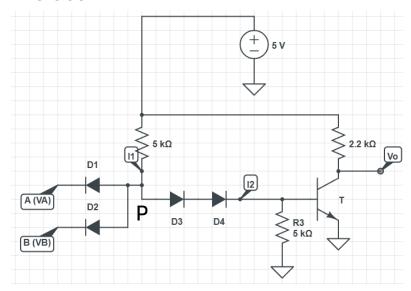
# **Basic Operation**

# **Exercise 1**



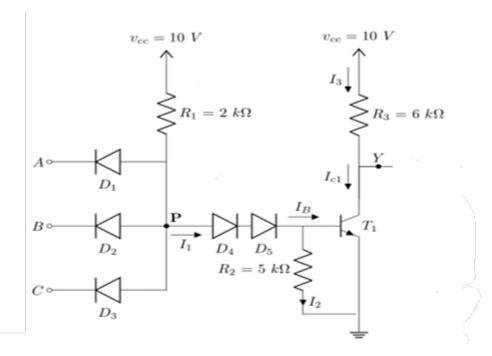
For the DTL NAND gate-Find all the voltages & currents for all logic cases with verification of assumption.

Assume high input = 5 V, low input = 0.2 V

$$V S.0, V S = _{o}V$$

$$Am S8.0 = _{\Omega A} _{z}I$$

$$Am I4.0 = _{z}I = _{z}I$$



For the above circuit,  $V_{OH}=9.5~V$  ,  $V_{OL}=0.1~V$  ,  $\beta_F=30$ 

- a) Find the value of  $\beta_{min}$  when all inputs are high.
- b) If all the inputs are high, what is the magnitude of noise voltage at input A, that would cause the gate to malfunction?
- c) If at least one input is low, what is the magnitude of noise voltage at input A, that would cause the gate to malfunction?

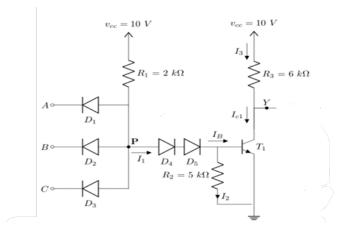
144.0 (n:2nh V 4.8 (d V 9.0 (2

# **Practice Problem 1:**

What is the current through  $D_B$  in the circuit of **Exercise 2**, for the logic case (1,0,0)?

# **Power Dissipation**

### **Exercise 3**



- a) Find power dissipation for all cases.
- b) Maximum & average power dissipation.

Wm 2.22, Wm 42.24 (s. snA) Wm 287.34, Wm 2.22 (d

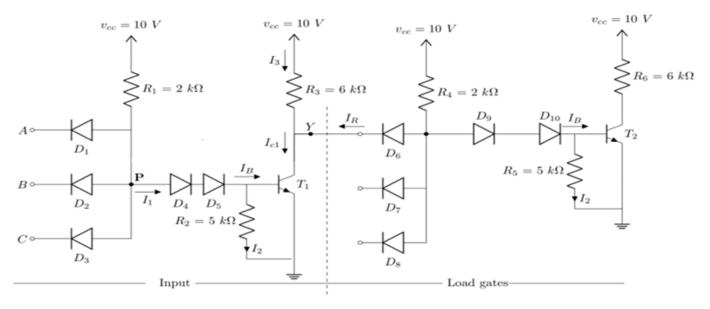
# **Practice Problem 2:**

If the number of inputs to the DTL NAND gate in **Exercise 3**, is increased to 5, what will be the maximum & average power dissipation?

Wm 28.24, Wm 2.22: snA

### **Fanout**

### **Exercise 4**



For the above circuit-  $V_{OH}=9.5~V$  ,  $V_{OL}=0.1~V$  ,  $\beta_F=30$ 

- a) Find the maximum fanout.
- b) Find the maximum power dissipation of the driver circuit, when N (maximum fanout) loads are connected.

