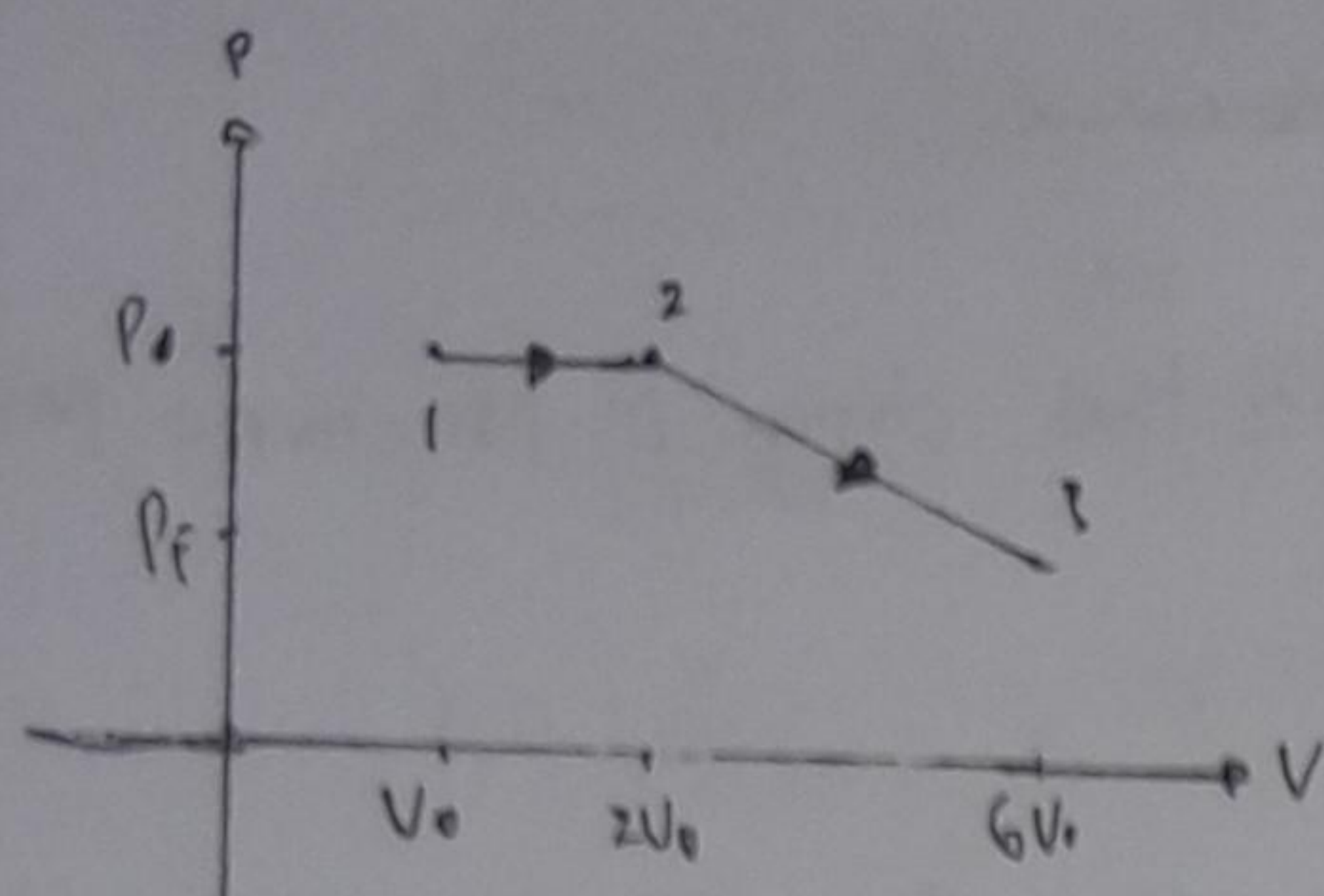
