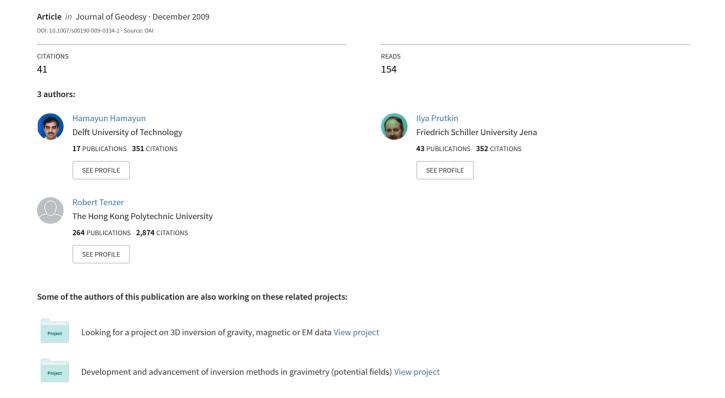
The optimum expression for the gravitational potential of polyhedral bodies having a linearly varying density distribution



ORIGINAL ARTICLE

The optimum expression for the gravitational potential of polyhedral bodies having a linearly varying density distribution

Hamayun · I. Prutkin · R. Tenzer

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Abstract When topography is represented by a simple regular grid digital elevation model, the analytical rectangular prism approach is often used for a precise gravity field modelling at the vicinity of the computation point. However, when the topographical surface is represented more realistically, for instance by a triangular irregular network (TIN) model, the analytical integration using arbitrary polyhedral bodies (the analytical line integral approach) can be implemented directly without additional data pre-processing (gridding or interpolation). The analytical line integral approach can also facilitate 3-D density models created for complex geometrical bodies. For the forward modelling of the gravitational field generated by the geological structures with variable densities, the analytical integration can be carried out using polyhedral bodies with a varying density. The optimal expression for the gravitational attraction vector generated by an arbitrary polyhedral body having a linearly varying density is known. In this article, the corresponding optimal expression for the gravitational potential is derived by means of line integrals after applying the Gauss divergence theorem.

Keywords Gravitational potential · Line integral · Linear density · Polyhedron

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1 Introduction

Various methods are applied to evaluate Newton's volume integral. Studying the local gravity field, a simple form of the integration volume can be used, such as the right rectangular parallelepiped (prism) with constant density within each individual integration volume. Bessel (1813) derived the closed analytical expression for the potential of a prism. The potential-related formulae for a prism were studied also by Zach (1811), Mollweide (1813), Everest (1830) and Mader (1951). More recently, Nagy et al. (2000) summarized the closed analytical expressions for the potential and its first and second derivatives of a rectangular prism of homogenous density. However, in most geological structures the constant density assumption does not hold. For this reason, some authors derived analytical expressions for volume elements with linearly or otherwise varying density distribution models. Chai and Hinze (1988) computed gravity anomalies using a rectangular prism with density changing linearly with depth. Gallardo-Delgado et al. (2003) derived the analytical solution for the forward gravity modelling utilizing a right rectangular prism with density varying according to a polynomial quadratic law. García-Abdeslem (1992, 2005) introduced the analytical expression for the right rectangular prism with depth dependent density distribution having a form of a cubic polynomial.

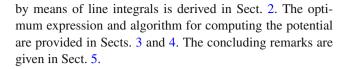
For the gravity field modelling of inhomogeneous density formations, the approximation of geological structures by more general geometrical forms than rectangular prisms are implemented. Hurbbert (1948) introduced a methodology called the line integral approach; the surface or volume integrals are converted to line integrals after applying the Gauss divergence theorem. Following this idea, Talwani et al. (1959) applied the line integral approach to the polygon in 2-D. Talwani and Ewing (1960), Collette (1965) and



Takin and Talwani (1966) decomposed the 3-D body into parallel, typically horizontal laminae. Paul (1974) and Barnett (1976) generalized this concept for a polyhedron in 3-D. Pohánka (1988) derived a simple algorithm for the attraction of a homogeneous polyhedral body using the line integral approach (see also Ivan 1990; Pohánka 1990). The formulae for polyhedral bodies with homogeneous density were studied also by Okabe (1979), Götze and Lahmeyer (1988), Kwok (1991), Holstein and Ketteridge (1996), Werner and Scheeres (1997), Holstein et al. (1999) and Holstein (2002a,b). Petrović (1996) presented in more complete form the formulae for the potential and its derivatives using the line integral approach for arbitrary polyhedral bodies of homogenous density (see also Tsoulis and Petrović 2001).

In forward modelling of the gravitational field of geological structures with the variable density distribution, the analytical expressions for volume elements with linearly or otherwise varying density distribution models improve the numerical efficiency. One example can be given in modeling the gravitational contribution of sedimentary basins where the density increases with depth due to compaction (e.g. Artemiev et al. 1994). Combining the benefits of using more generalized geometrical bodies and taking into account density variation models, Pohánka (1998) introduced the expression for the attraction of an arbitrary polyhedral body having a linearly varying density by means of line integrals. The alternative expression was derived by Hansen (1999). Holstein (2003) generalized their work deriving the formulae also for the potential and its second derivatives. To avoid singular terms and obtain a maximal numerical efficiency, Pohánka (1998) in his study derived the optimum expression and proposed a simple computational algorithm for computing the gravitational attraction.