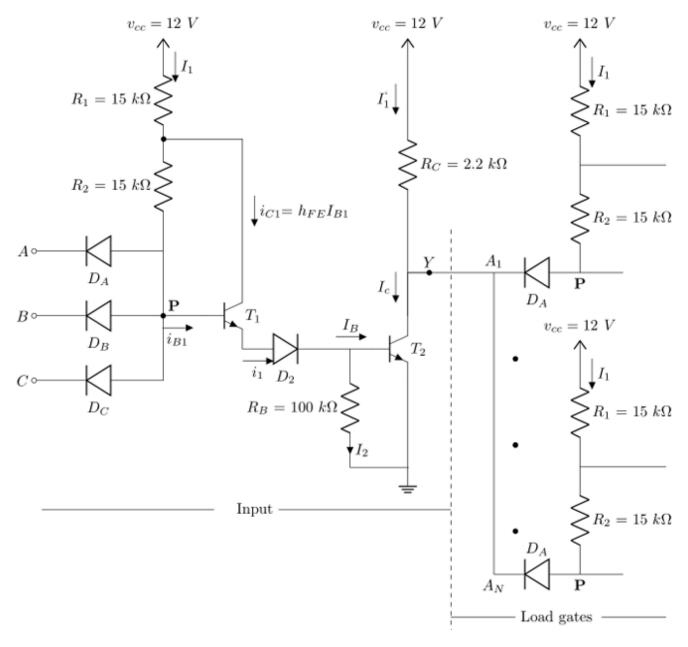
42 (n :2nA Wm 42.99 (d

# **Practice Problem 3:**

Find the value of  $R_3$  that would reduce the maximum fanout found in **Exercise 4** to 20.  $v_{06t}:su_{V}$ 

### **Modified DTL**

### **Exercise 5**



For the circuit above-  $V_{OH}=11.5~V$  ,  $V_{OL}=0.2~V$  ,  $\beta_F=30$ 

- a) Find the value of  $\beta_{min}$  when all inputs are high.
- b) Find the maximum fanout.
- c) Find the power dissipation of the driver for all cases.
- d) If all the inputs are high, what is the magnitude of noise voltage at the input

A, that would cause the gate to malfunction?

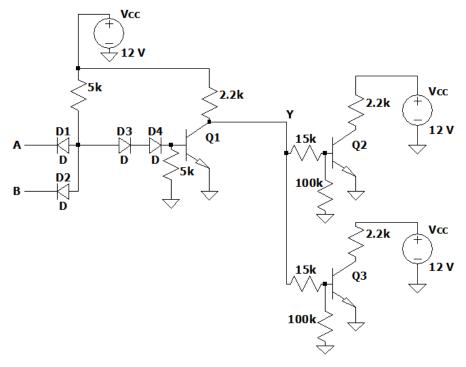
\$26.8 (\$\text{s.snh}}\$
\$2\text{c}\$ (\$a\$
\$\text{Wm 28.87,Wm 7884.4}\$ (\$a\$
\$\text{V 4.01 (\$b\$)}\$

### **Practice Problem 4:**

If at least one input is low, what is the magnitude of the noise voltage at input A, that would cause the gate to malfunction in **Exercise 5**?

V 8.0 : 2nA

### **Exercise 6**



For the given circuit:

$$V_{OH}=10~V, V_{OL}=0.2~V, \beta_F=30$$
 a) When N=1, what logic

- a) When N=1, what logic function do we get from the output of the load?
- b) Find the maximum fanout.
- c) For N=maximum fanout, find the maximum power dissipation in the loads.

BA = Y (b:snA) I (d)  $Wm \ 2.07 (a)$ 

### Solution:

For transistor T to be in saturation, at least 0.5 V must be between the base & emitter. For  $D_3 \& D_4$  both to be on, 0.6+0.6=1.4 V is required. Thus, the required voltage for  $D_3$ ,  $D_4$  & T to be on, at P,

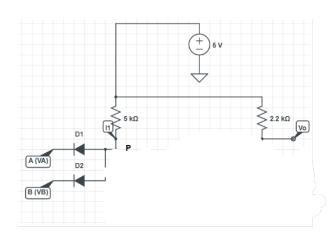
$$V_P = 0.6 \times 2 + 0.5 = 1.7 V$$

# Case (0,0):

Assuming  $D_1 \& D_2$  to be on (since low voltage 0.2 V at cathode), we get,

$$V_P = 0.2 + 0.7 = 0.9 V < 1.7 V$$

Thus,  $D_3$ ,  $D_4$  & T will be off. This leads to an open circuit-



Thus, 
$$V_o = 5 V$$

$$I_{5 k\Omega} = \frac{5 - V_P}{5} = \frac{5 - 0.9}{5} = 0.82 mA$$

$$I_{D_1} = I_{D_2} = \frac{I_{5 k\Omega}}{2} = 0.41 mA$$

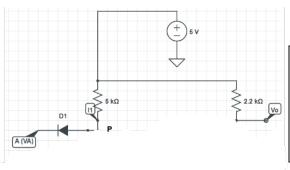
$$I_{D_1} = I_{D_2} = \frac{I_{5 k\Omega}}{2} = 0.41 \, mA$$

# Case (0,1):

Assuming  $D_1$  on &  $D_2$  off,

$$V_P = 0.2 + 0.7 = 0.9 < 1.7 V$$
 again.

