## A Design Study Approach to Classical Control

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## Homework F.3

- (a) Find the potential energy for the system.
- (b) Define the generalized coordinates and damping forces.
- (c) Find the generalized forces. Note that the right and left forces are more easily modeled as a total force on the center of mass, and a torque about the center of mass.
- (d) Derive the equations of motion for the planar VTOL system using the Euler-Lagrange equations.
- (e) Referring to Appendices P.1, P.2, and P.3, write a class or s-function that implements the equations of motion. Simulate the system using a variable force inputs  $f_r$  and  $f_\ell$ . The output should connect to the animation function developed in homework F.2.

## Solution

The generalized coordinates for the system are the lateral position of the center pod z, the altitude of the center pod h, and the angle of the rotors  $\theta$ . Therefore, let  $\mathbf{q} = (z, h, \theta)^{\top}$ .

Let  $P_0$  be the potential energy when z = 0, h = 0, and  $\theta = 0$ . Then the potential energy of the planar VTOL system is the sum of the potential

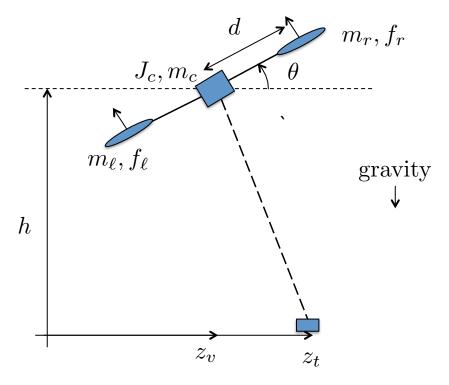


Figure 1: Finding the equations of motion for the planar VTOL system.

energy of the center of mass center pod, and the potential energy of each rotor, modeled as a point mass:

$$P = P_0 + m_c g h + m_r g (h + d \sin \theta) + m_l g (h - d \sin \theta)$$
  
=  $(m_c + 2m_r)g h + P_0$ .

The external forces acting in the direction of z, h, and  $\theta$  are

$$\tau_1 = -(f_r + f_l) \sin \theta$$
  

$$\tau_2 = (f_r + f_l) \cos \theta$$
  

$$\tau_3 = d(f_r - f_l).$$

Momentum drag induces a viscous friction term in the direction of z, therefore

$$-B\dot{\mathbf{q}} = \begin{pmatrix} -\mu & 0 & 0\\ 0 & 0 & 0\\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} \dot{z}\\ \dot{h}\\ \dot{\theta} \end{pmatrix} = \begin{pmatrix} -\mu\dot{z}\\ 0\\ 0 \end{pmatrix}.$$

From problem F.1, the kinetic energy is

$$K = \frac{1}{2}(m_c + 2m_r)\dot{z}^2 + \frac{1}{2}(m_c + 2m_r)\dot{h}^2 + \frac{1}{2}(J_c + 2m_r d^2)\dot{\theta}^2.$$

The Lagrangian is therefore given by

$$L = \frac{1}{2}(m_c + 2m_r)\dot{z}^2 + \frac{1}{2}(m_c + 2m_r)\dot{h}^2 + \frac{1}{2}(J_c + 2m_rd^2)\dot{\theta}^2 - (m_c + 2m_r)gh - P_0.$$

The Euler Lagrange equations are

$$\frac{d}{dt} \left( \frac{\partial L}{\partial \dot{z}} \right) - \frac{\partial L}{\partial z} = \tau_1 - \mu \dot{z}$$

$$\frac{d}{dt} \left( \frac{\partial L}{\partial \dot{h}} \right) - \frac{\partial L}{\partial h} = \tau_2$$

$$\frac{d}{dt} \left( \frac{\partial L}{\partial \dot{\theta}} \right) - \frac{\partial L}{\partial \theta} = \tau_3,$$

where

$$\frac{\partial L}{\partial \dot{z}} = (m_c + 2m_r)\dot{z}$$

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{z}}\right) = (m_c + 2m_r)\ddot{z}$$

$$\frac{\partial L}{\partial z} = 0$$

$$\frac{\partial L}{\partial \dot{h}} = (m_c + 2m_r)\dot{h}$$

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{h}}\right) = (m_c + 2m_r)\ddot{h}$$

$$\frac{\partial L}{\partial \dot{h}} = -(m_c + 2m_r)g$$

$$\frac{\partial L}{\partial \dot{\theta}} = (J_c + 2m_r d^2)\dot{\theta}$$

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\theta}}\right) = (J_c + 2m_r d^2)\ddot{\theta}$$

$$\frac{\partial L}{\partial \theta} = 0.$$

Therefore the equations of motion are

$$(m_c + 2m_r)\ddot{z} = -(f_r + f_l)\sin\theta - \mu\dot{z}$$
$$(m_c + 2m_r)\ddot{h} + (m_c + 2m_r)g = (f_r + f_l)\cos\theta$$
$$(J_c + 2m_rd^2)\ddot{\theta} = d(f_r - f_l)$$

Using matrix notation, this equation can be rearranged to isolate the second order derivatives on the left and side

$$\begin{pmatrix} m_c + 2m_r & 0 & 0 \\ 0 & m_c + 2m_r & 0 \\ 0 & 0 & J_c + 2m_r d^2 \end{pmatrix} \begin{pmatrix} \ddot{z} \\ \ddot{h} \\ \ddot{\theta} \end{pmatrix} = \begin{pmatrix} -(f_r + f_l)\sin\theta - \mu\dot{z} \\ -(m_c + 2m_r)g + (f_r + f_l)\cos\theta \\ d(f_r - f_l) \end{pmatrix}.$$
(1)

Equation (1) represents the simulation model for the ball on beam system.