

RIPASSONE

SISTEMA DINAMICO:

T.C.

$$\begin{cases} \dot{x} = A(t)x + B(t)u(t) \\ y(t) = C(t)x(t) + D(t)u(t) \end{cases}$$

$$\begin{cases} x(k+1) = f(x(k), u(k), k) \\ y(k) = g(x(k), u(k), k) \end{cases}$$

VAR. CONTROLLATA: y

VAR. DI CONTROLLO: u

SEGNALE DI RIF: w

- SISO: 1 ing, 1 uscita

- MIMO: molteplici ing e uscite

- STRETT. PROPRIO: $y = g(x(t), t)$, mo $u(t)$

- STAZIONARIO: $y = g(x(t), u(t))$, mo t

- NON-DINAMICO: $y = (u(t), t)$, mo $x(t)$

es. $p_1(t), p_2(t)$ posizioni k_1, k_2 cost. elastiche

$F_1(t), F_2(t)$ su carrelli

1- sistema MIMO, strett. proprio, stazionario, dinamico

$$\text{su } m_1: F_1 + k_2(p_2(t) - p_1(t)) - k_1 p_1(t) = m_1 \frac{d^2 p_1(t)}{dt^2} \rightarrow \ddot{p}_1(t) = \frac{k_2}{m_1} p_2(t) - \frac{k_2 + k_1}{m_1} p_1(t) + \frac{F_1}{m_1}$$

$$\text{su } m_2: F_2 - k_2(p_2 - p_1) = m_2 \frac{d^2 p_2}{dt^2}$$

$$\rightarrow \ddot{p}_2(t) = \frac{k_2}{m_2} p_1(t) - \frac{k_2}{m_2} p_2(t) + \frac{F_2}{m_2}$$

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -\frac{k_2 + k_1}{m_1} & 0 & \frac{k_2}{m_1} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_2}{m_2} & 0 & -\frac{k_2}{m_2} & 0 \end{bmatrix}$$

$$B = \begin{bmatrix} 0 & 0 \\ \frac{1}{m_1} & 0 \\ 0 & 0 \\ 0 & \frac{1}{m_2} \end{bmatrix}$$

$$C = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix}$$

$$D = 0$$

$$k_{1,2} = 1; m_1 = 1, m_2 = 2$$

$$\begin{cases} \dot{x}_1 = x_2(t) \\ \dot{x}_2(t) = -2x_1(t) + x_3(t) + u_1 \\ \dot{x}_3 = x_4(t) \\ \dot{x}_4(t) = \frac{1}{2}x_1 - \frac{1}{2}x_3 + \frac{u_2}{2} \\ y_1(t) = x_1(t) \\ y_2(t) = x_3(t) \end{cases}$$

$$x_2 = \dot{p}_1, x_1 = p_1, x_3 = p_2, x_4 = \dot{p}_2, u_1 = F_1, u_2 = F_2$$

→ SISTEMA LINEARE:

$$\begin{cases} \dot{x}(t) = A(t)x(t) + B(t)u(t) \\ y(t) = C(t)x(t) + D(t)u(t) \end{cases}$$

$$\begin{cases} x(k+1) = A(k)x(k) + B(k)u(k) \\ y(k) = C(k)x(k) + D(k)u(k) \end{cases}$$

→ EQUILIBRIO:

$$u(t) = \bar{u}$$

$$\dot{x}(t) = 0$$

$$\bar{y} = g(\bar{x}, \bar{u})$$

$$u(k) = \bar{u}, \bar{x}(k+1) = \bar{x}(k), y(k) = \bar{y}$$

$$\bar{x} = f(\bar{x}, \bar{u})$$

$$\bar{y} = g(\bar{x}, \bar{u})$$

trovo pti di equilibrio

→ FORMULA LAGRANGE:

$$x(t) = x_{t_0} e^{a(t-t_0)} + \int_{t_0}^t e^{a(t-z)} b u(z) dz$$

$$x(k) = A^{k-k_0} x(k_0) + \sum_{i=k_0}^{k-1} A^{k-i-1} B u(i)$$

$$y(k) = C A^{k-k_0} x_{k_0} + C \sum_{i=k_0}^{k-1} A^{k-i-1} B u(i) + D u(k)$$

de la soluzione $a, b, c, d \in \mathbb{R}$

$$\text{guad. statico } \bar{e}: \frac{\bar{y}}{\bar{u}} = C(I - A)^{-1} B + D$$

PER ENTRAMBI

SE A, B, C, D matrici: $x(t) =$ uguale ma con mat.

