Gas Dynamics — Work 1

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1 Part 1

1.1 Initial Values

The freestream properties at 18.00 km and Mach 3, as taken from website AeroToolbox (https://aerotoolbox.com/atmcalc/), are:

Table 1 – Freestream flow properties.

Property	Value	
P	7505 Pa	
M	3.000	
T	216.7 K	
ρ	0.1207kg/m^3	

1.2 Equation system

The flow across the planar 3-shockwave diffuser is assumed to be constant in the control volumes ∞ , 1, and 2. Inside control volume 3, the flow is subsonic and isentropic, but we are only interested in the values imediately after the shockwave, so we will not calculate the changes inside this volume.

Across the region boundaries, the flow goes through shockwaves. The flow after a shockwave can be calculated from the flow before the shockwave according to Eqs. (1.1) to (1.7) (ANDERSON JR., 2017), where the properties before and after the shock are represented by the subscripts 1 and 2, respectively. The right side of these equations depend only on the Mach number before the shockwave M_1 and the shockwave angle β . Alternatively, we can calculate β from θ , but that would lead to costlier calculations.

$$M_{n,1} = M_1 \sin \beta \tag{1.1}$$

$$M_{n,2}^{2} = \frac{1 + \frac{\gamma - 1}{2} M_{n,1}^{2}}{\gamma M_{n,1}^{2} - \frac{\gamma - 1}{2}}$$
(1.2)

$$\frac{\rho_2}{\rho_1} = \frac{(\gamma + 1)M_{n,1}^2}{2 + (\gamma + 1)M_{n,1}^2} \tag{1.3}$$

$$\frac{p_2}{p_1} = 1 + \frac{2}{\gamma + 1} (M_{n,1}^2 - 1) \tag{1.4}$$

$$\frac{T_2}{T_1} = \frac{p_2}{p_1} \frac{\rho_1}{\rho_2} \tag{1.5}$$

$$M_2 = \frac{M_{n,2}}{\sin(\beta - \theta)} \tag{1.6}$$

$$\tan \theta = 2 \cot \beta \frac{M_1^2 \sin^2 \beta - 1}{M_1^2 (\gamma + \cos(2\beta)) + 2}$$
 (1.7)

We are also interested in the total properties (represented with subscript 0) and in the sonic speed a. In any point of the flow, they can be calculated from the static properties using Eqs. (1.8) to (1.11) (ANDERSON JR., 2017).

$$\frac{T_0}{T} = 1 + \frac{\gamma - 1}{2}M^2 \tag{1.8}$$

$$\frac{p_0}{p} = \left(1 + \frac{\gamma - 1}{2}M^2\right)^{\frac{\gamma}{\gamma - 1}} \tag{1.9}$$

$$\frac{\rho_0}{\rho} = \left(1 + \frac{\gamma - 1}{2}M^2\right)^{\frac{1}{\gamma - 1}} \tag{1.10}$$

$$a = \sqrt{\gamma RT} \tag{1.11}$$

Using these equations, we can calculate the values of the flow properties at each control volume for given freestream properties and shockwave angles. Then, the efficiency function for an 3-shockwave diffuser is simply $P_{0_3}/P_{0_\infty}=f(M_\infty,\beta_2,\beta_2)$. This function can be calculated easily by repeated application of the shockwave equations, and a descent algorithm can be used to fing the local maximum.

1.3 Optimization

Finding the optimal diffuser is equivalent to finding the global maximum of the efficiency function $\eta(\beta_1, \beta_2)$. A script, shown in full in Appendix A, was used to find the optimal diffuser angles, and some important parts of the code will be discussed here.

The script uses a class, called Flow, to represent flow state. This class implements total/static properties conversions, and also a shockwave method. The shockwave method is shown in listing 1, though the actual implementation is a class method, not a plain function.

```
Listing 1: Shockwave function
def _shockwave(self, beta) -> Flow:
    Calculates flow properties after an oblique shockwave.
    Uses equations (9.13) through (9.18) @anderson2017.
    Parameters:
    beta: oblique angle of the shockwave [rad]
    Returns:
    The Flow object after the shockwave
    # Checks shockwave is valid (supersonic and positive theta)
    # Maybe subsonic flow could be accepted, and spit a supersonic flow?
    if (self.mach < 1) or ((theta := self.velocity_deflection(beta)) <= 0):</pre>
        return Flow(np.nan, np.nan, np.nan, np.nan, self.fluid)
    gamma = self.fluid.gamma
    # Equation (9.13) @anderson2017
    M_n_1 = self.mach * np.sin(beta)
    M_n_1 = M_n_1 * M_n_1
    # Equation (9.14) @anderson2017 (modified)
    M_n_2 = np.sqrt((2 + (gamma - 1) * M_n_1_sq) / (2 * gamma * M_n_1_sq - (gamma - 1)))
    # Equation (9.15) @anderson2017
    rho_2 = self.density * (gamma + 1) * M_n_1_sq / (2 + (gamma - 1) * M_n_1_sq)
    # Equation (9.16) @anderson2017
   p_2 = self.pressure * (1 + 2 * gamma * (M_n_1_sq - 1) / (gamma + 1))
    # Equation (9.17) @anderson2017
    T_2 = self.temperature * p_2 * self.density / (self.pressure * rho_2)
    # Equation (9.18) @anderson2017
    M_2 = M_n_2 / np.sin(beta - theta)
    flow_2 = Flow(p_2, M_2, T_2, rho_2, self.fluid)
    return flow_2
```

Using the Flow class, we can create a function that calculates the total pressure efficiency $\eta(M_{\infty}, \beta_1, \beta_2)$. In fact, the function is easily generalized to n-shockwave diffusers, so the general version was implemented. The implementation used in the script is shown in listing 2.

Listing 2: Total Pressure efficiency in an n-shockwave diffuser def nShock_p0_eff(betas: tuple[float, ...], flow_in: Flow) -> float: """ Calculates the total pressure efficiency in a diffuser with n-1 oblique and 1 normal shockwaves. Parameters: betas: angles of the n-1 oblique shockwaves [rad] flow_in: Flow object of the flown in the upstream Returns: Total pressure efficiency of the diffuser """ flow_after = flow_in for beta in betas: flow_after = flow_after.shockwave(beta) flow_after = flow_after.shockwave(np.pi / 2) return flow_after.total_pressure / flow_in.total_pressure

Finally, the script uses the SciPy module to implement the optimization algorithm. The algorithm implements minimization on a scalar function of n-dimensional inputs, i.e. it finds a local minimum. Since we want the local maximum, the optimized function was the total pressure loss $1-\eta$, instead of the efficiency η . The optimization method chosen takes a initial guess, which was chosen to be just above the minimum β angles to ensure existence. The implementation is shown in listing 3.