In gravimetric geoid modelling and related subjects not only the attraction-related term (direct effect) but also the potential-related terms (primary and secondary indirect effects) are computed. Following the concept used by Pohánka (1988, 1998) in this study we derive the optimum expression for computing the gravitational potential of an arbitrary polyhedral body having a linearly varying density. The optimum expression for the gravitational potential of the polyhedral body having a homogeneous density is given in Pohánka (1988). Our derivation is thus reduced to find the optimum expression only for the linear density variation term. In comparison to the formula for the potential given by Holstein (2003), the main advantage of adopting the computational strategy developed by Pohánka (1988, 1998) is that our expression does not have the singular terms. We also demonstrate that the computational algorithm for computing the attraction proposed by Pohánka (1998) can directly be applied for computing the potential. The potential of an arbitrary polyhedral body having a linearly varying density



2 Potential by means of line integrals

The gravitational potential V of the polyhedral body at the point \mathbf{r} is defined by the Newton volume integral

$$V(\mathbf{r}) = G \iiint_{D} \frac{\rho(\mathbf{r}')}{|\mathbf{r}' - \mathbf{r}|} d\tau', \tag{1}$$

where G is the gravitational constant, ρ the mass density distribution function inside the volume D of the polyhedral body, $d\tau'$ the volume element at the point \mathbf{r}' , and $|\mathbf{r}' - \mathbf{r}|$ the Euclidean spatial distance between the computation point \mathbf{r} and the running integration point \mathbf{r}' . Let us consider the linearly varying density (Pohánka 1998)

$$\rho(\mathbf{r}') = \rho_0 + \mathbf{\rho_1} \cdot \mathbf{r}',\tag{2}$$

where ρ_0 is the value of density at a suitably chosen origin of the local coordinate system used for a description of the density model within the volume D of the polyhedral body, and ρ_1 the gradient of a linear density distribution function. Combining Eqs. (1) and (2), we get

$$V(\mathbf{r}) = G(\rho_0 + \rho_1 \cdot \mathbf{r}) \iiint_D \frac{1}{|\mathbf{r}' - \mathbf{r}|} d\tau'$$

$$+ G\rho_1 \cdot \iiint_D \frac{\mathbf{r}' - \mathbf{r}}{|\mathbf{r}' - \mathbf{r}|} d\tau'. \tag{3}$$

Using the identities:

$$\nabla_{\mathbf{r}'} \cdot \frac{\mathbf{r}' - \mathbf{r}}{|\mathbf{r}' - \mathbf{r}|} = \frac{2}{|\mathbf{r}' - \mathbf{r}|}, \quad \nabla_{\mathbf{r}'} \left| \mathbf{r}' - \mathbf{r} \right| = \frac{\mathbf{r}' - \mathbf{r}}{|\mathbf{r}' - \mathbf{r}|},$$

Eq. (3) is further rewritten as

$$V(\mathbf{r}) = G \frac{\rho_0 + \mathbf{\rho_1} \cdot \mathbf{r}}{2} \iiint_D \nabla_{\mathbf{r}'} \cdot \frac{\mathbf{r}' - \mathbf{r}}{|\mathbf{r}' - \mathbf{r}|} d\tau'$$
$$+ G \mathbf{\rho_1} \cdot \iiint_D \nabla_{\mathbf{r}'} |\mathbf{r}' - \mathbf{r}| d\tau'. \tag{4}$$

To convert the volume integrals on the right-hand side of Eq. (4) to the surface integrals, the Gauss divergence theorem is applied. If $\mathbf{f}(\mathbf{r}')$ is a vector function with integrable gradient in the domain D, it holds

$$\iiint\limits_{D} \nabla_{\mathbf{r}'} \cdot \mathbf{f}(\mathbf{r}') \ d\tau' = \iint\limits_{S} \mathbf{f}(\mathbf{s}') \cdot d\sigma',$$

where the surface element vector $d\sigma'$ is defined as the product of the unit normal vector $\mathbf{n}(\mathbf{s}')$ oriented outwards from



the volume D and the scalar surface element $d\sigma'$ at the point \mathbf{s}' on the surface S, i.e. $d\sigma' = \mathbf{n}(\mathbf{s}')d\sigma'$. Correspondingly, if $f(\mathbf{r}')$ is a scalar function with integrable gradient in the domain D, the Gauss divergence theorem holds

$$\iiint\limits_{D} \nabla_{\mathbf{r}'} f(\mathbf{r}') \ d\tau' = \iint\limits_{S} f(\mathbf{s}') \ d\sigma'.$$

The application of the Gauss divergence theorem in Eq. (4) yields

$$V(\mathbf{r}) = G \frac{\rho_0 + \mathbf{\rho_1} \cdot \mathbf{r}}{2} \iint_{S} \frac{\mathbf{s}' - \mathbf{r}}{|\mathbf{s}' - \mathbf{r}|} \cdot d\mathbf{\sigma}'$$
$$+ G \mathbf{\rho_1} \cdot \iint_{S} |\mathbf{s}' - \mathbf{r}| d\mathbf{\sigma}', \tag{5}$$

where $|\mathbf{s}' - \mathbf{r}|$ is the Euclidean spatial distance between the computation point \mathbf{r} and the running integration point \mathbf{s}' on the surface S.

We further define the surface integrals on the right-hand side of Eq. (5) as a sum of the surface integrals over the polyhedral faces $\{S_k : k = 1, 2, ..., K\}$, where K is the total number of the polyhedral faces. At any surface point \mathbf{s}' of the k-th polyhedral face S_k we have $d\mathbf{\sigma}' = \mathbf{n}_k d\mathbf{\sigma}'$, where \mathbf{n}_k is the unit normal vector oriented outwards from the polyhedral face S_k . Hence,

$$V(\mathbf{r}) = G \frac{\rho_0 + \mathbf{\rho_1} \cdot \mathbf{r}}{2} \sum_{k=1}^{K} \iint_{S_k} \frac{\mathbf{s}' - \mathbf{r}}{|\mathbf{s}' - \mathbf{r}|} \cdot \mathbf{n}_k \, d\sigma'$$

$$+ G \sum_{k=1}^{K} \mathbf{\rho_1} \cdot \iint_{S_k} \mathbf{n}_k \, |\mathbf{s}' - \mathbf{r}| \, d\sigma'$$

$$= G \sum_{k=1}^{K} \left[\frac{\rho_0 + \mathbf{\rho_1} \cdot \mathbf{r}}{2} \mathbf{n}_k \cdot \iint_{S_k} \frac{\mathbf{s}' - \mathbf{r}}{|\mathbf{s}' - \mathbf{r}|} \, d\sigma'$$

$$+ \mathbf{\rho_1} \cdot \mathbf{n}_k \iint_{S_k} |\mathbf{s}' - \mathbf{r}| \, d\sigma' \right]. \tag{6}$$

