

5.) i) Q. 2.3.21a ignorando efeitos propulsivos

$$C_{m_K} = a(h - h_{\eta_{wb}}) - a_t \bar{V}_H \left( 1 - \frac{dE}{d\alpha} \right) \quad (I)$$

$$\bar{V}_H = \frac{l_t S_t}{\bar{c} S}$$

(II)

Q. 2.3.18

$$a = a_{wb} \left[ 1 + \frac{a_t S_t}{a_{wb} S} \left( 1 - \frac{dE}{d\alpha} \right) \right]$$

(III)

Usando  $C_{m\alpha} < 0$ , substituindo (II) e (III) em (I)

$$C_{m\alpha} = a(h - h_{nwb}) - a_t \bar{V}_H \left( 1 - \frac{\frac{dE}{d\alpha}}{2\alpha} \right) < 0$$

$$h < h_{nwb} + \frac{a_t \bar{l}_t S_t}{\bar{c} S} \left( 1 - \frac{\frac{dE}{d\alpha}}{2\alpha} \right)$$


---


$$a_{wb} \left[ 1 + \frac{a_t}{a_{wb}} \frac{S_t}{S} \left( 1 - \frac{\frac{dE}{d\alpha}}{2\alpha} \right) \right]$$

$$h < 0,5607$$

(IV)

ii) De 2.3. 22a ignorando efeitos propulsivos

$$C_{m_p} = C_{mac_{wb}} + a_t \bar{V}_H (\epsilon_0 + i_t) \left[ 1 - \frac{a_t}{a} \frac{S_t}{S} \left( 1 - \frac{2\epsilon}{2\alpha} \right) \right] \quad (V)$$

Usando  $C_{m_p} > 0$ , substituindo (II), (III) em (V)

$$C_{m_p} = C_{mac_{wb}} + a_t \bar{V}_H (\epsilon_0 + i_t) \left[ 1 - \frac{a_t}{a} \frac{S_t}{S} \left( 1 - \frac{2\epsilon}{2\alpha} \right) \right] > 0$$

$$i_t > -$$

$$C_{macwb}$$

$$- \varepsilon$$

$$\left[ \begin{array}{c} a_t \frac{l_t S_t}{\bar{c} S} \left( 1 - a_t \frac{S_t}{S} \left( 1 - \frac{\underline{\partial \varepsilon}}{\underline{\partial \alpha}} \right) \right) \\ a_{wb} \left[ 1 + \frac{a_t}{a_{wb}} \frac{S_t}{S} \left( 1 - \frac{\underline{\partial \varepsilon}}{\underline{\partial \alpha}} \right) \right] \end{array} \right]$$

(VI)

$$i_t > - 0,193^\circ$$

iii) Para voo trimado  $L_0 = 0$ , de 2.3.20a

$$C_m = C_{m_0} + C_{m_\alpha} \alpha = 0$$

(VII)

Em voo não acelerado, com  $C_L = a \alpha$

$$L = W = a \alpha \frac{\rho}{2} V^2 S$$

$$\alpha = \frac{2W}{\rho V^2 S a}$$

sendo

$$W = mg = 22600 \cdot 9,81 = 222491 \text{ N}$$

$$S = (25)^2 \cdot 0,139 = 86,875 \text{ m}^2$$

Encontra-se a de  $\textcircled{\text{III}}$ , logo  $\alpha = 3,141^\circ$   
Combinando  $\textcircled{\text{I}}, \textcircled{\text{V}}, \textcircled{\text{VIII}}$  em  $\textcircled{\text{XII}}$  temos  $i_t = f(h)$

