

A Design Study Approach to Classical Control

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Homework D.18

For this homework assignment we will use the loopshaping design technique to design a controller for the mass spring damper problem with dynamics given by

$$Z(s) = \left(\frac{\frac{1}{m}}{s^2 + \frac{b}{m}s + \frac{k}{m}} \right) F(s).$$

The controller designed in this problem will take the form

$$F = C(s)E(s),$$

where the error signal is $e = z_f^r - z$, where z_f^r is the prefiltered reference command. Find the controller $C(s)$ so that the closed loop system meets the following specifications.

- Reject constant input disturbances.
- Track reference signals with frequency content below $\omega_r = 0.1$ rad/s to within $\gamma_r = 0.03$.
- Attenuate noise on the measurement of z for all frequencies above $\omega_n = 500$ rad/s by $\gamma_n = 0.001$.
- The phase margin is close to $PM = 60$ degrees.
- Use a prefilter to reduce any peaking in the closed loop response.

Solution

From HW D.5, the transfer function model is

$$\tilde{Z}(s) = \frac{\frac{1}{m}}{s^2 + \frac{b}{m}s + \frac{k}{m}} \tilde{F}(s) \triangleq P(s) \tilde{F}(s).$$

Figure 1 shows the Bode plot for P together with the design specification on tracking and attenuating the noise. The requirement to reject constant input disturbances requires the inclusion of an integrator which is not shown in Figure 1.

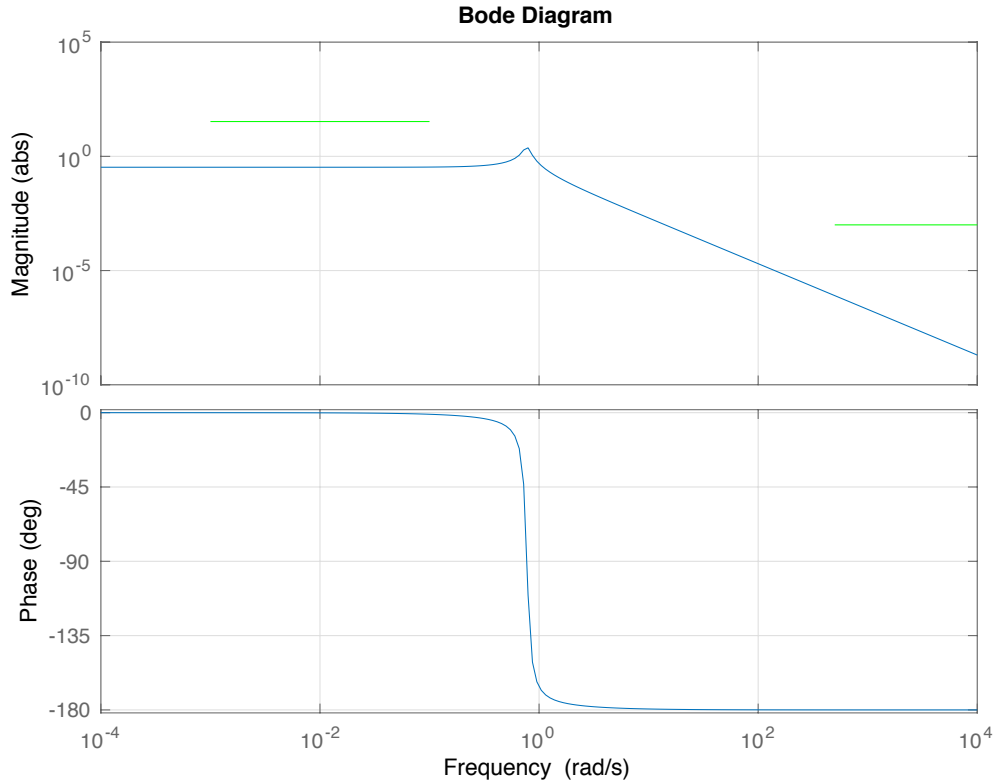


Figure 1: The Bode plot for the plant in HW D.18, together with the design specifications.