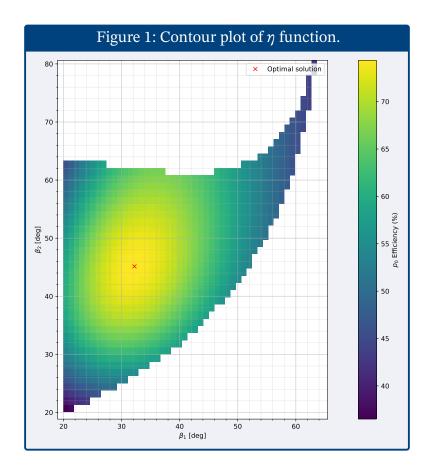
Listing 3: Optimization algorithm # Finds minimum beta values, aka beta when theta = 0 min_beta_1 = root_scalar(flow_inf.velocity_deflection, x0=0.1, x1=0.11).root assert 0 < min_beta_1 < np.pi / 2</pre> # Initial guess based on minimum beta angle (scaled to avoid evaluating on the boundary) initial_betas = (min_beta_1 * 1.01, min_beta_1 * 1.01) print("Solving...") # Minimizes the total pressure efficiency loss using a descent algorithm sol_weak = minimize(lambda betas: 1 - nShock_p0_eff(betas, flow_inf), initial_betas, method="SLSQP", options={"disp": True},) print("Done!") print(f"Solution: {sol_weak.x}") Solving... Optimization terminated successfully (Exit mode 0) Current function value: 0.2563475732605983 Iterations: 7 Function evaluations: 24 Gradient evaluations: 7 Done! Solution: [0.5622804 0.78800818]

To investigate wether our optimization was correct and if the maximum is global, we can plot coarse contour graph of η , shown in Fig. 1. As can be seen, the maximum does appear to be correct and global.

We can then use our solution to extract the values we want, i.e. the optimal diffuser angles and the optimal flow properties in each control volume. This is implemented in listing 4, along with some assertions, using the Flow class methods.

Listing 4: Extracting the optimal diffuser angles and flow properties

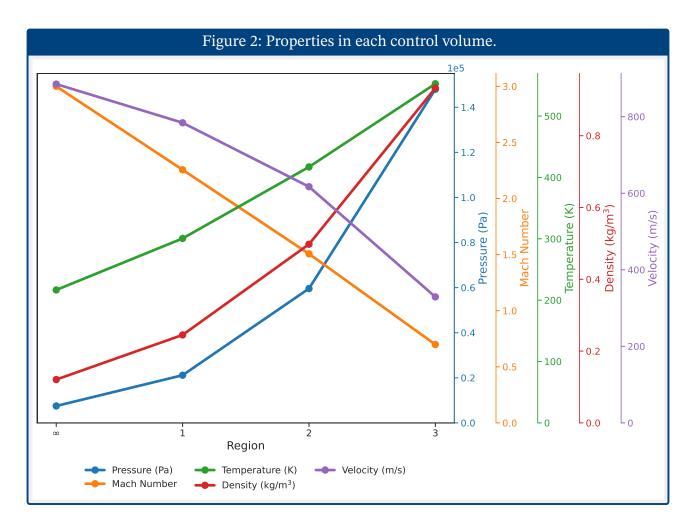
```
# Gets and prints all the solution values
betas = sol_weak.x
assert np.all(0 < betas) and np.all(betas < np.pi / 2)</pre>
p0_eff = 1 - sol_weak.fun
assert 0 < p0_eff < 1</pre>
print(f"Efficiency = {p0_eff:.4}")
print()
# Stores flow states into a list
flows = [flow_inf]
for n, beta in enumerate(betas):
    print(f"beta_{n+1}: {np.rad2deg(beta)}")
    print(f"theta_{n+1}: {np.rad2deg(flows[-1].velocity_deflection(beta))}")
    flows.append(flows[-1].shockwave(beta))
    print(f"Flow_{n+1}:", flows[-1], "\n")
flows.append(flows[-1].shockwave(np.pi / 2))
print(f"Flow_out: {flows[-1]}")
# Garbage Collection
gc.collect()
Efficiency = 0.7437
beta_1: 32.21629364825329
theta_1: 14.976701128986543
Flow_1: Flow(
        Pressure: 2.115e+04
        Mach: 2.256
        Temperature: 300.6
        Density: 0.2451
        fluid: Fluid(R=287.058, gamma=1.4)
)
beta_2: 45.14954292171187
theta_2: 18.814742838551123
Flow_2: Flow(
        Pressure: 5.959e+04
        Mach: 1.507
        Temperature: 417.1
        Density: 0.4977
        fluid: Fluid(R=287.058, gamma=1.4)
)
Flow_out: Flow(
        Pressure: 1.48e+05
        Mach: 0.6986
        Temperature: 552.7
        Density: 0.9328
        fluid: Fluid(R=287.058, gamma=1.4)
)
```



Then, we can plot the properties over each region. To better visualize relative changes in magnitude, we compared Pressure, Mach number, Temperature, Density, and Velocity in the Fig. 2. For easier lookup, the properties were also tabulated in Table 2.

Table 2 – Flow Properties in the 3-shockwave diffuser

Region	Pressure [Pa]	Mach Number	Temperature [K]	Density [kg/m ³]	Velocity [m/s]
∞	7505	3.000	216.7	0.1207	885.2
$\overbrace{1}$	21 150	2.256	300.6	0.2451	784.2
2	59 590	1.507	417.1	0.4977	617.1
3	148 000	0.6986	552.7	0.9328	329.2



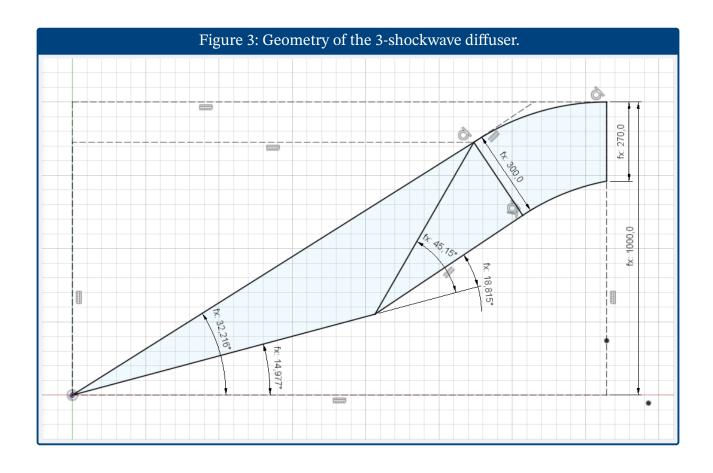
1.4 Optimal Geometry

With the optimal angles, the geometry is still under-determined. The external wall size, D can be scaled arbitrarily, and will be set as unitary for a geometry generalization. Scaling this value will scale the geometry uniformly. For the walls to normal shockwave to form adequately, both the inner and outer wall must be (nearly) tangent to the flow in the normal shockwave vicinity. Additionally, a constraint is put in place such that the outer wall ends in a horizontal direction, finishing the rotation of the flow.

The wedge walls can still be scaled (up to a limit) inside these constraints, changing the geometry of entry to the diffuser. To constrain this geometry, the cross-sectional length of the normal shockwave was set to $D_e = 0.3D$.

Lastly, the internal length $D_{\rm int}$ is also arbitrary. Oswatitsch (1944) and Hermann (1956) show some restrictions to the throat formed here, but not a conclusive answer to its value. The critical value (where the normal shockwave happens right at the entrance) depends on the geometry further down the flow. Thus, as an initial approximation, the $D_{\rm int}$ was set such that the diffuser exit length is equal to $D_o = 0.9D_e$.

The final geometry, then, was modeled on the CAD Software Fusion 360, and shown in Fig. 3.



2 Part 2

The flow inside the ramjet motor can be divided into 3 parts: Expansion, Heat Addition, and Nozzle.

