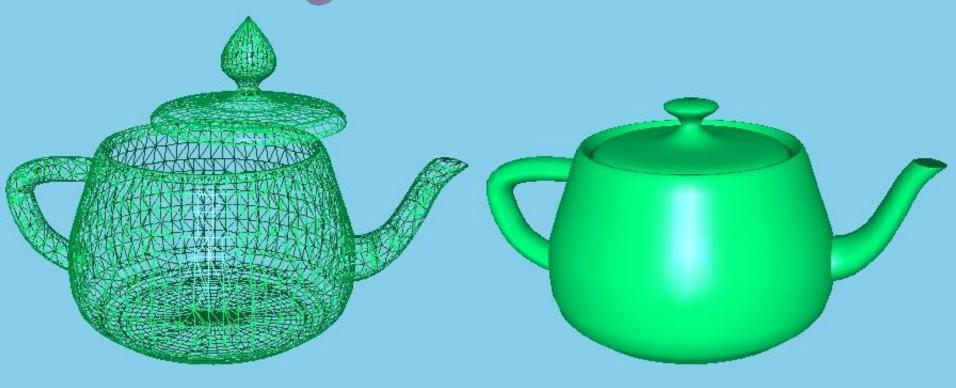
Modeling Curved Surfaces



Curved Surfaces

The use of <u>curved surfaces</u> allows for a higher level of modeling, especially for the construction of highly realistic models.

There are several approaches to modeling curved surfaces:

We can represent curved surfaces using mesh of curves. So we learn to create curves first then move to curved surfaces.

Curved Surfaces

There are two ways to construct a model: **Additive Modeling**

This is the process of building the model by assembling many simpler objects.

Subtractive Modeling

This is the process of removing pieces from a given object to create a new object.

For example, creating a (cylindrical) hole in a sphere or a cube.

Curved Surface Patch₃

Curve Representation

- There are three ways to represent a curve
 - Explicit: y = f(x)
 y = mx + b
 y = x²
 - (-) Must be a single valued function
 - (-) Vertical lines, say x = d?
 - Implicit: f(x,y) = 0 $x^2 + y^2 - r^2 = 0$
 - (+) y can be multiple valued function of x
 - (-) Vertical lines? (Continuity hard to detect)
 - Parametric: (x, y) = (x(t), y(t))
 (x, y) = (cost, sint)
 - (+) Easy to specify, modify and control
 - (-) Extra hidden variable t, the parameter

Explicit Representation

- Curve in 2D: y = f(x)
- Curve in 3D: y = f(x), z = g(x)
- Surface in 3D: z = f(x,y)
- Problems:
 - How about a vertical line x = c as y = f(x)?
 - Circle $y = \pm (r^2 x^2)^{1/2}$ two or zero values for x
- Rarely used in computer graphics

Implicit Representation

- Curve in 2D: f(x,y) = 0
 - Line: ax + by + c = 0
 - Circle: $x^2 + y^2 r^2 = 0$
- Surface in 3d: f(x,y,z) = 0
 - Plane: ax + by + cz + d = 0
 - Sphere: $x^2 + y^2 + z^2 r^2 = 0$
- f(x,y,z) can describe 3D object:
 - Inside: f(x,y,z) < 0
 - Surface: f(x,y,z) = 0
 - Outside: f(x,y,z) > 0

Parametric Form for Curves

- Curves: single parameter t (e.g. time)
 - x = x(t), y = y(t), z = z(t)
- Circle:
 - x = cos(t), y = sin(t), z = 0
- Tangent described by derivative

$$p(t) = \begin{bmatrix} x(t) \\ y(t) \\ z(t) \end{bmatrix} \qquad \frac{dp(t)}{dt} = \begin{bmatrix} \frac{dx(t)}{dt} \\ \frac{dy(t)}{dt} \\ \frac{dz(t)}{dt} \end{bmatrix}$$
• Magnitude is "velocity"