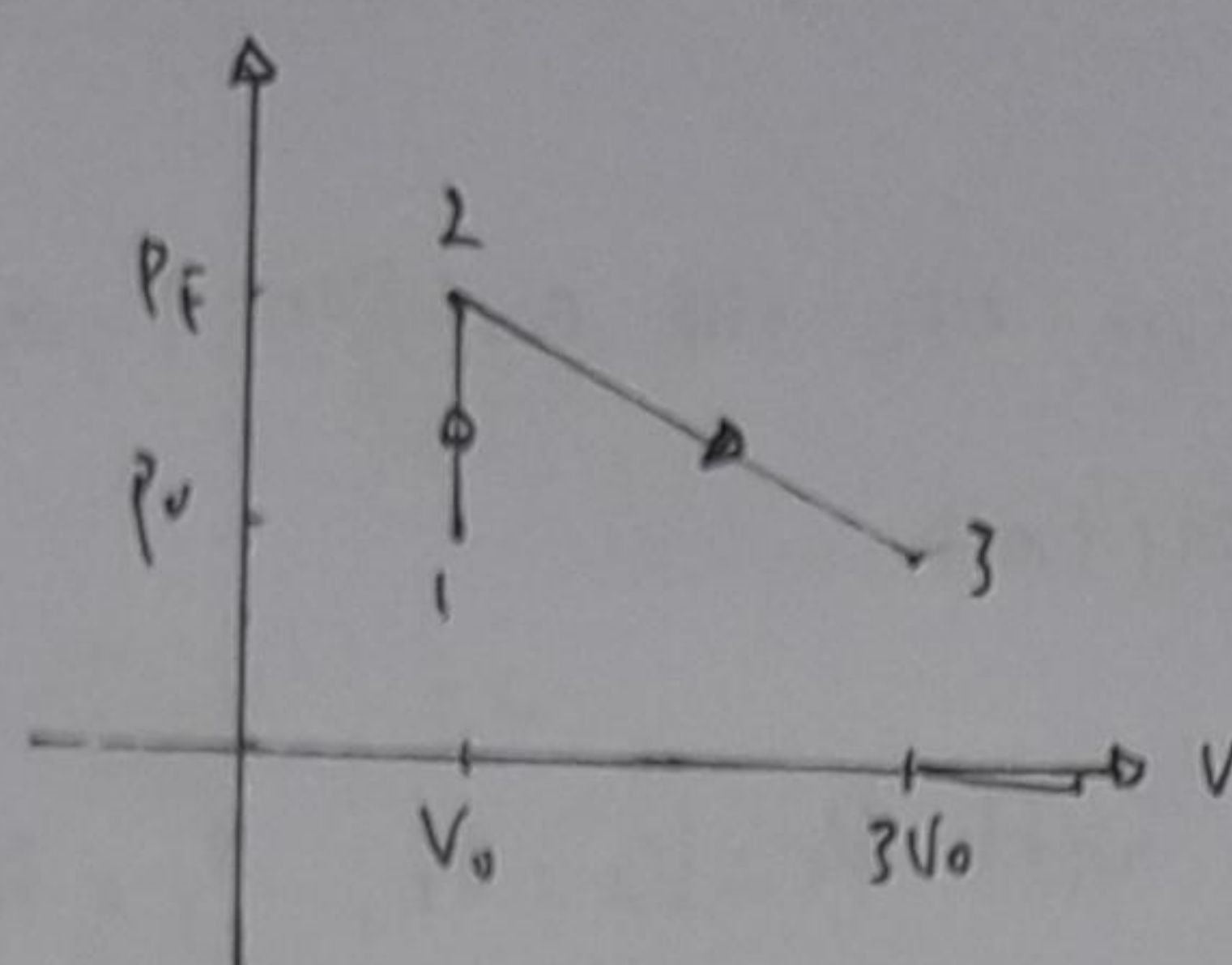


