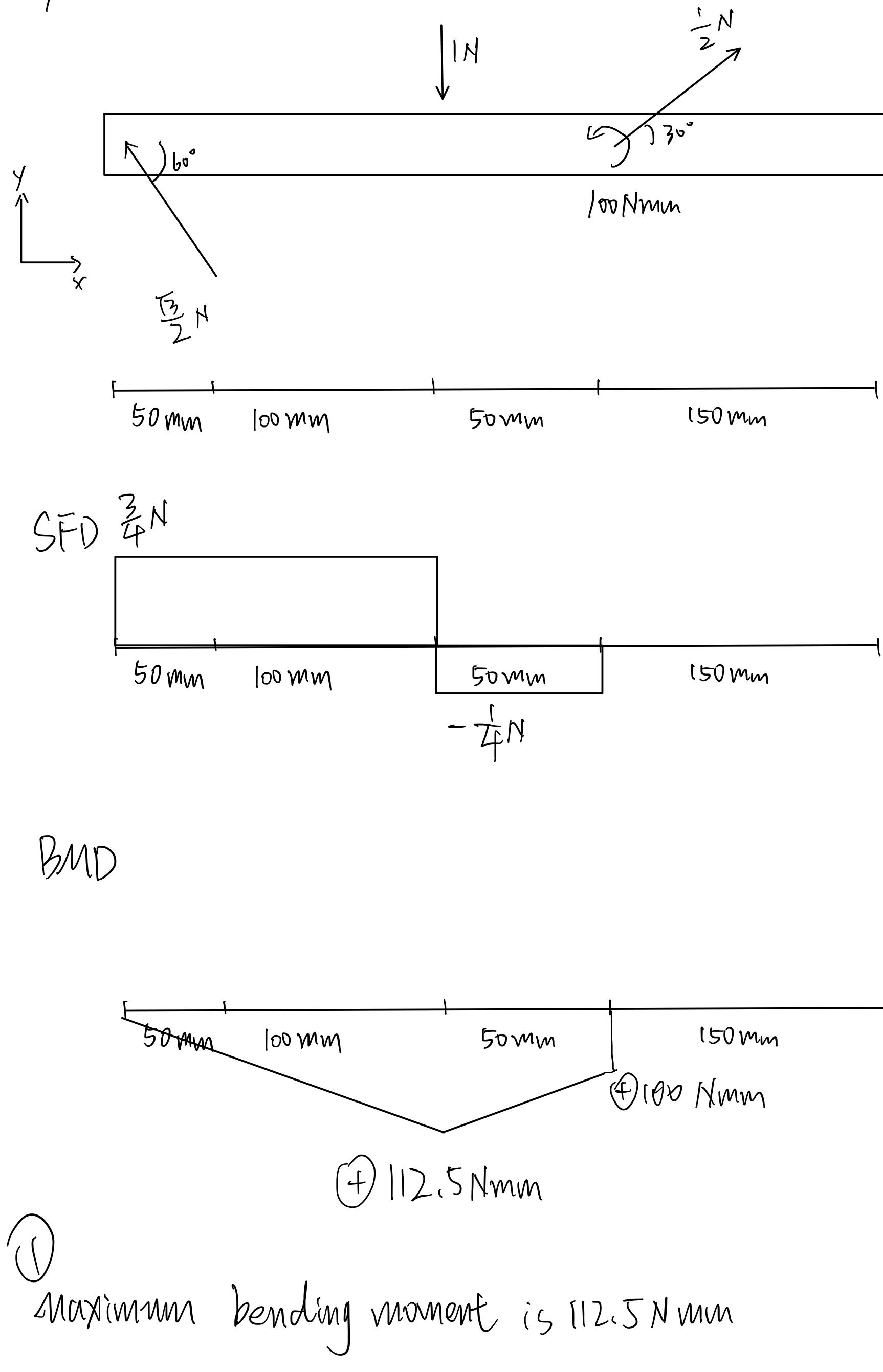


Base calculation

2020年9月28日 星期一 23:52

Assume Force on Tie is 1 N

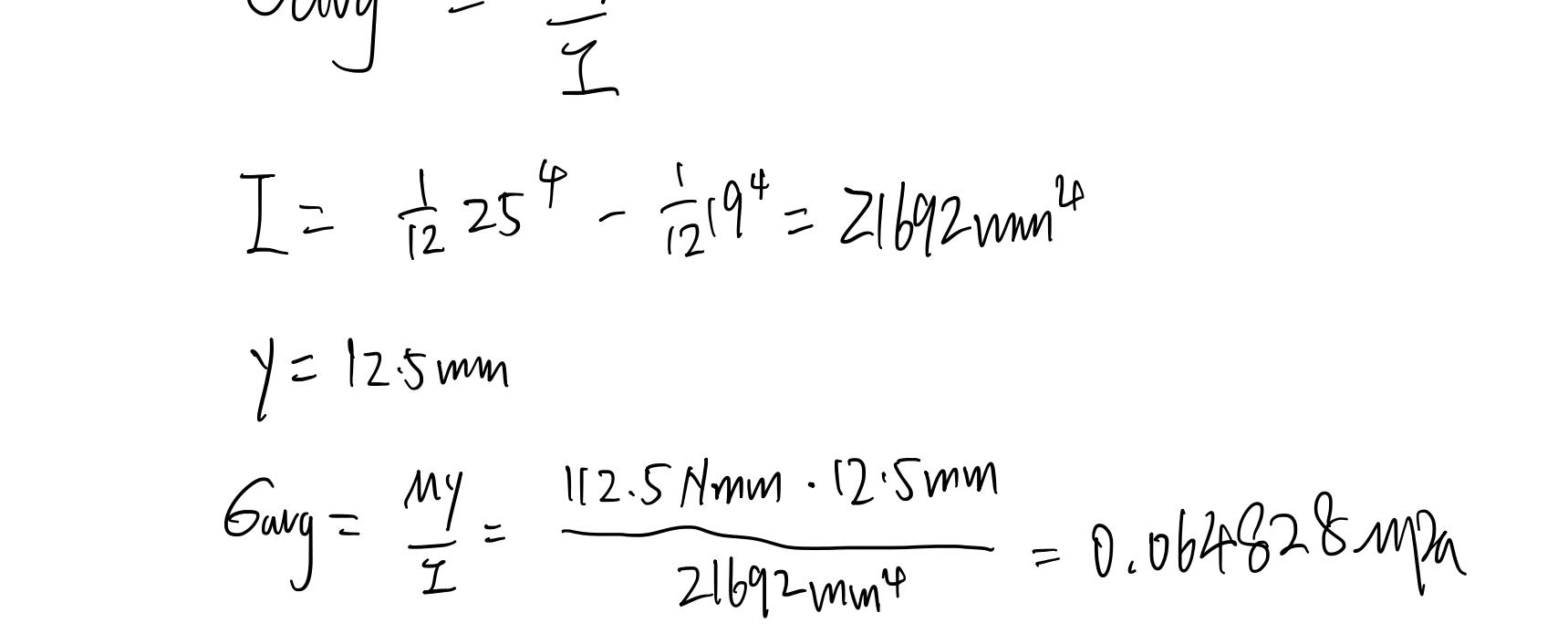


$$\sin 60^\circ = \frac{\sqrt{3}}{2}$$

$$\sin 30^\circ = 0.5$$

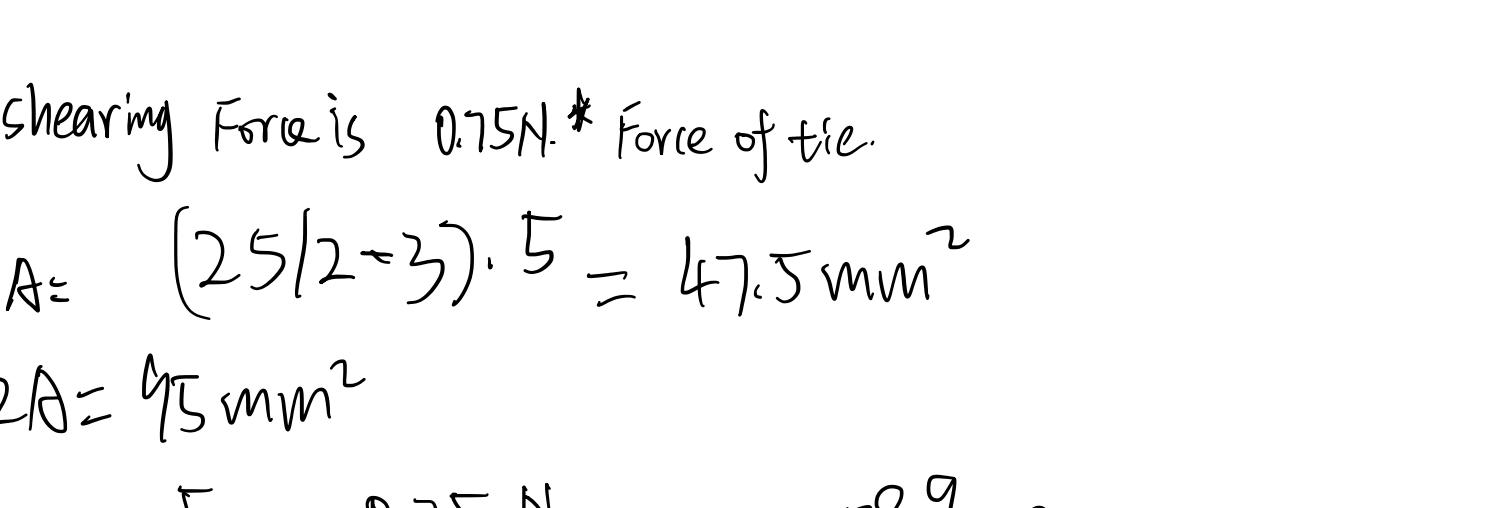
$$\cos 30^\circ = \frac{\sqrt{3}}{2}$$

$$\cos 60^\circ = 0.5$$



$$\text{axial Force: } \frac{\sqrt{3}}{4} N$$

BMD



$$\textcircled{1} 112.5 \text{ Nmm}$$

① Maximum bending moment is 112.5 Nmm



$$\sigma_{avg} = \frac{My}{I}$$

$$I = \frac{1}{12} 25^4 - \frac{1}{12} 19^4 = 21692 \text{ mm}^4$$

$$y = 12.5 \text{ mm}$$

$$\sigma_{avg} = \frac{My}{I} = \frac{112.5 \text{ Nmm} \cdot 12.5 \text{ mm}}{21692 \text{ mm}^4} = 0.064028 \text{ MPa}$$

Stress concentration factor around the hole.

$$\frac{d}{H} = \frac{10.5}{25} = 0.42 \quad k_{tg} = 3.8$$

$$\sigma_{max} = k_{tg} \sigma_{avg} = 0.2463464 \text{ MPa}$$

② Failure at the clamp:

Shearing Force is 0.75N * Force of tie.

$$A_s = (25/2 - 3) \cdot 5 = 47.5 \text{ mm}^2$$

$$2A = 95 \text{ mm}^2$$