2.1 Expansion

Quasi-one-dimensional, isentropic expansion follows the Area-Mach Number relationship (Eq. (2.1)). Even though a sonic throat is not present, the relationship still stands, and the Mach Number anywhere in the flow can be calculated from the area ratio with a point with known properties. In our case, the point with known properties will be the entrance right after the normal shockwave from Chapter 1. The area in the entrance is D_e , and the area after expansion is D.

$$\left(\frac{A}{A^*}\right)^2 = \frac{1}{M^2} \left[\frac{2}{\gamma + 1} \left(1 + \frac{\gamma - 1}{2} M^2 \right) \right]^{\frac{\gamma + 1}{\gamma - 1}} \tag{2.1}$$

To calculate the Mach Number, we can find A^* and numerically solve Eq. (2.1) for A = D. Thus, the implementation in the script can be reduced to the Area–Mach Number relationship implemented in listing 5 and the root search implemented in listing 6. Details of the implementation can be found in Appendix A.

```
Listing 5: Area-Mach Number relationship function

def area_mach(M: float, gamma: float) -> float:
    """
    Calculates the ratio A / A* in isentropic quasi-one-dimensional flow.
    Uses Equation (10.32) @anderson2017.

Parameters:
    M: Mach number
    gamma: Specific heat ratio
    """
    g_ratio = (gamma + 1) / (gamma - 1)
    # Equation (10.32) @anderson2017 (modified)
    return (2 / (gamma + 1) + M * M / g_ratio) ** (g_ratio / 2) / M
```

Listing 6: Finding Mach number after expansion # Calculates Mach number using the area-Mach relation # Calculates virtual throat D_virtual = D_entrance / area_mach(flows2[-1].mach, flows2[-1].fluid.gamma) # Solves area-Mach relation for the new Mach number expanded_mach = root_scalar(lambda M: area_mach(M, flows2[-1].fluid.gamma) - D / D_virtual, bracket=[1, 1e-2],method="brentq",).root # Appends new Flow to the list flows2.append(Flow.from_total_values(p0, expanded_mach, T0, rho0, flows2[-1].fluid)) print("Flow after expansion:", flows2[-1]) Flow after expansion: Flow(Pressure: 2.013e+05 Mach: 0.161 Temperature: 603.5 Density: 1.162 fluid: Fluid(R=287.058, gamma=1.4))

2.2 Heat Addition

The temperature variation ΔT will be considered as a change in static temperature. Equation (2.2) gives the relationship between Mach Number and static temperature (ANDERSON, 2021). Since we know the temperature before and after heat addition, the new Mach Number can be found by solving this equation.

When the new Mach Number is known, the new pressure and density can be calculated using Eqs. (2.3) and (2.4) (ANDERSON, 2021). Thus, the flow after heat addition is completely defined.

$$\frac{T_2}{T_1} = \left(\frac{1 + \gamma M_1^2}{\gamma M_2^2}\right)^2 \left(\frac{M_2^2}{M_1^2}\right) \tag{2.2}$$

$$\frac{p_2}{p_1} = \frac{1 + \gamma M_1^2}{1 + \gamma M_2^2} \tag{2.3}$$

$$\frac{\rho_2}{\rho_1} = \frac{p_2}{p_1} \frac{T_1}{T_2} \tag{2.4}$$

Using Eq. (2.2) the script can find the new Mach number as shown in listing 7, while the pressure and density were calculated as shown in listing 8, yielding a complete Flow object.

Listing 7: Finding Mach number after heat addition

```
# Calculates temperature after heat addition
expanded_temp = flows2[-1].temperature
heated_temp = expanded_temp + delta_temp
# Calculates Mach number after heat addition
# Part of Equation (3.81) @anderson2021 that doesn't depend on the new Mach number
const_part = (
   np.sqrt(heated_temp / expanded_temp)
    * expanded_mach
    / (1 + flows2[-1].fluid.gamma * expanded_mach * expanded_mach)
)
# Solves Equation (3.81) @anderson2021 (modified) for the new Mach number
heated_mach = root_scalar(
    lambda M: const_part - M / (1 + flows2[-1].fluid.gamma * M * M),
    bracket=[1, 0],
    method="brentq",
).root
print(f"New Mach number: {heated_mach:.4}")
New Mach number: 0.3358
```

Listing 8: Finding flow properties after heat addition # Calculates remaining Flow properties after heat addition # Equation (3.78) @anderson2021 heated_pressure = (flows2[-1].pressure * (1 + flows2[-1].fluid.gamma * expanded_mach * expanded_mach) / (1 + flows2[-1].fluid.gamma * heated_mach * heated_mach) # Equation (3.79) @anderson2021 heated_rho = (flows2[-1].density* heated_pressure / flows2[-1].pressure * expanded_temp / heated_temp) # Appends new Flow to the list flows.append(Flow(heated_pressure, heated_mach, heated_temp, heated_rho, flows2[-1].fluid) print("Flow after heat addition:", flows[-1]) Flow after heat addition: Flow(Pressure: 1.802e+05 Mach: 0.3358 Temperature: 2.103e+03 Density: 0.2984 fluid: Fluid(R=287.058, gamma=1.4))

2.3 Nozzle

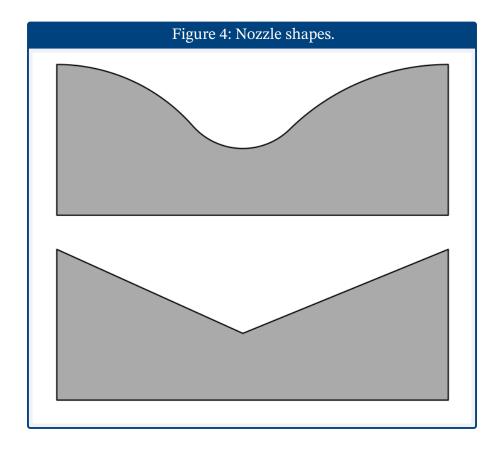
Just as in Section 2.1, the nozzle is a quasi-one-dimensional flow. The nozzle is defined by the area ratio, and the Mach Number. Using Eq. (2.1), one can find the critical throat area, implemented in the script as shown in listing 9.

```
Listing 9: Finding the throat area

# Calculates throat semi-area
D_throat = D / area_mach(heated_mach, flows[-1].fluid.gamma)
print(f"Throat area: {D_throat}")

Throat area: 0.542665144954579
```

With the nozzle throat area D_t known, the geometry of the nozzle is fully determined. The two nozzle shapes under study are shown in Fig. 4.

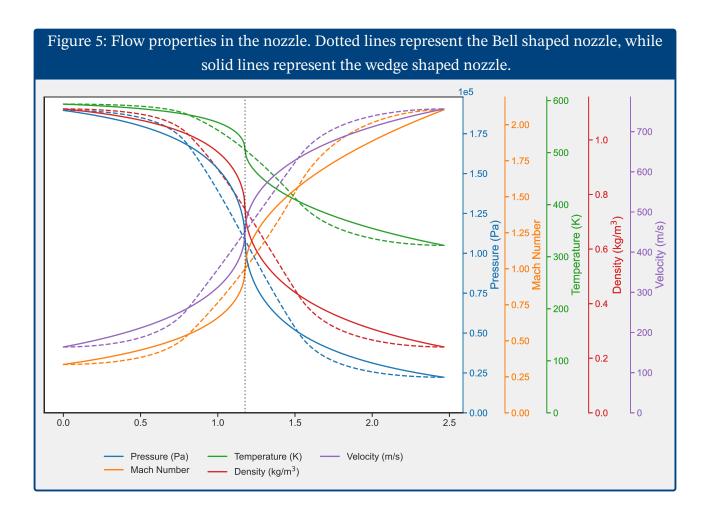


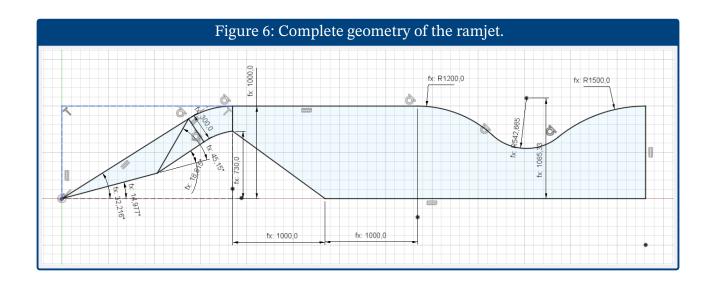
The walls for each shape were implemented as functions, and flow properties were calculated using Eq. (2.1) and Eqs. (1.8) and (1.11). The code implementing this calculation is shown in listing 10.

