

A Design Study Approach to Classical Control

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Homework E.16

For the inner loop of the ball & beam system, use the Matlab `bode` command to create a graph that simultaneously displays the Bode plots for (1) the plant, and (2) the plant under PD control, using the control gains calculated in Homework [E.8](#).

- (a) To what percent error can the closed loop system under PD control track the desired input if all of the frequency content of $\theta_r(t)$ is below $\omega_r = 1.0$ radians per second?
- (b) If the frequency content of the input disturbance is all contained below $\omega_{din} = 0.8$ radians per second, what percentage of the input disturbance shows up in the output?
- (c) If all of the frequency content of the noise $n(t)$ is greater than $\omega_{no} = 300$ radians per second, what percentage of the noise shows up in the output signal θ ?

For the outer loop of the ball & beam, use the Matlab `bode` command to create a graph that simultaneously displays the Bode plots for (1) the plant, and (2) the plant under PID control using the control gains calculated in Homework [E.10](#).

- (d) If the frequency content of an output disturbance is contained below $\omega_{dout} = 0.1$ radian/sec, what percentage of the output disturbance will be contained in the output under PID control?

- (e) If the reference signal is $y_r(t) = 2 \sin(0.6t)$ what is the output error under PID control?

Solution

The Bode plot of the inner loop $P_{in}(s)$, and the loop gain with PD control $P_{in}(s)C_{PD}(s)$, are shown in Figure 1.

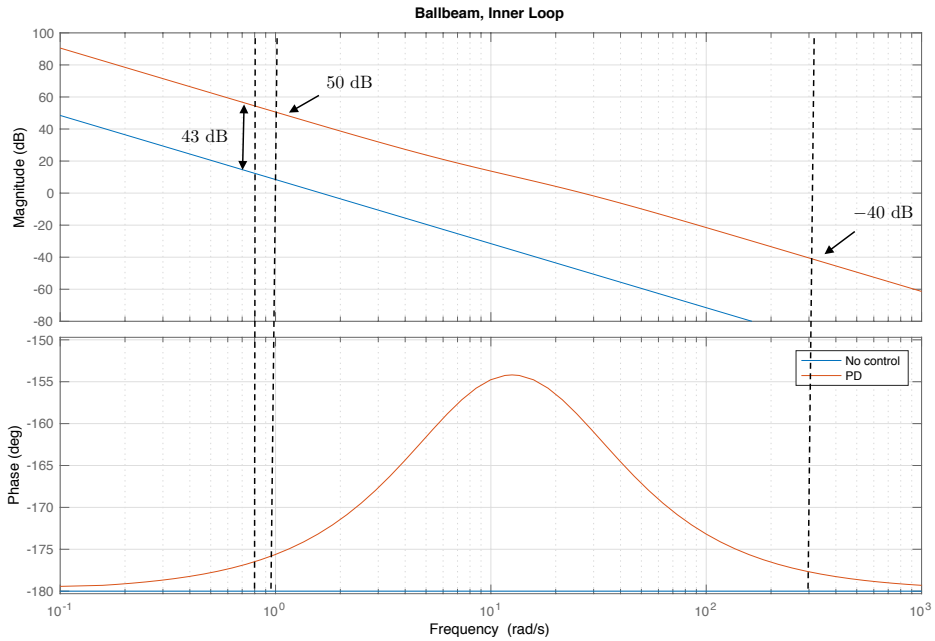


Figure 1: Bode plot for ball and beam inner loop, plant only, and under PD control.

(a) From Figure 1 we see that for $\omega < \omega_r = 1$ rad/sec, the loop gain is greater than $B_r = 50$ dB. Therefore, the tracking error satisfies

$$|e(t)| \leq 10^{-50/20} |r(t)| = 0.0032 |r(t)|,$$

which implies that tracking accuracy is to within 0.32%.

