

# A Design Study Approach to Classical Control

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## Homework C.11

The objective of this problem is to implement state feedback controller using the full state. Start with the simulation files developed in Homework ??.??.

- (a) Using the values for  $\omega_{n_\phi}$ ,  $\zeta_\phi$ ,  $\omega_{n_\theta}$ , and  $\zeta_\theta$  selected in Homework ??.??, find the desired closed loop poles.
- (b) Add the state space matrices  $A$ ,  $B$ ,  $C$ ,  $D$  derived in Homework ??.?? to your param file.
- (c) Verify that the state space system is controllable by checking that  $\text{rank}(\mathcal{C}_{A,B}) = n$ .
- (d) Find the feedback gain  $K$  so that the eigenvalues of  $(A - BK)$  are equal to desired closed loop poles. Find the reference gain  $k_r$  so that the DC-gain from  $\phi_r$  to  $\phi$  is equal to one.
- (e) Implement the state feedback scheme and tune the closed loop poles to get good response. You should be able to get much faster response using state space methods.

## Solution

From HW ??, the state space equations for the satellite are given by

$$\begin{aligned} \dot{x} &= \begin{pmatrix} 0 & 0 & 1.0000 & 0 \\ 0 & 0 & 0 & 1.0000 \\ -0.0300 & 0.0300 & -0.0100 & 0.0100 \\ 0.1500 & -0.1500 & 0.0500 & -0.0500 \end{pmatrix} x + \begin{pmatrix} 0 \\ 0 \\ 0.2 \\ 0 \end{pmatrix} u \\ y &= \begin{pmatrix} 1 & 0 & 0 & 0 \\ -1 & 1 & 0 & 0 \end{pmatrix} x \end{aligned} \quad (1)$$

where Equation (1) represents the measured outputs. The reference output is the angle  $\phi$ , which implies that

$$y_r = \begin{pmatrix} 0 & 1 & 0 & 0 \end{pmatrix} x.$$

**Step 1.** The controllability matrix is

$$\mathcal{C}_{A,B} = [B, AB, A^2B, A^3B] = \begin{pmatrix} 0 & 0.2000 & -0.0020 & -0.0059 \\ 0 & 0 & 0.0100 & 0.0294 \\ 0.2000 & -0.0020 & -0.0059 & 0.0007 \\ 0 & 0.0100 & 0.0294 & -0.0036 \end{pmatrix}.$$

The determinant is  $\det(\mathcal{C}_{A,B}) = -36,000 \neq 0$ , therefore the system is controllable.

**Step 2.** The open loop characteristic polynomial is

$$\Delta_{ol}(s) = \det(sI - A) = s^4 + 0.0600s^3 + 0.18s^2$$

which implies that

$$\begin{aligned} \mathbf{a}_A &= (0.06, 0.18, 0, 0) \\ \mathcal{A}_A &= \begin{pmatrix} 1 & 0.06 & 0.18 & 0 \\ 0 & 1 & 0.06 & 0.18 \\ 0 & 0 & 1 & 0.06 \\ 0 & 0 & 0 & 1 \end{pmatrix}. \end{aligned}$$

**Step 3.** The desired closed loop polynomial is

$$\begin{aligned} \Delta_{cl}^d(s) &= (s^2 + 2\zeta_\theta\omega_{n_\theta}s + \omega_{n_\theta}^2)(s^2 + 2\zeta_\phi\omega_{n_\phi}s + \omega_{n_\phi}^2) \\ &= s^4 + 4.9275s^3 + 12.1420s^2 + 14.6702s + 8.8637, \end{aligned}$$

when  $\omega_\theta = 1.9848$ ,  $\zeta_\theta = 0.707$ ,  $\omega_\phi = 1.5$ ,  $\zeta_\phi = 0.707$ , which implies that

$$\boldsymbol{\alpha} = (4.9275, 12.1420, 14.6702, 8.8637).$$

**Step 4.** The gains are therefore given by

$$\begin{aligned} K &= (\boldsymbol{\alpha} - \mathbf{a}_A) \mathcal{A}_A^{-1} \mathcal{C}_{A,B}^{-1} \\ &= (40.2842, 255.1732, 24.3375, 366.1825) \end{aligned}$$

The feedforward reference gain  $k_r = -1/C_r(A - BK)^{-1}B$  is computed using  $C_r = (0, 1, 0, 0)$ , which gives

$$\begin{aligned} k_r &= \frac{-1}{C_r(A - BK)^{-1}B} \\ &= 295.4573. \end{aligned}$$

Alternatively, we could have used the following Matlab script

```

1 % state space design
2 A = [...
3     0, 0, 1, 0;...
4     0, 0, 0, 1;...
5     -P.k/P.Js, P.k/P.Js, -P.b/P.Js, P.b/P.Js;...
6     P.k/P.Jp, -P.k/P.Jp, P.b/P.Jp, -P.b/P.Jp;...
7
8 ];
9 B = [0; 0; 1/P.Js; 0];
10 Cr = [0, 1, 0, 0];
11
12
13 % gains for pole locations
14 wn_th = 2*0.9924;
15 zeta_th = 0.707;
16 wn_phi = 1*1.5;
17 zeta_phi = 0.707;
18 ol_char_poly = charpoly(A);
19 des_char_poly = conv([1, 2*zeta_th*wn_th, wn_th^2], ...
20                     [1, 2*zeta_phi*wn_phi, wn_phi^2]);
21 des_poles = roots(des_char_poly);
22
23 % is the system controllable?
24 if rank(ctrb(A,B)) < 4, disp('System Not Controllable'); end
25 P.K = place(A,B,des_poles);
26 P.kr = -1/(Cr*inv(A-B*P.K)*B);

```

The Matlab code for the controller is given by

```
1 function tau=satellite_ctrl(in,P)
2     phi_d   = in(1);
3     phi     = in(2);
4     theta   = in(3);
5     t       = in(4);
6
7     % use a digital differentiator to find phidot and thetadot
8     persistent phidot
9     persistent phi_d1
10    persistent thetadot
11    persistent theta_d1
12    % reset persistent variables at start of simulation
13    if t<P.Ts,
14        phidot      = 0;
15        phi_d1      = 0;
16        thetadot    = 0;
17        theta_d1    = 0;
18    end
19    phidot = (2*P.tau-P.Ts)/(2*P.tau+P.Ts)*phidot...
20            + 2/(2*P.tau+P.Ts)*(phi-phi_d1);
21    thetadot = (2*P.tau-P.Ts)/(2*P.tau+P.Ts)*thetadot...
22            + 2/(2*P.tau+P.Ts)*(theta-theta_d1);
23    phi_d1 = phi;
24    theta_d1 = theta;
25
26    % construct the state
27    x = [phi; theta; phidot; thetadot];
28    % compute the state feedback controller
29    tau = sat( -P.K*x + P.kr*phi_d, P.taumax);
30 end
```