



Mfront user day 2023

Microstructure-based modelling of snow viscoplasticity using FFT-based simulations and MFront to model crystal plasticity

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T=0h



















The snowflake that falls out of the sky doesn't stay that way for long...

T= 35 h







The snowflake that falls out of the sky doesn't stay that way for long

The snowflakes change their form and become more rounded

Settlement is the **slow** deformation of the snow as it densifies and sags under the influence of **gravity**

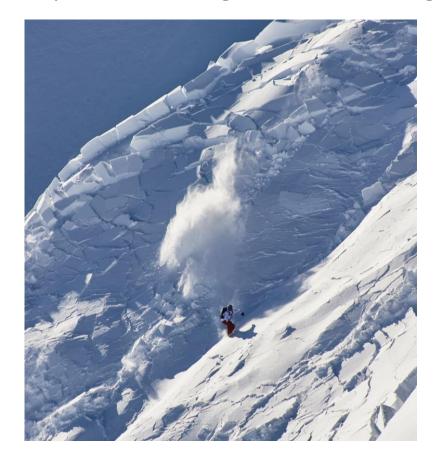
T = 38 h

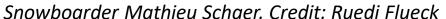


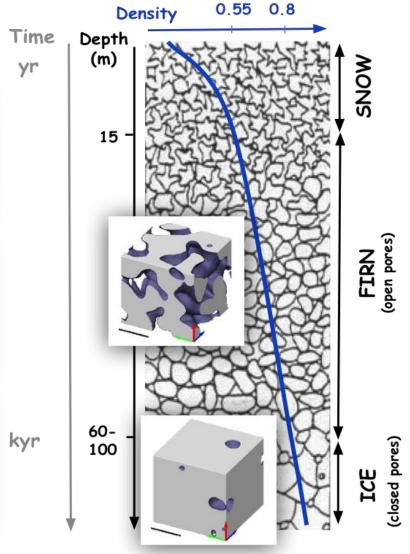


Context: applications

• Snowpack modelling, Paleoclimatology ...









Context: snow microstructure

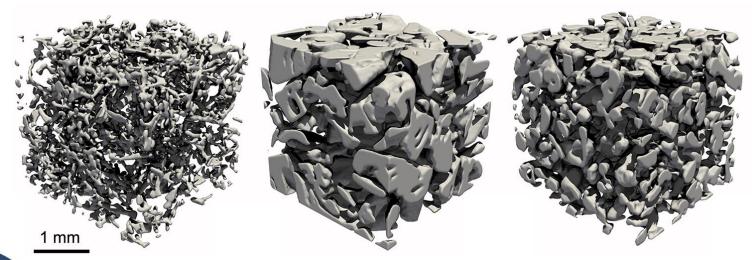
Snow = mixture of ice crystals sintered together, air and sometimes liquid water and impurities.

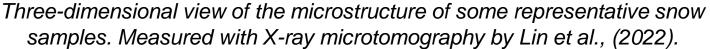
Material close to the melting temperature

Porosity → 95% fresh snow / 10% for dense firn

Large number of snow type → difficult to characterize

Snow settlement is mainly driven by the creep of the ice matrix undergoing viscoplastic deformations







Cup-shaped crystals in the snowpack (SLF).



Scientific questions:

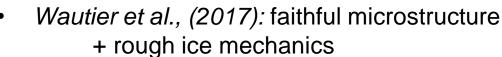
- How does the viscoplastic behaviour of ice scales to the snow mechanical behaviour?

Key bibliography:

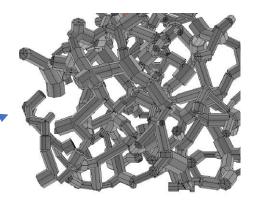
Investigation through microstructure-based simulations:

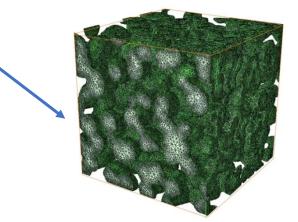
snow = 3D microstructure + ice mechanical properties

- Theile et al., (2011): highly simplified snow microstructure + advanced modelling of ice mechanics











Scientific questions:

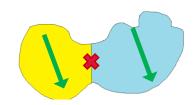
 How does the viscoplastic behaviour of ice scale to the snow mechanical behaviour?

Our work:

- Microstructure-based simulation: faithful microstructure + advanced ice mechanics, made possible via a suitable solver: AMITEX
- Direct evaluation based on previous creep experiments captured by tomography.

Contours of the study:

- Study of dry snow only, under isothermal conditions without metamorphism;
- Account only intra-crystalline deformation (inter-crystalline sliding is overlooked).





As our model cannot reproduce the evolution of the microstructure, we use the set of experimentally obtained microstructures to decompose the test into a set of instantaneous creep experiments.