Thus,  $D_3$ ,  $D_4$  & T will be off. This leads to an open circuit-



$$V_o = 5 V$$

$$I_{5 k\Omega} = \frac{5 - 0.9}{5} = 0.82 mA$$

$$I_{D_1} = I_{5 k\Omega} = 0.82 mA$$

$$I_{D_1} = I_{5 k\Omega} = 0.82 \, mA$$

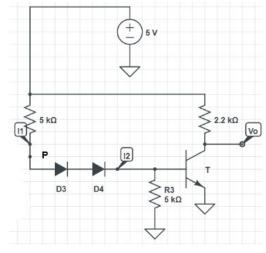
Case (1,0): Same as (0,1)

# Case (1,1):

Assuming both  $D_1$  &  $D_2$  off,  $D_3$ ,  $D_4$  & T can be assumed on, since there is no bound of  $V_P$  from the input diodes. Each diode will have 0.7 V & there will be 0.8 V between the base and emitter of T.

Thus, 
$$V_P = 0.7 + 0.7 + 0.8 = 2.2 V$$

### The circuit looks like:



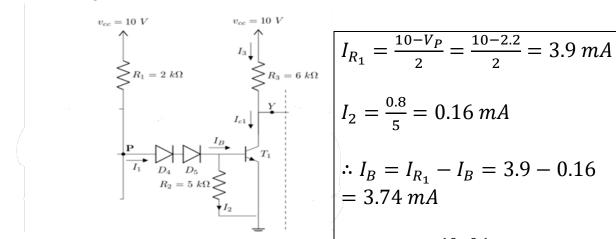
$$V_o = V_{CE_T} = 0.2 V$$

$$I_{5V} = I_1 + I_{2.2 k\Omega} = \frac{5-2.2}{5} + \frac{5-0.2}{2.2} = 2.74 mA$$

$$I_{R_3} = \frac{0.8}{5} = 0.16 mA$$

### Solution:

a) 
$$D_1$$
,  $D_2$ ,  $D_3$  all off.  $V_P = 0.7 \times 2 + 0.8 = 2.2 V$ 



$$I_{R_1} = \frac{10 - V_P}{2} = \frac{10 - 2.2}{2} = 3.9 \text{ mA}$$

$$I_2 = \frac{0.8}{5} = 0.16 \, mA$$

$$I_B = I_{R_1} - I_B = 3.9 - 0.16$$
$$= 3.74 \, mA$$

$$I_C = I_{R_3} = \frac{10 - 0.1}{6} = 1.65 \, mA$$
  
 $\therefore \beta_{min} = \frac{I_C}{I_B} = 0.441$ 

$$\therefore \beta_{min} = \frac{I_C}{I_B} = 0.441$$

This is the minimum value of  $\beta$  to keep T in saturation.

b) Let  $V_N$  be the noise voltage at A, that would cause the malfunction.

Thus, total voltage at input  $A = 10 + V_N$ 

It will malfunction if  $D_A$  turns on. The marginal voltage across the diode for this situation is the cut-in voltage (0.6 V) of the diode.

Thus, 
$$V_{D_A} = 0.6 = V_P - (10 + V_N)$$

Now, we found in (a),  $V_P = 2.2 V$  when all inputs are high.

So, 
$$V_N = 2.2 - 0.6 - 10 = -8.4 V$$

Magnitude of  $V_N = |-8.4| = 8.4 V$ 

c) If at least one input is low, it will cause  $D_4$ ,  $D_5$  &  $T_1$  to be off.

Thus,  $V_P = 0.1 + 0.7 = 0.8 V$  when no noise is present.

Let,  $V_N$  is the noise voltage.

