

# A Design Study Approach to Classical Control

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## Homework F.9

- (a) When the longitudinal controller for the VTOL system is PD control, what is the system type? Characterize the steady state error when  $h^d$  is a step, a ramp, and a parabola. How does this change if you add an integrator? What is the system type with respect to an input disturbance for both PD and PID control?
- (b) When the inner loop of the lateral controller for the VTOL system is PD control, what is the system type of the inner loop? Characterize the steady state error when  $\tilde{\theta}^d$  is a step, a ramp, and a parabola. What is the system type with respect to an input disturbance?
- (c) When the outer loop of the lateral controller for the VTOL system is PD control, what is the system type of the outer loop? Characterize the steady state error when  $z^d$  is a step, a ramp, and a parabola. How does this change if you add an integrator? What is the system type with respect to an input disturbance for both PD and PID control?

## Solution

The closed loop system is shown in Figure [1](#).

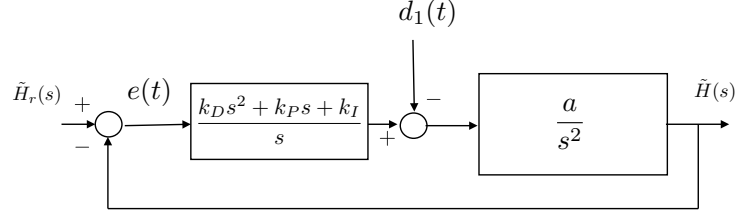


Figure 1: Closed loop system for problem HW F.9.

The open-loop transfer function is given by

$$P(s)C(s) = \left( \frac{a}{s^2} \right) \left( \frac{k_D s^2 + k_P s + k_I}{s} \right),$$

where

$$a = \frac{1}{m_c + 2m_r}.$$

Without the integrator ( $k_I = 0$ ) the system has two free integrators and is therefore type 2, which, from Table 9-1 implies that the tracking error when the input is a step and ramp is zero and when it is a parabola is

$$\lim_{t \rightarrow \infty} e(t) = \frac{1}{1 + M_a} = \frac{1}{1 + \lim_{s \rightarrow 0} s^2 P(s)C(s)} = \frac{1}{ak_P}.$$

With the integrator, the system is type 3 and there is zero steady state error to a step, ramp, and parabola.

For the input disturbance, the transfer function from  $D(s)$  to  $E(s)$  is given by

$$\begin{aligned} E(s) &= \frac{P(s)}{1 + P(s)C(s)} D(s) \\ &= \frac{as}{s^3 + (ak_D)s^2 + (ak_P)s + (ak_I)}. \end{aligned}$$

When  $D(s) = \frac{A}{s^{q+1}}$ , the steady state error is given by

$$\begin{aligned} \lim_{t \rightarrow \infty} e(t) &= \lim_{s \rightarrow 0} \frac{sP}{1 + PC} \frac{A}{s^{q+1}} \\ &= \lim_{s \rightarrow 0} \frac{as}{s^3 + (ak_D)s^2 + (ak_P)s + (ak_I)} \frac{A}{s^q}. \end{aligned}$$

Without the integrator we have

$$\lim_{t \rightarrow \infty} e(t) = \frac{A}{k_P}.$$

when  $q = 0$ . Therefore, to an input disturbance the system is type 0, and the steady state error to a constant step of size  $A$  on  $d(t)$  is  $\frac{A}{k_P}$ . With the integrator we have

$$\lim_{t \rightarrow \infty} e(t) = \frac{A}{k_I},$$

when  $q = 1$ . Therefore, to an input disturbance the system is type 1, and the steady state error to a constant ramp of size  $A$  on  $d(t)$  is  $\frac{A}{k_I}$ .

The inner loop for the lateral control is identical to part (a) with only a difference in the constant  $a$ .

The block diagram for the outer loop of the lateral controller is shown in Figure 2.

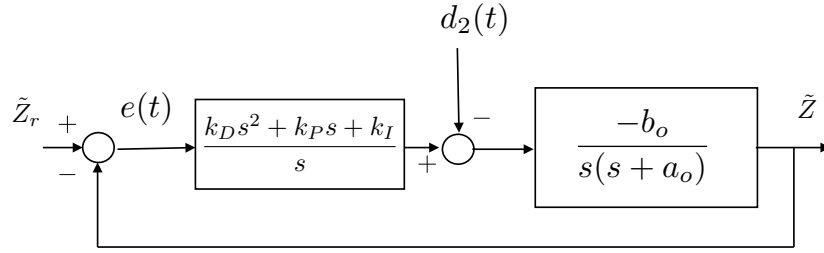


Figure 2: Outer loop system for problem HW F.9.

The open loop system is given by

$$P(s)C(s) = \left( \frac{-b_o}{s(s + a_o)} \right) \left( \frac{k_D s^2 + k_P s + k_I}{s} \right),$$

where

$$a_o = \frac{\mu}{m_c + 2m_r}$$

$$b_o = \frac{F_e}{m_c + 2m_r}.$$

When  $k_I = 0$  there is one free integrator in  $P(s)C(s)$  and the system is type 1, and from Table 9-1 the tracking error when the input is a step is

$$\lim_{t \rightarrow \infty} e(t) = \frac{1}{M_v} = \frac{1}{\lim_{s \rightarrow 0} sP(s)C(s)} = -\frac{a_o}{b_o k_P}.$$

When  $k_I \neq 0$ , there are two free integrators in  $P(s)C(s)$  and the system is type 2. From Table 9-1 the tracking error when the input is a parabola is

$$\lim_{t \rightarrow \infty} e(t) = \frac{1}{M_a} = \frac{1}{\lim_{s \rightarrow 0} s^2 P(s)C(s)} = -\frac{a_o}{b_o k_I}.$$

For the input disturbance, the transfer function from  $D(s)$  to  $E(s)$  is given by

$$\begin{aligned} E(s) &= \frac{P(s)}{1 + P(s)C(s)} D(s) \\ &= \frac{-b_o s}{s^3 + (a_o - b_o k_D)s^2 + (-b_o k_P)s + (-b_o k_I)}. \end{aligned}$$

When  $D(s) = \frac{A}{s^{q+1}}$ , the steady state error is given by

$$\begin{aligned} \lim_{t \rightarrow \infty} e(t) &= \lim_{s \rightarrow 0} \frac{sP}{1 + PC} \frac{A}{s^{q+1}} \\ &= \lim_{s \rightarrow 0} \frac{-b_o s}{s^3 + (a_o - b_o k_D)s^2 + (-b_o k_P)s + (-b_o k_I)} \frac{A}{s^q}. \end{aligned}$$

Without the integrator we have

$$\lim_{t \rightarrow \infty} e(t) = \frac{A}{k_P}$$

when  $q = 0$ . Therefore, to an input disturbance the system is type 0, and the steady state error to a constant step of size  $A$  on  $d(t)$  is  $\frac{A}{k_P}$ . With the integrator we have

$$\lim_{t \rightarrow \infty} e(t) = \frac{A}{k_I},$$

when  $q = 1$ . Therefore, to an input disturbance the system is type 1, and the steady state error to a constant ramp of size  $A$  on  $d(t)$  is  $\frac{A}{k_I}$ .