We use two mechanical tests performed by (Bernard et al., 2022):

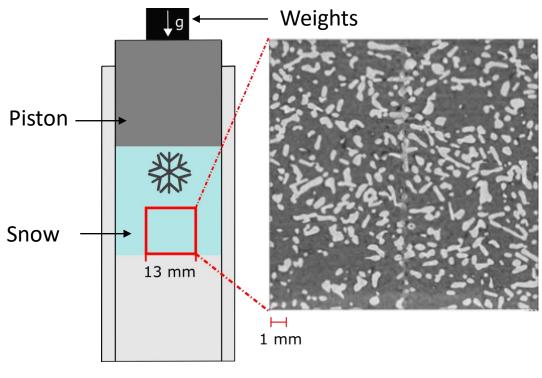
I) Load-controlled test:

- $\sigma_{\rm imp} = 2.1 \text{ kPa}$, $T_{\rm snow} = -8 \pm 0.5 \text{ °C}$
- Deformation determined based on density measurement

(X-Ray tomography)



Tomograph (Hagenmuller)



Experimental setup (Bernard et al., 2022)

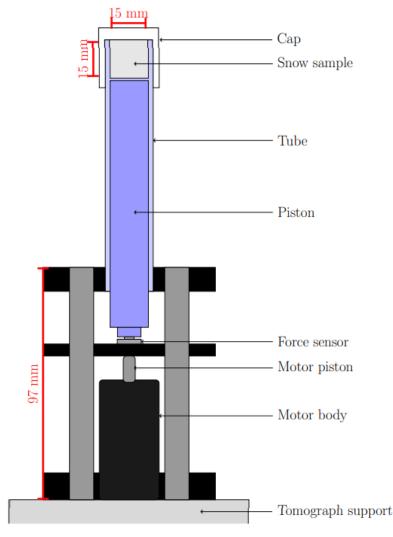


As our model cannot reproduce the evolution of the microstructure, we use the set of experimentally obtained microstructures to decompose the test into a set of instantaneous creep experiments.

We use two mechanical tests performed by (Bernard et al., 2022-2023):

II) Strain-rate-controlled compression test:

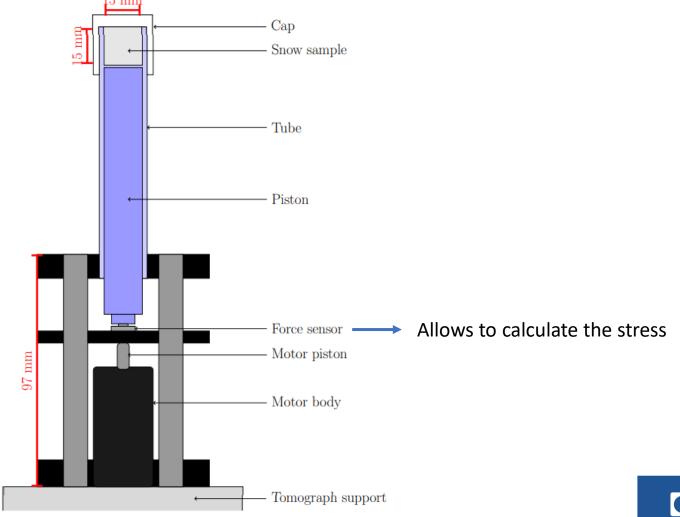
- $\dot{\varepsilon}_{\rm imp} = 1.8 \times 10^{-6} \, {\rm s}^{-1}$,
- $T_{\text{snow}} = -18 \pm 0.5 \,^{\circ}\text{C}$

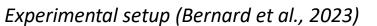


Experimental setup (Bernard et al., 2023)



