



ME338 – Manufacturing Process II

Lecture 6 : Thermal aspects in Machining

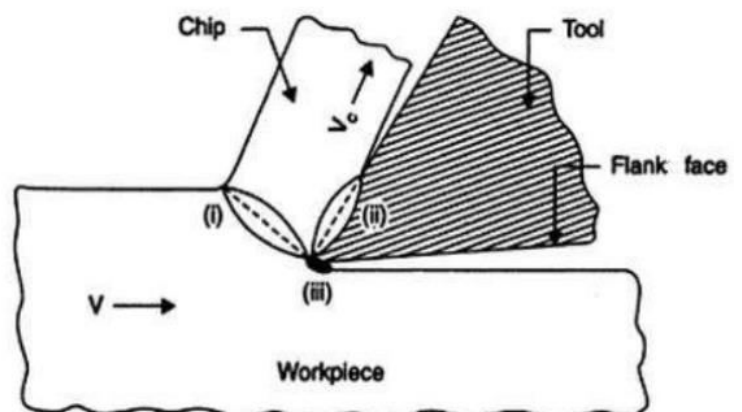
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Why is heat generated in machining ?



- In the elastic deformation:
 - Energy required for deformation is stored in the materials as strain energy and thus, no heat is generated
- In plastic deformation of metal machining:
 - Most of the energy used in converted into heat
- What are the regions where plastic deformation is taking place :
 - Primary shear deformation zone
 - Secondary chip tool interface
 - Territory Work-tool interface



Heat generation zones



- Region 1: Primary shear zone
 - Actual plastic deformation occurs, so heat is generated
 - Portion of this heat is carried by the chip, so chip temperature increases
 - Rest of the heat is retained by the workpiece
- Region 2: Tool-chip interface
 - Chip slides through the rake surface. Friction > heat generation
 - Portion of this heat is carried by the chip, so chip temperature further increases
 - Rest of the heat is transferred to cutting tool
 - Amount of heat generation depends on chip speed (and thus, cutting speed)
 - Tools are also coated with heat-resistant thin films for increased tool life
- Region 3: Tool-workpiece interface
 - In practical applications, tool edge does not remain sharp and becomes dull
 - Portion of Tool flank surface rubs against the workpiece
 - This heat is shared by tool, workpiece and coolant
 - This heat generation increases with the cutting time as the tool wears out

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How material properties affect temperature



- Amount of heat generated depends upon
 - Cutting parameters : cutting speed, use of coolants
 - Tool geometry : rake angle, nose radius
 - Material properties of workpiece and tool: specific heat, thermal conductivity
- Material properties:
 - In low strength material, heat generation and increased tool temperature is not issue
 - Higher hardness and tensile strength materials (Ferrous, Titanium, etc) , require more cutting force, thus increased tool temperature is high and therefore tool wear rate is very high
 - Lower thermal conductivity of workpiece >> more rise in temperature

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How cutting parameters affect temperature



- High machining speed is desired for high productivity, but high tool wear
- Shear angle affects the heat generation process
 - Larger shear angle > smaller shear plane area >> smaller shear force, >> small heat generation
- Positive rake angle > lower cutting force > lower temp
- Larger nose radius > more contact with tool surface > more heat conduction
- Large cross section of tool shank > more heat conduction > lower temperature
- Increasing cutting speed > higher friction > more rise in temperature
- Increasing feed, depth of cut also result in higher temperature
- Application of cutting fluid will lower temperature rise

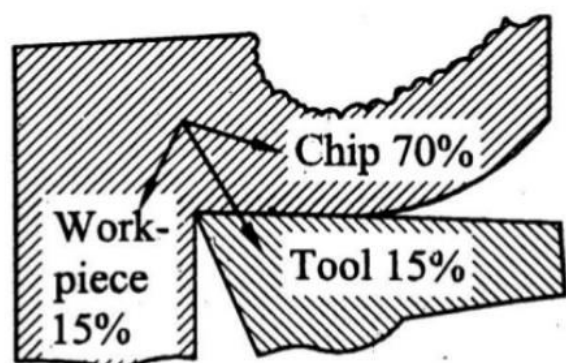
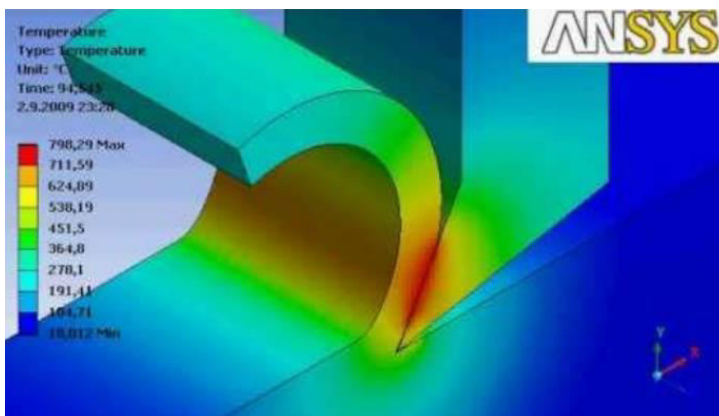
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Temperature effect on cutting tool