Parametric Form for Surfaces

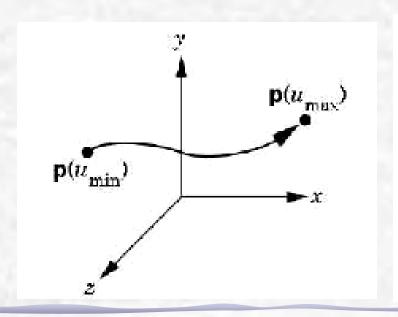
- Use parameters u and v
 - x = x(u,v), y = y(u,v), z = z(u,v)
- Describes surface as both u and v vary
- Partial derivatives describe tangent plane at each point $p(u,v) = [x(u,v) \ y(u,v) \ z(u,v)]^T$

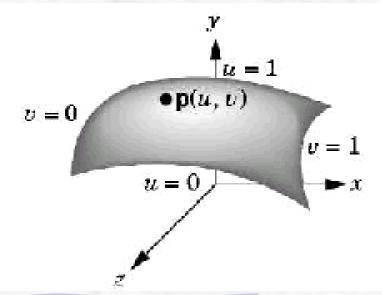
$$\frac{\partial p(u,v)}{\partial u} = \begin{bmatrix} \frac{\partial x(u,v)}{\partial u} \\ \frac{\partial y(u,v)}{\partial u} \\ \frac{\partial z(u,v)}{\partial u} \end{bmatrix}$$

$$\frac{\partial p(u,v)}{\partial v} = \begin{bmatrix} \frac{\partial x(u,v)}{\partial v} \\ \frac{\partial y(u,v)}{\partial v} \\ \frac{\partial z(u,v)}{\partial v} \end{bmatrix}$$

Advantages of Parametric Form

- Parameters often have natural meaning
- Easy to define and calculate
 - Tangent and normal
 - Curves segments (for example, $0 \le u \le 1$)
 - Surface patches (for example, $0 \le u, v \le 1$)





Lagrange Polynomial

- Given n+1 points (x_0, y_0) , (x_1, y_1) (x_n, y_n)
- To construct a curve that passes through these points we can use Lagrange polynomial defined as follows:.

$$y = f(x) = \sum_{k=0}^{n} y_k L_{n,k}$$

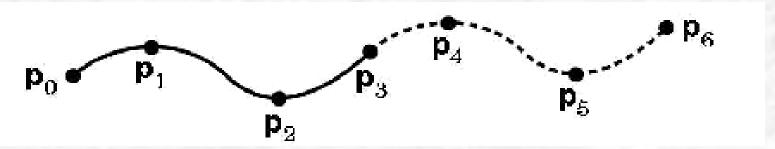
$$L_{n,k} = \frac{(x - x_o)(x - x_1) \cdots (x - x_{k-1})(x - x_{k+1}) \cdots (x - x_n)}{(x_k - x_o)(x_k - x_1) \cdots (x_k - x_{k-1})(x_k - x_{k+1}) \cdots (x_k - x_n)}$$

Problems:

- y=f(x), no multiple values
- Higher order functions tend to oscillate
- No local control (change any (x_i, y_i) changes the whole curve)
- Computationally expensive due to high degree.

Piecewise Linear Polynomial

- To overcome the problems with Lagrange polynomial
 - Divide given points into overlap sequences of 4 points
 - construct 3rd degree polynomial that passes through these points, p₀, p₁, p₂, p₃ then p₃, p₄, p₅, p₆ etc.
 - Then glue the curves so that they appear sufficiently smooth at joint points.



Questions:

- 1. Why 3rd Degree curves used?
- 2. How to measure smoothness at joint point?

Why Cubic Curves?

A curve is approximated by a <u>piecewise polynomial</u> curve.

<u>Cubic polynomials</u> are most often used because:

- (1) Lower-degree polynomials offer too little flexibility in controlling the shape of the curve.
- (2) Higher-degree polynomials can introduce unwanted wiggles and also require more computation.
 - (3) No lower-degree representation allows a curve segment to be defined by two given endpoints with given derivative at each endpoints.
 - (4) No lower-degree curves are nonplanar in 3D.

Measure of Smoothness

 G^0 Geometric Continuity $\Leftrightarrow C^0$ Parametric Continuity If two curve segments join together.

G¹ Geometric Continuity

If the **directions** (but not necessarily the magnitudes) of the two segments' tangent vectors are equal at a join point.