Strain-rate-controlled compression test

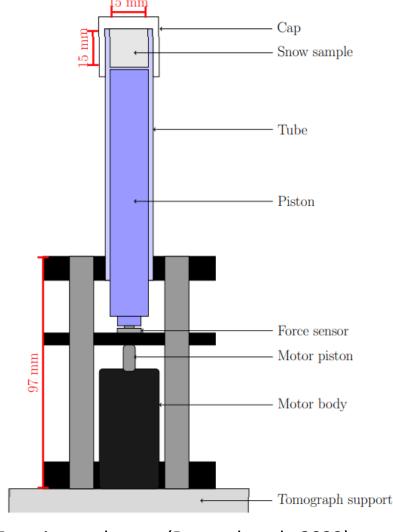


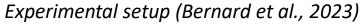




Experimental data 10^{-1} σ_{Y} (MPa) 10^{-2} 0.2 0.5 0.0 0.1 0.3 0.4 Strain ε

Strain-rate-controlled compression test

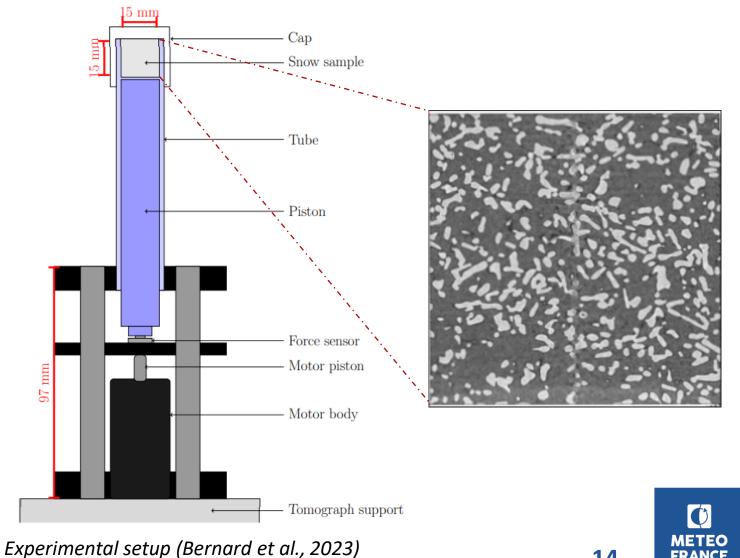






Experimental data 10^{-1} σ_{Y} (MPa) 10^{-2} 0.2 0.5 0.0 0.1 0.3 0.4 Strain ε

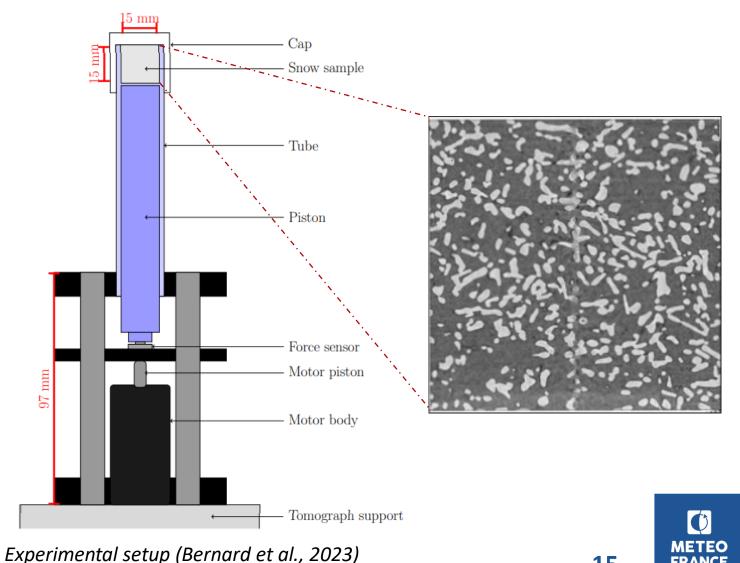
Strain-rate-controlled compression test



FRANCE

Experimental data Micro-CT Scan 10^{-1} σ_{Y} (MPa) 10^{-2} 0.2 0.5 0.0 0.1 0.3 0.4 Strain ε

Strain-rate-controlled compression test

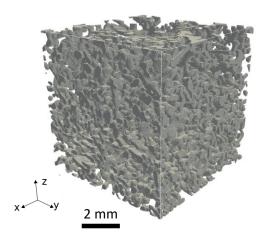


FRANCE

Methodology: numerical setup

Experimental data Micro-CT Scan 10^{-1} σ_γ (MPa) 10^{-2} 0.2 0.0 0.1 0.3 0.4 0.5 Strain ε

Binary segmentation



Homogeneous ice model 3D Norton law (Suquet, 1983)

$$\epsilon = \epsilon_{\rm e} + \epsilon_{\rm vp}$$

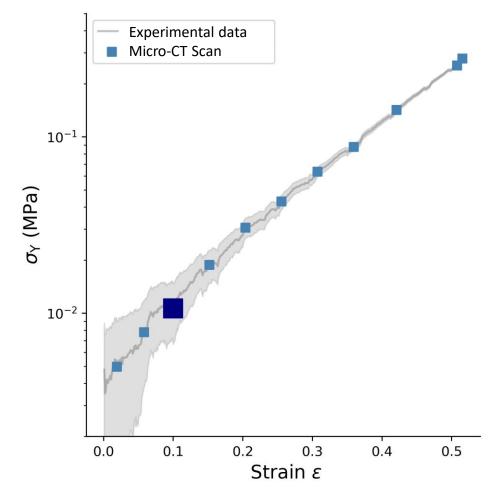
$$\dot{\boldsymbol{\epsilon}}_{\mathbf{vp}} = \frac{3}{2} A \, \sigma_{\mathrm{eq}}^{n-1} \, \boldsymbol{\sigma}'$$

with $\sigma_{\rm eq}$ the equivalent stress, σ' the deviatoric stress, $A=7.8\ 10^{-8}\ \rm MPa^{-n}\ s^{-1}$ and n=3

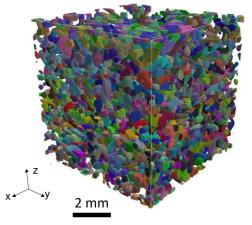
From Castelnau et al., 1998, Theile et al., 2011



Methodology: numerical setup



Grain segmentation

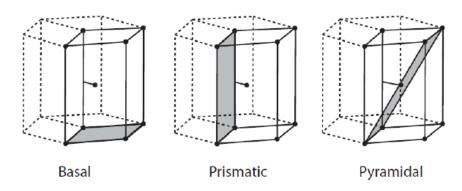


Sintered crystal model **Crystal plasticity**

$$\epsilon_{vp} = \sum_{k=1}^{12} \gamma^{(k)} \mu^k$$
 $\mu^k = \frac{1}{2} (n^k \otimes_{\mathcal{S}} b^k)$ the Schmid tensor

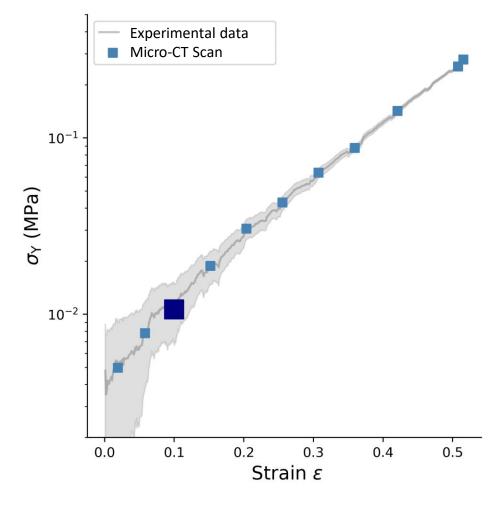
$$\dot{\gamma}^{(k)} = \dot{\gamma}_0^{(k)} \left(\frac{\left| \tau^{(k)} \right|}{\tau_0^k} \right)^{n^{(k)}} \operatorname{sgn} \left(\tau^{(k)} \right) \text{ with } \tau^{(k)} = \boldsymbol{\sigma} : \boldsymbol{\mu}^k$$

with $\tau_0^{(k)}$ the reference resolved shear stress, $\dot{\gamma}_{0}^{(k)} = 1 \,\mathrm{s}^{-1}$ the reference shear rate

