A Design Study Approach to Classical Control

Randal W. Beard Timothy W. McLain Brigham Young University

Updated: August 29, 2016

Homework B.6

Defining the states as $\tilde{x} = (\tilde{z}, \tilde{\theta}, \dot{\tilde{z}}, \dot{\tilde{\theta}})^{\top}$, the input as $\tilde{u} = \tilde{F}$, and the measured output as $\tilde{y} = (\tilde{z}, \tilde{\theta})^{\top}$, find the linear state space equations in the form

$$\begin{split} \dot{\tilde{x}} &= A\tilde{x} + B\tilde{u} \\ \tilde{y} &= C\tilde{x} + D\tilde{u}. \end{split}$$

Solution

The linear state space equations can be derived in two different ways: (1) directly from the linearized equations of motion, and (2) by linearizing the nonlinear equations of motion.

Starting with the linear state space equation in Equation (4.12) and solving for $(\ddot{\tilde{z}}, \ddot{\tilde{\theta}})^{\top}$ gives

$$\begin{pmatrix} \ddot{\tilde{z}} \\ \ddot{\tilde{\theta}} \end{pmatrix} = \frac{\begin{pmatrix} m_1 \frac{\ell^2}{4} & -m_1 \frac{\ell}{2} \\ -m_1 \frac{\ell}{2} & (m_1 + m_2) \end{pmatrix}}{m_1^2 \frac{\ell^2}{4} + m_1 m_2 \frac{\ell^2}{4} - m_1^2 \frac{\ell^2}{4}} \begin{pmatrix} -b \dot{\tilde{z}} + \tilde{F} \\ m_1 g \frac{\ell}{2} \tilde{\theta} \end{pmatrix}$$

$$= \begin{pmatrix} -\frac{b}{m_2} \dot{\tilde{z}} + \frac{1}{m_2} \tilde{F} - \frac{m_1 g}{m_2} \tilde{\theta} \\ 2\frac{b}{m_2 \ell} \dot{\tilde{z}} - \frac{2}{m_2 \ell} \tilde{F} + \frac{(m_1 + m_2)g}{m_2 \ell} \tilde{\theta} \end{pmatrix}.$$

Therefore, defining $\tilde{x} = (\tilde{x}_1, \tilde{x}_2, \tilde{x}_3, \tilde{x}_4)^{\top} \stackrel{\triangle}{=} (\tilde{z}, \tilde{\theta}, \dot{\tilde{z}}, \dot{\tilde{\theta}})^{\top}$, and $\tilde{u} = \tilde{F}$ gives

$$\dot{\tilde{x}} \stackrel{\triangle}{=} \begin{pmatrix} \dot{\tilde{x}}_1 \\ \dot{\tilde{x}}_2 \\ \dot{\tilde{x}}_3 \\ \dot{\tilde{x}}_4 \end{pmatrix} = \begin{pmatrix} \dot{\tilde{z}} \\ \dot{\tilde{\theta}} \\ \ddot{\tilde{z}} \\ \dot{\tilde{g}} \\ \dot{\tilde{g}} \end{pmatrix} = \begin{pmatrix} \tilde{x}_3 \\ \tilde{x}_4 \\ -\frac{b}{m_2} \tilde{x}_3 + \frac{1}{m_2} \tilde{u} - \frac{m_1 g}{m_2} \tilde{x}_2 \\ \frac{2b}{m_2 \ell} \tilde{x}_3 - \frac{2}{m_2 \ell} \tilde{u} + \frac{2(m_1 + m_2)g}{m_2 \ell} \tilde{x}_2 \end{pmatrix} \\
= \begin{pmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & -\frac{m_1 g}{m_2} & -\frac{b}{m_2} & 0 \\ 0 & \frac{2(m_1 + m_2)g}{m_2 \ell} & \frac{2b}{m_2 \ell} & 0 \end{pmatrix} \begin{pmatrix} \tilde{x}_1 \\ \tilde{x}_2 \\ \tilde{x}_3 \\ \tilde{x}_4 \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ \frac{1}{m_2} \\ -\frac{2}{m_2 \ell} \end{pmatrix} \tilde{u}.$$

Assuming that the measured output of the system is $\tilde{y} = (\tilde{z}, \tilde{\theta})^{\top}$, the linearized output is given by

$$\tilde{y} = \begin{pmatrix} \tilde{z} \\ \tilde{\theta} \end{pmatrix} = \begin{pmatrix} \tilde{x}_1 \\ \tilde{x}_2 \end{pmatrix} = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{pmatrix} \begin{pmatrix} \tilde{x}_1 \\ \tilde{x}_2 \\ \tilde{x}_3 \\ \tilde{x}_4 \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \end{pmatrix} \tilde{u}.$$