C¹ Parametric Continuity

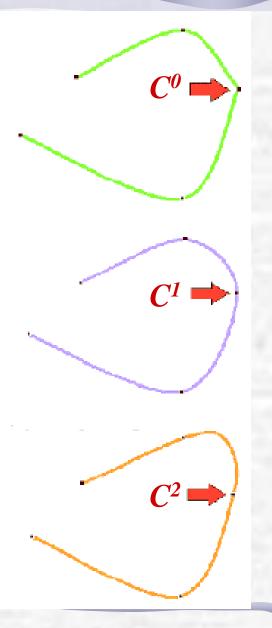
If the **directions and magnitudes** of the two segments' tangent vectors are equal at a join point.

C² Parametric Continuity

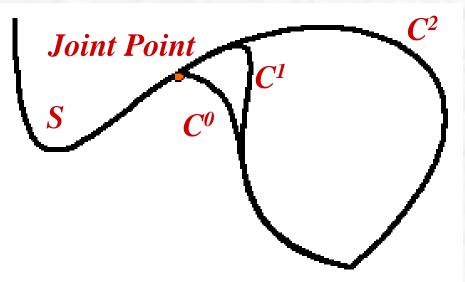
If the direction and magnitude of $Q^2(t)$ (curvature or **acceleration**) are equal at the join point.

Cⁿ Parametric Continuity

If the direction and magnitude of $Q^n(t)$ through the nth derivative are equal at the join point.

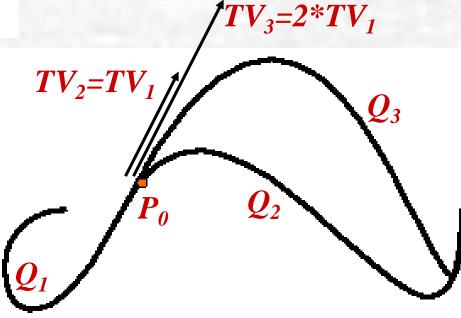


Measure of Smoothness



 By increasing parametric continuity we can increase smoothness of the curve.

- Q₁& Q₂ are C¹ and G¹ continuous
- Q_1 & Q_3 are G^1 continuous only as Tangent vectors have different magnitude.
- Observe the effect of increasing in magnitude of TV



Interpolation Vs. Approximation

Given n + 1 points $P_0(x_0, y_0), P_1(x_1, y_1), ..., P_n(x_n, y_n)$

we wish to find <u>a curve</u> that, in some sense, <u>fits the</u> <u>shape outlined by these points</u>.

Based on requirements we are faced with two problems:

Interpolation

If we require the curve to <u>pass through</u> all the points.

Approximation

If we require only that the curve be <u>near</u> these points.

Parametric Representation of Lines

- Interpolation of two points
- In Parametric form:

$$P(t) = P_1 + t \cdot (P_2 - P_1)$$

$$x(t) = x_1 + t \cdot (x_2 - x_1)$$

$$y(t) = y_1 + t \cdot (y_2 - y_1)$$

$$x(t) = TC_x = TMG_x = BG_x$$

$$y(t) = TC_y = TMG_y = BG_y$$

$$x(t) = \begin{bmatrix} t & 1 \end{bmatrix} \begin{bmatrix} x_2 - x_1 \\ x_1 \end{bmatrix} = \begin{bmatrix} t & 1 \end{bmatrix} \begin{bmatrix} -1 & 1 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 1 - t & t \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$
Parameter
Co-eff
Matrix
G
Matrix
G
Parameter
N
Blending
Function
B
Matrix
B
M

Parametric Cubic Curves

$$Q(t) = [x(t)y(t)z(t)] \begin{cases} x(t) = a_x t^3 + b_x t^2 + c_x t + d_x, \\ y(t) = a_y t^3 + b_y t^2 + c_y t + d_y, \\ z(t) = a_z t^3 + b_z t^2 + c_z t + d_z, \ 0 \le t \le 1 \end{cases}$$

$$\therefore Q(t) = \begin{bmatrix} t^3 & t^2 & t \\ T & t \end{bmatrix} \begin{bmatrix} a_x & a_y & a_z \\ b_x & b_y & b_z \\ c_x & c_y & c_z \\ d_x & d_y & d_z \end{bmatrix}$$

$$\therefore Q(t) = T \cdot C$$

Parametric Cubic Curves

 Now co-efficient matrix C can be expressed as a multiple of basis(weight) matrix M and geometry matrix G.

