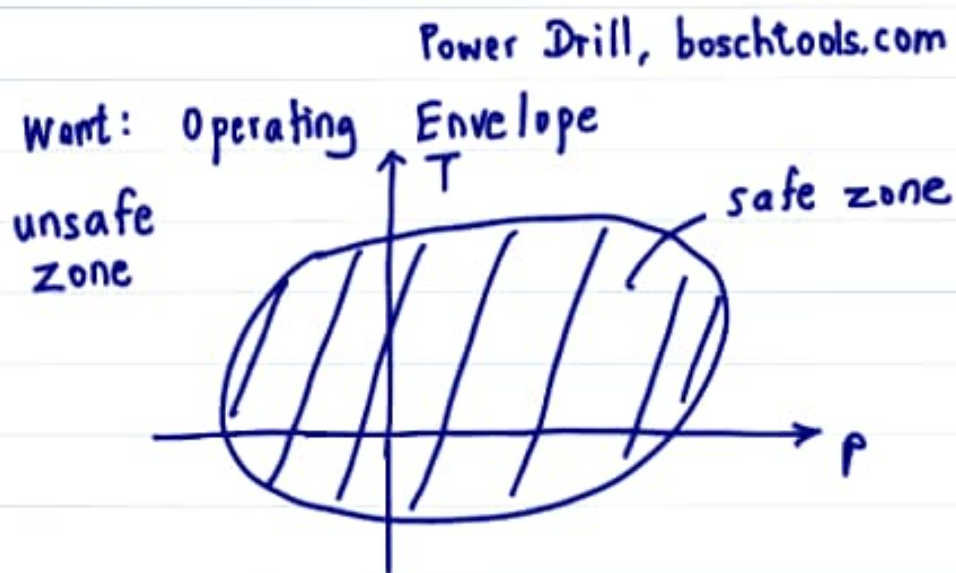
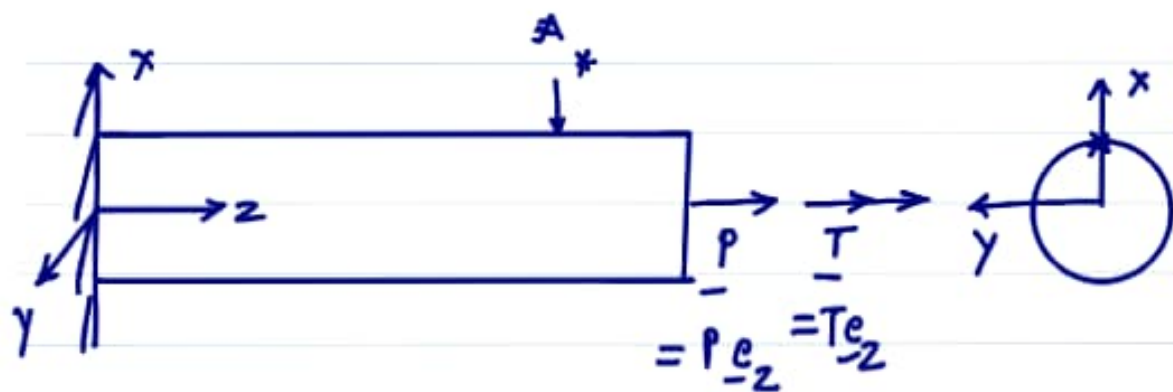


ME 202
LECTURE 6
13 JAN 2022





$$\sigma_{zz} = \frac{P}{A} = \frac{4P}{\pi D^2}$$

$*$ = point of interest
 $(\frac{D}{2}, 0)$

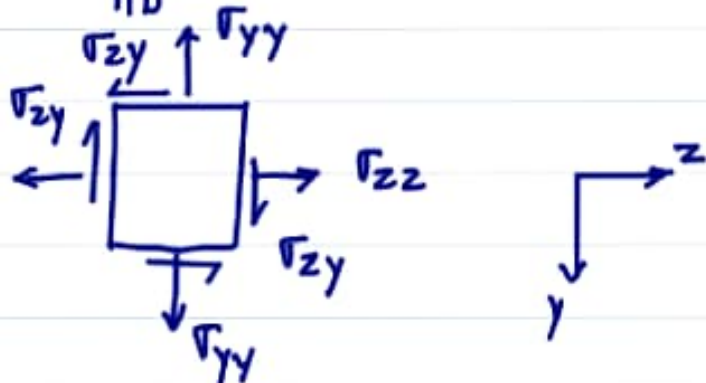
$$\sigma_{zy} = + G \alpha x = \frac{16T}{\pi D^3}$$

$$\sigma_{zx} = - G \alpha y = 0$$

$$\underline{\underline{\sigma}} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & \frac{16T}{\pi D^3} \\ 0 & \frac{16T}{\pi D^3} & \frac{4P}{\pi D^2} \end{pmatrix} \quad \text{2D stress @ } *$$

Stress element

Top of $*$



Theory of Failure.

