

# The scenarios that used in the simulation

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## 0.5b, c11 = c22

u1	u2	t11	t22	t12	c11	c22	b	a	sauc	r	se	sp
0.000	1.735	0.5	0.5	-0.15	0.5	0.5	0.5	-0.423	0.620	-0.3	0.5	0.85
0.000	1.735	0.5	0.5	-0.30	0.5	0.5	0.5	-0.461	0.702	-0.6	0.5	0.85
0.000	1.735	1.0	4.0	-0.60	0.5	0.5	0.5	-0.172	0.564	-0.3	0.5	0.85
0.000	1.735	1.0	4.0	-1.20	0.5	0.5	0.5	-0.255	0.620	-0.6	0.5	0.85
1.386	1.386	1.0	4.0	-0.60	0.5	0.5	0.5	-0.761	0.828	-0.3	0.8	0.80
1.386	1.386	1.0	4.0	-1.20	0.5	0.5	0.5	-0.843	0.846	-0.6	0.8	0.80
2.197	-0.405	1.0	4.0	-0.60	0.5	0.5	0.5	-0.199	0.892	-0.3	0.9	0.40
2.197	-0.405	1.0	4.0	-1.20	0.5	0.5	0.5	-0.282	0.877	-0.6	0.9	0.40

## 0.5b, c11 = 1, c22 = 0

u1	u2	t11	t22	t12	c11	c22	b	a	sauc	r	se	sp
0.000	1.735	0.5	0.5	-0.15	1	0	0.5	0.794	0.620	-0.3	0.5	0.85
0.000	1.735	0.5	0.5	-0.30	1	0	0.5	0.795	0.702	-0.6	0.5	0.85
0.000	1.735	1.0	4.0	-0.60	1	0	0.5	0.892	0.564	-0.3	0.5	0.85
0.000	1.735	1.0	4.0	-1.20	1	0	0.5	0.892	0.620	-0.6	0.5	0.85
1.386	1.386	1.0	4.0	-0.60	1	0	0.5	-0.569	0.828	-0.3	0.8	0.80
1.386	1.386	1.0	4.0	-1.20	1	0	0.5	-0.570	0.846	-0.6	0.8	0.80
2.197	-0.405	1.0	4.0	-0.60	1	0	0.5	-1.266	0.892	-0.3	0.9	0.40
2.197	-0.405	1.0	4.0	-1.20	1	0	0.5	-1.265	0.877	-0.6	0.9	0.40

## 0.5b, c11 = 0, c22 = 1

u1	u2	t11	t22	t12	c11	c22	b	a	sauc	r	se	sp
0.000	1.735	0.5	0.5	-0.15	0	1	0.5	-0.993	0.620	-0.3	0.5	0.85
0.000	1.735	0.5	0.5	-0.30	0	1	0.5	-0.996	0.702	-0.6	0.5	0.85
0.000	1.735	1.0	4.0	-0.60	0	1	0.5	-0.432	0.564	-0.3	0.5	0.85
0.000	1.735	1.0	4.0	-1.20	0	1	0.5	-0.438	0.620	-0.6	0.5	0.85
1.386	1.386	1.0	4.0	-0.60	0	1	0.5	-0.113	0.828	-0.3	0.8	0.80
1.386	1.386	1.0	4.0	-1.20	0	1	0.5	-0.106	0.846	-0.6	0.8	0.80
2.197	-0.405	1.0	4.0	-0.60	0	1	0.5	1.727	0.892	-0.3	0.9	0.40
2.197	-0.405	1.0	4.0	-1.20	0	1	0.5	1.732	0.877	-0.6	0.9	0.40