In accordance with Pohánka (1998, Eq. 11), we denote

$$\mathbf{G}_{k}(\mathbf{r}) = \iint_{S_{k}} \frac{\mathbf{s}' - \mathbf{r}}{|\mathbf{s}' - \mathbf{r}|} d\sigma', \tag{7}$$

and introduce

$$H_k(\mathbf{r}) = \iint_{S_k} |\mathbf{s}' - \mathbf{r}| d\sigma'.$$
 (8)

The gravitational potential V in Eq. (6) then takes the following form

$$V(\mathbf{r}) = G \sum_{k=1}^{K} \left[\frac{\rho_0 + \mathbf{\rho_1} \cdot \mathbf{r}}{2} \mathbf{n}_k \cdot \mathbf{G}_k(\mathbf{r}) + \mathbf{\rho_1} \cdot \mathbf{n}_k H_k(\mathbf{r}) \right].$$
(9)

The solution of the surface integral in the vector function $\mathbf{G}_k(\mathbf{r})$ was derived by Pohánka (1998). We use a similar procedure for finding a closed analytical solution of the surface integral in the scalar function $H_k(\mathbf{r})$. Firstly, we apply the Gauss divergence theorem for converting the surface integral to a sum of line integrals along the closed polygon L_k which forms the boundary of the polyhedral face S_k . If $\mathbf{h}_k(\mathbf{s}')$ is a vector function with integrable gradient in the domain S_k , and $\mathbf{n}_k \cdot \mathbf{h}_k(\mathbf{s}') = 0$ (i.e. the vector $\mathbf{h}_k(\mathbf{s}')$ lies in the plane of the polyhedral face S_k), it holds

$$\iint\limits_{S_{l}} \nabla_{\mathbf{s}'} \cdot \mathbf{h} \left(\mathbf{s}' \right) d\sigma' = \oint\limits_{I_{l}} \mathbf{h} \left(\mathbf{l}' \right) \cdot d\boldsymbol{\xi}', \tag{10}$$

where the line element vector $d\xi'$ at the point \mathbf{l}' on the curve L_k is orthogonal to the curve L_k and to the vector \mathbf{n}_k , and it is oriented outwards from the domain S_k . To convert the surface integral in Eq. (8) to a sum of line integrals, we have to find the vector function $\mathbf{h}_k(\mathbf{s}')$ in the domain S_k which satisfies the following two conditions:

$$\nabla_{\mathbf{s}'} \cdot \mathbf{h}_k \left(\mathbf{s}' \right) = \left| \mathbf{s}' - \mathbf{r} \right|, \tag{11}$$

and

$$\mathbf{n}_k \cdot \mathbf{h}_k \left(\mathbf{s}' \right) = 0. \tag{12}$$

For this purpose, we decompose the vector $\mathbf{s}' - \mathbf{r}$ into two subcomponents; the first component $(\mathbf{s}' - \mathbf{r})_{||}$ is parallel to the polyhedral face S_k , and the second component $(\mathbf{s}' - \mathbf{r})_{\perp}$ is perpendicular to the polyhedral face S_k ; i.e.,

$$(\mathbf{s}' - \mathbf{r})_{\perp} = Z_k \mathbf{n}_{\mathbf{k}}, \quad Z_k = \mathbf{n}_{\mathbf{k}} \cdot (\mathbf{s}' - \mathbf{r}),$$
 (13)

$$(\mathbf{s}' - \mathbf{r})_{\parallel} = \mathbf{s}' - \mathbf{r} - (\mathbf{s}' - \mathbf{r})_{\perp}$$
$$= \mathbf{s}' - \mathbf{r} - \mathbf{n}_k \mathbf{n}_k \cdot (\mathbf{s}' - \mathbf{r}). \tag{14}$$

It follows from the second condition (cf. Eq. (12) that the vector $\mathbf{h}_k(\mathbf{s}')$ lies in the plane of the polyhedral face S_k . Therefore, we can write

$$\mathbf{h}_{k}(\mathbf{s}') = (\mathbf{s}' - \mathbf{r})_{||} g(\rho_{k}, z_{k}), \tag{15}$$

where $g(\rho_k, z_k)$ is a scalar function to be found in order to satisfy the first condition given in Eq. (11). The parameters ρ_k and z_k read

$$\rho_k = \left| \left(\mathbf{s}' - \mathbf{r} \right)_{||} \right|, \quad z_k = |Z_k|.$$



The substitution from Eq. (15) to Eq. (11) yields

$$\nabla_{\mathbf{s}'} \cdot \left(\mathbf{s}' - \mathbf{r} \right)_{||} g(\rho_k, z_k) = \left| \mathbf{s}' - \mathbf{r} \right|. \tag{16}$$

We further apply

$$g(\rho_{k}, z_{k}) \nabla_{\mathbf{s}'} \cdot (\mathbf{s}' - \mathbf{r})_{||} + (\mathbf{s}' - \mathbf{r})_{||} \cdot \nabla_{\mathbf{s}'} g(\rho_{k}, z_{k})$$
$$= |\mathbf{s}' - \mathbf{r}|. \tag{17}$$

Since $\nabla_{\mathbf{s}'} \cdot (\mathbf{s}' - \mathbf{r})_{||} = 2$, Eq. (17) becomes

$$2g(\rho_k, z_k) + (\mathbf{s}' - \mathbf{r})_{||} \cdot \nabla_{\mathbf{s}'} g(\rho_k, z_k) = |\mathbf{s}' - \mathbf{r}|, \qquad (18)$$

where $(\mathbf{s}' - \mathbf{r})_{||} \cdot \nabla_{\mathbf{s}'} = \rho_k \ \partial/\partial \rho_k$ (cf. Pohánka 1998).

