

AMT Tutorial-2

① M.W. of inlet gas = $0.1 \times 64 + 0.9 \times 29$
 $= 32.5$

molar flow rate of inlet gas, $G = \frac{1500}{32.5} = 46.15 \text{ kmol/h}$

Molar flow rate of solvent-free gas, $G_s = 0.9 G$
 $= 41.5385 \text{ kmol/h}$

Mole ratios: $Y_{\text{entry}} = \frac{0.1}{0.9} = 0.11$

$Y_{\text{exiting}} = 0.11 \times 0.03 = 0.0033$

$X_{\text{entry}} = 0$

At minimum solvent flow rate, % Exiting solvent will be in equilibrium with entering vapour.

a) $\frac{L_{s \text{ min}}}{G_s} = \frac{Y_1 - Y_2}{X_{\text{exit}} - X_{\text{entry}}} \Rightarrow L_{s \text{ min}} = 1646.7 \times 10^3 \text{ kmol/h}$

b) $L_s = 1.25 L_{s \text{ min}} \text{ (given)}$

$\Rightarrow L_s = 2058.4 \text{ kmol/h}$

To obtain the height of the packed bed we need to evaluate

$$H = \int_{Y_{\text{exit}}}^{Y_{\text{entry}}} \frac{G_s' dy}{k_y a \cdot (1-y)(y-Y_i)} = \left(\frac{V_s}{k_y A} \right) \int \frac{(1+Y) dy}{(1-y)(y-Y_i)}$$

where G_s' is molar flow rate per unit area (flux)
 Y_i is the interfacial concentration of solute.

→ Using 2 film theory we know, $k_n(x_1 - x_i) = k_y(y_1 - y_i)$
 → Since (x_1, y_1) will lie on eqbm curve and (x_i, y_i) will lie on operating line, all we need to do is draw lines of slope $-\frac{k_n}{k_y}$ from a point on operating line and find out where it intersects the eqbm curve (the gradient of intersection is the required y_i)

→ This is done in MATLAB by taking 10 points along the ~~curve~~ operating line and solving the equation: $\left(\frac{k_y}{k_n} (y_i - y) + x_1\right) - f(y_i) = 0$.

where $f(y_i)$ is the eqbm curve.

→ Using y_i we can evaluate the necessary functions in the integral

→ Use trapezoidal rule and integrate w.r.t y .

→ Area under curve is found to be 22.448.

$$\therefore \text{Height of packed bed} = \left(\frac{V_S}{k_y a A} \right) \times 22.448$$

$$= \frac{415385}{3600 \times 0.075 \times 0.781} \times 22.448$$

$$\Rightarrow \boxed{\text{Height} = 4.42 \text{ m.}}$$

AMT CH3030 - Tutorial 2

② Inlet & outlet feed flow rate

$$V_{entry} = \frac{P \dot{V}}{RT} = \frac{0.4 \times 1.013 \times 10^5}{8.314 \times 297} = 16.41 \text{ mol/s}$$

$$Y_{entry} = \frac{\text{partial pressure of solute}}{\text{partial pressure of solvent}} = \frac{50}{710} = 0.0704$$

$$Y_{exit} = \frac{y_{exit}}{1 - y_{exit}} = \frac{5 \times 10^{-3}}{1 - 5 \times 10^{-3}} = 5.025 \times 10^{-3}$$

$$V_s = \frac{710}{760} \times V_{entry} = 15.33 \text{ mol/s}$$

Eqbm curve : Raoult's law.

$$y_{P_{total}} = x(P_{vapour})$$

$$\Rightarrow y = 0.455x$$

At L_{min} , x_{exit} will be in equilibrium with Y_{entry}

$$\Rightarrow x_{exit} = 0.1689 \approx 0.169$$

$$a) \therefore \text{min. liquid gas ratio, } \frac{L_{min}}{V_s} = \frac{Y_{entry} - Y_{exit}}{x_{exit} - x_{entry}} = \boxed{0.387}$$

$$b) \text{ If } \frac{L_s}{V_s} = 1.5 \frac{L_{min}}{V_s}, \text{ then } L_s = 8.9 \text{ mol/s}$$

$$= 8.9 \times 3600 \times 0.16 \text{ kg/h}$$

$$\Rightarrow \boxed{L_s = 5768.9 \text{ kg/h}}$$

c) For no. of steps graphical method, starting we start from bottom of operating line (x_{entry}, y_{exit}) move to eqm curve keeping y constant, then keep x constant and move to the operating line. this procedure is repeated till we cross the $y = y_{entry}$. Number of steps were found to be 6

Kremser's method

Absorption factor, $A = \frac{\text{slope of operating line}}{\text{slope of equilibrium curve}} = \frac{0.581}{0.425}$

≈ 1.28

$$N = \log \left(\frac{\left(\frac{y_{entry} - K x_{entry}}{y_{exit} - K x_{exit}} \right) \times \left(1 - \frac{1}{A} \right) + \frac{1}{A}}{\log A} \right)$$

$K \rightarrow$ slope of equilibrium curve.

(note: all are mole fractions)

$\Rightarrow N = 5.298$

\therefore No. of steps = 6

d) Given $\mu = 2 \text{ cP} = 2 \times 10^{-3} \text{ Pa.s}$, $\rho = 0.81 \times 10^3 = 810 \text{ kg/m}^3$ and molecular weight = 18 g/mol .

value of x -axis = $\frac{(\text{slope of eqm curve}) \times (\text{mol. weight})}{\rho \mu}$

$$= 2.02 \times 10^{-4}$$

From the overall ^{tray} efficiency graph, we can see that

$$E_o \approx 0.25 \quad (\text{efficiency})$$

$$E_o = \frac{\text{no. of ideal trays}}{\text{real no. of trays reqd.}}$$

$$\Rightarrow \text{Real number of trays required} = \frac{N}{E_o} = \frac{6}{0.25}$$
$$= 24 \text{ trays}$$

(⊗ Note: if we put $N = 5.29$ (value obtained through Kremser eqn) we will get 22 trays)