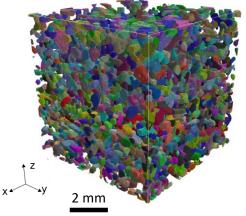


The three slip systems present in ice crystal (Poerschke, 2009)

Methodology: numerical setup



Grain segmentation



Sintered crystal model **Crystal plasticity**

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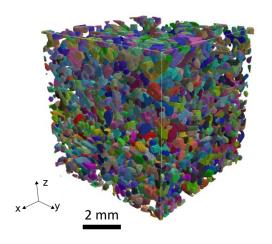
Family	Systems	$n^{(k)}$	$ au_0^{(k)}$ (MPa)
Basal [0001]<1120>	3	3	13
Prismatic $[01\overline{1}0]$ < $2\overline{1}\overline{1}0$ >	3	3	260
Pyramidal [$11\overline{2}2$]< $11\overline{2}\overline{3}$ >	6	3	260

Monocrystalline ice parameters of viscoplastic model at −10 °C adapted from Lebensohn et al., 2009 and Hondoh, 2000

Methodology: numerical setup

Experimental data Micro-CT Scan 10^{-1} ى_۲ (MPa) 10^{-2} 0.0 0.1 0.2 0.3 0.4 0.5 Strain ε

Grain segmentation



Sintered crystal model Crystal plasticity

$$\boldsymbol{\epsilon}_{vp} = \sum_{k=1}^{12} \gamma^{(k)} \boldsymbol{\mu}^k$$

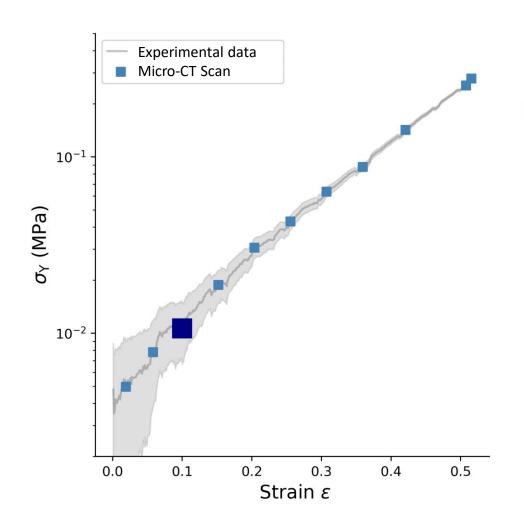
 $\mu^k = \frac{1}{2} (n^k \bigotimes_s b^k)$ the Schmid tensor

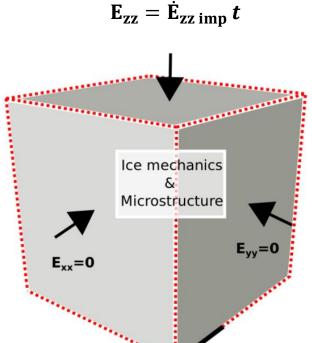
$$\dot{\gamma}^{(k)} = \dot{\gamma}_0^{(k)} \left(\frac{\left| \tau^{(k)} \right|}{\tau_0^k} \right)^{n^{(k)}} \operatorname{sgn} \left(\tau^{(k)} \right) \text{ with } \tau^{(k)} = \boldsymbol{\sigma} : \boldsymbol{\mu}^k$$

with $au_0^{(k)}$ the reference resolved shear stress, $\dot{\gamma}_0^{(k)} = 1~{\rm s}^{-1}$ the reference shear rate

→ Implemented with the StandardElastoViscoPlasticity brick (Helfer et al., 2019)

Methodology: numerical setup





Hypothesis no lateral friction: $\boldsymbol{\Sigma}_{xy} = \boldsymbol{\Sigma}_{yz} = \boldsymbol{\Sigma}_{xz} = \boldsymbol{0}$

Use **AMITEX** (Gélébart et al.,2020)

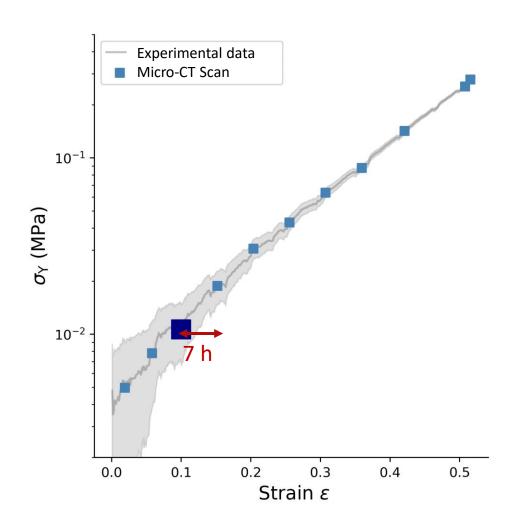
→ Voxel images are the direct input
 of the simulations
 → Benefits from the MPI
 parallelisation

Simulations on a Representative Elementary Volume (REV) $5.1 \times 5.1 \times 5.1 \text{ mm}^3$

as $L_{macro} \gg L_{micro}$

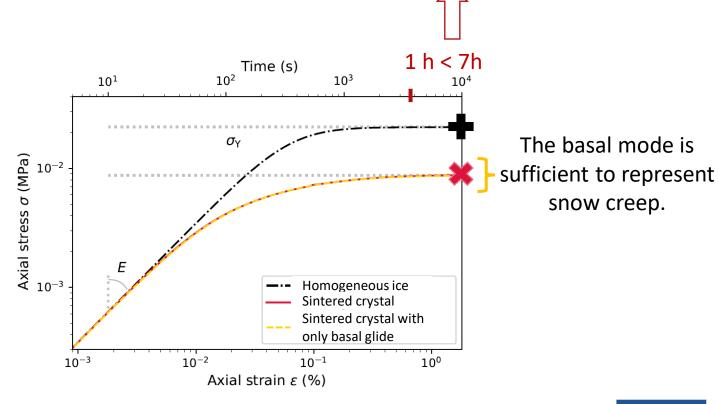


Results: compression tests



"instantaneous creep experiment "

topological changes negligeable



Stress evolution with the strain for the different ice models.



