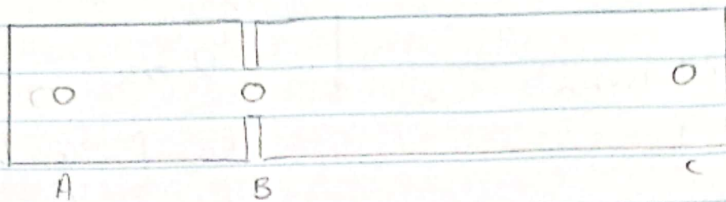
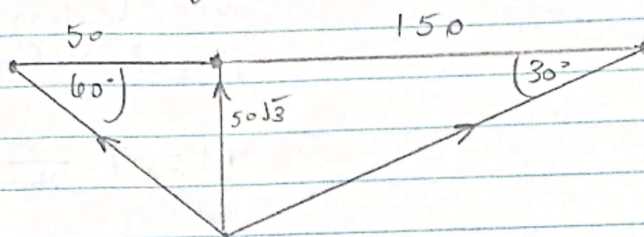


## Beam (cable)

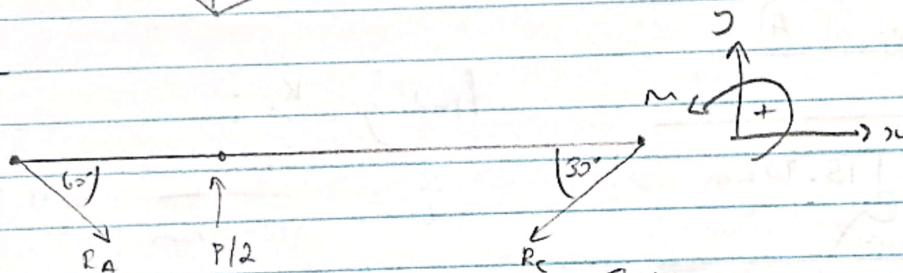


Assumptions:

- due to bearing nut, P/2 force is experienced by the beam
- geometry remains constant during loadings negligible change in angles upon loading



\* FBD



$$\sum F_y = 0$$

$$\frac{P}{2} = R_A \sin 60^\circ + R_C \sin 30^\circ$$

$$\therefore P = 2 \left( R_A \frac{\sqrt{3}}{2} + R_C \frac{1}{2} \right)$$

$$\therefore P = \sqrt{3} R_A + R_C$$

$$\sum F_x = 0$$

$$R_A \cos 60^\circ = R_C \cos 30^\circ$$

$$\therefore \frac{R_A}{R_C} = \frac{\sqrt{3}}{2}$$

$$\therefore R_A = R_C \sqrt{3}$$

$$P = \sqrt{3} (R_C \sqrt{3}) + R_C$$

$$= 3R_C + R_C$$

$$P = 4R_C //$$

$$\therefore R_C = P \cdot \frac{1}{4}$$

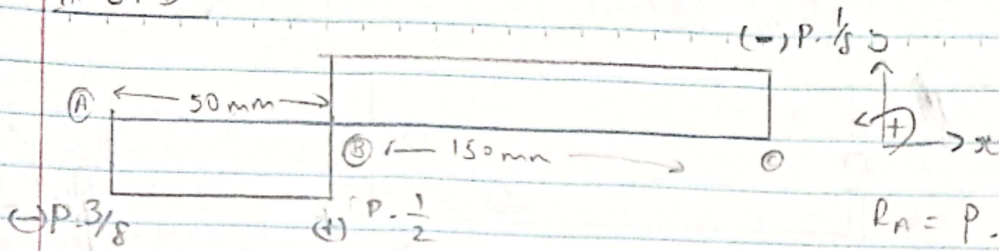
$$\therefore R_A = P \cdot \frac{\sqrt{3}}{4}$$

hence:

$$R_{A,y} = P \cdot \frac{\sqrt{3}}{4} \cdot \sin 60^\circ = P \cdot \frac{\sqrt{3}}{4} \cdot \frac{\sqrt{3}}{2} = P \cdot \frac{3}{8} \text{ N}$$

$$R_{C,y} = P \cdot \frac{1}{4} \cdot \sin 30^\circ = P \cdot \frac{1}{4} \cdot \frac{1}{2} = P \cdot \frac{1}{8} \text{ N}$$