Therefore, the linearized state space equations are given by

$$\dot{\tilde{x}} = \begin{pmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & -\frac{m_1 g}{m_2} & -\frac{b}{m_2} & 0 \\ 0 & \frac{2(m_1 + m_2)g}{m_2 \ell} & \frac{2b}{m_2 \ell} & 0 \end{pmatrix} \tilde{x} + \begin{pmatrix} 0 \\ 0 \\ \frac{1}{m_2} \\ -\frac{2}{m_2 \ell} \end{pmatrix} \tilde{u}$$

$$\tilde{y} = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{pmatrix} \tilde{x}.$$
(1)

Alternatively, the linearized state space equations can be derived from the nonlinear equations of motion. Starting with Equation (3.2) and solving for $(\ddot{z}, \ddot{\theta})^{\top}$ gives

$$\begin{pmatrix} \ddot{z} \\ \ddot{\theta} \end{pmatrix} = \frac{\begin{pmatrix} m_1 \frac{\ell^2}{4} & -m_1 \frac{\ell}{2} \cos \theta \\ -m_1 \frac{\ell}{2} \cos \theta & (m_1 + m_2) \end{pmatrix}}{m_1 m_2 \frac{\ell^2}{4} + m_1^2 \frac{\ell^2}{4} \sin^2 \theta} \begin{pmatrix} m_1 \frac{\ell}{2} \dot{\theta}^2 - b \dot{z} + F \\ m_1 g \ell \sin \theta \end{pmatrix}$$

$$= \frac{\begin{pmatrix} m_1 \frac{\ell^2}{4} \dot{\theta}^2 \sin \theta - b m_1 \frac{\ell^2}{4} \dot{z} + m_1 \frac{\ell^2}{4} F - m_1^2 \frac{\ell^2}{4} g \sin \theta \cos \theta \\ -m_1^2 \frac{\ell^2}{4} \dot{\theta}^2 \sin \theta \cos \theta - b m_1 \frac{\ell^2}{4} \dot{z} \cos \theta - m_1 \frac{\ell}{2} \cos \theta F + (m_1 + m_2) m_1 g \frac{\ell}{2} \sin \theta \end{pmatrix}$$

$$= \frac{m_1 m_2 \frac{\ell^2}{4} \dot{\theta}^2 \sin \theta \cos \theta - b m_1 \frac{\ell^2}{4} \dot{z} \cos \theta - m_1 \frac{\ell}{2} \cos \theta F + (m_1 + m_2) m_1 g \frac{\ell}{2} \sin \theta}{m_1 m_2 \frac{\ell^2}{4} + m_1^2 \frac{\ell^2}{4} \sin^2 \theta}$$

Defining $x \stackrel{\triangle}{=} (z, \theta, \dot{z}, \dot{\theta})^{\top}$, u = F, and $y = (z, \theta)^2$ results in the nonlinear state space equations

$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{pmatrix} = \begin{pmatrix} x_3 \\ x_4 \\ \frac{m_1^2 \frac{\ell^2}{4} x_4^2 \sin x_2 - b m_1 \frac{\ell^2}{4} x_3 + m_1 \frac{\ell^2}{4} u - m_1^2 \frac{\ell^2}{4} g \sin x_2 \cos x_2}{m_1 m_2 \frac{\ell^2}{4} + m_1^2 \frac{\ell^2}{4} \sin^2 x_2} \\ \frac{-m_1^2 \frac{\ell^2}{4} x_4^2 \sin x_2 \cos x_2 - b m_1 \frac{\ell^2}{4} x_3 \cos x_2 - m_1 \frac{\ell}{2} \cos \theta u + (m_1 + m_2) m_1 g \frac{\ell}{2} \sin x_2}{m_1 m_2 \frac{\ell^2}{4} + m_1^2 \frac{\ell^2}{4} \sin^2 x_2} \end{pmatrix} \stackrel{\triangle}{=} f(x, u)$$

$$y = \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} \stackrel{\triangle}{=} h(x, u).$$

Taking the Jacobians about the equilibrium $x_e = (z_e, 0, 0, 0)^{\mathsf{T}}$ gives

resulting in the linearized state space equations given in Equation (1).