Freundlich is othern;

9 = k C /n ; parameters: 9 and n. Model is feit using nlingit function in MATLAB.

k = 5.655 n = 2.176=> 9 = 5.655 C

Mean Squared error = 3.467

Langmuir I gotherm:

9 = 2mKC; parameters: mand K.

Model is fit using ulingit function in MATCAB.

K = 0.0433 1 9m = 52.002 = 2.252 & C

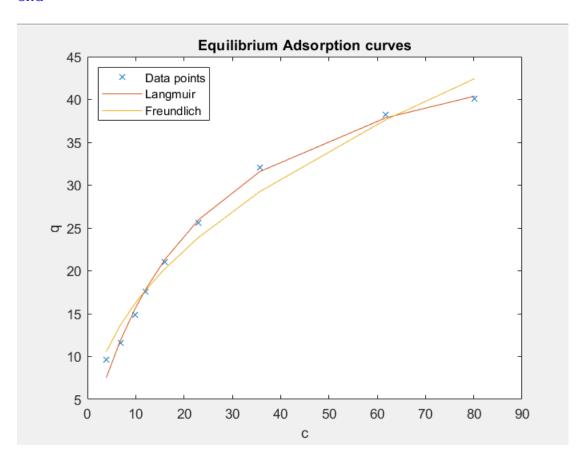
140.04336

Mean squared errol = 0.801.

By comparing the mean squared errors as well as the visual enamination of the attar adsorption isothern plots, we find that Largenuir isothern best fits the data. (K=8655, N=2176) 9M=52.002)

Question 1 MATLAB CODE AND PLOT

```
clear; close all; clc;
c = [3.9; 6.8; 9.9; 12; 16; 23; 35.7; 61.8; 80.2];
q= [9.6;11.6;14.9;17.6;21.0;25.6;32.1;38.2;40.1];
options = statset('MaxIter',500);
[beta,R,J,COVB,MSE] = nlinfit(c,q,@Freund,[1,1]);
[beta1,R1,J1,COVB1,MSE1] =
nlinfit(c,q,@Lang,[0.00001,2*10000],options);
qlang = Lang(beta1,c);
qfreund = Freund(beta,c);
plot(c,q,'x',c,qlang,c,qfreund);
title('Equilibrium Adsorption curves');
legend('Data points','Langmuir', 'Freundlich');
xlabel('c');
ylabel('q');
function y = Freund(parms,c)
    k = parms(1);
    n = parms(2);
    y = k.*(c.^(1./n));
end
function y= Lang(parms,c)
    k = parms(1);
    qm = parms(2);
    y = qm.*(k.*c./(1+k.*c));
end
```



$$=3. \times 1 = 50(0.1)^{0.32}$$

$$=) W = 10 \times (3.5 - 0.1)$$

$$= 23.932$$

$$D_{AB} = 1.5 \times 10^{-5} \text{ cm}^2 / s = 1.5 \times 10^{-9} \text{ m}^2 / s$$

$$D_{AB} = 1.5 \times 10^{-5} \text{ cm}^2 / s = 1.5 \times 10^{-3} \text{ m}^2 / s$$

$$h = 30$$
.; particle dramas.
 $k = \frac{1-5 \times 10^{-9} \times 30}{2 \times 10^{-3}} = \frac{2.25 \times 10^{-5} \text{ m/s}}{2.25 \times 10^{-3}}$.

c is the concentration of adsorbate in the solution at any time to. a is the surface area of charcoal per unitioliume of solution. 5 m² (kg charval x (2.841×10-3 kg charval) 10 1×10-3 m3 solution = 1.421 m2/m3 solution. C* is the expos concentration of adsorbate in solution $\Rightarrow c^* = \left(\frac{(c_i - c_i)L}{WK}\right)^n$, mglLFrom the given isotherm, $N = \frac{1}{0.32} = 3.125$, K = 50Substituting all the values in the ign, $\frac{-\partial c}{\partial t} = k L a \left(c - \left(\frac{(c_1 - c_1)(c_1)}{w k} \right) \right)$ $\int d\xi = \int \frac{-dC}{\left(k_{L} a \left(C - \left(\frac{|Ci-9|}{wk}\right)^{h}\right)\right)}$ $3.5 \int d\xi = \int \frac{-dC}{\left(k_{L} a \left(C - \left(\frac{|Ci-9|}{wk}\right)^{h}\right)\right)}$ J kla (c- (ci-c) L)h) } Integrating this enpression numerically in MATLAB, $t = 1.1428 \times 10^5 \text{ s}$ = | 31.743 hours

Question 2 MATLAB CODE

```
clear; close all;
kl = 2.25*10^{-5}; %m/s
L = 10; %Litres
wmin = (3.5-0.1)/(50*0.1^{(0.32)})*L;%q
w = 2*wmin; %g
ci = 3.5; %mq/L
K = 50; %q \text{ should be in } mg/g, c \text{ in } mg/L
a = 5; %m^2/kq
time = integral(@dtbydc, 3.5, 0.1);
t inhours = time/3600;
function val = dtbydc(c)
    kl = 2.25*10^{-5}; %m/s
    L = 10; %Litres
    wmin = (3.5-0.1)/(50*0.1^{(0.32)})*L;%g
    w = 2*wmin; %q
    ci = 3.5; %mg/L
    K = 50; %q \text{ should be in } mg/g, c \text{ in } mg/L
    a = 5; %m^2/kq
    %units of val
    %c is the conc in solution, second term is the ideal
c in soln
    val = -1./(kl*(a*w/L).*(c-((ci-
c) *L/(w*K)).^(1/0.32)));
end
```