The first step is to add PI compensation to meet the requirement on rejecting input disturbances. Figure 2 shows the loop gain after adding the

PI control

$$C_{int} = \frac{s + 0.2}{s}.$$

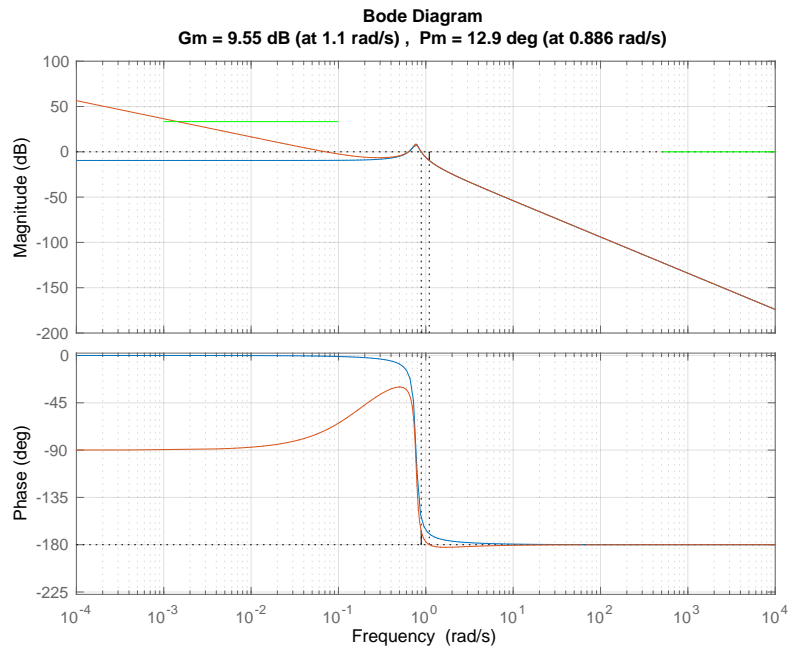


Figure 2: The Bode plot for the outer loop system in HW [D.18](#), with PI control.

Our goal is to cross over the system midway between the low and high

frequency constraints. Let's choose $\omega_{co} = 7 \text{ rad/s}$. At this frequency, the PM is slightly negative. We will add 60 deg of PM to stabilize and add damping to the system. Figure 3 shows the loopgain with the addition of the phase lead filter

$$C_{lead} = \frac{s + 1.88}{s + 26.1},$$

and the proportional gain $k_P = 13.9$.