\* SFD

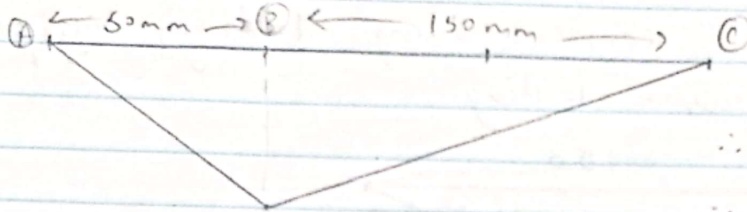


$$R_A = P \cdot \frac{3}{8} \quad (-)$$

$$R_B = P \cdot \frac{1}{2} \quad (+)$$

$$R_C = P \cdot \frac{1}{8} \quad (-)$$

\* BMD

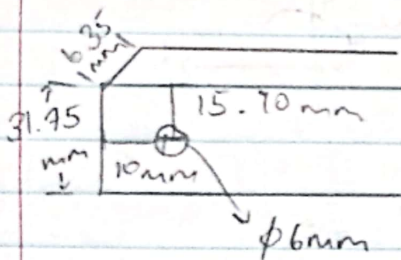


$\therefore$  max bending at (B)

$$M = P \cdot \frac{3}{8} \text{ N} \times 0.05 \text{ m}$$

$$\therefore M = P \cdot \frac{3}{160} \text{ Nm}$$

\* stresses at A



finding  $K_t$ :

$$\frac{d}{b} = \frac{6 \text{ mm}}{31.75 \text{ mm}} = 0.189 \approx 0.2$$

$$\therefore K_t \approx 5.5 \text{ (considering "pin loaded web")}$$

finding  $\sigma_{max}$ :

$$\sigma_{max} = K_t \cdot \sigma_{nom}$$

$$\sigma_{max} = 5.5 \times 0.00229 \cdot P \text{ MPa}$$

$$= 0.0126 \times P \text{ MPa}$$

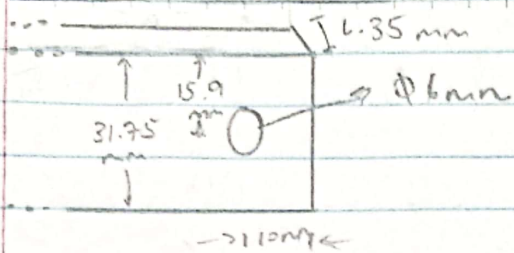
$$\sigma_{nom} = \frac{P}{(b-d)h}$$

$$= \frac{P \cdot \frac{3}{8} \text{ N}}{(31.75 \text{ mm} - 6 \text{ mm})(6.35 \text{ mm})}$$

$$= 0.00229 \cdot P \text{ MPa}$$



\* STRESS at (C)



finding  $K_t$ :

$$\frac{d}{h} = \frac{6 \text{ mm}}{31.75 \text{ mm}} = 0.1889 \approx 0.20$$

$$\Rightarrow K_t \approx 5.5 \text{ ("pin loaded hole")}$$

finding  $\sigma_{max}$ :

$$\sigma_{max} = K_t \cdot \sigma_{nom}$$

$$\therefore \sigma_{max} = 5.5 \times 0.00076 \text{ P MPa}$$

$$= 0.0042 \text{ P MPa}$$

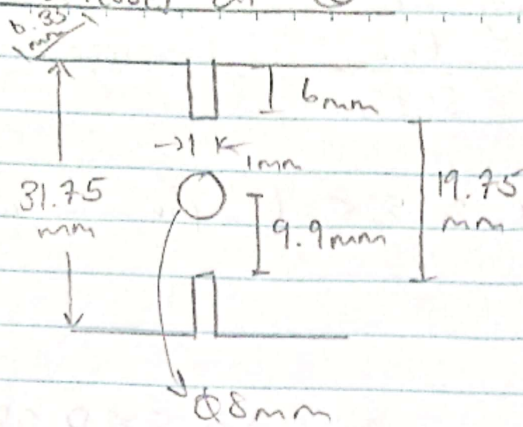
$$\sigma_{nom} = \frac{P}{(h-d)h}$$

$$P: 1/8 \text{ N}$$

$$= \frac{(31.75 \text{ mm} - 6 \text{ mm})(6.35 \text{ mm})}{P}$$

$$= 0.00076 \text{ P MPa}$$

\* Stresser at (B)



considering "hole":