Listing 10: Calculating flow properties in the nozzle nozzles_flows = np.empty([len(nozzle_curves), len(x)], Flow) p0_nozzle, T0_nozzle, rho0_nozzle = flows2[-1].total_values() for n, curve in enumerate(nozzle_curves): # Calculates the Mach number across the nozzle. crit_index = np.argmin(curve[1]) D_crit = curve[1, crit_index] crit_x = curve[0, crit_index] machs = np.array(Ε root_scalar(lambda M: area_mach(M, flows2[-1].fluid.gamma) - y_ / D_crit, # The sign function selects solution branch according to starting flow # and position relative to critical length $bracket=[1, 100 ** np.sign((1 - flows2[-1].mach) * (x_ - crit_x))],$ method="brentq",).root for x_, y_ in curve.T]) nozzles_flows[n, :] = np.array(Flow.from_total_values(p0_nozzle, mach, T0_nozzle, rho0_nozzle, flows2[-1].fluid) for mach in machs])

Some flow properties were calculated and plotted in Fig. 5, where one can compare their relative changes as well as the differences between the two nozzle shapes.

Finally, the full ramjet design sketch can be seen in Fig. 6. Some dimensions remained unconstrained (namely the length of the expansion region and of the combustion chamber), and were set to *D*.





APPENDIX A - Source Code

```
# %% [markdown]
    # # SETUP
3
    # %% [markdown]
5
    # ## Imports
6
   # %%
8
   from __future__ import annotations
9
    from scipy.optimize import minimize, root_scalar
10
11
    import numpy as np
    import matplotlib.pyplot as plt
12
    from functools import lru_cache
13
    import gc
14
15
16
    # %% [markdown]
17
    # ## Classes
18
19
   # %%
20
21
    class Fluid:
        0.00
22
        Stores the constant properties R and gamma of a fluid
23
24
25
        def __init__(self, R: float, gamma: float) -> None:
26
            self.R = R
27
            self.gamma = gamma
28
29
        def __str__(self) -> str:
30
            return f"Fluid(R={self.R}, gamma={self.gamma})"
31
32
33
    # %% [markdown]
34
    # Flow class uses a few equations from @anderson2017, repeated here as they appear in the
35
       book:
36
    # %% [markdown]
37
38
   # From chapter 8:
39
40
   # $$\tag{8.25}
41
        a = \sqrt{\gamma R T}
42
   # $$
43
```

```
#
44
45
               # $$\tag{8.40}
                             \frac{T_0}{T} = 1 + \frac{\log - 1}{2}M^2
46
               # $$
47
48
               # $$\tag{8.42}
49
                               50
               # $$
51
               # $$\tag{8.43}
53
                \# \frac{1}{2}M^2 \right) ^{1}{\frac{1}{\gamma_0}} = \left(1 + \frac{1}{\gamma_0}\right) ^{1}{\frac{1}{\gamma_0}} 
54
                 → 1}}
               # $$
55
56
57
58
               # %% [markdown]
               # From chapter 9
59
               # $$\tag{9.13}
60
               # M_{n,1} = M_1 \cdot \sum_{i=1}^{n} beta
61
               # $$
62
63
               # $$\tag{9.14}
64
                                {M_{n,2}}^2 = \frac{frac}{}
65
                                         1 + \frac{(n,1)}^2
66
                                }{
                #
67
                                         \mbox{gamma } \{M_{n,1}\}^2 - \frac{\mbox{gamma - 1}}{2}
68
                                }
69
               # $$
70
               #
71
72
                # $$\tag{9.15}
                         \frac{\rho_1}{2}{\rho_1} = \frac{(\gamma_1)^2}{2} {2 + (\gamma_1)^2}^2 
73
               # $$
74
75
               # $$\tag{9.16}
76
                                \frac{p_2}{p_1} = 1 + \frac{2}{\gamma + 1} ( \{M_{n,1}\}^2 - 1 )
77
               # $$
78
79
               # $$\tag{9.17}
80
                               \frac{T_2}{T_1} = \frac{p_2}{p_1} \frac{\pi_0}{\pi_0}
81
               # $$
82
83
               # $$\tag{9.18}
84
85
               # M_2 = \frac{M_{n,2}}{\sin(\beta - \beta)}
               # $$
86
87
               # $$\tag{9.23}
88
                               \tan\theta = 2 \cot \beta {M_1}^2 \sin^2\theta - 1 {M_1}^2 (\gamma + \beta - 1)^2 (\gamma 
                 \hookrightarrow \cos(2\beta)) + 2 }
```

```
# $$
90
91
    # %%
92
    class Flow:
93
         0.00
94
         Stores the defining properties of a flow:
95
96
         Pressure (p)
97
         Mach Number (M)
98
         Temperature (T)
99
         Density (rho)
100
         Fluid (fluid)
101
         Speed of sound (a)
102
103
         Velocity (V)
104
105
         Care should be taken to use consistent units.
106
107
         def __init__(self, p: float, M: float, T: float, rho: float, fluid: Fluid) -> None:
108
109
             Constructs a Flow object from the defining properties and calculates some
110
             auxiliary properties.
111
             Uses Equations (8.25), (8.40), (8.42), (8.43) @anderson2017.
112
113
             Parameters:
114
             p: pressure [Pa]
115
             M: Mach number
116
             T: temperature [K]
117
             rho: density [kg/m<sup>3</sup>]
118
             fluid: Fluid object
119
             0.00
120
121
             self.pressure = p
122
             self.mach = M
123
             self.temperature = T
124
             self.density = rho
125
             self.fluid = fluid
126
127
             # Equation (8.25) @anderson2017
128
             self.snd_spd = np.sqrt(fluid.gamma * fluid.R * self.temperature)
129
             # From the definition of Mach Number
130
             self.vel = M * self.snd_spd
131
132
133
             aux_const = 1 + (fluid.gamma - 1) * M * M / 2
             # Equation (8.40) @anderson2017
134
             self.total_temperature = T * aux_const
135
             # Equation (8.42) @anderson2017
136
             self.total_pressure = p * aux_const ** (fluid.gamma / (fluid.gamma - 1))
137
             # Equation (8.43) @anderson2017
138
```

```
self.total_density = rho * aux_const ** (1 / (fluid.gamma - 1))
139
140
             self.shockwave = lru_cache(maxsize=8)(self._shockwave)
141
142
         @classmethod
143
         def from_total_values(
144
             cls, p0: float, M: float, T0: float, rho0: float, fluid: Fluid
145
         ):
146
             f = 1 / Flow(1 / p0, M, 1 / T0, 1 / rho0, fluid).total_values()
147
             return Flow(f[0], M, f[1], f[2], fluid)
148
149
         def _p_ratio(M, gamma):
150
151
             Calculates the pressure ratio of a shockwave.
152
             Uses equation (9.19) @anderson2017.
153
154
155
             Parameters:
             M: Mach number
156
157
             gamma: ratio of specific heats
158
159
             Returns:
             Pressure ratio
160
             0.00
161
162
             return (1 + (gamma - 1) * M * M / 2) ** (gamma / (gamma - 1))
163
164
         def __str__(self) -> str:
165
             return (
166
                  "\n\t".join(
167
                      168
                          "Flow(",
169
                          f"Pressure: {self.pressure:.4}",
170
                          f"Mach: {self.mach:.4}",
171
                          f"Temperature: {self.temperature:.4}",
172
                          f"Density: {self.density:.4}",
173
                          f"fluid: {self.fluid}",
174
                      ]
175
                 )
176
                 + "\n)"
177
             )
178
179
         def static_values(self) -> np.ndarray:
180
181
182
             Outputs the defining properties of a flow as an ndarray.
             Uses same order as __init__, but excludes the fluid property.
183
             [p, M, T, rho]
184
             0.00
185
             return np.array([self.pressure, self.mach, self.temperature, self.density])
186
187
```

```
def total_values(self) -> np.ndarray:
188
189
             Outputs the stagnation properties of a flow as an ndarray.
190
             [p0, T0, rho0]
191
             0.00
192
             return np.array(
193
                 [self.total_pressure, self.total_temperature, self.total_density]
194
             )
195
196
         def aux_values(self) -> np.ndarray:
197
198
             Outputs the auxiliary properties of a flow as an ndarray.
199
200
             [a, V]
             0.00
201
             return np.array([self.snd_spd, self.vel])
202
203
204
         def _shockwave(self, beta) -> Flow:
             0.00
205
206
             Calculates flow properties after an oblique shockwave.
             Uses equations (9.13) through (9.18) @anderson2017.
207
208
             Parameters:
209
             beta: oblique angle of the shockwave [rad]
210
211
             Returns:
212
             The Flow object after the shockwave
213
214
215
             # Checks shockwave is valid (supersonic and positive theta)
216
217
             # Maybe subsonic flow could be accepted, and spit a supersonic flow?
             if (self.mach < 1) or ((theta := self.velocity_deflection(beta)) <= 0):</pre>
218
                 return Flow(np.nan, np.nan, np.nan, np.nan, self.fluid)
219
220
             gamma = self.fluid.gamma
221
222
             # Equation (9.13) @anderson2017
223
             M_n_1 = self.mach * np.sin(beta)
224
             M_n_1 = M_n_1 * M_n_1
225
             # Equation (9.14) @anderson2017 (modified)
226
             M_n_2 = np.sqrt(
227
                 (2 + (gamma - 1) * M_n_1_sq) / (2 * gamma * M_n_1_sq - (gamma - 1))
228
229
             # Equation (9.15) @anderson2017
230
231
             rho_2 = self.density * (gamma + 1) * M_n_1_sq / (2 + (gamma - 1) * M_n_1_sq)
             # Equation (9.16) @anderson2017
232
             p_2 = self.pressure * (1 + 2 * gamma * (M_n_1_sq - 1) / (gamma + 1))
233
             # Equation (9.17) @anderson2017
234
             T_2 = self.temperature * p_2 * self.density / (self.pressure * rho_2)
235
             # Equation (9.18) @anderson2017
236
```

```
M_2 = M_n_2 / np.sin(beta - theta)
237
238
                                              flow_2 = Flow(p_2, M_2, T_2, rho_2, self.fluid)
239
                                              return flow_2
240
241
                                def velocity_deflection(self, beta: float) -> float:
242
243
                                              Calculates the velocity deflection angle theta for an oblique shockwave
244
                                              Uses equations (9.13), (9.23) @anderson2017
245
246
                                              Parameters:
247
                                              beta: oblique angle of the shockwave [rad]
248
249
                                              Returns:
250
                                              angle of deflection of velocity [rad]
251
252
253
                                              M = self.mach
254
255
                                              gamma = self.fluid.gamma
256
                                               # Equation (9.13) @anderson2017
257
                                              M_n_1 = M * np.sin(beta)
258
259
                                               # Equation (9.23) @anderson2017
260
                                               theta = np.arctan(
261
262
                                                             / np.tan(beta)
263
                                                             * (M_n_1 * M_n_1 - 1)
264
                                                             / (M * M * (gamma + np.cos(2 * beta)) + 2)
265
266
                                              )
                                              return theta
267
268
269
                # %% [markdown]
270
                # ## Functions
271
272
                # %% [markdown]
273
                # Area-Mach number relation @anderson2017:
274
                # $$\tag{10.32}
275
                \hookrightarrow \frac{\gamma - 1}{2} M^2 \right) \right]^{\frac{1}{2} M^2 \right]^{\frac{1}{2}} H^2 \right]^{\frac{1}{2}} H^2 \right]^{\frac{1}{2}} H^2 \left(\frac{1}{2} M^2 \right)^{\frac{1}{2}} H^
                # $$
277
2.78
279
                # %%
                def area_mach(M: float, gamma: float) -> float:
280
281
                               Calculates the ratio A / A* in isentropic quasi-one-dimensional flow.
282
                                Uses Equation (10.32) @anderson2017.
283
284
```

```
Parameters:
285
286
         M: Mach number
         gamma: Specific heat ratio
287
288
         g_ratio = (gamma + 1) / (gamma - 1)
289
         # Equation (10.32) @anderson2017 (modified)
290
         return (2 / (gamma + 1) + M * M / g_ratio) ** (g_ratio / 2) / M
291
292
293
    # %%
294
    def nShock_p0_eff(betas: tuple[float, ...], flow_in: Flow) -> float:
295
296
         Calculates the total pressure efficiency in a diffuser with n-1 oblique and 1 normal
297
298
         shockwaves.
299
300
         Parameters:
         betas: angles of the n-1 oblique shockwaves [rad]
301
         flow_in: Flow object of the flown in the upstream
302
303
         Returns:
304
         Total pressure efficiency of the diffuser
305
         0.00
306
307
         flow_after = flow_in
308
         for beta in betas:
309
             flow_after = flow_after.shockwave(beta)
310
         flow_after = flow_after.shockwave(np.pi / 2)
311
         return flow_after.total_pressure / flow_in.total_pressure
312
313
314
    # %%
315
    def bellNozzleGenerator(R_in, R_throat, R_out, L_throat, L_in=1, L_out=None):
316
317
         Generates a function describing the geometry of a planar nozzle defined by 3 arcs.
318
319
         Parameters:
320
         R_in: Radius of the inlet arc
321
         R_throat: Radius of the throat arc
322
         R_out: Radius of the outlet arc
323
         L_throat: semi-length of the throat
324
325
         L_in: semi-length of the inlet arc
         L_out: semi-length of the outlet arc
326
327
328
         Returns:
         bellCurve: The function describing the geometry of the nozzle
329
         crit_len: The length where minimum area occurs
330
         max_len: The length of the nozzle
331
         if L_out is None:
333
```

```
L_{out} = L_{in}
334
335
         L1 = (
             np.sqrt((R_in + R_throat) ** 2 - (R_in - L_in + R_throat + L_throat) ** 2)
336
             * R_in
337
             / (R_in + R_throat)
338
339
         11 = L1 * R_{throat} / R_{in}
340
         L2 = (
341
             np.sqrt((R_throat + R_out) ** 2 - (R_out - L_out + R_throat + L_throat) ** 2)
342
             * R_out
343
             / (R_throat + R_out)
344
345
         12 = L2 * R_{throat} / R_{out}
346
         max_len = L1 + 11 + 12 + L2
347
         crit_len = L1 + 11
348
349
350
         def bellCurve(x):
             if not isinstance(x, np.ndarray):
351
                 x = np.array(x)
352
             y = np.zeros_like(x)
353
             # First arc
354
             i1 = (0 \le x) & (x \le L1)
355
             y[i1] = L_{in} - R_{in} + np.sqrt(R_{in}**2 - (x[i1] - 0) ** 2)
356
             # Second arc
357
             i2 = (L1 < x) & (x < max_len - L2)
358
             y[i2] = L_{throat} + R_{throat} - np.sqrt(R_{throat**2} - (x[i2] - (L1 + 11)) ** 2)
359
             # Third arc
360
             i3 = (max_len - L2 \le x) & (x \le max_len)
361
             y[i3] = L_out - R_out + np.sqrt(R_out**2 - (x[i3] - max_len) ** 2)
362
             return y
363
364
         return bellCurve, crit_len, max_len
365
366
367
    # %%
368
    def coneNozzleGenerator(crit_len, max_len, L_throat, L_in=1, L_out=None):
369
370
         Generates a function describing the geometry of a planar nozzle defined by 2 slopes.
371
372
         Parameters:
373
         max_len: Length of the nozzle
374
         crit_len: Length where minimum area occurs
375
         L_throat: Semi-length of the throat
376
377
         L_in: Semi-length of the inlet
         L_out: Semi-length of the outlet
378
379
         Returns:
380
         coneCurve: The function describing the geometry of the nozzle
381
         crit_len: The length where minimum area occurs
382
```

```
max_len: The length of the nozzle
383
384
         if L_out is None:
385
             L_{out} = L_{in}
386
387
         def coneCurve(x):
388
             if not isinstance(x, np.ndarray):
389
                  x = np.array(x)
390
             y = np.zeros_like(x)
391
             # First slope
392
             i1 = (0 <= x) & (x <= crit_len)
393
             y[i1] = L_in + x[i1] * (L_throat - L_in) / crit_len
394
             # Second slope
395
             i2 = (crit_len < x) & (x <= max_len)</pre>
396
             y[i2] = L_{throat} + (x[i2] - crit_len) * (L_out - L_throat) / (
397
398
                  max_len - crit_len
399
             return y
400
401
         return coneCurve, crit_len, max_len
402
403
404
    # %%
405
     styles = ["default", "fivethirtyeight", "seaborn-white"]
406
     colors = plt.rcParams["axes.prop_cycle"].by_key()["color"]
407
408
409
    def plot_flow_evolution(flow_data: np.ndarray, pos: np.ndarray, fig_ax=None, cols=None):
410
         # Plots the relevant properties of the flow
411
412
         if fig_ax is None:
             fig = plt.figure(figsize=(10, 10))
413
             ax = plt.axes()
414
         else:
415
416
             fig, ax = fig_ax
417
         if cols is None:
418
             cols = list(range(flow_data.shape[-1]))
419
420
         # Different vertical axes
421
         v_axes = [ax.twinx() for _ in cols]
422
423
         # Line labels
424
         labels = [
425
             "Pressure (Pa)",
426
              "Mach Number",
427
              "Temperature (K)",
428
             "Density (kg/m\$^3\$)",
429
              "Speed of Sound (m/s)",
430
              "Velocity (m/s)",
431
```

```
"Total Pressure (Pa)",
432
             "Total Temperature (K)",
433
             "Total Density (kg/m$^3$)",
434
         1
435
436
         labels = [labels[c] for c in cols]
437
438
         flow_data = flow_data[:, cols]
439
440
         # Generates the actual plot lines
441
         lines = [
442
             v_ax.plot(pos, property, color=color, label=label)[0]
443
             for v_ax, property, label, color in zip(v_axes, flow_data.T, labels, colors)
444
445
446
447
         # Tick appearance
         tick_params = dict(size=6, width=1.5)
448
449
         # Configures the scale axes
450
         for v_ax, label, line, n in zip(v_axes, labels, lines, range(len(lines))):
451
             v_ax.set_ylabel(label)
452
             v_ax.yaxis.label.set_color(line.get_color())
453
             v_ax.spines.right.set_color(line.get_color())
454
             v_ax.tick_params(axis="y", colors=line.get_color(), **tick_params)
455
             v_ax.ticklabel_format(axis="y", scilimits=(-3, 3))
456
             v_ax.yaxis.offsetText.set_position((1.025 + 0.10 * n, 0))
457
             v_ax.spines.right.set_position(("axes", 1 + 0.10 * n))
458
             v_ax.set_ylim(bottom=0)
459
460
461
         # Ticks on main ax
         ax.tick_params(axis="y", which="both", left=False, right=False)
462
         ax.tick_params(axis="x", **tick_params)
463
464
         # fig.legend(loc="upper left", handles=lines, ncol=3)
465
         box = ax.get_position()
466
         ax.set_position([box.x0, box.y0 + box.height * 0.1, box.width, box.height * 0.9])
467
468
         # Put a legend below current axis
469
         ax.legend(
470
             handles=lines,
471
472
             loc="upper center",
             bbox_to_anchor=(0.5, -0.1),
473
             fancybox=True,
474
475
             ncol=3,
476
         ax.set_yticks([])
477
         return fig, [ax, *v_axes]
478
479
```