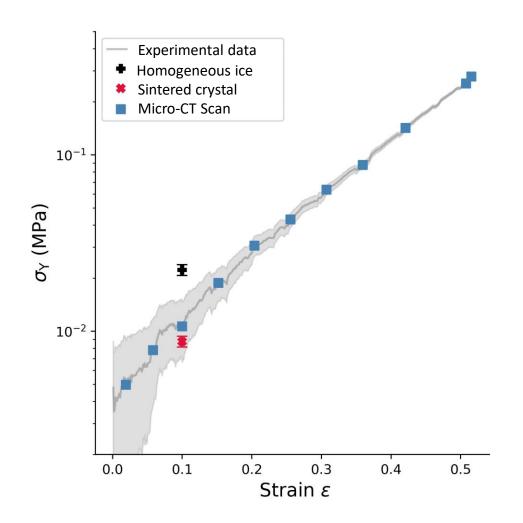
The basal mode is

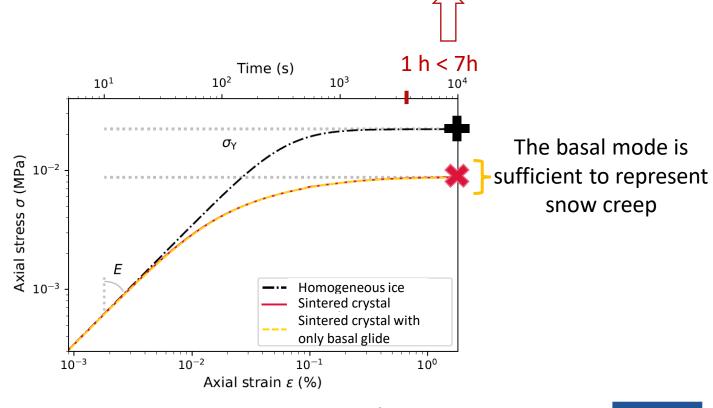
snow creep.

Results: experimental comparison

"instantaneous creep experiment "

topological changes negligeable



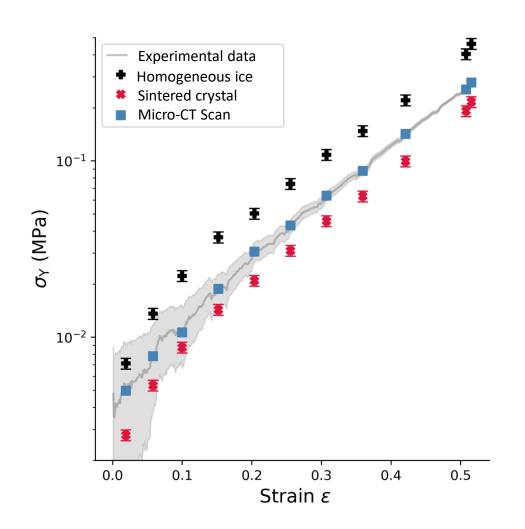




The basal mode is

snow creep

Results: experimental comparison



The same method is repeated for each scan ...

Study of the nonlinear viscosity:

$$B = \frac{\sigma^n}{\dot{\epsilon}}$$

with n=3 by homogeneization (Wautier et al., 2017)

The same process is repeated for the load-controlled test



Results: experimental comparison

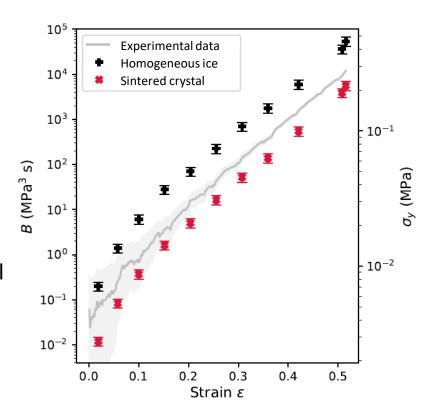
Ice in snow should not be considered as a foam of ice,

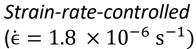


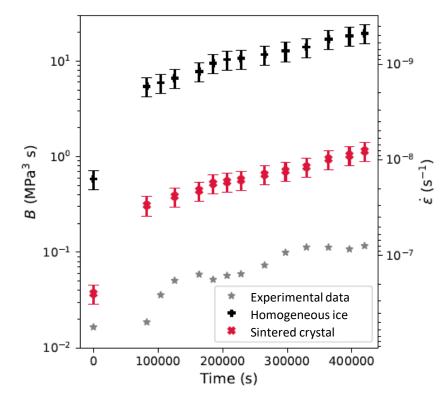
Homogeneous ice model

Sintered crystal model

➤ The gap between the two models decreases as density increases.





