

Q1: 50 pieces of discs (outer diameter 100 mm, inner diameter: 8 mm) are to be faced on a vertical-boring machine with a feed of 0.25 mm and depth of cut of 5 mm. The machine has an automatic control device by which the cutting speed is continuously adjusted to allow maximum power utilization at the cutting tool of 3 kW. However, the maximum rotational frequency of the spindle is limited to 0.7 s^{-1} . If the specific cutting energy for the work material is 2.27 GJ/m^3 and it takes 600 s to unload a machined disc, load an unmachined disc, and return the tool to the beginning of the cut, calculate the total production time for the batch, in minutes. [10]

Q2: In a slab-milling operation, the cutter has 20 teeth and is 100 mm in diameter. The rotational frequency of the cutter is 5 s^{-1} , the workpiece feed speed is 1.3 mm/s, the depth of cut is 6 mm, and the width of the workpiece is 50 mm. The relationship between the maximum undeformed chip thickness (t_0) and the specific cutting energy U in gigajoules per cubic meter (GJ/m^3), for the work material is:

$$U = 1.4 \left[1 + \frac{1.25 \times 10^{-6}}{t_0} \right]$$

Estimate:

- a. The maximum metal removal rate [5]
- b. The maximum power, in kilowatts (kW), required at the cutter [5]

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Solution:

Q14) $N = 20$ (teeth) $a_p = 50$ mm
 $d_t = 100$ mm $a_e = 6$ mm
 $n = 5$ s⁻¹ $p_s = 1.4 \left[1 + \frac{25 \times 10^{-6}}{a_{c, \max}} \right] \frac{\text{GJ}}{\text{m}^3}$
 $v_f = 1.3$ mm/s

a) $a_e Z_w = a_p a_e v_f = 50 \times 6 \times 1.3 = 390 \text{ mm}^3/\text{s}$

b) $a_{c, \text{avg}} = a_f \sqrt{\frac{a_e}{d_t}} ; a_{c, \max} = \frac{2 v_f}{N n} \sqrt{\frac{a_e}{d_t}}$
 $\downarrow (v_f / N n)$

$a_{c, \max} = \frac{2 \times 1.3}{20 \times 5} \sqrt{\frac{6}{100}} = 6.37 \times 10^{-3} \text{ mm}$
 $= 6.37 \times 10^{-6} \text{ m}$

c) $P_{m, \max} = p_s \cdot Z_{w, \max} = 1.4 \left[1 + \frac{25 \times 10^{-6}}{6.37 \times 10^{-6}} \right] \times 10^6 \frac{\text{kJ}}{\text{m}^3} \times [390 \times 10^{-9} \text{ m}^3/\text{s}] = 2.69 \text{ kW}$

Q6) $a_b = f = 0.25$ mm $n_w = 0.7$ rad/s
 $a_p = 5$ mm $p_s = 2.27 \frac{\text{GJ}}{\text{m}^3}$
 $P_m = 3$ kW $t_{cu} = 600$ s

$(P_m)_{\max} = p_s \cdot Z_{w, \max} = p_s a_b a_p \pi n_w d_{\max}$

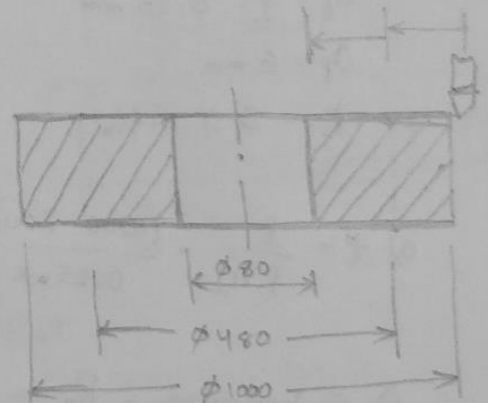
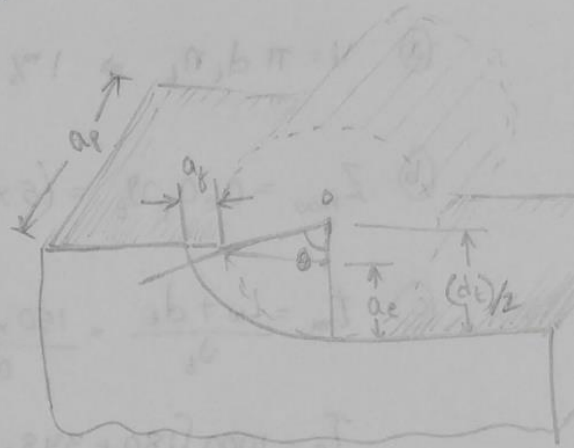
$(3 \text{ kW}) = (2.27 \times 10^6 \frac{\text{kJ}}{\text{m}^3}) (0.25 \times 10^{-3} \text{ m}) (5 \times 10^{-3} \text{ m}) (\pi \times 0.7 \text{ s}^{-1} \times d_{\max})$

$d_{\max} = 0.481 \text{ m}$

\therefore Upto 0.481 m of diameter, $(n_w)_{\max} = 0.7 \text{ s}^{-1}$ can be maintained.

If facing is done for diameter $> 0.481 \text{ m}$, n_w will be $< 0.7 \text{ s}^{-1}$

So find ' n_w ' at 1000 mm of diameter (which is $> 0.481 \text{ m}$ of dia)



$$(n_w d)_{@481\text{ mm}} = (n_w d)_{@1000\text{ mm}} \quad \left[\because P_m \text{ is constant} \right]$$

$$\therefore n_w @ 1000\text{ mm} = \frac{0.481\text{ m} \times 0.7\text{ s}^{-1}}{1\text{ m}} = 0.3365\text{ s}^{-1}$$

$$(n_w)_{\text{avg}} \text{ between diameters } 1000\text{ mm \& } 481\text{ mm is } \frac{0.7 + 0.3365}{2} = 0.52\text{ s}^{-1}$$

$$t_{s-m} = \frac{(1000-481)/2}{(0.52)(0.25)} = 1996.15\text{ s} \quad (\text{start to max. dia})$$

$$t_{m-e} = \frac{(481-80)/2}{(0.7)(0.25)} = 1145.7\text{ s} \quad (\text{max dia to end})$$

$$T = (t_{s-m} + t_{m-e} + t_{u,e}) 50 = 3741.86 \times 50 = 187.1 \text{ kiloseconds.}$$