HW 2 FFKG

Problem 1



Process A



Process B

An ideal gas (with number of moles n and molar specific heat C_v) inside a sealed container is expanded following two different processes shown in the figure above. Express only in terms of n , C_v , T_0 , V_0 , and R .

A. Determine the value of P_f and T_f in these processes!

* Process A.

We will use the $PV = nRT$ equation. Since n and R are constant, we can simply use the $\frac{P \cdot V}{T}$ equation to compare it with another position.

→ For process A, Compare the 1 and 2 position to find T_f .

$$\frac{P_1 V_1}{T_1} = \frac{P_2 V_2}{T_2}, \text{ since } P_1 = P_0 = P_2, V_1 = V_0, V_2 = 2V_0 \text{ and we can let } T_1 = T_0, T_2 = T_f.$$

$$\frac{P_0 V_0}{T_0} = \frac{P_0 \cdot 2V_0}{T_f} \Rightarrow \underline{T_f = 2T_0} \text{ So, } T_f \text{ is equal to } 2T_0. \text{ Isobaric process occurs in position 1 and 2.}$$

→ To find P_f , we can compare the 2 and 3 position.

$$\frac{P_2 V_2}{T_2} = \frac{P_3 V_3}{T_3}, \text{ since } \text{adiabatic process occurs. } P_2 = P_0, P_3 = P_f, V_2 = 2V_0, V_3 = 6V_0, T_2 = 2T_0, T_3 = T_0$$

$$\frac{P_0 \cdot 2V_0}{2T_0} = \frac{P_f \cdot 6V_0}{T_0} \Rightarrow P_f = \frac{P_0}{3} \text{ So, } P_f \text{ is equal to } \frac{P_0}{3}. \text{ But, we can't express in terms of } P_0.$$

So, the P_f will be expressed by $P_2 V_3 = nRT_3$, with n and R constant

$$P_f \cdot 6V_0 = nRT_0 \Rightarrow P_f = \frac{nRT_0}{6V_0}$$

$$\underline{P_f = \frac{nRT_0}{6V_0}}$$

* Process B.

→ We can use position 2 and 3 to find P_F . since that change is isothermal process, The temperature is constant.

$$\frac{P_2 \cdot V_2}{T_2} = \frac{P_3 \cdot V_3}{T_3}, \text{ with } P_2 = P_F, P_3 = P_0, V_2 = V_0, V_3 = 3V_0, T_2 = T_3 = T_F.$$

$$\frac{P_F \cdot V_0}{T_F} = \frac{P_0 \cdot 3V_0}{T_F} \Rightarrow P_F = 3P_0. \text{ In other form, we can write}$$

→ To find T_F , we can use the position 1 and 2. since that change is isochoric process, The volume is constant

$$\frac{P_1 \cdot V_1}{T_1} = \frac{P_2 \cdot V_2}{T_2}, \text{ with } V_1 = V_2 = V_0, P_1 = P_0, P_2 = P_F, T_1 = T_0, T_2 = T_F$$

$$\frac{P_0 \cdot V_0}{T_0} = \frac{P_F \cdot V_0}{T_F} \Rightarrow \frac{P_0}{T_0} = \frac{P_F}{T_F}. \text{ From previous equation, we know that } P_F = 3P_0.$$

$$\frac{P_0}{T_0} = \frac{3P_0}{T_F} \Rightarrow \underline{T_F = 3T_0}.$$

→ Since P_F is expressed in term of P_0 . we can express it in other form.

$$P_2 \cdot V_2 = n R T_2, \text{ with } P_2 = P_0, V_2 = V_0, T_2 = T_F = 3T_0$$

$$P_F \cdot V_0 = n R 3T_0$$

$$P_F = \frac{n R 3T_0}{V_0}$$

$$\underline{\underline{\frac{n R 3T_0}{V_0}}}$$

B. Determine the amount of heat Q added into the system.

* Process A.

→ Since the process 2 and 3 is adiabatic process, there is no change in heat of the system or $\Delta Q = 0$.