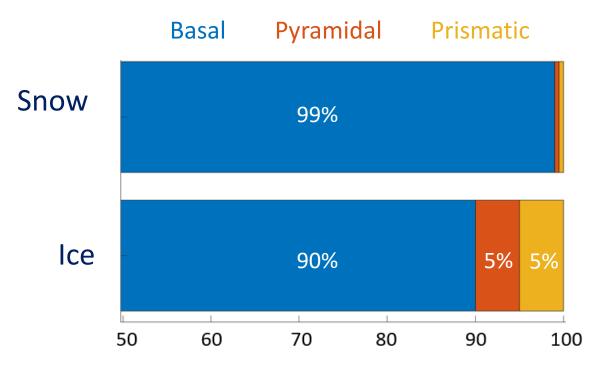


Load-controlled
$$(\sigma_{imp} = 2.1 \text{ kPa})$$



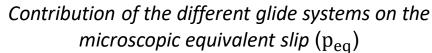


An accommodation of the basal slip different from ice!



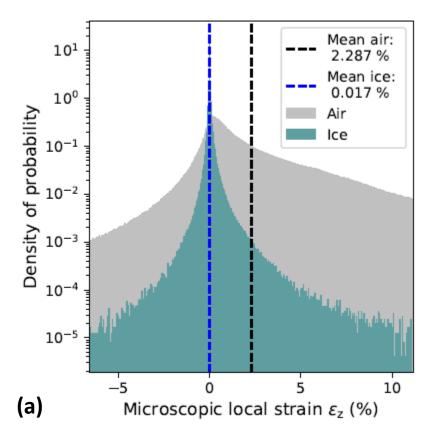
➤ In snow: accommodation between crystals is permitted by the pore space

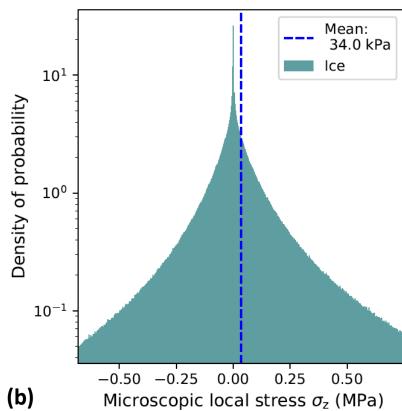










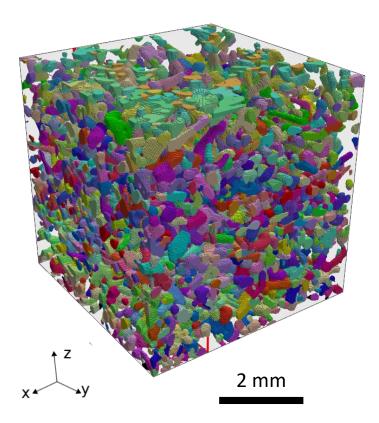


- Macroscopic deformation is mainly due to air deformation and accommodation of the ice matrix.
- Hight stress concentration: 5 % of the microstructure reaches a vertical stress value higher than 0.51 MPa (58 times the macroscopic loading).



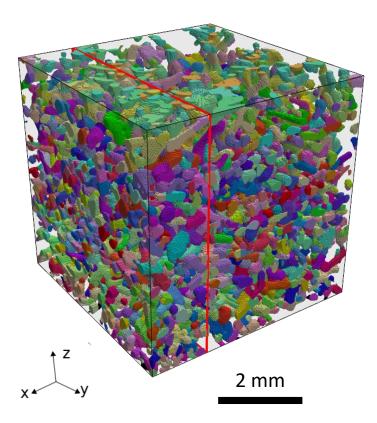
Histogram of the microscopic: (a) local strain ϵ_z distribution, (b) vertical stress σ_z distribution.





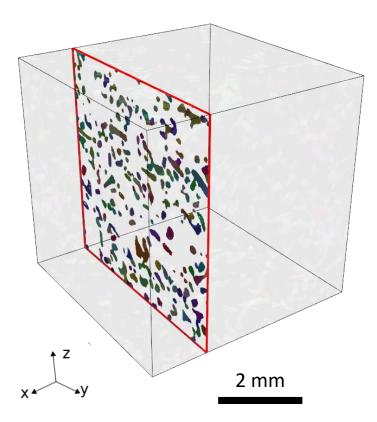






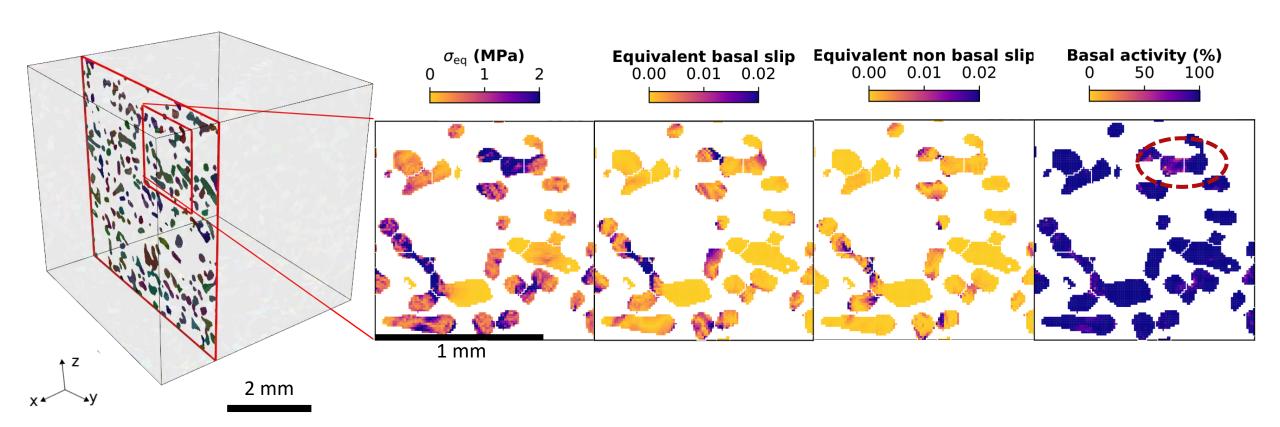














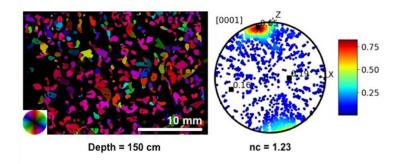
> Equivalent slip occurred preferentially at **crystal bond**, where stress is concentrated

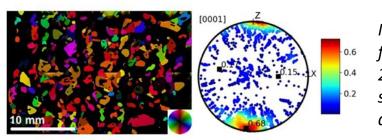


Conclusion and outlooks

First time that a **single-crystal plasticity model** has been used to study the mechanical behaviour of snow.

