dot{\theta}$ , we can multiply 4 by  $\cos(\theta)$ , 5 by  $\sin(\theta)$ , and add.

$$(M - m)(klc^2\dot{\theta}) + \frac{c^2b\dot{\theta}}{l} + \frac{mgsc^2}{l} + mls\dot{\theta}^2 = 0$$

$$(m - M)(kls^2\dot{\theta}) - \frac{bs^2\dot{\theta}}{l} - \frac{mgs^3}{l} - mls\dot{\theta}^2 - mgsc = 0$$

Giving

$$(M - m)(kl\dot{\theta}) + \frac{b\dot{\theta}}{l} + \frac{mgs}{l} + mgsc = 0$$

Then we can solve for  $\dot{\theta}$  and integrate to get  $\theta$

$$\dot{\theta} = \frac{1}{(M - m)kl + \frac{b}{l}}(-mgsc - \frac{mgs}{l})$$

$$\theta = \frac{1}{(M - m)kl + \frac{b}{l}}(-\frac{mgc^2}{2} + \frac{mgc}{l})$$

If we substitute these expressions back into our control laws  $\bar{u}$  and  $\bar{v}$ , we get

$$\bar{u} = \frac{kml}{(M - m)kl + \frac{b}{l}} * c(-mgsc - \frac{mgs}{l})$$

$$\bar{v} = \frac{-kml}{(M - m)kl + \frac{b}{l}} * s(-mgsc - \frac{mgs}{l})$$

Ignoring constants those expressions roughly look like

$$\bar{u} = \cos(\theta) * (-\sin(\theta) \cos(\theta) - \sin(\theta))$$

$$\bar{v} = \sin(\theta) * (-\sin(\theta) \cos(\theta) - \sin(\theta))$$

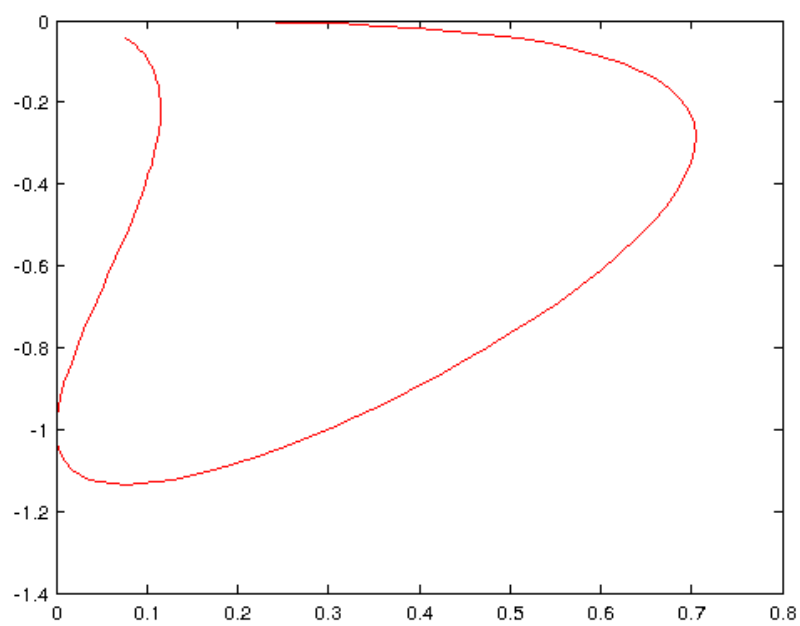


Figure 2