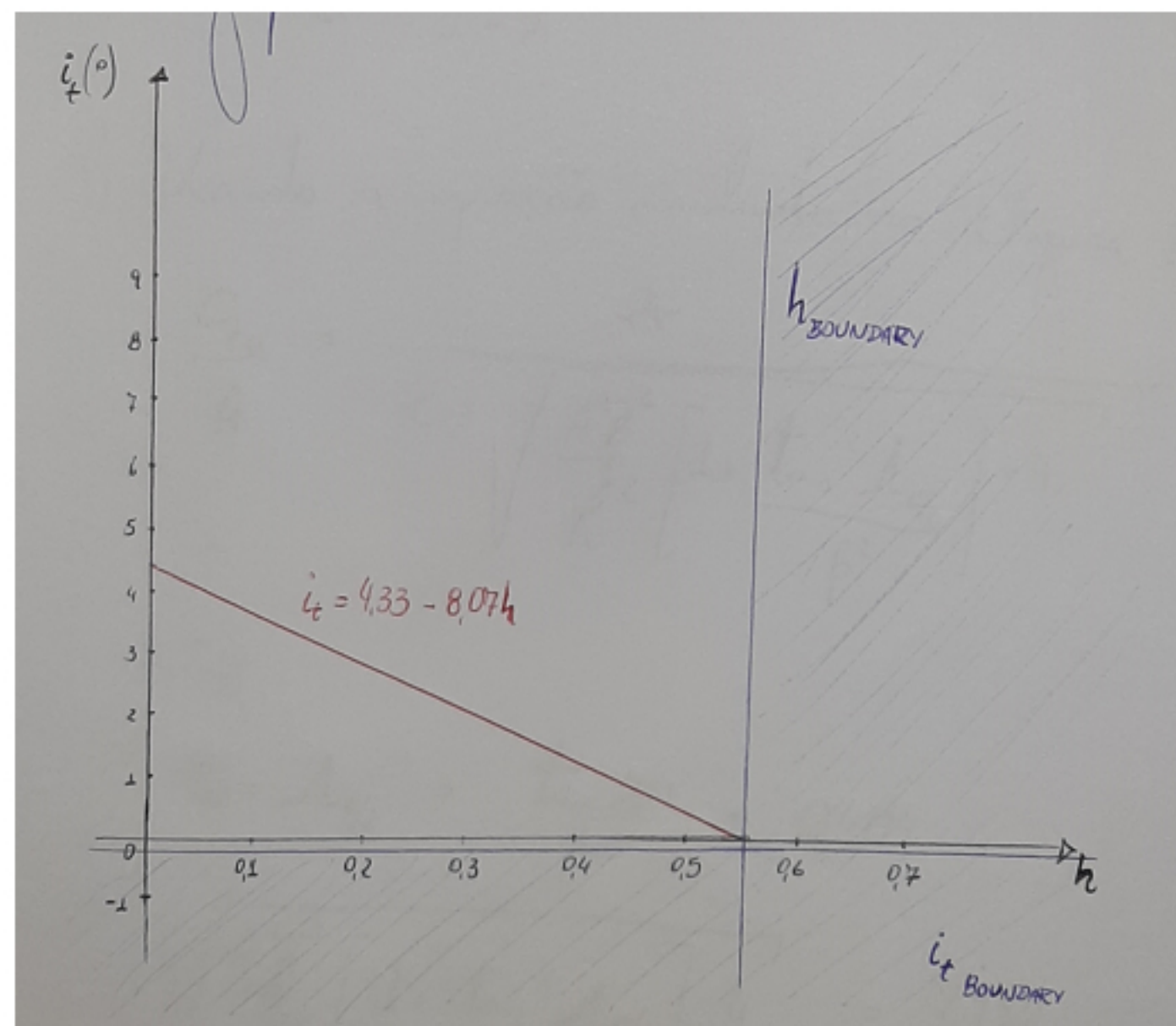
$$C_{m_0} + C_{m_\alpha} \propto 0$$

$$C_{macwb} + a_t \bar{V}_H (\epsilon_0 + i_t) \left[ 1 + \frac{a_t \bar{S}_t}{a \bar{S}} \left( 1 - \frac{2\epsilon}{2\alpha} \right) \right] + \left[ a(h - h_{nwb}) - a_t \bar{V}_H \left( 1 - \frac{2\epsilon}{2\alpha} \right) \right] \frac{2W}{\rho V^2 S a} = 0 \quad (IX)$$

$$i_t = \frac{-C_{macwb} - \left[ a(h - h_{nwb}) - a_t \bar{V}_H \left( 1 - \frac{2\epsilon}{2\alpha} \right) \right] \frac{2W}{\rho V^2 S a}}{a_t \bar{V}_H \left[ 1 + \frac{a_t \bar{S}_t}{a \bar{S}} \left( 1 - \frac{2\epsilon}{2\alpha} \right) \right]} - \epsilon_0 \quad (X)$$



$$i_t = (4,33 - 8,07h) \text{ deg}$$





6) i) De C.2, Tenues

$$A = \frac{b^2}{5} = 7,16$$

(I)

$$d = \frac{c_t}{c_m} = 0,236$$

(II)

Da tabela C.1

$$\bar{c} = \frac{2c_m}{3} \frac{1 + d + d^2}{1 + d} = 7,92 \text{ m (25,99 ft)}$$

(III)

ic) Da eq. incluída na fig. B.1-2

$$\frac{C_{La}}{A} = \frac{2\pi}{2 + \sqrt{\frac{A^2 \beta^2}{K^2} \left[ 1 + \frac{\tan^2 \alpha_{c/2}}{\beta^2} \right] + 4}}$$

(IV)

temos:  $\tan \alpha_{c/2} = \tan 22^\circ = 0,404$

$$\sqrt{\frac{A^2 \beta^2}{K^2} \left[ 1 + \frac{\tan^2 \alpha_{c/2}}{\beta^2} \right] + 4} = 7,977$$