480

```
# %% [markdown]
481
    # # PART 1
482
483
    # %% [markdown]
484
    # ## Initial data
485
486
    # %%
487
    # Gets data from problem conditions
488
    M_{inf} = 3.0
489
    h = 18e3 \# [m]
490
491
    # Atmospheric conditions @aerotoolbox
492
    p_inf = 7505.00 # [Pa]
493
    T_{inf} = 216.65 \# [K]
494
    rho_inf = 0.12068 \# [kg/m^3]
495
496
497
    # Air constants
    gamma_air = 1.4
498
    R_{air} = 287.058
499
500
501
    # %%
502
    # Creates initial Objects
503
    air = Fluid(R_air, gamma_air)
504
    flow_inf = Flow(p_inf, M_inf, T_inf, rho_inf, air)
505
506
    print(f"Freestream flow: {flow_inf}")
507
508
509
510
    # %% [markdown]
    # ## Minimization
511
512
    # %% [markdown]
513
    # Minimizes over beta angles instead of over theta angles, as `theta(beta)` is a much less

    ⇔ expensive function to calculate than `beta(theta)`

515
    # %%
516
    # Finds minimum beta values, aka beta when theta = 0
517
    min_beta_1 = root_scalar(flow_inf.velocity_deflection, x0=0.1, x1=0.11).root
518
    assert 0 < min_beta_1 < np.pi / 2</pre>
519
520
521
522
    # %%
523
    # Solves the minimization problem
524
    # Initial guess based on minimum beta angle (scaled to avoid evaluating on the boundary)
525
    initial_betas = (min_beta_1 * 1.01, min_beta_1 * 1.01)
526
527
    print("Solving...")
528
```

```
# Minimizes the total pressure efficiency loss using a descent algorithm
529
530
     sol_weak = minimize(
         lambda betas: 1 - nShock_p0_eff(betas, flow_inf),
531
         initial_betas,
532
         method="SLSQP",
533
         options={"disp": True},
534
    )
535
    print("Done!")
536
    print(f"Solution: {sol_weak.x}")
537
538
539
    # %% [markdown]
540
    # ## Results
541
542
543
    # %% [markdown]
544
    # ### Optimal geometry and flow
545
546
    # %%
    # Gets and prints all the solution values
547
    betas = sol_weak.x
548
    assert np.all(0 < betas) and np.all(betas < np.pi / 2)</pre>
549
550
    p0_eff = 1 - sol_weak.fun
551
    assert 0 < p0_eff < 1
552
553
    print(f"Efficiency = {p0_eff:.4}")
554
    print()
555
556
    # Stores flow states into a list
557
    flows = [flow_inf]
558
    for n, beta in enumerate(betas):
559
         print(f"beta_{n+1}: {np.rad2deg(beta)}")
560
         print(f"theta_{n+1}: {np.rad2deg(flows[-1].velocity_deflection(beta))}")
561
         flows.append(flows[-1].shockwave(beta))
562
         print(f"Flow_{n+1}:", flows[-1], "\n")
563
    flows.append(flows[-1].shockwave(np.pi / 2))
564
    print(f"Flow_out: {flows[-1]}")
565
    # Garbage Collection
566
    gc.collect()
567
568
569
    # %%
570
    print(flows[-1].temperature)
571
    print(flows[-1].pressure)
572
573
    # %% [markdown]
574
    # ### Plot minimization locus
575
576
    # %%
577
```

```
# Calculates the efficiency over a grid of beta_1 and beta_2
578
    b1v = np.linspace(min_beta_1, np.deg2rad(65), 50)
579
    b2v = np.linspace(min_beta_1, np.deg2rad(80), 50)
580
    d = np.empty((len(b2v), len(b1v)))
581
    for j, b1 in enumerate(b1v):
582
         for i, b2 in enumerate(b2v):
583
             d[i, j] = nShock_p0_eff((b1, b2), flow_inf)
584
    assert np.nanmax(d) < p0_eff</pre>
585
    assert np.nanmin(d) > 0
586
     # Garbage collection for all the dereferenced values
587
    gc.collect()
588
589
590
591
    # %%
    # Plots the efficiency distribution
592
    plt.figure(figsize=(10, 10))
593
594
    plt.pcolormesh(
         np.rad2deg(b1v),
595
         np.rad2deg(b2v),
596
         100 * d,
597
         cmap="viridis",
598
599
     cb = plt.colorbar(label="$p_0$ Efficiency (%)")
600
601
     # Plots optimal solution in red X
602
    plt.plot(*np.rad2deg(betas[:2]), "rx", label="Optimal solution")
603
604
    # plt.title(r"Total Pressure Efficiency as a function of $\beta_1$ and $\beta_2$")
605
    plt.xlabel(r"$\beta_1$ [deg]")
606
    plt.ylabel(r"$\beta_2$ [deg]")
607
    plt.legend()
608
609
    # Grid and ticks
610
    plt.axis("scaled")
611
    plt.minorticks_on()
612
    plt.grid(visible=True, axis="both", which="major", linewidth=1, alpha=0.6)
613
    plt.grid(visible=True, axis="both", which="minor", linewidth=0.5, alpha=0.3)
614
615
    # Color bar
616
    plt.savefig("gradient.pdf", bbox_inches="tight")
617
    plt.show()
618
619
620
621
     # %% [markdown]
    # ### Plot optimal flow properties
622
623
    # %%
624
    # Prepares the data as a matrix
625
    data = np.stack(
626
```

```
[(*f.static_values(), *f.aux_values(), *f.total_values()) for f in flows]
627
628
    )
    # Saves data to CSV file
629
    np.savetxt("data.csv", data, fmt="%8.5g", delimiter=",")
630
631
    # %%
633
    # Plots the flow variation over the diffuser
634
    xt = np.arange(len(data))
635
    with plt.style.context(styles), plt.rc_context(
636
         rc={"lines.marker": "o", "lines.markersize": 10}
637
    ):
638
         fig, axes = plot_flow_evolution(data, xt, cols=[0, 1, 2, 3, 5])
639
         # Sets the lower axis
640
         axes[0].set_xlabel("Region")
641
642
         axes[0].set_xticks(xt)
         axes[0].set_xticklabels([r"$\infty$", *np.arange(1, len(data))])
643
    plt.savefig("diffuser_properties.pdf", bbox_inches="tight")
644
    plt.show()
645
646
647
    # %% [markdown]
648
    # # PART 2
649
650
    # %% [markdown]
651
    # ## Initial data
652
653
    # %%
654
    # Sets problem parameters
655
    # The cross-sectional area after the normal shockwave can be arbitrarily small. For this
    # geometry, it can also be as large as about 0.3 * D.
657
658
    # D was chosen to be unitary;
659
    D = 1
660
    D_{inlet} = 1 * D
661
    D_{outlet} = 1 * D
662
    # The cross sectional area was arbitrarily chosen to be 0.25 * D
    D_{entrance} = 0.3 * D
664
    # Temperature change
665
    delta_temp = 1500
666
    # Total Values from Part 1
667
    p0, T0, rho0 = flows[-1].total_values()
668
    # Creates new Flow list for Part 2
669
    flows2 = [flows[-1]]
670
    print("Flow after diffuser:", flows2[-1])
671
672
673
    # %% [markdown]
674
    # ## Expansion
675
```

```
676
677
    # %%
    # Calculates Mach number using the area-Mach relation
678
    # Calculates virtual throat
679
    D_virtual = D_entrance / area_mach(flows2[-1].mach, flows2[-1].fluid.gamma)
680
    # Solves area-Mach relation for the new Mach number
681
    expanded_mach = root_scalar(
682
         lambda M: area_mach(M, flows2[-1].fluid.gamma) - D / D_virtual,
683
         bracket=[1, 1e-2],
684
         method="brentq",
685
    ).root
686
687
688
    # Appends new Flow to the list
    flows2.append(Flow.from_total_values(p0, expanded_mach, T0, rho0, flows2[-1].fluid))
689
    print("Flow after expansion:", flows2[-1])
690
691
692
    # %%
693
    print(D_virtual / D)
694
695
    # %% [markdown]
696
    # ## Heat addition
697
698
    # %% [markdown]
699
    # To calculate the properties after heat addition, equations (3.78), (3.79), (3.81) from
700
     ← @anderson2021. These equations are written down here as needed before they are
        implemented.
701
    # %% [markdown]
702
703
    # $$\tag{3.81}
    \# \frac{T_2}{T_1} = \left( \frac{1 + \gamma_1^2}{\gamma_1^2} \right)^2 \right)
704
                          \left( \frac{M_2}^2}{M_1}^2 \right) \right)
705
    # $$
706
707
    # %%
708
    # Calculates temperature after heat addition
709
    expanded_temp = flows2[-1].temperature
710
    heated_temp = expanded_temp + delta_temp
711
712
    # Calculates Mach number after heat addition