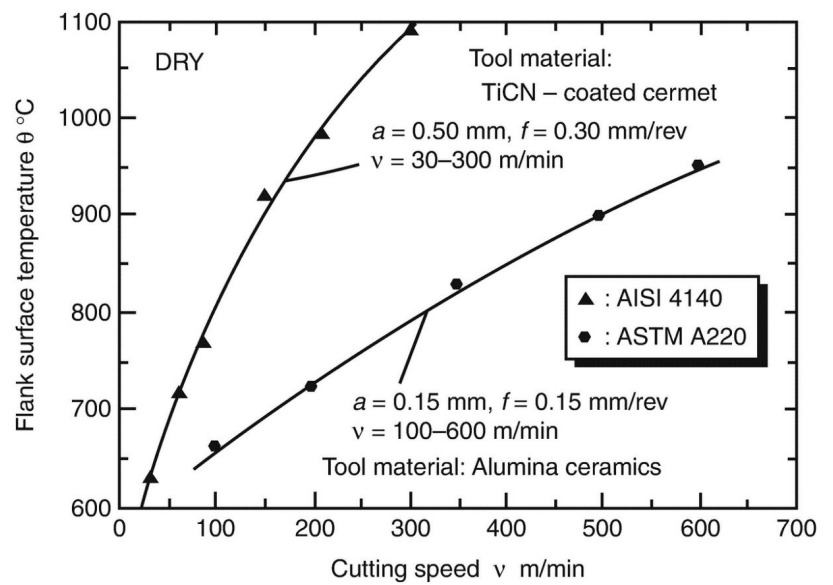
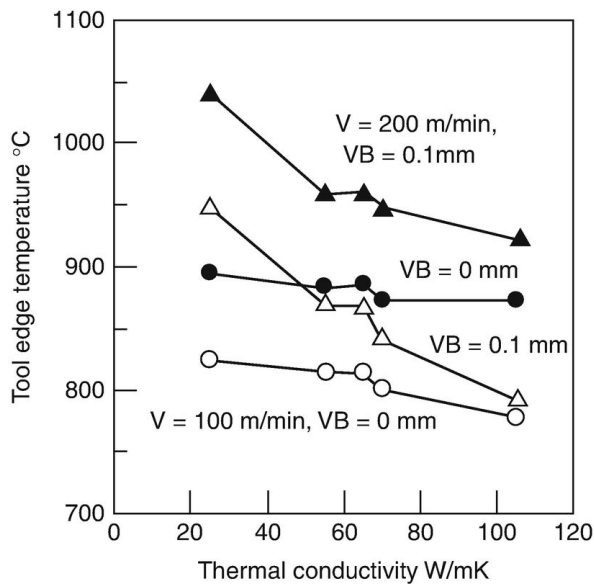


- Heat is distributed between chip (~70%), tool (~15%) and workpiece (~15%)
- Temperature may reach beyond 700°C (beyond recrystallization temp)
- Effect on cutting tool:
 - Thermal expansion of the cutting tool
 - Plastic deformation of cutting edges
 - Formation of build up edge > poor surface finish, dimensional inaccuracy
 - Rapid tool wear
- Increased heat causes uneven dimensional changes in the part being machined, making it difficult to control its dimensional accuracy and tolerances