Soy, material brittle. \Rightarrow fail by fracture.
 Max Normal Stress Theory.



nucleation + growth

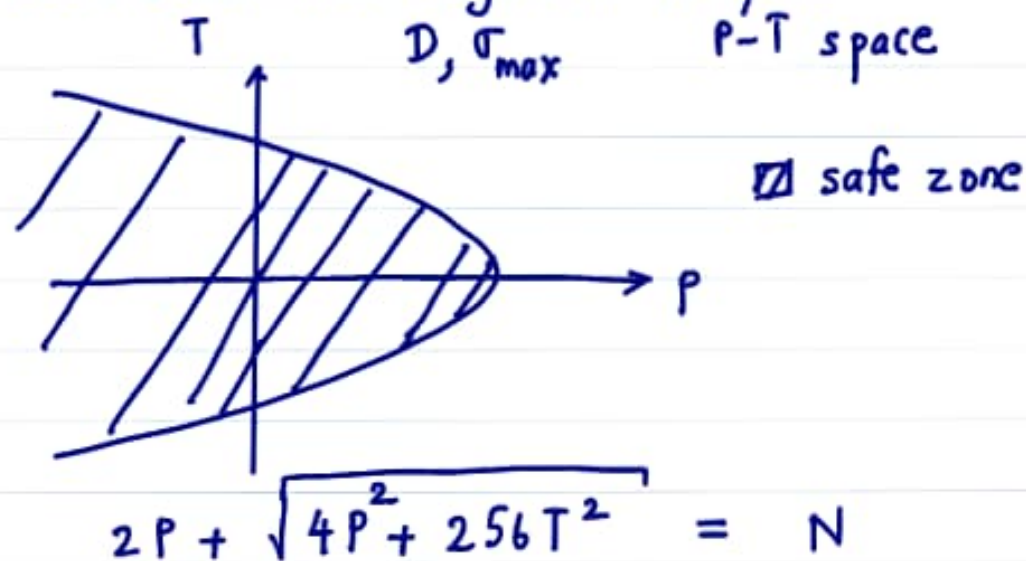
Use formulas from Mohr's circle

$$\sigma_{\max} = \underset{\substack{\uparrow \\ \text{center}}}{c} + \underset{\substack{\uparrow \\ \text{radius}}}{R}$$

$$= \left(\frac{\sigma_{zz} + \cancel{\sigma_{yy}}}{2} \right) + \sqrt{\left(\frac{\sigma_{zz} - \cancel{\sigma_{yy}}}{2} \right)^2 + \tau_{zy}^2}$$

$$\underset{\substack{\uparrow \\ \text{known exptly.}}}{\sigma_{\max}} = \frac{4P}{2\pi D^2} + \sqrt{\frac{4P^2}{\pi^2 D^4} + \frac{256T^2}{\pi^2 D^6}}$$

Used either for design or analysis.



Material ductile \Rightarrow fails by plastic deformation
Movement of dislocations.



\downarrow
slip

Max shear stress theory.

from Mohr's circle,

$$R = \sqrt{\left(\frac{\sigma_{zz} - \sigma_{yy}}{2}\right)^2 + \tau_{zy}^2}$$

$$\sqrt{\left(\frac{4P}{2\pi D^2}\right)^2 + \left(\frac{16T}{\pi D^3}\right)^2} = \tau_{\max}$$

↑
from expts.

$$P^2 D^2 + 64T^2 = \left(\frac{\sigma_Y \pi D^3}{4}\right)^2 = \frac{\sigma_Y}{2} \leftarrow \text{yield stress from tensile test}$$

Ellipse in P-T space.

Homework:



At free end, $M \underline{e}_y + T \underline{e}_z$

$$\sigma_{zz} = \frac{P}{A} + \left(-\frac{M}{I} x \right)$$

Euler-Bernoulli beam theory.

$$\sigma_{zy} = \frac{16T}{\pi D^3}$$

will review in later class.

Find operating envelope in P, M, T space for safe operation of shaft, max shear stress theory τ_{\max} given from expts

Torsion of Non-circular cross-sections

□ Angle of Twist

□ T_{max} for safe operation



c/s Wing / Turbine blade

Theory based on circular c/s, at some z .

⊙ centroid

origin here for now.



$$OP = OP'$$

$\theta = \alpha z$, α unit angle of twist
small angles.

$$u = -\alpha y z$$

$$v = +\alpha x z$$

$$w = w(x, y) \quad \text{warping.}$$



from expt observations

or prove formally $w \neq 0$ for non-circ c/s
later.

Disp \rightarrow Strains \rightarrow Stresses \rightarrow Torque
 α T

$$\text{Goal: } T = K_t \alpha$$

\uparrow
Torsional stiffness (G , geometry)