→ For the position 1 and 2. the process is isochoric process which means there is some amount of heat Q added. we can calculate by

$$Q = n (C_v + R) \cdot \Delta T$$

$$Q = n (C_v + R) \cdot (T_F - T_0), \text{ since } T_F = 3T_0, T_F - T_0 \text{ is equal to } 2T_0$$

$$\underline{Q = n (C_v + R) \cdot 2T_0}.$$

So, the amount of heat Q added to the system is equal to $n(C_v + R) \cdot 2T_0$, as shown in the equation above.

* Process B

→ the position 1 and 2 is isochoric process. We know that there is some heat added by calculating

$$Q_{12} = n \cdot C_V \cdot \Delta T$$

$$Q_{12} = n \cdot C_V \cdot (T_F - T_0) \text{ , since } T_F = 3T_0, T_F - T_0 = 2T_0.$$

$$Q_{12} = n \cdot C_V \cdot 2T_0$$

→ The position 2 and 3 is isothermal process. We can calculate the amount of heat added by

$$Q_{23} = nRT_F \ln \frac{V_F}{V_0} \text{ , since } V_F = 3V_0, \text{ and } T_F = 3T_0$$

$$Q_{23} = 3nRT_0 \ln \frac{3V_0}{V_0}$$

$$Q_{23} = 3nRT_0 \ln 3$$

→ Sum up both Q_{12} and Q_{23} , we get the total amount of heat Q added.

$$Q = Q_{12} + Q_{23} = nC_V \cdot 2T_0 + 3nRT_0 \ln 3$$

$$Q = n \cdot T_0 (2C_V + 3R \ln 3)$$

Problem 2.

M_A, C_A, T_A	M_B, C_B, T_B
-----------------	-----------------

Metal block with mass M_A and initial temperature T_A touches another metal block with mass M_B and initial temperature T_B . Suppose that the specific heat of two metal are C_A and C_B .

* A. Determine the final temperature T_F of the two metal blocks!

→ when two different metal blocks with their respective mass, initial temperature, and specific heat touches, there will be thermal equilibrium with given equation $Q_A + Q_B = 0$

⇒ $M_A \cdot C_A \cdot \Delta T_A + M_B \cdot C_B \cdot \Delta T_B = 0$, where ΔT is the difference between initial temperature and equilibrium or final temperature.

$$M_A \cdot C_A (T_F - T_A) + M_B \cdot C_B (T_F - T_B) = 0$$

$$M_A \cdot C_A \cdot T_F - M_A \cdot C_A \cdot T_A + M_B \cdot C_B \cdot T_F - M_B \cdot C_B \cdot T_B = 0$$

$$T_F (M_A \cdot C_A + M_B \cdot C_B) = M_A \cdot C_A \cdot T_A + M_B \cdot C_B \cdot T_B$$

$$T_F = \frac{M_A \cdot C_A \cdot T_A + M_B \cdot C_B \cdot T_B}{M_A \cdot C_A + M_B \cdot C_B}$$

So, the final temperature is $T_F = \frac{M_A \cdot C_A \cdot T_A + M_B \cdot C_B \cdot T_B}{M_A \cdot C_A + M_B \cdot C_B}$

B. Determine the ΔT_A and ΔT_B !

$$\Delta T_A = T_F - T_A$$

We can substitute T_F from previous equation.

$$\begin{aligned} \Delta T_A &= \frac{M_A \cdot C_A \cdot T_A + M_B \cdot C_B \cdot T_B}{M_A \cdot C_A + M_B \cdot C_B} - T_A \\ &= \frac{M_A \cdot C_A \cdot T_A + M_B \cdot C_B \cdot T_B - M_A \cdot C_A \cdot T_A - M_B \cdot C_B \cdot T_A}{M_A \cdot C_A + M_B \cdot C_B} \\ &= \frac{M_B \cdot C_B \cdot T_B - M_B \cdot C_B \cdot T_A}{M_A \cdot C_A + M_B \cdot C_B} = \frac{M_B \cdot C_B \cdot (T_B - T_A)}{M_A \cdot C_A + M_B \cdot C_B} \end{aligned}$$