$$Q(t) = [x(t) \ y(t) \ z(t)] = T \cdot C = T \cdot M \cdot G$$

$$Q(t) = \begin{bmatrix} t^3 & t^2 & t \end{bmatrix} \begin{bmatrix} m_{11} & m_{12} & m_{13} & m_{14} \\ m_{21} & m_{22} & m_{23} & m_{24} \\ m_{31} & m_{32} & m_{33} & m_{34} \\ m_{41} & m_{42} & m_{43} & m_{44} \end{bmatrix} \begin{bmatrix} G_1 \\ G_2 \\ G_3 \\ G_4 \end{bmatrix}$$
basis matr ix
$$\begin{bmatrix} G_1 \\ G_2 \\ G_3 \\ G_4 \end{bmatrix}$$

- Each element of geometry vector G has 3 component for x, y and z.
- Components of G can be expressed as G_x, G_y and G_z.

Parametric Cubic Curves

Multiplying out only the x-component we get

$$x(t) = T \cdot M \cdot G_{x} = \begin{bmatrix} t^{3} & t^{2} & t \end{bmatrix} \begin{bmatrix} m_{11} & m_{12} & m_{13} & m_{14} \\ m_{21} & m_{22} & m_{23} & m_{24} \\ m_{31} & m_{32} & m_{33} & m_{34} \\ m_{41} & m_{42} & m_{43} & m_{44} \end{bmatrix} \begin{bmatrix} g_{1x} \\ g_{2x} \\ g_{3x} \\ g_{4x} \end{bmatrix}$$

$$x(t) = (t^{3}m_{11} + t^{2}m_{21} + tm_{31} + m_{41})g_{1x}$$

$$+ (t^{3}m_{12} + t^{2}m_{22} + tm_{32} + m_{42})g_{2x}$$

$$+ (t^{3}m_{13} + t^{2}m_{23} + tm_{33} + m_{43})g_{3x}$$

$$+ (t^{3}m_{14} + t^{2}m_{24} + tm_{34} + m_{44})g_{4x}$$

- The curve is a weighted sum of the elements of geometry matrix
- The weights are each cubic polynomials of t called *blending function*

Derivative of Q(t)

 Derivative of Q(t) is the parametric tangent vector of the curve.

$$\frac{dQ(t)}{dt} = Q'(t) = \begin{bmatrix} \frac{d}{dt}x(t) & \frac{d}{dt}y(t) & \frac{d}{dt}z(t) \end{bmatrix}$$

$$Q'(t) = \frac{d}{dt} T \cdot C = \begin{bmatrix} 3t^2 & 2t & 1 & 0 \end{bmatrix} \cdot C$$

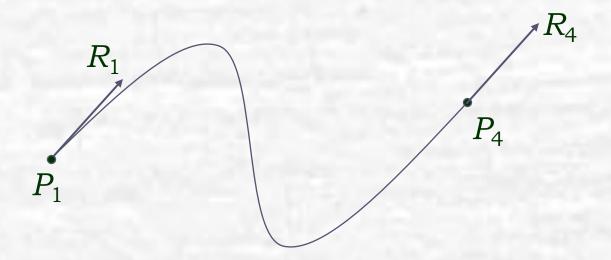
$$Q'(t) = \begin{bmatrix} 3a_x t^2 + 2b_x t + c_x & 3a_y t^2 + 2b_y t + c_y & 3a_z t^2 + 2b_z t + c_z \end{bmatrix}$$

Curve Design: Determining C

A curve segment Q(t) is defined by <u>constraints</u> on:

- (1) endpoints
- (2) tangent vectors
- and (3) continuity between segments

Each cubic polynomial of *Q*(*t*) has <u>4 coefficients</u>, so <u>4 constraints</u> will be needed, allowing us to formulate <u>4 equations in the 4 unknowns</u>, then solving for the unknowns.