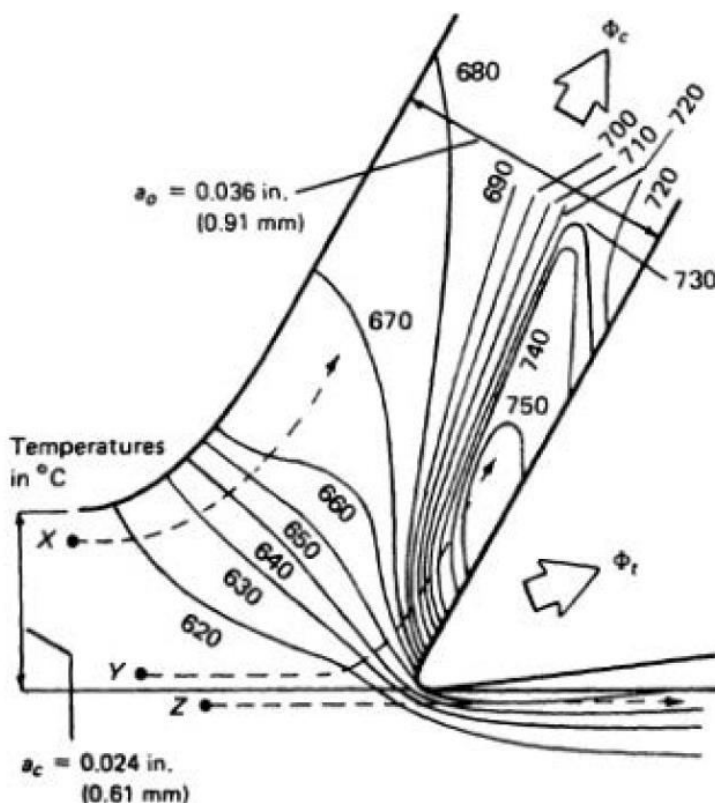
Effect of Thermal conductivity & Cutting speed



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Temperature distribution in work piece and tool



For machining mild steel, cutting speed is 0.38 m/s, width of cut is 6.35 mm. Normal rake is 30 degree, and the workpiece temperature is 611°C

Point X, Y and Z:

Point X is moving towards cutting tool and passing through primary shear zone.

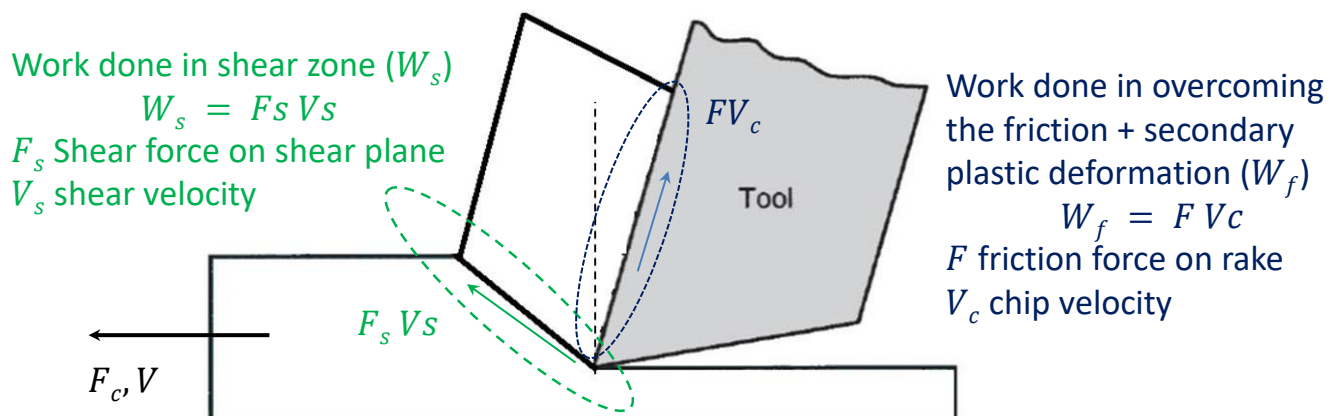
Point Y will experience both primary as well as secondary shear zone

Point Z is inside the material

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Work done in cutting action



- Total work done in cutting action $W_c = F_c V = W_s + W_f$
 - Work done in shearing $W_s = F_s V_s$
 - work done in friction $W_f = F V_c$
- Assuming no losses, total work done W = work supplied by electric motor W_m
- W_m = **Work consumed in cutting action** + Work done in **feeding motion**
- $W_m \approx$ Work consumed in cutting action W_c (neglecting work in feeding motion)
- $W_m \approx W_c = W_s + W_f$;
- $F_c V = F_s V_s + F V_c$