So, the temperature change of metal A is $\Delta T_A = \frac{M_B \cdot C_B \cdot (T_B - T_A)}{M_A \cdot C_A + M_B \cdot C_B}$

$$\Delta T_B = T_F - T_B$$

Also, we can substitute T_F from previous equation.

$$\begin{aligned} \Delta T_B &= \frac{M_A \cdot C_A \cdot T_A + M_B \cdot C_B \cdot T_B}{M_A \cdot C_A + M_B \cdot C_B} - T_B \\ &= \frac{M_A \cdot C_A \cdot T_A + M_B \cdot C_B \cdot T_B - M_A \cdot C_A \cdot T_B - M_B \cdot C_B \cdot T_B}{M_A \cdot C_A + M_B \cdot C_B} \\ &= \frac{M_A \cdot C_A \cdot T_A - M_A \cdot C_A \cdot T_B}{M_A \cdot C_A + M_B \cdot C_B} = \frac{M_A \cdot C_A \cdot (T_A - T_B)}{M_A \cdot C_A + M_B \cdot C_B} \end{aligned}$$

So, the temperature change of metal B is $\Delta T_B = \frac{M_A \cdot C_A \cdot (T_A - T_B)}{M_A \cdot C_A + M_B \cdot C_B}$

c. Let assume that $M_A = M_B$ and $|\Delta T_A| > |\Delta T_B|$. Which metal block has higher specific heat?

* Since both metal have same mass, we can just compare the temperature change and specific heat.

~~Q. 10.10~~ $C_A \cdot |\Delta T_A| = C_B \cdot |\Delta T_B|$

$$\frac{C_B}{C_A} = \frac{|\Delta T_A|}{|\Delta T_B|}$$

Since $|\Delta T_A| > |\Delta T_B|$ as the ~~condition~~ given condition, we know that from that comparison that $C_B > C_A$. So, that the Metal B has higher specific heat. Proved by the ~~condition~~ above condition.

Problem 3.

Inside the sealed container with temperature T , there exist N_0 atoms/molecules of gas with mass m . The speed distribution of the gas atoms/molecules follows a function describe as follows.

$$N_V(v) = 4\pi N_0 \left(\frac{m}{2\pi K_B T} \right)^{3/2} v^2 e^{-mv^2/2K_B T}$$

Which called as a Maxwell-Boltzmann distribution. The distribution have speed between v and $v+dv$ is given by

$$dN = N_V(v) dv$$

So that when we want to determine the total atom/molecule that have speed between v_1 and v_2 , we need to perform the equation

$$N = \int_{v_1}^{v_2} N_V(v) dv$$

Hint: $\int_0^\infty x^3 e^{-ax^2} = \frac{1}{2a^2}$

$$\int_0^\infty x^4 e^{-ax^2} = \frac{3}{8} \sqrt{\frac{\pi}{a}}$$

Prove the following statement.

a. RMS of speed

$$V_{RMS} = \sqrt{\frac{3K_B T}{m}}$$

$$* V_{RMS} = \sqrt{\bar{v}^2}$$

$$\bar{v}^2 = \frac{\int_0^\infty v^2 N_V(v) dv}{N_0}, \text{ substituting from the equation above, we get}$$

$$\bar{v}^2 = \frac{\int_0^\infty v^2 \cdot 4\pi N_0 \left(\frac{m}{2\pi K_B T} \right)^{3/2} v^2 e^{-mv^2/2K_B T} dv}{N_0}$$

$$\bar{v}^2 = \frac{4\pi N_0 \left(\frac{m}{2\pi k_B T}\right)^{3/2} \int_0^\infty v^4 e^{-mv^2/2k_B T} dv}{N_0}, \text{ since } \int_0^\infty v^4 e^{-av^2} = \frac{3}{8} \sqrt{\frac{\pi}{a}}$$

and $a = m/2k_B T$

$$\bar{v}^2 = 4\pi \left(\frac{m}{2\pi k_B T}\right)^{3/2} \cdot \frac{3}{8} \sqrt{\frac{\pi}{\left(\frac{m}{2\pi k_B T}\right)^5}}$$