Realizing that $\mathbf{s}' - \mathbf{r} = (\mathbf{s}' - \mathbf{r})_{||} + (\mathbf{s}' - \mathbf{r})_{\perp} = (\mathbf{s}' - \mathbf{r})_{||} + Z_k \mathbf{n}_k$, we define the right-hand side of Eq. (18) as follows

$$|\mathbf{s}' - \mathbf{r}| = \sqrt{|(\mathbf{s}' - \mathbf{r})_{||}|^2 + |Z_k|^2} = \sqrt{\rho_k^2 + z_k^2}.$$
 (19)

From Eqs. (18) and (19), we get

$$\frac{1}{\rho_k} \frac{\partial}{\partial \rho_k} \rho_k^2 g(\rho_k, z_k) = \sqrt{\rho_k^2 + z_k^2}.$$
 (20)

The general solution of Eq. (20) is found to be

$$g(\rho_k, z_k) = \frac{1}{3\rho_k^2} \left[\left(\rho_k^2 + z_k^2 \right)^{\frac{3}{2}} + c \right], \tag{21}$$

where c is an arbitrary integration constant. However, in order to have the function $\mathbf{h}_k(\mathbf{s}')$ which satisfies the condition of the applicability of the Gauss divergence theorem (i.e. the function $\mathbf{h}_k(\mathbf{s}')$ has the integrable gradient in the whole domain S_k), we have to treat the singularity when $\rho_k \to 0$. The limit $\lim_{\rho_k \to 0} g(\rho_k, z_k) = 0$ only if the integration constant $c = -z_k^3$. The expression in Eq. (21) then becomes

$$g(\rho_k, z_k) = \frac{1}{3\rho_k^2} \left[\left(\rho_k^2 + z_k^2 \right)^{\frac{3}{2}} - z_k^3 \right]. \tag{22}$$

The right-hand side of Eq. (22) is finally rearranged as follows

$$g(\rho_k, z_k) = \frac{1}{3} \frac{\left(\sqrt{\rho_k^2 + z_k^2} - z_k\right) \left(\rho_k^2 + z_k^2 + z_k\sqrt{\rho_k^2 + z_k^2} + z_k^2\right)}{\rho_k^2} = \frac{1}{3} \left(\sqrt{\rho_k^2 + z_k^2} + \frac{z_k^2}{\sqrt{\rho_k^2 + z_k^2} + z_k}\right).$$
(23)

Substituting from Eq. (23) to Eq. (15), we get

$$\mathbf{h}_{k}(\mathbf{s}') = (\mathbf{s}' - \mathbf{r})_{\parallel} \frac{1}{3} \left(\sqrt{\rho_{k}^{2} + z_{k}^{2}} + \frac{z_{k}^{2}}{\sqrt{\rho_{k}^{2} + z_{k}^{2}} + z_{k}} \right).$$
(24)

Consequently, the substitution from Eqs. (13), (14) and (19) to Eq. (24) yields

$$\mathbf{h}_{k}(\mathbf{s}') = \frac{\mathbf{s}' - \mathbf{r} - \mathbf{n}_{k} \mathbf{n}_{k} \cdot (\mathbf{s}' - \mathbf{r})}{3} \times \left[|\mathbf{s}' - \mathbf{r}| + \frac{|\mathbf{n}_{k} \cdot (\mathbf{s}' - \mathbf{r})|^{2}}{|\mathbf{s}' - \mathbf{r}| + |\mathbf{n}_{k} \cdot (\mathbf{s}' - \mathbf{r})|} \right]. \tag{25}$$

From Eqs. (8) and (10), the function $H_k(\mathbf{r})$ becomes

$$H_k(\mathbf{r}) = \oint_{L_k} \mathbf{h}(\mathbf{l}') \cdot d\xi'. \tag{26}$$

Finally, the substitution from Eq. (25) to Eq. (26) yields

$$\begin{aligned}
H_{k}(\mathbf{r}) &= \oint_{L_{k}} \frac{\mathbf{l}' - \mathbf{r} - \mathbf{n}_{k} \mathbf{n}_{k} \cdot (\mathbf{l}' - \mathbf{r})}{3} \\
&\times \left[|\mathbf{l}' - \mathbf{r}| + \frac{|\mathbf{n}_{k} \cdot (\mathbf{l}' - \mathbf{r})|^{2}}{|\mathbf{l}' - \mathbf{r}| + |\mathbf{n}_{k} \cdot (\mathbf{l}' - \mathbf{r})|} \right] \cdot d\xi', \quad (27)
\end{aligned}$$

where $|\mathbf{l'} - \mathbf{r}|$ is the Euclidean spatial distance between the computation point \mathbf{r} and the running integration point $\mathbf{l'}$ on the polygon L_k . Since the vector $\mathbf{d}\boldsymbol{\xi'}$ is perpendicular to the vector \mathbf{n}_k , i.e. $\mathbf{n}_k \cdot \mathbf{d}\boldsymbol{\xi'} = 0$, we write

$$H_{k}(\mathbf{r}) = \oint_{L_{k}} \frac{\mathbf{l}' - \mathbf{r}}{3} \left[|\mathbf{l}' - \mathbf{r}| + \frac{|\mathbf{n}_{k} \cdot (\mathbf{l}' - \mathbf{r})|^{2}}{|\mathbf{l}' - \mathbf{r}| + |\mathbf{n}_{k} \cdot (\mathbf{l}' - \mathbf{r})|} \right] \cdot d\mathbf{\xi}'.$$
(28)