713
714
    # Part of Equation (3.81) @anderson2021 that doesn't depend on the new Mach number
715
    const_part = (
         np.sqrt(heated_temp / expanded_temp)
716
717
         * expanded_mach
         / (1 + flows2[-1].fluid.gamma * expanded_mach * expanded_mach)
718
719
    # Solves Equation (3.81) @anderson2021 (modified) for the new Mach number
720
    heated_mach = root_scalar(
721
         lambda M: const_part - M / (1 + flows2[-1].fluid.gamma * M * M),
722
```

```
bracket=[1, 0],
723
         method="brentq",
724
725
    ).root
    print(f"New Mach number: {heated_mach:.4}")
726
727
728
    # %% [markdown]
729
    # $$\tag{3.78}
730
    \# \frac{p_2}{p_1} = \frac{1 + \gamma_1^2}{1 + \gamma_2}{1 + \gamma_2}^2
731
732
733
    # $$\tag{3.79}
734
    \# \frac{rho_2}{rho_1} = \frac{p_2}{p_1} \frac{T_1}{T_2}
735
736
737
738
    # %%
    # Calculates remaining Flow properties after heat addition
739
    # Equation (3.78) @anderson2021
740
    heated_pressure = (
741
         flows2[-1].pressure
742
         * (1 + flows2[-1].fluid.gamma * expanded_mach * expanded_mach)
743
         / (1 + flows2[-1].fluid.gamma * heated_mach * heated_mach)
744
    )
745
    # Equation (3.79) @anderson2021
746
    heated_rho = (
747
         flows2[-1].density
748
         * heated_pressure
749
         / flows2[-1].pressure
750
         * expanded_temp
751
752
         / heated_temp
753
    )
754
    # Appends new Flow to the list
755
    flows.append(
756
         Flow(heated_pressure, heated_mach, heated_temp, heated_rho, flows2[-1].fluid)
757
758
    print("Flow after heat addition:", flows[-1])
759
760
761
    # %% [markdown]
762
    # ## Nozzle
763
764
    # %% [markdown]
765
    # ### Geometry
766
767
    # %%
768
    # Calculates throat semi-area
769
    D_throat = D / area_mach(heated_mach, flows[-1].fluid.gamma)
770
    print(f"Throat area: {D_throat}")
771
```

```
772
773
774
    # %%
    # Creates the 2 nozzle geometries
775
    bellFunc, crit_len, max_len = bellNozzleGenerator(
776
         1.2 * D_inlet, D_throat, 1.5 * D_outlet, D_throat, D_inlet, D_outlet
777
778
    coneFunc, _, _ = coneNozzleGenerator(crit_len, max_len, D_throat, D_inlet, D_outlet)
779
780
    x = np.hstack(
781
         Г
782
             np.linspace(0, crit_len, 200, endpoint=False),
783
             np.linspace(crit_len, max_len, 200),
784
         ],
785
    )
786
787
    bell = np.array([x, bellFunc(x)])
     cone = np.array([x, coneFunc(x)])
788
    nozzle_curves = [bell, cone]
789
790
791
    # %%
792
    for x, y in nozzle_curves:
793
         plt.figure(figsize=(10, 10))
794
         plt.fill_between(x, y, 0, facecolor="#aaa", edgecolor="black", linewidth=2)
795
         plt.axis("scaled")
796
         plt.axis("off")
797
         plt.tight_layout()
798
    plt.show()
799
800
801
    # %% [markdown]
802
    # ### Flow properties
803
804
    # %%
805
    nozzles_flows = np.empty([len(nozzle_curves), len(x)], Flow)
806
    p0_nozzle, T0_nozzle, rho0_nozzle = flows2[-1].total_values()
807
    for n, curve in enumerate(nozzle_curves):
808
         # Calculates the Mach number across the nozzle.
809
         crit_index = np.argmin(curve[1])
810
         D_crit = curve[1, crit_index]
811
812
         crit_x = curve[0, crit_index]
         machs = np.array(
813
             Γ
814
815
                 root_scalar(
                     lambda M: area_mach(M, flows2[-1].fluid.gamma) - y_ / D_crit,
816
                     # The sign function selects solution branch according to starting flow
817
                     # and position relative to critical length
818
                     bracket=[1, 100 ** np.sign((1 - flows2[-1].mach) * (x_ - crit_x))],
819
                     method="brentq",
820
```

```
).root
821
822
                 for x_, y_ in curve.T
             1
823
         )
824
         nozzles_flows[n, :] = np.array(
825
             Ε
826
                 Flow.from_total_values(
827
                     p0_nozzle, mach, T0_nozzle, rho0_nozzle, flows2[-1].fluid
828
                 )
829
                 for mach in machs
830
             ]
831
         )
832
833
834
    # %% [markdown]
835
836
     # ### Contour plots
837
    # %%
838
    def plot_nozzle_prop(prop_name, flow_list, nozzle_curve, ax=None):
839
         from mpl_toolkits.axes_grid1.inset_locator import inset_axes
840
841
         if ax is None:
842
             ax = plt.gca()
843
         prop = np.array([flow.__getattribute__(prop_name) for flow in flow_list])
844
         x, y = nozzle_curve
845
         plot = plt.contourf([x, x], [np.zeros_like(y), y], [prop, prop], levels=10)
846
         plt.axis("scaled")
847
         # cb = plt.colorbar(label=prop_name, orientation="vertical")
848
         axins = inset_axes(
849
850
             plt.gca(),
             width="5%",
851
             height="100%",
852
             loc="lower left",
853
             bbox_to_anchor=(1.02, 0.0, 1, 1),
854
             bbox_transform=ax.transAxes,
855
             borderpad=0,
856
857
         cb = plt.gcf().colorbar(plot, cax=axins, label=prop_name)
858
         cb.formatter.set_powerlimits((-3, 3))
859
         cb.formatter.set_scientific(True)
860
861
862
     def plot_nozzles_props(prop_list, nozzle_flow_list, curve_list):
863
864
         for property in prop_list:
             for nozzle_flow, curve in zip([*nozzle_flow_list], curve_list):
865
                 plt.figure()
866
                 plot_nozzle_prop(property, nozzle_flow, curve)
867
         plt.show()
868
869
```

```
870
871
     # %%
    with plt.rc_context({"figure.figsize": (10, 10)}):
872
         plot_nozzles_props(
873
             ["pressure", "mach", "temperature", "density", "vel"],
874
             nozzles_flows,
875
             nozzle_curves,
876
         )
877
878
879
     # %% [markdown]
880
     # ### Line plot
881
882
883
    # %%
    with plt.style.context(styles):
884
885
         fig, ax = plt.subplots(figsize=(10, 10))
         for nozzle_flows, line_style in zip(nozzles_flows, ["dashed", "solid", "-."]):
886
             with plt.rc_context(
887
                 {"lines.linestyle": line_style, "lines.marker": "", "lines.linewidth": 2}
888
             ):
889
                 data2 = np.stack(
890
                      Ε
891
                          (*f.static_values(), *f.aux_values(), *f.total_values())
892
                          for f in nozzle_flows
893
                     ]
894
                 )
895
                 _, axes = plot_flow_evolution(data2, x, (fig, ax), cols=[0, 1, 2, 3, 5])
896
         plt.axvline(crit_len, color="black", linestyle="dotted", linewidth=2, alpha=0.5)
897
         plt.savefig("nozzle_evolution.pdf", bbox_inches="tight")
898
         plt.show()
899
900
901
    # %%
902
    with plt.style.context("default"):
903
         plt.figure(figsize=(10, 10))
904
         for prop, color in zip(
905
             ["pressure", "mach", "temperature", "density", "vel"], colors
906
         ):
907
             plt.title(prop)
908
             for nozzle_flows, nozzle_names, line_style in zip(
909
                 nozzles_flows, ["Bell", "Cone"], ["-", "--"]
910
             ):
911
                 y = [f.__getattribute__(prop) for f in nozzle_flows]
912
913
                 y = y / y[crit_index]
                 plt.plot(
914
915
                      х,
916
                     у,
                      linestyle=line_style,
917
                      color=color,
918
```