Then, malfunction will happen when due to  $V_N$ ,  $V_P$  will be high enough to turn  $D_4$ ,  $D_5$  &  $T_1$  on.

$$V_{P_{malfunction}} = \left(V_{D_1}\right)_{cut-in} + \left(V_{D_2}\right)_{cut-in} + V_{T_{1\gamma}} = 0.6 \times 2 + 0.5 = 1.7 \ V$$
 $V_P = V_N + 0.1 + 0.7 = V_N + 0.8$ 
Considering marginal condition,
 $V_P = V_{P_{malfunction}} \to V_N + 0.8 = 1.7 \to V_N = 0.9$ 

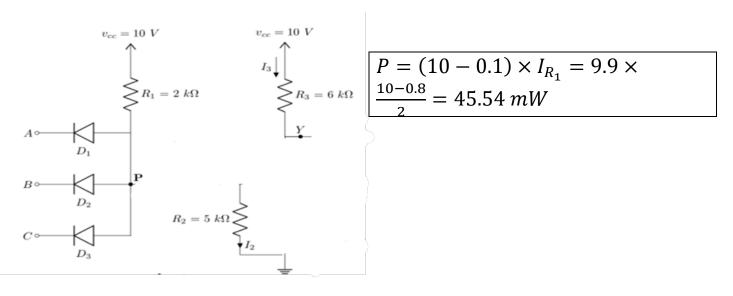
### Solution:

a) Case (at least one input low) [(0,0,0), (0,0,1), (0, 1, 0), (0, 1, 1), (1, 0, 0), (1, 0, 1), (1, 1, 0)]:

As we found in Exercise 2,

$$V_P = 0.1 + 0.7 = 0.8 V$$

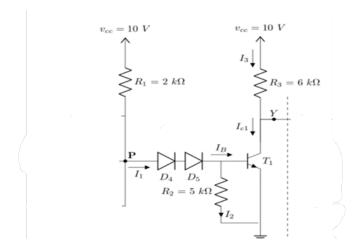
 $D_4$ ,  $D_5$ ,  $T_1$  all off



Case (1,1,1):

From **Exercise 2**, we found that for this case,  $V_P = 2.2 V$ 

 $D_4$ ,  $D_5$ ,  $T_1$  all on



$$P = (10 - 0) \times I_{R_1} + (10 - 0) \times I_{R_3}$$
$$= 10 \times \frac{10 - 2.2}{2} + 10 \times \frac{10 - 0.1}{6} = 55.5 \text{ mW}$$

b) 
$$P_{max} = \max(55.5, 45.54) = 55.5 \ mW$$

$$P_{avg} = \frac{7 \times 45.54 + 55.5}{8} = 46.785 \ mW$$

### **Exercise 4**

### **Solution:**

# a) **Step 1**:

Current flows from loads toward the driver circuit. Thus, the condition for maximum fanout is the marginal case, when  $T_1$  transitions from saturation to forward active.

# Step 2:

Case (at least 1 input low at the driver):

Output  $V_Y$  is high, which turns  $D_6$  of loads off. Thus, no current enters the driver circuit.

$$\therefore Fanout = \infty$$

Case (all inputs high):

Output  $V_Y$  is low,  $D_6$  is on. KCL at Y,

$$I_{c1} = I_3 + I_R = \frac{10 - 0.1}{6} + \frac{10 - 0.8}{2} \times N = 1.65 + 4.6N$$

Here, we have considered the case (1,0,0) at all N loads connected. This is because maximum current will flow through  $D_6$  in this situation, as all other diodes &  $T_2$  will be off. The anode node voltage of  $D_6$  will be 0.8 V for the same reasons described in previous examples (0.1+0.7).

$$I_B = I_1 - I_2 = \frac{10 - 2.2}{2} - \frac{0.8}{5} = 3.74 \, mA$$
  
Now,  $\beta_{forced} = \frac{I_C}{I_B} = \beta_F = 30 \rightarrow \frac{1.65 + 4.6N}{3.74} = 30 \rightarrow N = floor  $\left(\frac{3.74 \times 30 - 1.65}{4.6}\right) = 24$$ 

# Step 3:

 $\therefore$  *Maximum fanout* = min( $\infty$ , 24) = 24

b) We see, the difference in this case from the previous problem is that, the load currents will add to the collector current of  $T_1$ . The load currents  $I_R$  will flow between  $V_Y$  & ground. Thus,

$$\begin{aligned} P_{max} &= (10-0) \times I_1 + (10-0) \times I_3 + (V_Y - 0) \times I_R \times N \\ &= 10 \times \frac{10-2.2}{2} + 10 \times \frac{10-0.1}{6} + (0.1-0) \times 24 \times \frac{10-0.8}{2} = 66.54 \ mW \end{aligned}$$

### **Exercise 5**

### Solution:

a) When all inputs are high,

 $T_1$  in forward active mode,  $D_2$  on,  $T_2$  in saturation mode, and load diodes are off. Hence, loads are disconnected.