By analogy with the notation used in Pohánka (1988), the polygon segments $\{L_{k,l}: l=1,2,\ldots,L(k)\}$ form the closed polygon L_k of the polyhedral face S_k ; L(k) is the total number of polygon segments $L_{k,l}$ of the polyhedral face S_k . We further denote the position vectors $\mathbf{a}_{k,l}$ and $\mathbf{a}_{k,l+1}$ of the end points of the polygon segment $L_{k,l}$ (note that the vertices of the polyhedral face S_k are numbered in the counter-clockwise sense as viewed from outside, and $\mathbf{a}_{k,L(k)+1} = \mathbf{a}_{k,1}$). For every polygon segment $L_{k,l}$ we define the unit vectors $\mathbf{\mu}_{k,l}$ and $\mathbf{v}_{k,l}$. The unit vector $\mathbf{\mu}_{k,l}$ is parallel with the polygon segment $L_{k,l}$ and has the same orientation. It reads

$$\mu_{k,l} = \frac{\mathbf{a}_{k,l+1} - \mathbf{a}_{k,l}}{d_{k,l}},\tag{29}$$

where $d_{k,l}$ is the length of the segment $L_{k,l}$; i.e.,

$$d_{k,l} = |\mathbf{a}_{k,l+1} - \mathbf{a}_{k,l}|. \tag{30}$$

The unit vector $\mathbf{v}_{k,l}$ is perpendicular to the polygon segment $L_{k,l}$ and lies in the plane of the polyhedral face S_k . It reads

$$\mathbf{v}_{k,l} = \mathbf{\mu}_{k,l} \times \mathbf{n}_k. \tag{31}$$



We define the position vector \mathbf{l}' of the point on the polygon segment $L_{k,l}$ as a function of the unit vector $\boldsymbol{\mu}_{k,l}$ in the following form

$$\mathbf{l}' = \mathbf{a}_{k,l} + \mu_{k,l} \xi' \quad (0 \le \xi' \le d_{k,l}). \tag{32}$$

Similarly, we define the line element vector $d\xi'$ as a function of the unit vector $\mathbf{v}_{k,l}$. We have

$$d\mathbf{\xi}' = \mathbf{v}_{k,l} d\mathbf{\xi}', \tag{33}$$

where $d\xi'$ is the scalar line element of the polygon segment $L_{k,l}$.

Since $\mathbf{n}_k \cdot \mathbf{\mu}_{k,l} = 0$, the quantity $\mathbf{n}_k \cdot (\mathbf{l'} - \mathbf{r}) = \mathbf{n}_k \cdot (\mathbf{a}_{k,l} - \mathbf{r})$ in Eq. (28) neither depends on ξ' nor on the index l. Let us denote

$$z_k(\mathbf{r}) = \left| \mathbf{n}_k \cdot (\mathbf{l}' - \mathbf{r}) \right| = \left| \mathbf{n}_k \cdot (\mathbf{a}_{k,1} - \mathbf{r}) \right|. \tag{34}$$

The line integral in Eq. (28) then takes the following form

$$H_k(\mathbf{r}) = \oint_{I_{,k}} \frac{\mathbf{l}' - \mathbf{r}}{3} \left[\left| \mathbf{l}' - \mathbf{r} \right| + \frac{z_k^2(\mathbf{r})}{\left| \mathbf{l}' - \mathbf{r} \right| + z_k(\mathbf{r})} \right] \cdot d\mathbf{\xi}'. \quad (35)$$

The polygon L_k in Eq. (35) is further rewritten as a sum of the polygon segments $L_{k,l}$. After substituting from Eqs. (32) and (33) to Eq. (35), we have

$$\begin{split} H_k(\mathbf{r}) &= \sum_{l=1}^{L(k)} \int\limits_0^{d_{k,l}} \frac{\mathbf{v}_{k,l} \cdot \left(\mathbf{a}_{k,l} - \mathbf{r} + \mathbf{\mu}_{k,l} \xi'\right)}{3} \\ &\times \left[\left| \mathbf{a}_{k,l} - \mathbf{r} + \mathbf{\mu}_{k,l} \xi'\right| + \frac{z_k^2(\mathbf{r})}{\left| \mathbf{a}_{k,l} - \mathbf{r} + \mathbf{\mu}_{k,l} \xi'\right| + z_k(\mathbf{r})} \right] \mathrm{d} \xi'. \end{split}$$

Since $\mathbf{v}_{k,l} \cdot \mathbf{\mu}_{k,l} = 0$, we arrive at

$$H_{k}(\mathbf{r}) = \sum_{l=1}^{L(k)} \int_{0}^{d_{k,l}} \frac{\mathbf{v}_{k,l} \cdot (\mathbf{a}_{k,l} - \mathbf{r})}{3}$$

$$\times \left[\left| \mathbf{a}_{k,l} - \mathbf{r} + \mathbf{\mu}_{k,l} \xi' \right| + \frac{z_{k}^{2}(\mathbf{r})}{\left| \mathbf{a}_{k,l} - \mathbf{r} + \mathbf{\mu}_{k,l} \xi' \right| + z_{k}(\mathbf{r})} \right] d\xi'. \quad (36)$$

We decompose the vector $\mathbf{a}_{k,l} - \mathbf{r}$ in Eq. (36) into the vector components $\boldsymbol{\mu}_{k,l}$, $\boldsymbol{v}_{k,l}$ and \mathbf{n}_k , and adopt the following notation (cf. Pohánka 1998, Eqs. 28 and 29)

$$u_{k,l}(\mathbf{r}) = \mathbf{\mu}_{k,l} \cdot (\mathbf{a}_{k,l} - \mathbf{r}),$$

$$w_{k,l}(\mathbf{r}) = \mathbf{v}_{k,l} \cdot (\mathbf{a}_{k,l} - \mathbf{r}),$$

$$Z_k(\mathbf{r}) = \mathbf{n}_k \cdot (\mathbf{a}_{k,l} - \mathbf{r}).$$
(37)