Specific cutting energy

- Specific energy u = Total energy consumed ($F_c V$) / volume of metal removed
 - $u = F_c V / V w t_1$
- Specific cutting energy u_c : $F_c / w t_1$
- Specific shear energy u_s : $F_s / w t_1$
- Specific friction energy u_f : $F / w t_1$
- $u_c = u_s + u_f$
- $W_c = W_s + W_f$
 - W_c = Power consumed in machining = $F_c V = u_c (V w t_1)$
 - W_s = Power consumed in primary shear zone = $F_s V_s = u_s (V w t_1)$
 - W_f = Power consumed in overcoming friction in secondary zone = $F V_c = u_f (V w t_1)$
- Typically, 60-70% of the energy in the metal cutting is consumed in the shear zone alone
- Remaining 40-30% is consumed at the tool-chip interface (assuming a perfectly sharp tool)
 - Energy consumed in the Tool-workpiece contact (due to tool rubbing) is neglected

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Temperature in primary shear zone



- Power consumed in Shear zone $W_s = W_c - W_f$
 - $W_s = F_c V - F V_c$
- Cutting velocity (V) and chip velocity (V_c) are related by chip thickness ratio (r)
 - $V_c = r V = \frac{\sin \phi}{\cos(\phi - \alpha)} V$
- $W_s = F_c V - F V_c = V(F_c - F r)$
- From experimental analysis, it is observed that typically, 60-70% of the energy in the metal cutting is consumed in the shear zone alone
- Majority of the energy consumed in the shear zone (W_s), goes into the chip
- Remaining energy is more or less equally distributed and goes into the cutting tool and the workpiece

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Temperature in primary shear zone

- If γ is fraction of primary heat which goes to the work piece, then $(1 - \gamma)$ will taken by chips
- Value of γ depends upon shear angle ϕ and thermal conductivity k

$$\gamma = 0.15 \ln \left(\frac{27.5}{\lambda \tan \phi} \right) \quad \lambda = \frac{\rho c V t_1}{k}$$

γ : fraction of primary heat which conducted to the work piece,

ρ : density of workpiece material

c : specific heat of workpiece material

k : thermal conductivity of workpiece material

V : cutting velocity

t_1 : uncut chip thickness

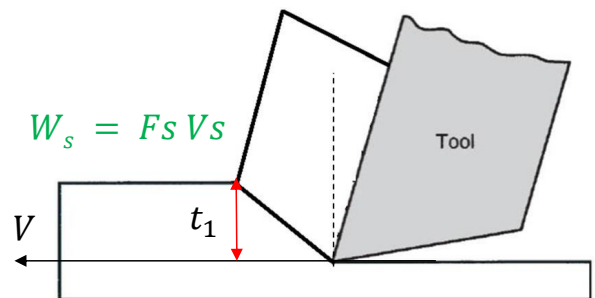
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Temperature in primary shear zone



$$W_s = F_c V - F V_c$$



- If γ : fraction of primary heat which conducted to the work piece, then $(1 - \gamma)$ fraction will taken by chips.
- Heat taken away by the chips: $(1 - \gamma)W_s$
- Ignoring heat loss to atmosphere,
- Heat taken by chip = heat absorbed by chip
- Heat absorbed by chip: $m c \Delta \theta$
- Mass of material removed per unit time : $m = V w t_1 \rho$
- Temperature rise of material passing through shear zone: $\Delta \theta = \frac{(1 - \gamma)W_s}{V w t_1 \rho c}$

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Temperature in secondary shear zone



- Maximum temperature rise $\Delta\theta_f$ when material passes through the rake surface

$$\Delta\theta_f \approx 1.13 \sqrt{\frac{\lambda t_c}{l}} \left(\frac{W_f}{\rho c V w t_1} \right) \quad \lambda = \frac{\rho c V t_1}{k}$$

- Here, l is the length of contact between tool and chip

$$\frac{l}{t_c} = [1 + \tan(\phi - \alpha)] \quad \Delta\theta_f = 1.13 \sqrt{\frac{1}{\rho c V t_1 k [1 + \tan(\phi - \alpha)]}} \frac{W_f}{w}$$

- Average temperature rise of material passing through secondary shear zone
- Final temperature is given as :
– $\theta = \theta_0 + \Delta\theta_s + \Delta\theta_f$

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Example 3



- A planing process is being used to machine a 300 mm x 300 mm x 25 mm flat mild steel block. The sharp single point cutting tool has a normal rake angle $\alpha = 10^\circ$. Other process parameters are as follows: cutting speed $V = 2$ m/s, undeformed chip thickness = 0.25 mm, width of cut per pass $w = 2.5$ mm, deformed chip thickness = 0.83 mm. The cutting and thrust forces were measured during each pass with a cutting force dynamometer and found to be as follows: $F_c = 890$ N and $F_t = 667$ N. Assume Planing is an orthogonal cutting process.
- Calculate the percentage of total power dissipated in the primary zone of deformation (shear zone).