(b) From Figure 1 we see that for $\omega \leq \omega_{d_{in}} = 0.8$ rad/sec, the Bode magnitude plot satisfies

$$20 \log_{10} |P(j\omega)C(j\omega)| - 20 \log_{10} |P(j\omega)| \geq B_{d_{in}} = 43 \text{ dB}.$$

Therefore, the contribution of the input disturbance to the error satisfies

$$|e(t)| \leq 10^{-43/20} |d_{in}(t)| = 0.0071 |d_{in}(t)|,$$

which implies that 0.71% of the input disturbance shows up in the output θ .

(c) For $\omega \geq \omega_{no} = 300$ rad/sec, we see from Figure 1 that $B_{no} = -40$ dB. Therefore, $\gamma_n = 10^{-40/20} = 0.01$ which implies that 1% of the noise will show up in the output signal.

The Bode plot of the outer loop $P_{out}(s)$, and the loop gain with PD control $P_{in}(s)C_{PD}(s)$, and with PID control $P_{in}(s)C_{PID}(s)$ are shown in Figure 2.

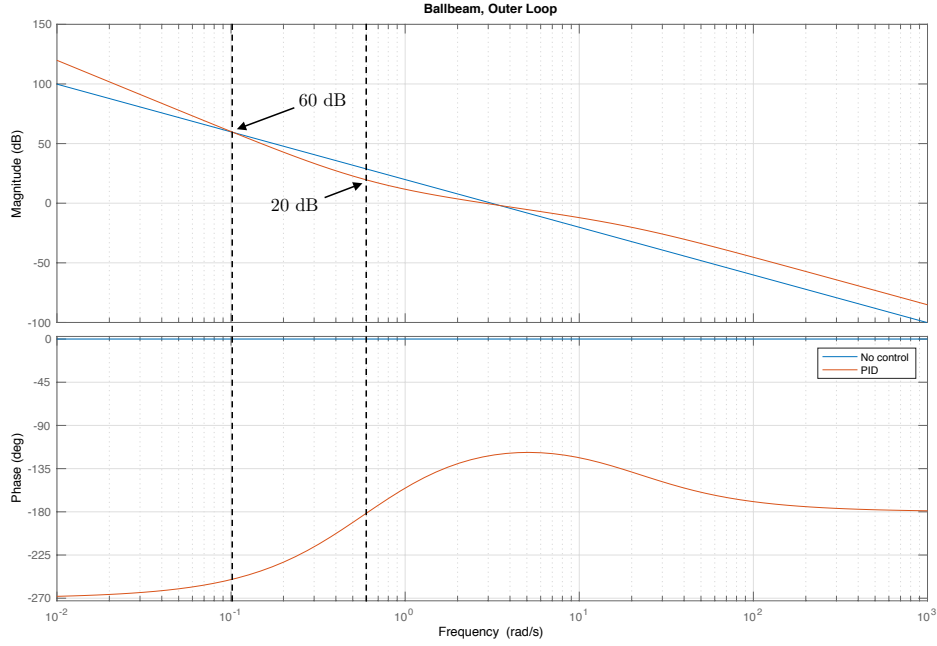


Figure 2: Bode plot for ball and beam outer loop, plant only, under PD control, and under PID control.

(d) For $\omega \leq \omega_{d_{out}} = 0.1$ rad/sec, we see from Figure 2 that for PID control $B_{d_{out}} = 60$ dB. Therefore, $\gamma_{d_{in}} = 10^{-60/20} = 0.001$, which implies that 0.1% of the output disturbance will show up in the output signal.

(e) At $\omega_0 = 0.6$ rad/sec, we see from Figure 2 that the loop gain is

$20 \log_{10} |P(j\omega_0)C_{PD}(j\omega_0)| = 20$ dB. Therefore, the tracking error will be

$$|e(t)| = \left| \frac{1}{1 + P(j\omega_0)C(j\omega_0)} \right| \cdot 2 \approx \left| \frac{1}{P(j\omega_0)C(j\omega_0)} \right| \cdot 2 = \frac{2}{10^{20/20}} = 0.2.$$