From Eqs. (32) and (37), we write

$$|\mathbf{l}' - \mathbf{r}| = |\mathbf{a}_{k,l} - \mathbf{r} + \boldsymbol{\mu}_{k,l} \boldsymbol{\xi}'|$$

$$= \sqrt{(u_{k,l}(\mathbf{r}) + \boldsymbol{\xi}')^2 + w_{k,l}^2(\mathbf{r}) + z_k^2(\mathbf{r})}.$$
(38)

The substitution from Eqs. (37) and (38) to Eq. (36) yields

$$H_k(\mathbf{r}) = \sum_{l=1}^{L(k)} \int_0^{d_{k,l}} \frac{w_{k,l}(\mathbf{r})}{3}$$

$$\times \left[\sqrt{\left(u_{k,l}(\mathbf{r}) + \xi' \right)^2 + w_{k,l}^2(\mathbf{r}) + z_k^2(\mathbf{r})} \right]$$

$$+ \frac{z_k^2(\mathbf{r})}{\sqrt{\left(u_{k,l}(\mathbf{r}) + \xi' \right)^2 + w_{k,l}^2(\mathbf{r}) + z_k^2(\mathbf{r})} + z_k(\mathbf{r})} d\xi'.$$

Furthermore, after applying the substitution $u_{k,l}(\mathbf{r}) + \xi' = \xi$, we get

$$H_{k}(\mathbf{r}) = \sum_{l=1}^{L(k)} \int_{u_{k,l}}^{v_{k,l}} \frac{w_{k,l}(\mathbf{r})}{3} \left[\sqrt{\xi^{2} + w_{k,l}^{2}(\mathbf{r}) + z_{k}^{2}(\mathbf{r})} + \frac{z_{k}^{2}(\mathbf{r})}{\sqrt{\xi^{2} + w_{k,l}^{2}(\mathbf{r}) + z_{k}^{2}(\mathbf{r})} + z_{k}(\mathbf{r})} \right] d\xi,$$
(39)

where

$$v_{k,l}(\mathbf{r}) = u_{k,l}(\mathbf{r}) + d_{k,l}. \tag{40}$$

Denoting

$$\Phi(u, v, w, z) = \int_{u}^{v} \frac{w}{\sqrt{\xi^2 + w^2 + z^2} + z} \, \mathrm{d}\xi,\tag{41}$$

$$\Phi_3(u, v, w, z) = \int_u^v w\sqrt{\xi^2 + w^2 + z^2} \,\mathrm{d}\xi,\tag{42}$$

we finally arrive at

$$H_k(\mathbf{r}) = \frac{1}{3} \sum_{l=1}^{L(k)} \left\{ z_k^2(\mathbf{r}) \, \Phi(u_{k,l}(\mathbf{r}), v_{k,l}(\mathbf{r}), w_{k,l}(\mathbf{r}), z_k(\mathbf{r})) + \Phi_3(u_{k,l}(\mathbf{r}), v_{k,l}(\mathbf{r}), w_{k,l}(\mathbf{r}), z_k(\mathbf{r})) \right\}. \tag{43}$$

The closed analytical expressions for Φ read (Pohánka 1988, 1998)

$$\Phi(u, v, w, z) = wL(u, v, w, z) + 2zA(u, v, w, z), \tag{44}$$

integrating the right-hand side of Eq. (42), we get

$$\Phi_{3}(u, v, w, z) = \frac{w}{4} (v - u) \left[\frac{(v + u)^{2}}{T(u, v, w, z)} + T(u, v, w, z) \right] + \frac{w}{2} \left(w^{2} + z^{2} \right) L(u, v, w, z), \tag{45}$$

where

$$L(u, v, w, z) = \ln \frac{\sqrt{v^2 + w^2 + z^2} + v}{\sqrt{u^2 + w^2 + z^2} + u},$$
(46)

$$A(u, v, w, z) = -\arctan \frac{2w(v - u)}{T(u, v, w, z)^2 - (v - u)^2 + 2zT(u, v, w, z)},$$
(47)

$$T(u, v, w, z) = \sqrt{u^2 + w^2 + z^2} + \sqrt{v^2 + w^2 + z^2}.$$
 (48)

3 The optimum expression for the potential

By analogy with Pohánka (1988, 1998), we optimize the expression for the potential by reducing the number of logarithm and arctangent terms, treating the undefined operations (e.g. expressions of the type 0/0), and improving the computational accuracy. The optimum expression for numerical calculation of the vector function $\mathbf{G}_k(\mathbf{r})$ in Eq. (9) was derived by (Pohánka 1998, Eqs. 33, 34 and 35) in the following form

$$\mathbf{G}_{k}(\mathbf{r}) = \sum_{l=1}^{L(k)} \left\{ \Phi_{2}(u_{k,l}(\mathbf{r}), v_{k,l}(\mathbf{r}), w_{k,l}(\mathbf{r}), Z_{k}(\mathbf{r})) \mathbf{v}_{k,l} + Z_{k}(\mathbf{r}) \Phi(u_{k,l}(\mathbf{r}), v_{k,l}(\mathbf{r}), w_{k,l}(\mathbf{r}), z_{k}(\mathbf{r})) \mathbf{n}_{k} \right\},$$
(49)

where the expression for Φ_2 reads (Pohánka 1998)

$$\Phi_{2}(u, v, w, Z) = \frac{1}{4} (v - u) \left[\frac{(v + u)^{2}}{T(u, v, w, z)} + T(u, v, w, z) \right] + \frac{1}{2} (w^{2} + z^{2}) L(u, v, w, z).$$
(50)