A cubic Hermite curve segment interpolating the endpoints P_1 and P_4 is determined by constraints on the endpoints P_1 and P_4 and tangent vectors at the endpoints R_1 and R_4

The Hermite Geometry Vector:
$$G_H = \begin{bmatrix} P_1 \\ P_4 \\ R_1 \\ R_4 \end{bmatrix}$$

$$x(t) = a_x t^3 + b_x t^2 + c_x t + d_x = T \cdot C_x = T \cdot M_H \cdot G_{H_x}$$
$$= \begin{bmatrix} t^3 & t^2 & t & 1 \end{bmatrix} M_H \cdot G_{H_x}$$

The constraints on x(0) and x(1):

$$x(0) = P_{1x} = \begin{bmatrix} 0 & 0 & 0 & 1 \end{bmatrix} M_H \cdot G_{H_x}$$

 $x(1) = P_{4x} = \begin{bmatrix} 1 & 1 & 1 & 1 \end{bmatrix} M_H \cdot G_{H_x}$

$$x'(t) = \begin{bmatrix} 3t^2 & 2t & 1 & 0 \end{bmatrix} M_H \cdot G_{H_x}$$

Hence the tangent-vector constraints:

$$x'(0) = R_{1x} = \begin{bmatrix} 0 & 0 & 1 & 0 \end{bmatrix} M_H \cdot G_{H_x}$$

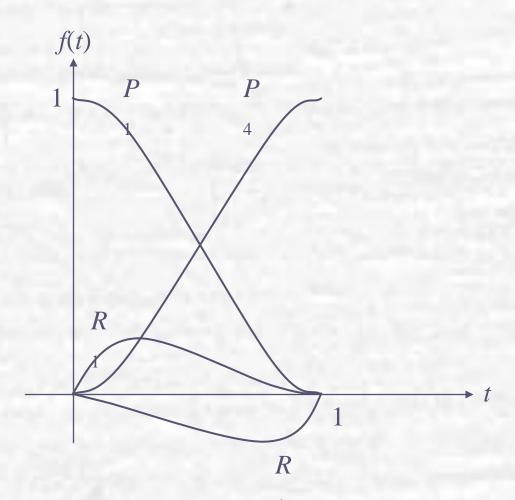
 $x'(1) = R_{4x} = \begin{bmatrix} 3 & 2 & 1 & 0 \end{bmatrix} M_H \cdot G_{H_x}$

The 4 constraints can be written as:

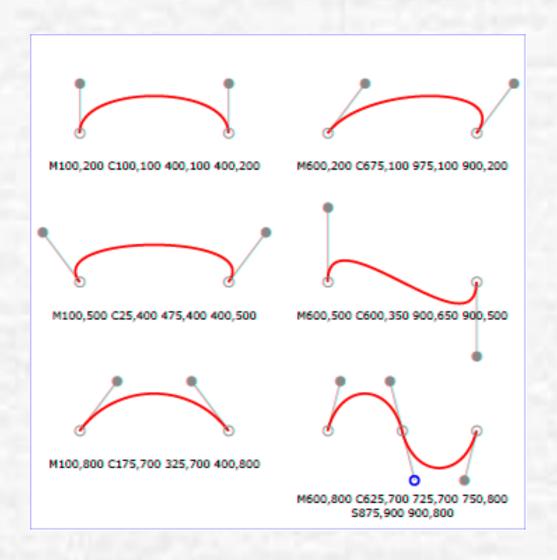
$$\begin{bmatrix} P_1 \\ P_4 \\ R_1 \\ R_4 \end{bmatrix}_x = G_{H_x} = \begin{bmatrix} 0 & 0 & 0 & 1 \\ 1 & 1 & 1 & 1 \\ 0 & 0 & 1 & 0 \\ 3 & 2 & 1 & 0 \end{bmatrix} M_H \cdot G_{H_x}$$

$$M_{H} = \begin{bmatrix} 0 & 0 & 0 & 1 \\ 1 & 1 & 1 & 1 \\ 0 & 0 & 1 & 0 \\ 3 & 2 & 1 & 0 \end{bmatrix}^{-1} = \begin{bmatrix} 2 & -2 & 1 & 1 \\ -3 & 3 & -2 & -1 \\ 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \end{bmatrix}$$

$$Q(t) = [x(t) \quad y(t) \quad z(t)] = T \cdot M_H \cdot G_H = B_H \cdot G_H$$
$$= (2t^3 - 3t^2 + 1)P_1 + (-2t^3 + 3t^2)P_4$$
$$+ (t^3 - 2t^2 + t)R_1 + (t^3 - t^2)R_4$$