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Example 3



$$P_c = F_c V = (890)(2) = 1780 \text{ W}$$

$$P_s = F_s V_s = R \cos(\phi + \beta - \alpha) V_s$$

$$R = \sqrt{F_c^2 + F_t^2} = 1112.2 \text{ N}$$

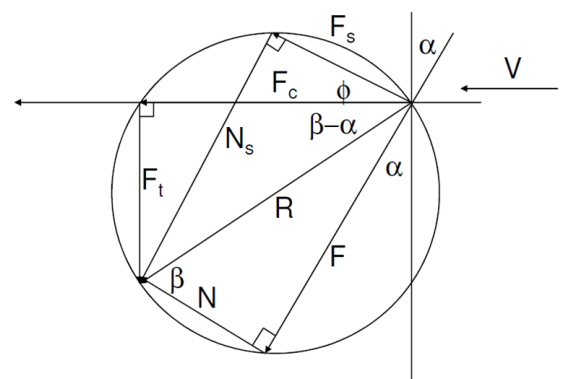
$$\tan \phi = \frac{r \cos \alpha}{1 - r \sin \alpha} = \frac{(0.25/0.83) * \cos(10)}{1 - (0.25/0.83) * \sin(10)} \Rightarrow \phi = 17.3 \text{ deg}$$

$$V_s = \frac{V \cos \alpha}{\cos(\phi - \alpha)} = 1.986 \text{ m/s}$$

$$P_s = F_s V_s = 1293.63 \text{ W}$$

% of total power dissipated in shear zone =

$$\frac{P_s}{P_c} \times 100 = 72.6\%$$



Example : Temperature rise

Determine the maximum temperature along the rake face of the tool when machining mild steel (ms), given

work material (ms) shear stress = $400 \times 10^6 \text{ N/m}^2$,

$\alpha = 0^\circ$, $v = 2 \text{ m/sec}$, $t_1 = 0.25 \text{ mm}$,

$w = 2 \text{ mm}$, $\mu = 0.5$, $\rho = 7200 \text{ kg/m}^3$,

$k = 43.6 \text{ W/m-}^\circ\text{C}$, $c = 502 \text{ J/kg-}^\circ\text{C}$, $\theta_0 = 40^\circ\text{C}$.

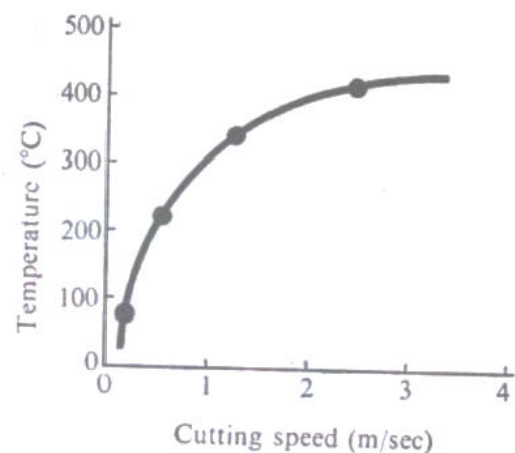
Use the Lee and Shaffer shear angle relationship.

Overall temperature and cutting speed



- Nature of variation in the overall chip-tool interface temperature (θ_{ov}) with major parameters can be determined through dimensional analysis

- $\theta_{ov} \propto U_c \sqrt{\frac{vt_1}{k\rho c}}$
- Overall temperature rise is proportional to the square root of the cutting speed
- Cutting speed has major effect on the overall temperature rise