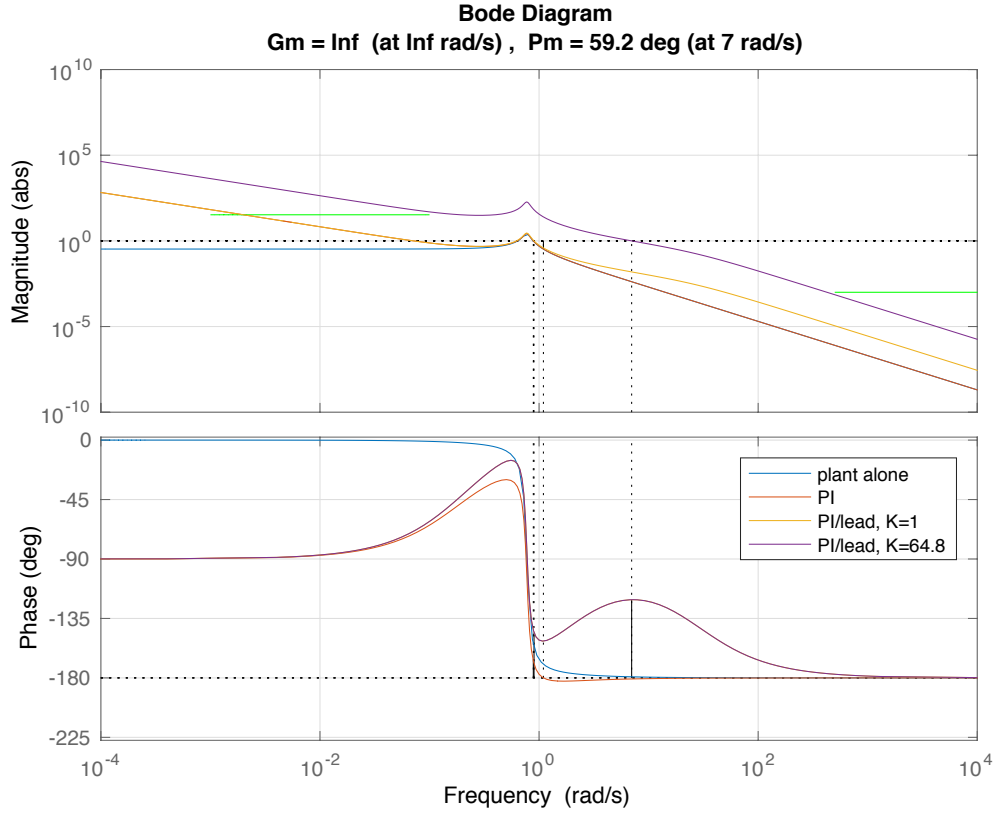


Figure 3: The Bode plot for the system in HW D.18, with integral, phase lead, and proportional control.

Since the phase margin is $PM = 59.2 \text{ deg}$, we consider the phase margin specification to be satisfied. The resulting compensator is

$$C(s) = 903 \left(\frac{s + 0.2}{s} \right) \left(\frac{s + 1.88}{s + 26.1} \right).$$

The closed-loop response, as well as the unit-step response for the output and control signal are all show in Figure 4, where the prefilter

$$F(s) = \frac{2}{s + 2}$$

has been added to reduce the peaking in the closed loop response.