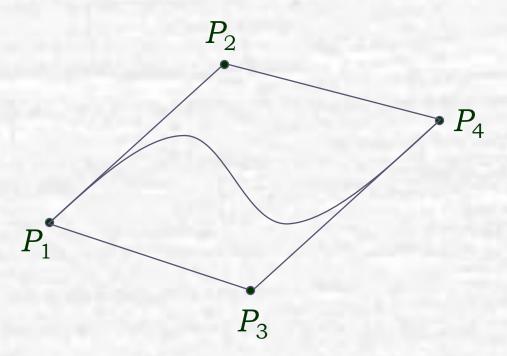
The Hermite Blending Functions



$$P_{1}, P_{2}, P_{3}, P_{4}, P_{5}, P_{6}, P_{7}$$

$$\begin{bmatrix} P_{1} \\ P_{4} \\ P_{4} \\ R_{1} \\ R_{4} \end{bmatrix} = \begin{bmatrix} P_{4} \\ P_{7} \\ kR_{4} \\ R_{7} \end{bmatrix}$$

$$G^{0}, G^{1}, C^{1}$$



Indirectly specifies the endpoint tangent vectors by specifying two intermediate points that are not on the curve.

$$R_1 = Q'(0) = P_1 P_2 = 3(P_2 - P_1)$$

$$R_4 = Q'(1) = P_3 P_4 = 3(P_4 - P_3)$$

The Bézier Geometry Vector:
$$G_B = \begin{bmatrix} P_1 \\ P_2 \\ P_3 \\ P_4 \end{bmatrix}$$

$$G_{H} = \begin{bmatrix} P_{1} \\ P_{4} \\ R_{1} \\ R_{4} \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ -3 & 3 & 0 & 0 \\ 0 & 0 & -3 & 3 \end{bmatrix} \begin{bmatrix} P_{1} \\ P_{2} \\ P_{3} \\ P_{4} \end{bmatrix} = M_{HB} \cdot G_{B}$$

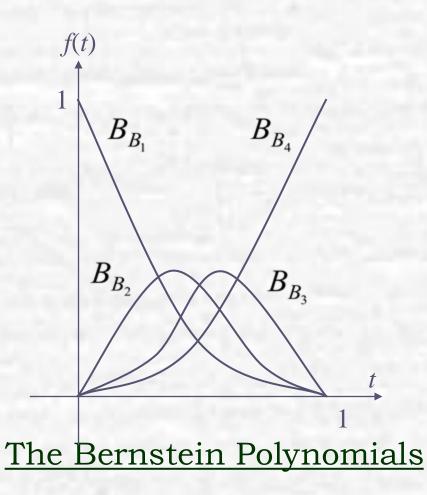
$$Q(t) = T \cdot M_H \cdot G_H = T \cdot M_H \cdot (M_{HB} \cdot G_B)$$
$$= T \cdot (M_H \cdot M_{HB}) \cdot G_B = T \cdot M_B \cdot G_B$$

$$M_B = M_H \cdot M_{HB} = \begin{bmatrix} -1 & 3 & -3 & 1 \\ 3 & -6 & 3 & 0 \\ -3 & 3 & 0 & 0 \\ 1 & 0 & 0 & 0 \end{bmatrix}$$

$$Q(t) = T \cdot M_B \cdot G_B$$

= $(1-t)^3 P_1 + 3t(1-t)^2 P_2 + 3t^2 (1-t)P_3 + t^3 P_4$

The 4 polynomials in $B_B = T$. M_B are called the Bernstein polynomials.