$$R_B = P/2 \text{ N}$$

$$\therefore \frac{d}{L} = \frac{8 \text{ mm}}{19.75 \text{ mm}} = 0.405 \approx 0.40$$

$$\therefore K_t \approx 2.25 \text{ ("Unbored hole")}$$

$$\therefore \sigma_{\max} = K_t \cdot \sigma_{\text{nom}}$$

$$\begin{aligned} \therefore \sigma_{\text{nom}} &= \frac{P}{(b-d)L} \\ &= \frac{P \cdot 1/2 \text{ N}}{(19.75 \text{ mm} - 8 \text{ mm})(6.35 \text{ mm})} \\ &= 0.0067 \cdot P \text{ MPa} \end{aligned}$$

$$\begin{aligned} \therefore \sigma_{\max} &= 2.25 \times 0.0067 P \\ &= 0.01508 P \text{ MPa (axial)} \end{aligned}$$

$$\frac{d}{L} = \frac{8 \text{ mm}}{19.75 \text{ mm}} = 0.405 \approx 0.40$$

$$\frac{d}{b} = \frac{8 \text{ mm}}{6.35 \text{ mm}} = 1.26 \approx 1.25$$

$$M_B = P \cdot \frac{3}{160} \text{ Nm}$$

$$\therefore K_t \approx 1.25$$

$$\begin{aligned} \therefore \sigma_{\max} &= 1.25 \times 1507.8 P \text{ Pa} \\ &= 1884.74 P \text{ Pa} \\ &= 1.88 P \text{ MPa (bending)} \end{aligned}$$

$$\sigma_{\max} = K_t \cdot \sigma_{\text{nom}}$$

$$\begin{aligned} \sigma_{\text{nom}} &= \frac{6M}{(b-d)L^2} \\ &= \frac{6(P \cdot 3/160 \text{ Nm})}{(19.75 \text{ mm} - 8 \text{ mm})(6.35 \text{ mm})^2} \\ &= 1507.8 P \text{ Pa} \end{aligned}$$



considering "notch":

$$R_B = P/2 \text{ N}$$

Assumption

→ approximate notch of radius  $r \Rightarrow r = 6 \text{ mm}$

$$\therefore \frac{r}{h} = \frac{6 \text{ mm}}{19.75 \text{ mm}} = 0.303 \approx 0.30$$

$$\therefore \frac{H}{h} = \frac{31.75 \text{ mm}}{19.75 \text{ mm}} = 1.607 \approx 1.60$$

$$\therefore K_t = 1.8$$

$$\therefore \sigma_{\max} = 1.8 \times \sigma_{\text{nom}} \\ = 0.00718P \text{ MPa (axial)}$$

$$\therefore \sigma_{\max} = K_t \cdot \sigma_{\text{nom}}$$

$$\Rightarrow \sigma_{\text{nom}} = \frac{P}{bh} \\ = \frac{P/2 \text{ N}}{6.35 \text{ mm} \times 19.75 \text{ mm}} \\ = 0.00398P \text{ MPa}$$

$$M_B = P \cdot \frac{3}{160} \text{ Nm}$$

$$\therefore \frac{r}{h} = \frac{6 \text{ mm}}{19.75 \text{ mm}} = 0.303 \approx 0.30$$

$$\frac{H}{h} = \frac{31.75 \text{ mm}}{19.75 \text{ mm}} = 1.607 \approx 1.60$$

$$\therefore K_t = 1.5$$

$$\therefore \sigma_{\max} = 1.5 \sigma_{\text{nom}}$$

$$\therefore \sigma_{\max} = K_t \cdot \sigma_{\text{nom}}$$

$$= 68.1P \text{ MPa}$$

(bending)

$$\therefore \sigma_{\text{nom}} = \frac{bm}{bh^2} \\ = \frac{6(P \cdot 3/160 \text{ Nm})}{(6.35 \text{ mm})(19.75 \text{ mm})^2}$$

$$= 45419.7P \text{ Pa}$$

$$= 45.42P \text{ MPa}$$

\* Superimpose to find total stress concentration at 8:

$$\sigma_{max} = \sigma_{max, axial, hole} + \sigma_{max, bend, hole} \\ + \sigma_{max, axial, notch} + \sigma_{max, bend, notch}$$

$$= 0.01508P + 1.88P + 0.02718P + 6P.1P$$

$$= 70P$$