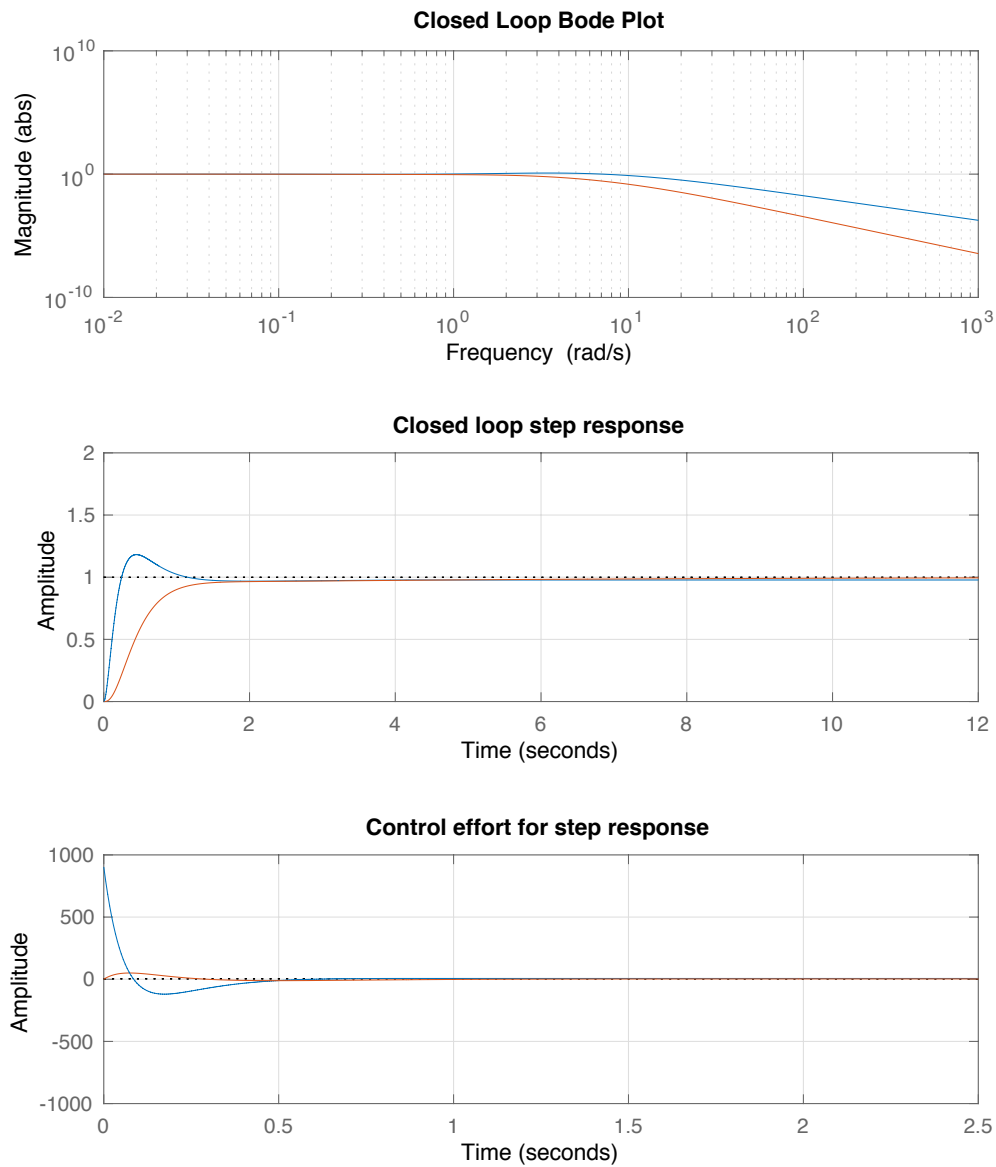


Figure 4: The closed loop bode response, the unit step response for the output, and the unit step response for the input for the design in HW [D.18](#).

The Matlab code used to design the outer loop is shown below.

```

1
2 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```

```

3   Define Design Specifications
4   %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
5
6   --- general tracking specification ---
7       omega_r = 0.1; % track signals below this frequency
8       gamma_r = 0.03; % tracking error below this value
9       w = logspace(log10(omega_r)-2,log10(omega_r));
10
11  --- noise specification ---
12      omega_n = 500; % attenuate noise above this frequency
13      gamma_n = 0.001; % attenuate noise by this amount
14      w = logspace(log10(omega_n),2+log10(omega_n));
15
16  %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
17  Control Design
18      C = tf(1,1);
19  %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
20
21  integral control:
22      k_I = 0.2; % frequency at which integral action ends
23      Integrator = tf([1,k_I],[1,0]);
24      C = C*Integrator;
25
26  phase lead: increase PM (stability)
27      w_max = 7; % location of maximum frequency bump
28      phi_max = 60*pi/180;
29      M = (1+sin(phi_max))/(1-sin(phi_max)) % lead ratio
30      z = w_max/sqrt(M)
31      p = w_max*sqrt(M)
32      Lead = tf([1/z 1],[1/p 1]);
33      C = C*Lead;
34
35  find gain to set crossover at w_max = 7 rad/s
36      [m,p] = bode(C*Plant,w_max);
37      K = 1/m;
38      C = K*C;
39
40  %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
41  Prefilter Design
42      F = tf(1,1);
43  %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
44
45  low pass filter
46      p = 2; % frequency to start the LPF
47      LPF = tf(p, [1,p]);

```



```

48     F = F*LPF;
49
50 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
51 Convert controller to state space equations
52 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
53     [num,den] = tfdata(C, 'v');
54     [P.A_C,P.B_C,P.C_C,P.D_C]=tf2ss(num,den);
55
56     [num,den] = tfdata(F, 'v');
57     [P.A_F, P.B_F, P.C_F, P.D_F] = tf2ss(num,den);

```

The complete Simulink files are on the wiki associated with the book.