A Bézier curve is bounded by the convex hull of its control points. (B : sum 1 and nonnegative)

Curve Rendering

- Brute-Force method
- Forward differencing
- Recursive sub-division

Brute-Force method

```
t = 0;

for (i=0; i <= 100; i++) \{

x(t) = a_x t^3 + b_x t^2 + c_x t + d_x

y(t) = a_y t^3 + b_y t^2 + c_y t + d_y

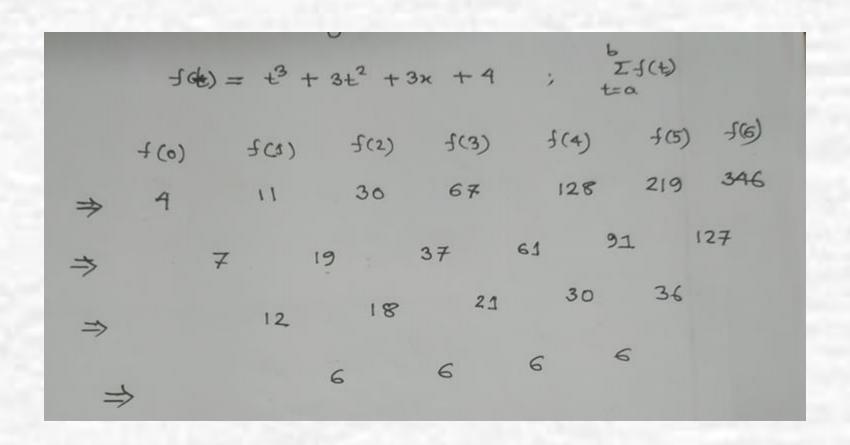
z(t) = a_z t^3 + b_z t^2 + c_z t + d_z

Plot3d(x(t), y(t), z(t));

t += 0.01;
```

Cost: 9 multiplication 10 Sum

Forward differencing method



Curve Rendering

Forward differencing method

 $\Delta f(t+\delta) = \Delta f(t) + \Delta^2 f(t)$

$$f(t) = at^{3} + bt^{2} + ct + d$$

$$f(t+\delta) = a(t+\delta)^{3} + b(t+\delta)^{2} + c(t+\delta) + d$$

$$\Delta f(t) = f(t+\delta) - f(t)$$

$$= 3a\delta t^{2} + (3a\delta^{2} + 2b\delta)t + (a\delta^{3} + b\delta^{2} + c\delta)$$

$$\Delta f(t) = f(t) + \Delta f(t)$$

$$\Delta f(t) = 3a\delta t^{2} + (3a\delta^{2} + 2b\delta)t + (a\delta^{3} + b\delta^{2} + c\delta)$$

$$\Delta f(t+\delta) = 3a\delta(t+\delta)^{2} + (3a\delta^{2} + 2b\delta)t + (a\delta^{3} + b\delta^{2} + c\delta)$$

$$\Delta f(t+\delta) = 3a\delta(t+\delta)^{2} + (3a\delta^{2} + 2b\delta)(t+\delta) + (a\delta^{3} + b\delta^{2} + c\delta)$$

$$\Delta^{2} f(t) = \Delta f(t+\delta) - \Delta f(t)$$

$$= 6a\delta^{2}t + (6a\delta^{3} + 2b\delta^{2})$$

$$\Delta^{2} f_{n+1} = \Delta f_{n+1} - \Delta f_{n-1}$$

Afr = Afr-1 + A2fr-1

Curve Rendering

Forward differencing method

$$\Delta^2 f(t) = 6a\delta^2 t + (6a\delta^3 + 2b\delta^2)$$

$$\Delta^2 f(t+\delta) = 6a\delta^2 (t+\delta) + (6a\delta^3 + 2b\delta^2)$$

$$\Delta^3 f(t) = \Delta^2 f(t+\delta) - \Delta^2 f(t)$$

$$=6a\delta^3$$

$$\Delta^2 f(t+\delta) = \Delta^2 f(t) + \Delta^3 f(t)$$

$$\Delta^{2}f_{n+1} = \Delta^{2}f_{n} + \Delta^{3}f_{n}$$

$$\Delta^{2}f_{n-1} = \Delta^{2}f_{n-2} + \Delta^{3}f_{n-2} - CIII)$$

$$f_o = d$$

$$\Delta f_o = a\delta^3 + b\delta^2 + c\delta$$

$$\Delta^2 f_o = 6a\delta^3 + 2b\delta^2$$

$$\Delta^3 f_o = 6a\delta^3$$

Ref:

Foley: Chapter 11