Thus, 
$$I_{C_{T_2}} = I_1' = \frac{12 - 0.1}{2.2} = 5.41 \, mA$$

$$I_{B_{T_2}} = i_1 - \frac{0.8}{100} = (\beta_F + 1) \times I_{C_{T_1}} - 0.008 = (30 + 1) \times \frac{V_{C_{T_1}} - 2.2}{15} - 0.008$$
Now, KCL at  $V_{C_{T_1}}$ ,
$$\frac{V_{C_{T_1}} - 2.2}{15} + 30 \times \frac{V_{C_{T_1}} - 2.2}{15} = \frac{(12 - V_{C_{T_1}})}{15} \rightarrow V_{C_{T_1}} = 2.51 \, V$$
Thus,  $I_{B_{T_2}} = 0.625 \, mA$ 

$$\therefore \beta_{forced} = \frac{I_{C_{T_2}}}{I_{B_T}} = 8.654 < \beta_F(30)$$

# b) Step 1:

The current flows from the loads toward the driver. Thus, the condition for maximum fanout is the marginal condition when  $T_2$  transitions from saturation to forward active.

# Step 2:

Cases with at least one low input:

 $T_1, D_2, T_2$  all of f

Output is high, and all load diodes will be off.

 $\therefore$  Fanout =  $\infty$ 

Case (1,1,1):

 $T_1$  in forward active mode,  $D_2$  on,  $T_2$  in saturation mode

$$I_{C_{T_2}} = I_1' + N \times I_L = \frac{12 - 0.1}{2.2} + N \times \frac{12 - 0.1 - 0.7}{15 + 15} = 5.41 + 0.373N$$

 $I_{B_{T_2}} = 0.625 \, mA$ 

$$\therefore \frac{5.41 + 0.373N}{0.625} = 30 \rightarrow N = 35$$

c)  $P_{at\ least\ one\ input\ is\ low\ cases} = (12 - 0.1) \times I_1 = 11.9 \times \frac{12 - 0.7 - 0.1}{15 + 15} = 4.4387\ mW$ 

$$P_{1,1,1} = (12 - 0) \times \frac{12 - V_{C_{T_1}}}{15} + (0.1 - 0) \times N \times I_1 = 12 \times \frac{12 - 2.51}{15} + 0.1 \times 35 \times 0.373 = 73.82 \ mW$$

d) 
$$V_A + V_{D_A} = V_P = 2.2 \rightarrow 12 + V_N + 0.6 = 2.2 \rightarrow V_N = -10.4 V$$
  
  $\therefore |V_N| = 10.4 V$ 

# **Exercise 6**

# **Solution:**

a) 
$$Y = \overline{AB}$$

# b) **Step 1**:

Current flows from driver to loads. Hence, the condition for maximum fanout is supply-demand balance.

# Step 2:

Case (1,1):

$$D_3, D_4, Q_1 on, D_1 \& D_2 of f$$

Maximum supply current from the driver,  $I_{2.2k} = \frac{12-0.2}{2.2} = 5.363 \, mA$ Since the output of the driver is low, loads will be off. Thus, demand current = 0.

: 
$$Fanout = \frac{5.363}{0} = \infty$$
  
Case (0,0)/(0,1)/(1,0):

$$D_3, D_4, Q_1 \text{ of } f, D_1 \& D_2 \text{ on }$$

Maximum supply current from the driver,  $I_{2.2k} = \frac{12-10}{2.2} = 0.91 \, mA$ Since the output of the driver is high, loads will be in saturation. Thus demand current,

$$I_L = \frac{10 - 0.8}{15} = 0.613 \ mA$$
  
 $\therefore Fanout = floor\left(\frac{0.91}{0.613}\right) = 1$ 

# Step 3:

- $\therefore$  *Maximum fanout* = min (1,  $\infty$ )
- c) N=1 load will be in saturation mode when driver output is high. Thus, maximum power dissipation in the single load,

$$P_{max} = (10 - 0) \times I_L + (12 - 0) \times I_{C_{load}} = 10 \times \frac{(10 - 0.8)}{15} + 12 \times \frac{12 - 0.2}{2.2} = 70.5 \text{ mW}$$