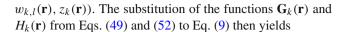
Comparing the expressions for Φ_3 and Φ_2 in Eqs. (45) and (50), the following relation between them is obtained

$$\Phi_3(u, v, w, z) = w \ \Phi_2(u, v, w, Z). \tag{51}$$

Utilizing Eq. (51), the expression for the scalar function $H_k(\mathbf{r})$ in Eq. (43) becomes

$$H_k(\mathbf{r}) = \frac{1}{3} \sum_{l=1}^{L(k)} \left\{ z_k^2(\mathbf{r}) \, \Phi(u_{k,l}(\mathbf{r}), v_{k,l}(\mathbf{r}), w_{k,l}(\mathbf{r}), z_k(\mathbf{r})) + w_{k,l}(\mathbf{r}) \, \Phi_2(u_{k,l}(\mathbf{r}), v_{k,l}(\mathbf{r}), w_{k,l}(\mathbf{r}), Z_k(\mathbf{r})) \right\}$$
(52)

The vectors $\mathbf{\mu}_{k,l}$ and $\mathbf{v}_{k,l}$ are perpendicular to \mathbf{n}_k , i.e. $\mathbf{n}_k \cdot \mathbf{\mu}_{k,l} = 0$ and $\mathbf{n}_k \cdot \mathbf{v}_{k,l} = 0$. From Eq. (50), it also follows that $\Phi_2(u_{k,l}(\mathbf{r}), v_{k,l}(\mathbf{r}), w_{k,l}(\mathbf{r}), Z_k(\mathbf{r})) = \Phi_2(u_{k,l}(\mathbf{r}), v_{k,l}(\mathbf{r}), v_{k,l}(\mathbf{r}))$



$$V(\mathbf{r}) = G \sum_{k=1}^{K} \left[\sum_{l=1}^{L(k)} \left(\frac{\rho_0 + \mathbf{\rho_1} \cdot \mathbf{r}}{2} Z_k(\mathbf{r}) + \frac{\mathbf{\rho_1} \cdot \mathbf{n}_k}{3} z_k^2(\mathbf{r}) \right) \right] \times \Phi(u_{k,l}(\mathbf{r}), v_{k,l}(\mathbf{r}), w_{k,l}(\mathbf{r}), z_k(\mathbf{r})) + \sum_{l=1}^{L(k)} \frac{\mathbf{\rho_1} \cdot \mathbf{n}_k}{3} w_{k,l}(\mathbf{r}) \Phi_2(u_{k,l}(\mathbf{r}), v_{k,l}(\mathbf{r}), v_{k$$

As seen from Eq. (9) only those components of the function $G_k(\mathbf{r})$ contribute to the potential which are parallel to the surface normal (i.e. the components along the unit normal vector \mathbf{n}_k).

The expression for the potential in Eq. (53) has very close resemblances with the formula for the attraction derived by (Pohánka, 1998, Eq. 52). To obtain the final form of Eq. (53) in the same way as Pohánka proposed by introducing a small positive number ε in order to avoid any undefined operations when the computation point is near to the surface of the polyhedral body, cf. Pohánka (1988, 1998), the functions $\Phi(u, v, w, z)$ and $\Phi_2(u, v, w, z)$ are replaced by the functions $\Phi(u, v, w, z, \varepsilon)$ and $\Phi_2(u, v, w, z, \varepsilon)$, respectively. From Eq. (53), we have

$$V(\mathbf{r}, \varepsilon)$$

$$= G \sum_{k=1}^{K} \left[\sum_{l=1}^{L(k)} \left(\frac{\rho_0 + \mathbf{\rho_1} \cdot \mathbf{r}}{2} Z_k(\mathbf{r}) + \frac{\mathbf{\rho_1} \cdot \mathbf{n}_k}{3} z_k^2(\mathbf{r}) \right) \right]$$

$$\times \Phi(u_{k,l}(\mathbf{r}), v_{k,l}(\mathbf{r}), w_{k,l}(\mathbf{r}), z_k(\mathbf{r}), \varepsilon)$$

$$+ \sum_{l=1}^{L(k)} \frac{\mathbf{\rho_1} \cdot \mathbf{n}_k}{3} w_{k,l}(\mathbf{r}) \Phi_2(u_{k,l}(\mathbf{r}), v_{k,l}(\mathbf{r}), v_{k,l}$$

where

$$\Phi(u, v, w, z, \varepsilon) = wL(u, v, w, z + \varepsilon)
+ 2zA(u, v, w, z + \varepsilon),$$
(55)

$$\Phi_{2}(u, v, w, z, \varepsilon) = \frac{1}{4} (v - u) \left[\frac{(v + u)^{2}}{T(u, v, w, z + \varepsilon)} + Tu, v, w, z + \varepsilon) \right] + \frac{1}{2} (w^{2} + z^{2}) L(u, v, w, z + \varepsilon).$$
(56)

The appropriate choice of the parameter ε is discussed in detail in Pohánka (1988, 1998).



4 The algorithm of calculation

For an efficient calculation of the potential given in Eq. (54) we adopted the same optimum algorithm as proposed by Pohánka (1998). The input parameters are: the value of density ρ_0 at a suitably chosen origin of the local coordinate system used for a description of the density model within the volume of the polyhedral body (we note that this coordinate origin can be located either inside or outside of the polyhedral body), the gradient of a linear density distribution function ρ_1 , the total number of polyhedral faces K, and the total number of polygon segments L(k) given for every polyhedral face S_k . For every vertex of the polyhedral face S_k , we compute the radius vector $\mathbf{a}_{k,l}$. As stated previously, the vertices of the polyhedral face S_k are numbered in the counter-clockwise sense as viewed from outside, and $\mathbf{a}_{k,L(k)+1} = \mathbf{a}_{k,1}$. The last input is the radius vector \mathbf{r} of the computation point. We note here that the expression in Eq. (54) for the potential holds for any computation point outside and on the surface of the polyhedral body.