> Snow cannot be considered as a foam of ice, behaviour of single-crystals need to be considered.





Depth = 246 cm

Microstructure and C-axis pole figure from samples extracted at 150 (A) and 246 (B) cm depth along the EastGRIP snow pit (adapted from Montagnat et al., 2020)





Conclusion and outlooks

First time that a **single-crystal plasticity model** has been used to study the mechanical behaviour of snow.

> Snow cannot be considered as a foam of ice, behaviour of single-crystals need to be considered.

➤ Micro-scale mechanisms not yet understood, particularly at grain boundaries. Hypothesis:

- ➤ Superplasticity (Alley, 1987, Raj & Ashby, 1971)
- ➤ Ductile failure (Kirchner et al. 2001)

→ New behaviour to model and further experiments planned





References

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- Bernard, A., Hagenmuller, P., Montagnat, M., & Chambon, G. (2022, 12). Disentangling creep and isothermal metamorphism during snow settlement with X-ray tomography.
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- ➤ Kirchner, H. O., Michot, G., Narita, H., & Suzuki, T. (2001). Snow as a foam of ice: Plasticity, fracture and the brittle-to-ductile transition. Philosophical Magazine A, 81 (9), 2161–2181.
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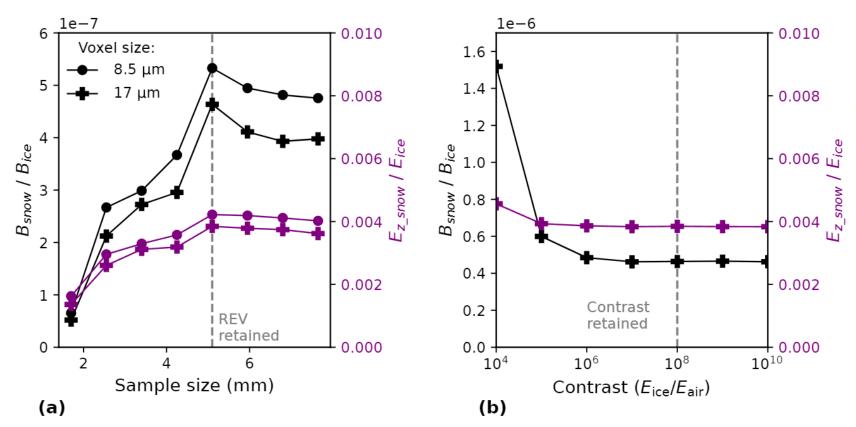
Appendix

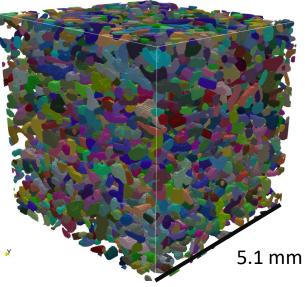




Sensitivity analysis

Representative Elementary Volume and mechanical contrast





Sample studied. Voxel size: 17 μ m $ho = 255~{\rm kg}~{\rm m}^{-3}$, $r_{\rm eq} = 121~{\rm \mu}$ m,



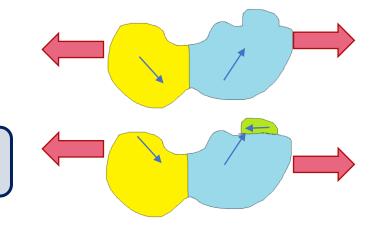
Convergence analysis of the nonlinear viscosity and Young's modulus with respect to: (a) the sample length and (b) the mechanical contrast.

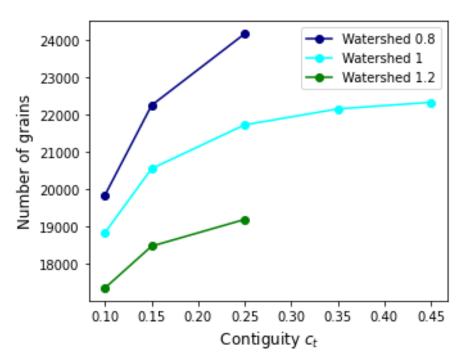


Sensitivity analysis

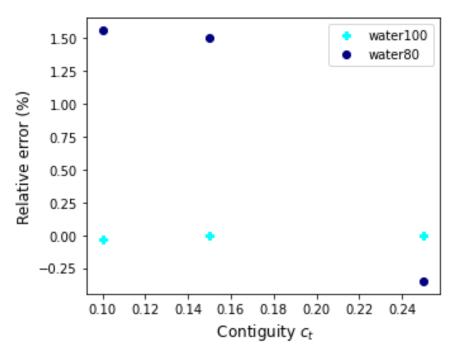
Grain segmentation

Low effect compared to uncertainty (REV, temperature, experimental measurement)





Number of geometrical grains as a function of c_t for different values of $\tilde{\kappa}_t$.