(V)

$$\omega_{aw} = C_{La} = \frac{2\pi A}{2 + \sqrt{\frac{A^2 \beta^3}{K^2}} + 1 + \frac{\tan^2 \Delta \phi_2}{\beta^2} + 4} \quad (VI)$$

$$\omega_{aw} = C_{La} = 4,51 \text{ rad}^{-1}$$

iii) Jermos

$$\frac{2\epsilon}{2\alpha} = \frac{2a_w}{\pi A} = 0.4$$

$$a_t = 0.068 \text{ deg}^{-1} = 3.90 \text{ rad}^{-1}$$

D. 2.3.18

$$a = a_{wb} \left[ 1 + \frac{a_t}{a_{wb}} \frac{S_t}{S} \left( 1 + \frac{2\epsilon}{2\alpha} \right) \right]$$

$$a = 5.05 \text{ rad}^{-1}$$

(VII)

(VIII)

(IX)

iv)  $l_t = \bar{l}_t$ , então  $V_H = \bar{V}_H$

De 2.2.11

$$V_H = \bar{V}_H - \bar{S}_t (h - h_{nwb})$$

Como  $V_H = \bar{V}_H$

$$h = h_{nwb}$$

De 2.3.23 com  $h_{nwb} = h$

$$h - h_n = -\frac{a_1}{a} \bar{V}_H \left( 1 - \frac{2\varepsilon}{2\alpha} \right)$$

(X)

(XI)

(XII)

Q<sub>2</sub> 2.2.10

$$\bar{V}_H = \frac{\bar{l}_t S_t}{\bar{c} S}$$

Q<sub>3</sub> 2.3.25 c

$$C_{m\alpha} = a(h - h_\eta)$$

Substi. (XII) e (XIII) em (XIV)

$$C_{m\alpha} = -a_t \bar{V}_H \left( 1 - \frac{1\epsilon}{2\alpha} \right)$$

(XIII)

(XIV)

$$C_{m\alpha} = -a_t \frac{\bar{l}_t S_t}{\bar{c} S} \left( 1 - \frac{2\epsilon}{2\alpha} \right) = -1,90 \text{ rad}^{-1} \quad (\text{XV})$$



v) Do gráfico  $C_m$  versus  $C_L$  observa-se que  $C_{m_{L_e}}$  é independente de  $C_L$  e  $C_m$  e  $A$  de apenas muda as linhas por uma constante

$$C_{m_{L_e}} = \frac{dC_m}{dL_e} = \frac{\Delta C_m}{\Delta L_e} = \frac{C_{m_f} - C_{m_i}}{L_{ef} - L_{ei}} = \frac{-0,56}{20}$$

$$C_{m_{L_e}} = -0,028 \text{ deg}^{-1}$$

(XVI)

$P_e$   $L_{\text{trim}}$   $C_{\text{trim}}$

• Para  $h = 0,35$

$$\frac{d L_{\text{trim}}}{d C_{\text{trim}}} = \frac{\Delta L_{\text{trim}}}{\Delta C_{\text{trim}}} = \frac{L_{\text{trim}f} - L_{\text{trim}i}}{C_{\text{trim}f} - C_{\text{trim}i}} = \frac{-22,0}{2}$$

$$\frac{d L_{\text{trim}}}{d C_{\text{trim}}} = -11,4^\circ$$

(X VII)

• Para  $h = 0,25$

$$\frac{d}{dC_{\text{trim}}} L_{\text{trim}} = \frac{-278}{1,05} = -15,03^\circ$$

(XVIII)

De 2.4.13c

$$\begin{aligned} \frac{d}{dC_{\text{trim}}} L_{\text{trim}} &= - \frac{C_{L\alpha}}{a} (h - h_n) \\ &= - \frac{a}{a} (h - h_n) \end{aligned}$$

(XIX)

sendo  $\det = C_{L\alpha} C_{m_{Le}} - C_{L_e} C_{m\alpha}$

(XX)

De (XIX)

$$h - h_n = - \frac{\det}{a} \frac{d}{dC_{L_{trim}}} L_{e_{trim}}$$

para as duas posições da CG temos:

$$\begin{cases} 0,35 - h_n = \frac{11,4 \text{ det}}{a} \\ 0,25 - h_n = \frac{15,03 \text{ det}}{a} \\ \text{Assim encontramos} \end{cases}$$

$$h_n = 0,665$$

De 2.3. 25c

XXII

(a)

(b)

XXIII

$$C_{m\alpha} \approx a (h - h_n)$$

$$\text{para } h = 0,30$$

$$C_{m\alpha} \approx -1,84 \text{ rad}^{-1}$$