The computation is then realized as follows: We compute the lengths $\{d_{k,l}: l = 1, 2, ..., L(k); k = 1, 2, ..., K\}$ of the polygon segments $L_{k,l}$, and the corresponding unit vectors $\{\mu_{k,l}: l = 1, 2, ..., L(k); k = 1, 2, ..., K\}$ according to the following equations (cf. Eqs. (29), (30))

$$d_{k,l} = |\mathbf{a}_{k,l+1} - \mathbf{a}_{k,l}|, \quad \mathbf{\mu}_{k,l} = \frac{\mathbf{a}_{k,l+1} - \mathbf{a}_{k,l}}{d_{k,l}}.$$

For every polyhedral face $\{S_k : k = 1, 2, ..., K\}$ we compute the unit normal vector \mathbf{n}_k oriented outwards from the polyhedral face S_k using the following expression:

$$\mathbf{n}_k = \frac{\mathbf{N}_k}{|\mathbf{N}_k|},$$

where

$$\mathbf{N}_k = \sum_{l=2}^{L(k)-1} \left(\mathbf{a}_{k,l} - \mathbf{a}_{k,1} \right) \times \left(\mathbf{a}_{k,l+1} - \mathbf{a}_{k,1} \right).$$

For all polygon segments $\{L_{k,l}: l=1,2,\ldots,L(k)\}$ of the polyhedral face S_k we compute the normal unit vectors $\{v_{k,l}: l=1,2,\ldots,L(k)\}$ using Eq. (31); i.e.,

$$\mathbf{v}_{k,l} = \mathbf{\mu}_{k,l} \times \mathbf{n}_k$$
.

We further compute the parameters $u_{k,l}$, $v_{k,l}$, $w_{k,l}$, Z_k and z_k which depend on the position vector **r** of the computation point. With reference to Eqs. (37) and (40), we have

$$u_{k,l} = \mathbf{\mu}_{k,l} \cdot (\mathbf{a}_{k,l} - \mathbf{r}),$$

$$v_{k,l} = u_{k,l} + d_{k,l},$$

$$w_{k,l} = \mathbf{v}_{k,l} \cdot (\mathbf{a}_{k,l} - \mathbf{r}),$$

$$Z_k = \mathbf{n}_k \cdot (\mathbf{a}_{k,1} - \mathbf{r}), \quad z_k = |Z_k|.$$

For the sake of completeness we recapitulate the computation steps given by Pohánka (1998). For the given numbers u, v(v = u + d, d > 0), w, z(z > 0) and the parameter ε , the computation of the functions $\Phi(u, v, w)$ z, ε) and $\Phi_2(u, v, w, z, \varepsilon)$ in Eqs. (55) and (56) is carried out in the following consecutive steps:

- $\begin{array}{ll} \text{(a)} & z_{\varepsilon}=z+\varepsilon,\\ \text{(b)} & W^2=w^2+z^2,\,W_{\varepsilon}^2=w^2+z_{\varepsilon}^2,\\ \text{(c)} & U_{\varepsilon}=\sqrt{u^2+W_{\varepsilon}^2},\,V_{\varepsilon}=\sqrt{v^2+W_{\varepsilon}^2}, \end{array}$
- (d) $T_{\varepsilon} = U_{\varepsilon} + V_{\varepsilon}$,
- (e) $\operatorname{sign}(u) = \operatorname{sign}(v)$: $L_{\varepsilon} = \operatorname{sign}(v) \ln \frac{V_{\varepsilon} + |v|}{U_{\varepsilon} + |u|}$, $\operatorname{sign}(u) \neq$ $\mathrm{sign}(v) \colon L_{\varepsilon} = \ln \frac{\left(V_{\varepsilon} + |v|\right) \left(U_{\varepsilon} + |u|\right)}{W_{c}^{2}},$
- (f) $A_{\varepsilon} = -\arctan \frac{2wd}{(T_{\varepsilon} + d)|T_{\varepsilon} d| + 2T_{\varepsilon}z_{\varepsilon}}$
- (g) $\Phi(u, v, w, z, \varepsilon) = wL_{\varepsilon} + 2z A_{\varepsilon}$,

$$\Phi_2(u, v, w, z, \varepsilon) = \frac{1}{4}d\left[\frac{(v+u)^2}{T_\varepsilon} + T_\varepsilon\right] + \frac{1}{2}W^2 L_\varepsilon.$$

Finally, the potential $V(\mathbf{r}, \varepsilon)$ is obtained from Eq. (54).

5 Concluding remarks

We have derived the analytical formula by means of line integrals for the gravitational potential of an arbitrary polyhedral body having a linearly varying density. The corresponding analytical formula for the Cartesian coordinate components of the gravitational attraction vector was given by Pohánka (1998). As seen from Eq. (9), the derivation of the gravitational potential was reduced to finding only the closed analytical solution of the surface integral in the scalar function $H_k(\mathbf{r})$, while the solution of the surface integral in the vector function $G_k(\mathbf{r})$ was already derived in Pohánka (1998). We further adopted the optimized expressions from Pohánka (1988, 1998) in forming the optimal expression for the gravitational potential by reducing the number of logarithm and arctangent terms, treating the undefined operations, and improving the precision of numerical operations when the computation point is far away from the polyhedral body. Finally, we adopted the optimum algorithm as proposed by Pohánka (1998) for computing the gravitational potential. The optimum expressions and uniform algorithm for computing the gravitational potential and attraction are numerically very simple and they are valid for any point outside and on the surface of the polyhedral body.

The main advantage of using the line integral approach in detailed local gravity field modelling is that it can be utilized for any irregular digital terrain and density models without



additional data pre-processing. The analytical expressions for volume elements with linearly varying density distribution models improve the numerical efficiency in the forward modelling of the gravitational field of geological structures with the variable density distribution such as sedimentary basins where the density increases with depth due to compaction. Moreover, they improve to some extent the numerical efficiency when used for modelling the gravitational field of inhomogeneous density structures which can accurately be approximated by the pricewise linear density model.

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