Role of cutting fluids in machining

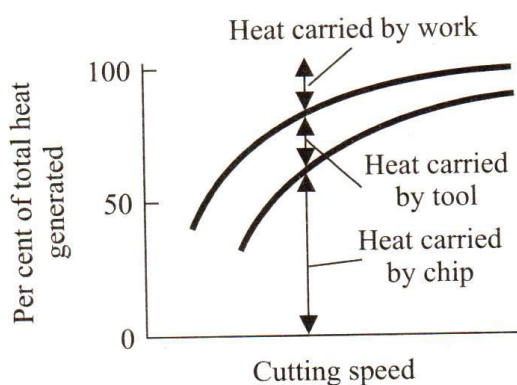


- As temperature affects the tool wear, thus productivity
 - Need to reduce temperature to Increases tool life
 - Reduced friction on the rake surface
- Ways in which cutting fluid affects machining
 - Cooling down of chip-tool-work zone by carrying away generated heat
 - Reducing the coefficient of friction a chip-tool Interface
- Cutting fluids should have following properties:
 - Large specific heat and good thermal conductivity,
 - Low viscosity and small molecular size,
 - Suitable reactive constituent/ Nonpoisonous/Inexpensive
- Types of cutting fluids:
 - Water based (contains salt or soluble oils)
 - Mineral oil
 - Synthetic oil

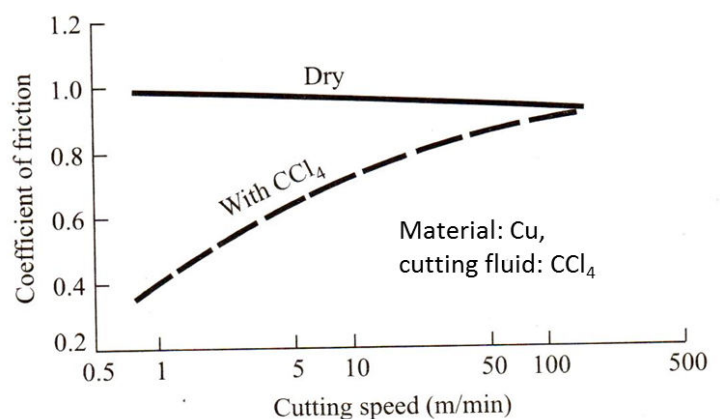
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Effect of cutting fluid – heat generation, friction



- At higher cutting speed, effectiveness of cutting fluids reduces as it take some finite time to work
- At higher speed, chip carries away most of the heat



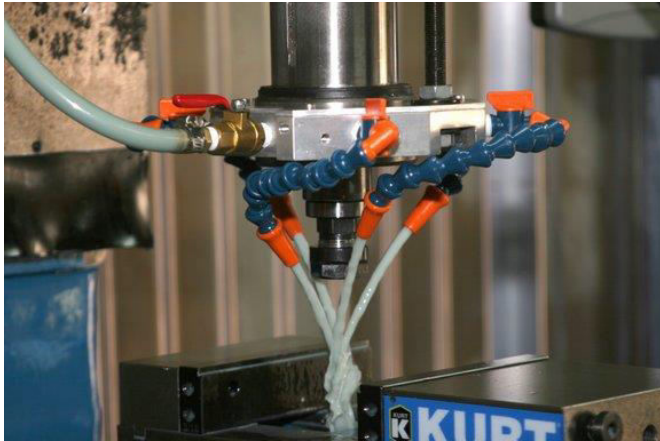
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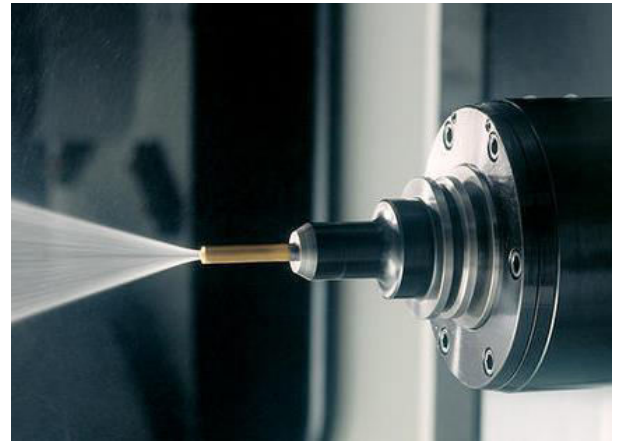
Cutting Fluid : Application methods



- Cutting fluid can be applied by several ways:
 - By using manual brush/ By flood exposure / Through spindle cooling
- Amount of cutting fluid should be minimum
 - Cutting fluid in form of Mist is a popular technique
 - Small droplets to ensure direct interaction with surface



Cutting Fluid : Spray cooling



Cutting Fluid : Through spindle cooling