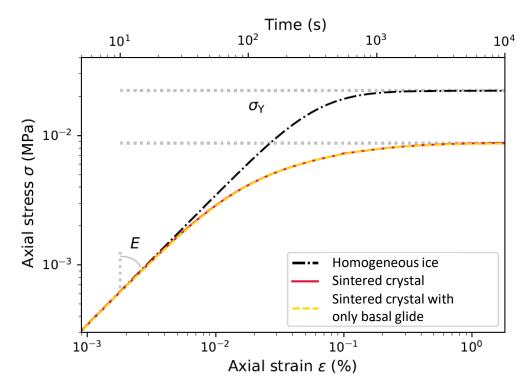


Relative error in the calculation of the snow B as a function of $c_{\rm t}$ for different values of $\tilde{\kappa}_{\rm t}$ (reference $c_{\rm t}=0.15$; $\tilde{\kappa}_{\rm t}=1$)

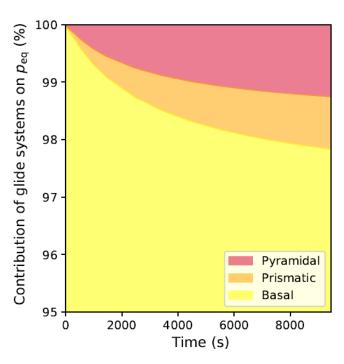




Influence of non-basal slip systems:



Evolution of yield stress with the strain for the different constitutive equations of ice.



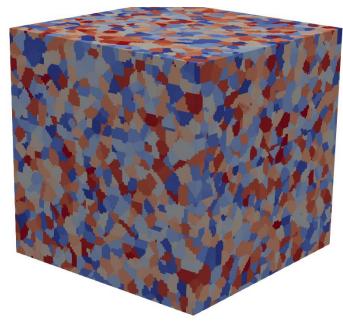
Temporal evolution of the contribution of the different glide systems on the microscopic equivalent slip (p_{eq})





Preliminary study:

Modelling of the viscoplastic behaviour of ice



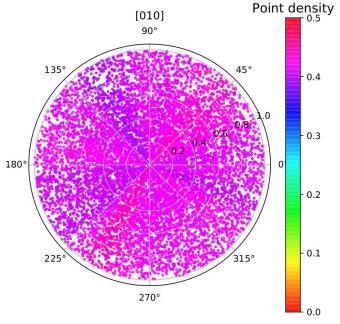
Voronoi, 9261 grains, 106^3 *voxels*

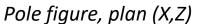
Boundary conditions:

Constant strain rate compression test with stress-free boundary condition

Implementation of the two material laws:

- polycrystalline
- monocrystalline: unknown grain orientation, random draw c-axis









Elasto-viscoplasticity: preliminary study Modelling of the viscoplastic behaviour of ice

Macroscopic laws identified:

• Polycristalline model:

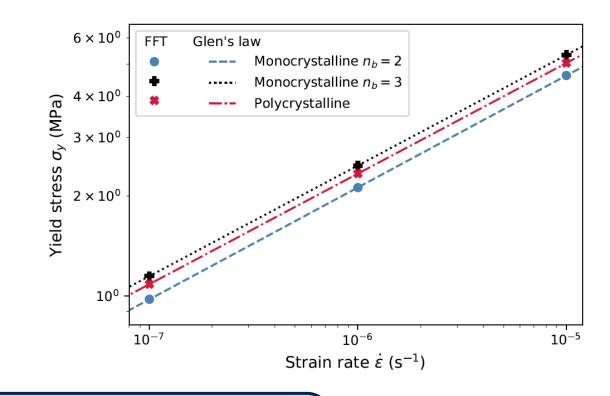
$$\dot{\epsilon} = 7.8 \times 10^{-8} \, \sigma_V^3$$

• Monocristalline model ($n_{basal} = 3$):

$$\dot{\epsilon} = 6.59 \times 10^{-8} \, \sigma_V^3$$

• Macroscopic laws identified ($n_{basal} = 2$):

$$\dot{\epsilon} = 1.12 \times 10^{-8} \, \sigma_Y^{2.96}$$



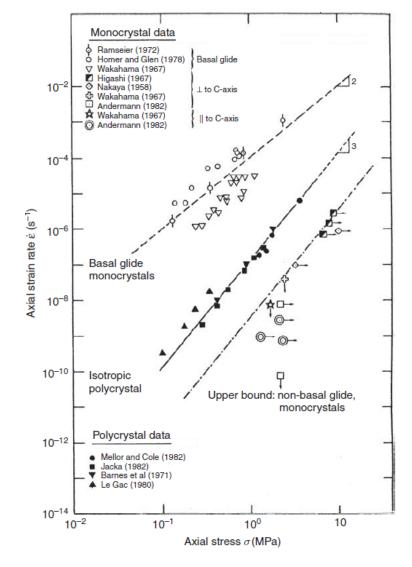
- Simplified geometry
- Incertainties on the prefactor A of $\pm 25\%$
 - Neglieable compared to error committed on snow





Limits and outlooks

- Basal slip system is main deformation mechanism
- Experiments show that basal slip system has an exponent 2 (3 for all systems in our study)
 - need to calibrate a new crystal plasticity model on polycrystalline ice
- Homogenization of an elasto-viscoplastic law for a wide range of snow microstructures, to develop improved formulations of snow settlement in detailed snowpack simulation tools.



Stress—strain rate relationship for steady-state basal and non-basal slip in single crystals at -10 °C.

(Schulson and Duval, 2009)



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