$$\bar{v}^2 = \frac{3\pi}{2} \sqrt{\left(\frac{m}{2\pi k_B T}\right)^3} \cdot \sqrt{\frac{\pi}{\left(\frac{m}{2\pi k_B T}\right)^5}}$$

$$= \frac{3}{2} \pi \cdot \pi$$

$$\Rightarrow \bar{v}^2 = \frac{3\pi}{2} \cdot \sqrt{\frac{m}{2\pi k_B T}} \cdot \frac{\pi}{2\pi k_B T} \cdot \frac{2 k_B^2 T^2 \sqrt{2\pi k_B T}}{m^2 \sqrt{m}} = \frac{3 k_B T}{m}$$

$$\text{Since } v_{rms} = \sqrt{\bar{v}^2}$$

$$v_{rms} = \sqrt{3 k_B T / m} \quad \square$$

So, the equation is proven.

$$B. v_{avg} = \sqrt{\frac{k_B T}{\pi m}}$$

$$* v_{avg} = \frac{\int_0^\infty v N(v) dv}{N_0}, \text{ substituting from the Maxwell Boltzmann function, we get}$$

$$v_{avg} = \frac{\int_0^\infty v \cdot 4\pi \cdot N_0 \cdot \left(\frac{m}{2\pi k_B T}\right)^{3/2} v^2 e^{-mv^2/2k_B T} dv}{N_0}$$

$$v_{avg} = \frac{4\pi N_0 \left(\frac{m}{2\pi k_B T}\right)^{3/2} \int_0^\infty v^3 e^{-mv^2/2k_B T} dv}{N_0}, \text{ since } \int_0^\infty x^3 e^{-ax^2} = \frac{1}{2a^2}$$

$$v_{avg} = 4\pi \left(\frac{m}{2\pi k_B T}\right)^{3/2} \cdot \frac{1}{2 \left(m/2k_B T\right)^2} = 2\pi \left(\frac{m}{2\pi k_B T}\right) \sqrt{\frac{m}{2\pi k_B T}} \cdot \frac{4 k_B^2 T^2}{m^2}$$

$$v_{avg} = \sqrt{\frac{k_B T}{\pi m}} \quad \square$$

So, the equation is proven.

C. Most probable speed of the gas atom/molecule is given by

$$V_{mp} = \sqrt{\frac{2K_B T}{m}}$$

* Since most probable speed or V_{mp} is the maximum value of distribution ($Nv(v)$). We can calculate when the derivative is equal to zero.

$$\frac{dNv(v)}{dv} = 0$$

$$\frac{d \left(4n N_0 \left(\frac{m}{2\pi K_B T} \right)^{3/2} v^2 e^{-mv^2/2K_B T} \right)}{dv} = 0$$

$$4n \left(\frac{m}{2\pi K_B T} \right)^{3/2} \left(2v e^{-mv^2/2K_B T} + v^2 \left(-\frac{mv}{K_B T} \right) e^{-mv^2/2K_B T} \right) = 0$$

$$4n \left(\frac{m}{2\pi K_B T} \right)^{3/2} e^{-mv^2/2K_B T} v \left(2 - \frac{m}{K_B T} v^2 \right) = 0$$

Thus, we have two possible solutions

$$v=0 \quad \text{or} \quad 2 - \frac{m}{K_B T} v^2 = 0$$

Since $v=0$ is the minimum value, we use the $2 - \frac{m}{K_B T} v^2 = 0$.

$$2 - \frac{m}{K_B T} v^2 = 0$$

$$\frac{m}{K_B T} v^2 = 2$$

$$v^2 = \frac{2K_B T}{m}$$

$$v = \sqrt{\frac{2K_B T}{m}}$$

Since we calculate the most probable speed, $v = V_{mp}$, thus, we know that the condition is satisfied and the formula ~~given~~ is proven.