$$T = \frac{F}{A} = \frac{0.75 \text{ N}}{95 \text{ mm}^2} = 0.00789 \text{ MPa}$$

Using von Mises:

$$\sigma_{max} = \frac{T}{\sqrt{3}} = 0.004558 \text{ MPa}$$

③ Failure at welding near clamp

ER70S6

Tensile strength = 70 MPa

Subject to Bending moment 37.5 Nmm shear Force 0.75N

Axial force $\frac{\sqrt{3}}{4} N$ compression

④ Failure at welding near base beam

Subject to transverse load.

Safety factor: 3.

Yield strength of weld metal: 70 MPa

assume shear failure at throat area of the shorter weld.

$$A = 0.707 \times 4 \times 14.43 = 40.8084 \text{ mm}^2$$

Using distortion energy theory:

$$\sigma_{sy} = 0.585 = 0.58 \times 70 = 40.6 \text{ MPa}$$

$$\sigma = \frac{F}{A} = \frac{0.5 F}{40.8084} = 0.01225 F \text{ (MPa)}$$

Subject to Torsional load:

Polar moment of Inertia



Find CG

$$x = \frac{\sum A_i x_i}{\sum A_i} = \frac{\frac{25}{\sqrt{3}} t \cdot \frac{25}{\sqrt{3}} + \frac{50}{\sqrt{3}} t \cdot \frac{25}{\sqrt{3}}}{\frac{25}{\sqrt{3}} t + \frac{50}{\sqrt{3}} t} = \frac{\frac{25^2}{\sqrt{3}} t + \frac{2 \times 25^2}{\sqrt{3}} t}{\frac{25}{\sqrt{3}} t + \frac{50}{\sqrt{3}} t} = \frac{\frac{25^2}{\sqrt{3}} t}{\frac{75}{\sqrt{3}} t} = \frac{25^2}{75} = 6.11 \text{ mm}$$