$$y(t) = C e^{A(t-t_0)} x_{t_0} + C \int_{t_0}^t e^{A(t-z)} B u(z) dz + D u(t)$$

$$\rightarrow e^{At} = I + At + A^2 \frac{t^2}{2!} + A^3 \frac{t^3}{3!} + \dots$$

$$= \mathcal{L}^{-1}[(sI - A)^{-1}]$$

→ LINEARIZZAZIONE: $\dot{x}(t) = f(\bar{x} + \delta x(t), \bar{u} + \delta u(t))$

$$\bar{y} + \delta y(t) = g(\bar{x} + \delta x(t), \bar{u} + \delta u(t))$$

Sost. $x(t) = \bar{x} + \delta x(t)$
 \hookrightarrow eq.

→ SEGNALI:
 periodico

$$p(t) = \sum_{m=-\infty}^{+\infty} F_m e^{jm\omega_0 t}$$

$$p(t) = p(t + T)$$

$$\omega_0 = \frac{2\pi}{T}$$

$$F_m = \frac{1}{T} \int_T p(t) e^{-jm\omega_0 t} dt$$

→ TRASF. DI FOUR:

$$F(j\omega) = \mathcal{F}[p(t)] = \int_{-\infty}^{+\infty} p(t) e^{-j\omega t} dt$$

$$p(t) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} F(j\omega) e^{j\omega t} d\omega$$

→ TRASF. LAPLACE:

$$F(s) = \int_{-\infty}^{+\infty} p(t) e^{-st} dt$$

$$p(t) = \frac{1}{2\pi} \int_{\sigma-i\infty}^{\sigma+i\infty} F(s) e^{st} ds \quad \text{inversa}$$

→ RITARDO:

$$\mathcal{L}[p(t)] = F(s) \rightarrow \mathcal{L}[p(t-z)] = e^{-zs} F(s)$$

$$\mathcal{L}[e^{\alpha t} p(t)] = F(s-\alpha)$$

→ DERIVAZ:

$$\mathcal{L}[\dot{p}(t)] = sF(s) - p(0) \quad \left(\text{se } + \text{ volte } m \right)$$

→ INTEG:

$$\mathcal{L}[\int p(\tau) d\tau] = \frac{1}{s} F(s)$$

→ FdT:

$$G(s) = C(sI - A)^{-1} B + D$$

→ F GENERALE:

$$\mathcal{L}[t^m e^{\alpha t} \cos(\omega t)] = \frac{m!}{(s-\alpha)^{m+1}}$$

→ FUNZIONI DI SENSIBILITÀ:

• sensitività:

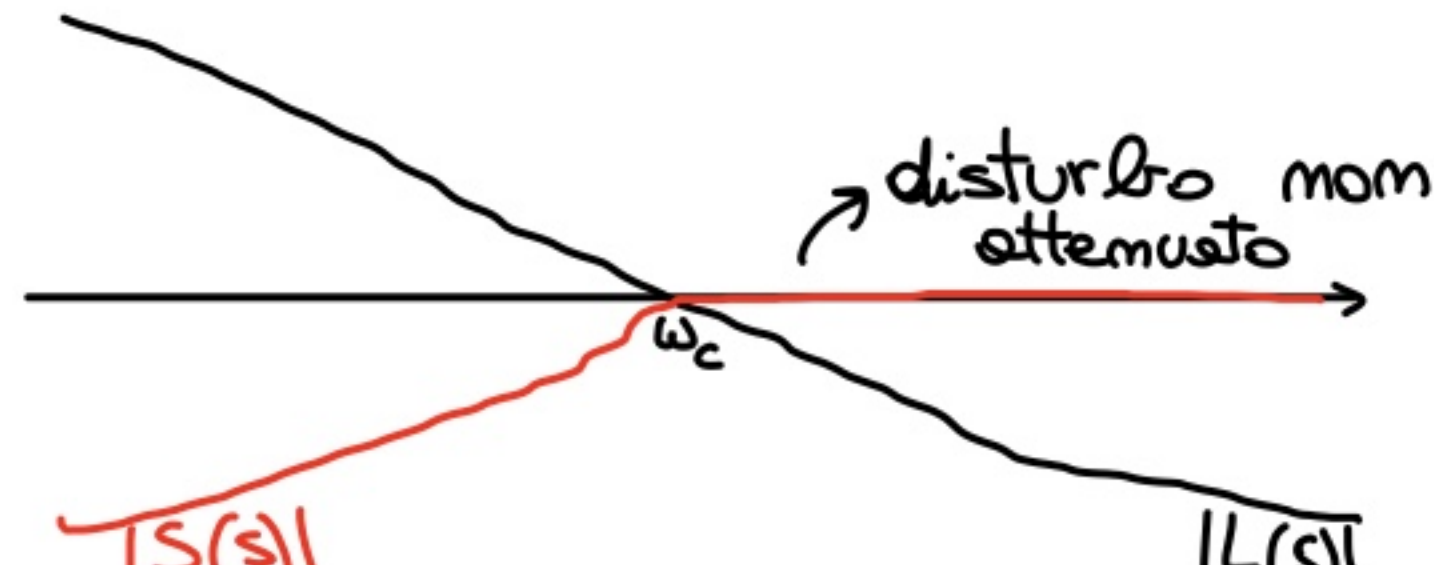
$$\frac{Y(s)}{D(s)} = S(s) = \frac{1}{1+L(s)}$$

$$\lim_{s \rightarrow 0} S(s) = \begin{cases} \frac{1}{1+\mu} & , g=0 \\ 0 & , g>0 \\ 1 & , g<0 \end{cases}$$

idealmente $S(s) = 0$

$$|S(j\omega)| = \frac{1}{1+|L(j\omega)|} = \begin{cases} \frac{1}{|L(j\omega)|} & \omega \ll \omega_c \\ 1 & \omega \gg \omega_c \end{cases}$$

[FILTRO PASSA-ALTO]



$$\delta x(k+1) = \frac{\partial f}{\partial x} \Big|_{\substack{x=\bar{x} \\ u=\bar{u}}} \delta x(k) + \frac{\partial f}{\partial u} \Big|_{\substack{x=\bar{x} \\ u=\bar{u}}} \delta u(k)$$

$$\delta y(k) = \frac{\partial g}{\partial x} \Big|_{\substack{x=\bar{x} \\ u=\bar{u}}} \delta x(k) + \frac{\partial g}{\partial u} \Big|_{\substack{x=\bar{x} \\ u=\bar{u}}} \delta u(k)$$

\bar{x}, \bar{u} pto di equilibrio

$$p(k) = \sum_N F_m e^{jm\theta_0 k}$$

$$p(k) = p(k+N)$$

$$\theta_0 = \frac{2\pi}{N}$$

\hookrightarrow tipo il periodo

$$F_m = \frac{1}{N} \sum_N p(k) e^{-jm\theta_0 k}$$

$$F(e^{j\theta}) = \mathcal{F}^*[p(k)] = \sum_{k=-\infty}^{+\infty} p(k) e^{-j\theta k}$$

$$p(k) = \frac{1}{2\pi} \int_{-\pi}^{\pi} F(e^{j\theta}) e^{j\theta k} d\theta$$

→ TRASF. ZETA:

$$F(z) = \sum_{k=-\infty}^{+\infty} p(k) z^{-k}$$

$$p(k) = \frac{1}{2\pi j} \oint F(z) z^{k-1} dz$$

$$\mathcal{Z}[p(k)] = F(z) \rightarrow \mathcal{Z}[p(k-1)] = z^{-1} F(z)$$

→ ANTICIPO:

$$\mathcal{Z}[p(k)] = F(z) \rightarrow \mathcal{Z}[p(k+1)] = z F(z)$$

$$\mathcal{Z}[kp(k)] = -z \frac{dF(z)}{dz}$$

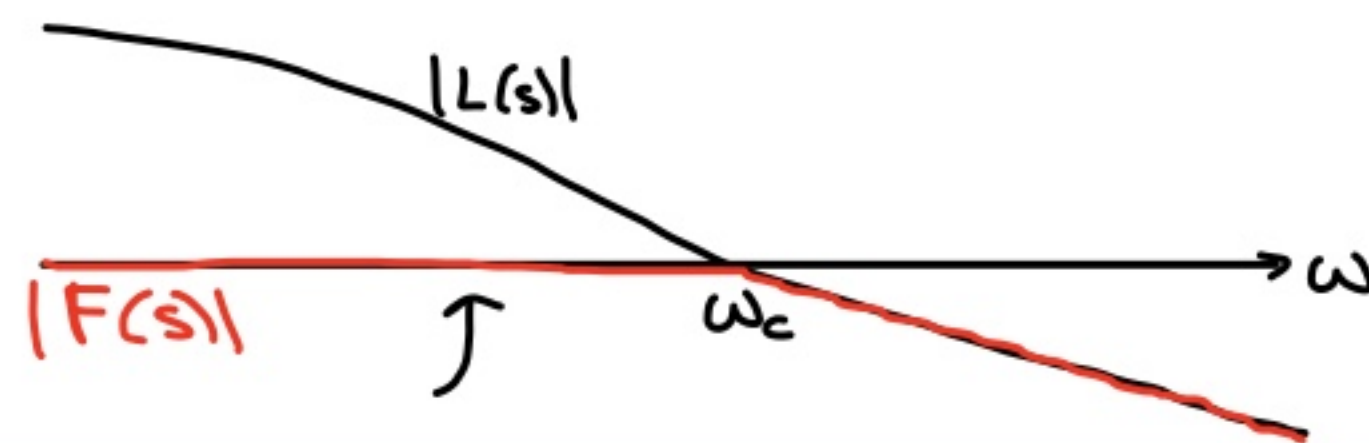
$$G(z) = C(zI - A)^{-1} B + D$$

• sensit. complement.: $\frac{Y(s)}{N(s)} = F(s) = \frac{-L(s)}{1+L(s)}$ idealmente $F(s)=1$

disturbo su
retroaz.

$$\lim_{s \rightarrow 0} F(s) = \begin{cases} \frac{\mu}{1+\mu}, & q=0 \\ 0, & q<0 \\ 1, & q>0 \end{cases}$$

$$|F(j\omega)| = \frac{|L(j\omega)|}{|1+L(j\omega)|} = \begin{cases} 1 & \omega \ll \omega_c \\ |L(j\omega)| & \omega \gg \omega_c \end{cases}$$



→ se $\varphi_m < 75^\circ$: $T_s = \frac{5}{\xi \omega_c}$

$\xi = \frac{\varphi_m}{100}$

$$F(s) \approx \begin{cases} \frac{1}{1+s/\omega_c} & \varphi_m > 50^\circ \\ \frac{\omega_c^2}{s^2 + 2\xi\omega_c s + \omega_c^2} & \varphi_m < 50^\circ \end{cases}$$

• sensit. del controllo: $\frac{U(s)}{Y^*(s)} = Q(s) = \frac{R(s)}{1+R(s)G(s)} = R(s)S(s) = F(s)G^{-1}(s)$

$$|Q(j\omega)| = \frac{|R(j\omega)|}{|1+L(j\omega)|} \begin{cases} \frac{1}{|G(j\omega)|} & \omega \ll \omega_c \\ |R(j\omega)| & \omega \gg \omega_c \end{cases}$$

→ CONTROLLORI P, PI, PID, PD:

• PID: $R(s) = K_p + \frac{K_I}{s} + K_D s = K_p \left(1 + \frac{1}{sT_I} + sT_D \right)$ → aggiungo polo in alta freq. per compensare 2 zeri

→ semplicità di realizzazione, efficacia, affidabilità ed economicità, semplicità taratura parametri o taratura automatica.

• PI: $R(s) = \frac{K_p s + K_I}{s} = K_p \frac{1 + T_I s}{sT_I}$ cancello polo lento