a) Lempt = 0.2 m. Msuperfruial = 0-29 m/s cr = 0. 11 gm of 1 m3. Breaktheough time: time at which c: 20.03. => |tb = 20.626 minutes Contained using Spline interpolation in MATLAB) Ui £e. At Staichionetric tinh Area about cum = Area labore Area below the cure $\int \frac{c}{c_i} dt = (x(te-ts) - \int \frac{c}{c_i} dt)$ bs $\int \frac{C}{cc} dt + \int \frac{C}{ci} dt = |te-ts|$ te is the saturation time - the bed is fully

te is the saturation time - the bed is fund used up. (>/ci = 1) - => from the data te = 108.6 minute

Performing the subsegration numerically;

$$bs = 45 \cdot 18 \quad \text{menutes}$$

$$Us = \frac{L}{45 \cdot 18} = \frac{0.2}{45 \cdot 18} = \frac{4 \cdot 427 \times 10^{-3} \text{ m/min}}{45 \cdot 18}$$

$$= 45 \cdot 18 \quad \text{menutes}$$

$$Us = 0.2 \times \left(1 - \frac{t_b}{t_s}\right)$$

$$= 0.2 \times \left(1 - \frac{20.63}{45 \cdot 18}\right)$$

$$= 0.2 \times \left(1 - \frac{20.63}{45 \cdot 18}\right)$$

$$\Rightarrow 20.1087 \text{ m.} = 0.109 \text{ m.}$$
Since the curve is not symmetric ($\frac{c}{c_1}$ vs $\frac{t}{c_2}$)
We can't use MTZ = 2×10^{13} .

Instead we use the general empression:

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Instead we use the general empression:

A true dought of mass transferzone = $L \times \left(1 - \frac{t_b}{t_e}\right)$

$$\Rightarrow 2 \times 10^{13} \text{ mass transferzone} = \frac{1}{10^{13}} \cdot \frac{162 \text{ m}}{10^{13}}$$

$$\Rightarrow 2 \times 10^{13} \cdot \frac{1}{10^{13}} \cdot \frac{162 \text{ m}}{10^{13}} \cdot \frac{162 \text{ m}}{10^{13}$$

V = 3000 m3/h. = 3000 m3/s => V = 0-833 m3/vae i Usuperficial = 0.29 m/s Area of Bid = V Usuperficial. J. Diameter of bet = z 1.913m. Adsorption cycle, t = 8 hours of length of used bed - Usxt LVB and length of mass transfer zone will remain same before and after scale up breause the wavefront is the same. => Length of bed = Length used + Length unused → L = 2.125 + 0.1087 =) L+otal = 2.233 m. Weight of adsorbate adsorbed till w= VxCixtb. (: Cenit 40)

J W= 2640 gmol = 190.37 kg Average loading = Mars of adsorbate 72.11gmd) Mass of bed has of advorbate Shed XD L total. = 0.5876 gmd/kg bed = 0.0424 kg adsorbate /kg bed. man of adsorbate Manunum loading = was of used part of hed Shed A D2 Lusid of Marinum Loading = 0.6177 gmol [leg bed 44 0.0445 kg MEK/ leg Bed.

Question 3 MATLAB CODE AND PLOT

```
clear; close all;
%% Given data
u superficial = 0.29;
t =
[9.5,19,21,25.7,34.3,39,42,46.7,51.4,56.2,64.7,68.6,72.4,
77.1,84.8,97.1,104.7,108.6];
te = 108.6;
C =
[0,0.018,0.037,0.083,0.287,0.435,0.491,0.62,0.713,0.768,0
.852, 0.935, 0.952, 0.963, 0.97, 0.987, 0.991, 1];
L = 0.2;
ci = 0.11;
plot(t,c);
title('c/ci vs t');
ylabel('c/ci');
xlabel('time');
%% Part a
t break = spline(c, t, 0.03);
pp = spline(t,c);
n = 40;
time = linspace(9.5, 108.6, n*(10));
ts = te - trapz(time, ppval(pp, time));
% Following code evaluates both the integrals numerically
and minimises it.
% No need to run this part because we have already
simplified it into a simple linear eqn in ts.
% min = trapz(time, ppval(pp, time));
% ts = 230;
% ar diff = zeros (n*10-1,1);
% l = length(time);
% for i = 2:1-1
      ar diff(i) = trapz(time(1:1), ppval(pp, time(1:1))) -
(108.6-time(i));
      if min > abs(ar diff(i))
9
          min = abs(ar diff(i));
          ts = time(i);
      end
% end
us = L/ts*60; %m/h
LUB = L*(1-t break/ts);
MTZ = (te-t break)/te*L; %Since curve is NOT symmetric
%% Part b
V = 3000/60/60; %m^3/s
D = sqrt(4*V/(u superficial*pi));
```

```
t_cycle = 8;
bed_density = 700;
L_used = 8*us;
L_scaleup = LUB + L_used;
sol_adsorbed = V*ci*t_cycle*3600;
avg_loading =
sol_adsorbed/(L_scaleup*bed_density*pi*D^2/4);
max_loading = sol_adsorbed/(L_used*bed_density*pi*D^2/4);
```