$$y = \frac{\sum A_i y_i}{\sum A_i} = 0 + 0 = 0$$

$J = I_x + I_y$

$$= \left(\frac{25}{\sqrt{3}} t \right)^2 + \frac{50}{\sqrt{3}} t \left(\frac{50}{\sqrt{3}} t - \frac{25}{\sqrt{3}} t \right)^2 + \frac{25}{\sqrt{3}} t \left(\frac{25}{\sqrt{3}} t - \frac{25}{\sqrt{3}} t \right)^2 + \frac{(25)}{\sqrt{3}} t^2 = 27564.5 t^2 \text{ mm}^4$$

$$= 250.58 t + 16.13 t + 333.05 t + 204.68 t = 27564.5 t^2 \text{ mm}^4$$

$$\sigma_{torsion} = \frac{T}{J} = \frac{T \cdot 16.13 \text{ mm}}{27564.5 \cdot 4 \text{ mm}^4} = 0.00148742 T \text{ (MPa)}$$

Relate it to the force on tie. $T = 100 F$

$$\sigma_{torsion} = 0.00148742 \cdot 100 F = 0.148742 F$$

Total shear due to transverse force and torsional:

$$\sigma_{total} = 0.148742 F + 0.01225 F = 0.16099 F$$

$$\sigma_{sy} = 40.6 \text{ MPa}$$

$$\rightarrow 0.3325 \cdot 29 F < 40.6 \text{ MPa}$$

$$F < 122 \text{ N}$$

Double part the $2F = 244 \text{ N}$